## GROUNDWATER EXTRACTION AND TREATMENT SYSTEM DESIGN REPORT



## **FRANKLIN CLEANERS SITE**

Village of Hempstead Nassau County, New York (Site Registry No. 1-30-050)

WORK ASSIGNMENT NO. D003600-10

**Prepared For** 

## New York State Department of Environmental Conservation

DECEMBER 2000



CONSULTING ENGINEERS A DIVISION OF WILLIAM F. COSULICH ASSOCIATES, P.C.

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FOR THE

FRANKLIN CLEANERS SITE INCORPORATED VILLAGE OF HEMPSTEAD NASSAU COUNTY, NEW YORK

**PREPARED BY** 

DVIRKA AND BARTILUCCI CONSULTING ENGINEERS WOODBURY, NEW YORK



**DECEMBER 2000** 

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#### FRANKLIN CLEANER SITE GROUNDWATER EXTRACTION AND TREATMENT SYSTEM DESIGN REPORT

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# **Section 1**

#### 1.0 INTRODUCTION

#### 1.1 Background

As part of New York State's program to investigate and remediate hazardous waste sites, the New York State Department of Environmental Conservation (NYSDEC) has issued a work assignment to Dvirka and Bartilucci Consulting Engineers (D&B) under its Superfund Standby Contract with NYSDEC to design a remedial measure (RM) to address groundwater contamination migrating from the Franklin Cleaners Site located in the Town of Hempstead, Nassau County, New York.

As a result of the findings of a remedial investigation/feasibility study conducted for the site, and previous investigations on and in the vicinity of the site, a plume of contaminated groundwater has been documented to be migrating from the Franklin Cleaners Site, which poses a potential threat to a number of downgradient public supply wells.

Based on the documented groundwater contamination and potential threat to public water supply, NYSDEC has elected in a Record of Decision issued for the site to control the migration of groundwater contamination near the leading edge of the plume by installing a groundwater extraction and treatment system to mitigate the potential for future impacts to downgradient supply wells. This RM is being performed with funds allocated under the New York State Superfund Program.

#### 1.2 Site Location and Access

The Franklin Cleaners Site is a former dry cleaning facility located at 206-208B South Franklin Street in the Incorporated Village of Hempstead, Nassau County, New York. The groundwater extraction and treatment system will be located near the leading edge of the groundwater plume approximately one mile downgradient (south) of the site. The groundwater extraction and treatment system will be located on property owned by the New York State Office of Parks, Recreation and Historic Preservation. This location is bordered by Molloy College and Mercy Hospital to the south, the Southern State Parkway to the north, Hempstead Avenue to the east and Peninsula Boulevard to the west (see Figure 1-1). Access to the location for construction of the groundwater remediation system will be via Hempstead Avenue or Molloy College pending acceptance of an access agreement with Molloy College.

#### 1.3 Site History

In March 1990, the Nassau County Department of Health (NCDOH) investigated a complaint of tainted drinking water from a private residence on Linden Avenue. The residence was found to have two private water supply wells: a drinking water well (approximately 45 feet deep) and an irrigation well (approximately 32 feet deep). The water supply well was sampled and found to contain tetrachloroethene (PCE) at 5,500 micrograms per liter (ug/l). The irrigation well contained PCE at 29,000 ug/l. The drinking water and groundwater standard for PCE is 5 ug/l. The residence was connected to the Village of Hempstead public water supply system following the detection of PCE.

Since the Franklin Cleaners Site is located upgradient of the wells on Linden Avenue, NCDOH performed an inspection of the dry cleaner premises and collected surface soil samples from the basement of the existing building and at the rear of the former dry cleaner property. Soil samples from the basement were found to contain PCE concentrations as high as 9,400 micrograms per kilogram (ug/kg). A sample from the rear of the property contained PCE at 650,000 ug/kg, trichloroethene (TCE) at 1,700 ug/kg and dichloroethene (DCE) at 680 ug/kg.

In 1993, the Nassau County Department of Public Works (NCDPW) performed a Preliminary Site Assessment at the Franklin Cleaners site. As part of this investigation, four groundwater monitoring wells were installed. One of the wells, FC-1, was installed upgradient of the former dry cleaner site to a depth of 40 feet. The other three wells, FC-2, FC-3 and FC-4, were installed downgradient of the site, each to a depth of 37 feet. Groundwater samples



collected from the wells showed that monitoring well FC-2 contained PCE at 83 ug/l and that none of the contaminants of concern were detected in FC-1, FC-3 and FC-4.

As a result of these findings, the Franklin Cleaners site was listed on the Registry of Inactive Hazardous Waste Disposal Sites in New York State on June 17, 1993 (site registry number 1-30-050). In response to a determination that the presence of hazardous waste at the site presents a significant threat to human health and the environment, the New York State Department of Environmental Conservation (NYSDEC) completed a Remedial Investigation/Feasibility Study (RI/FS). The purpose of the RI was to define the nature and extent of contamination resulting from previous activities at the site. The RI was conducted between December 1996 and April 1997. A draft RI report was issued in October 1997 and a final RI report was issued in February 1998.

Based on the results of interior soil sampling, elevated levels of contamination exist primarily in the vicinity of the former "cooker" and other dry cleaning equipment which was located near the concrete pad in the southeast corner of the basement. The elevated levels found at this location indicate that PCE spills or disposal occurred in this portion of the basement. The basement floor of the building is in poor condition with numerous cracks and broken concrete, which apparently allowed the spilled PCE to migrate to the underlying soil. The contamination in the vicinity of the "cooker" appears to be limited to the surface soil and shallow subsurface soil less than 4 feet in depth. Although the surface soil samples exhibited very high levels of PCE (maximum concentration of 240,000 ug/kg), the samples collected with depth (greater than 4 feet), in general, did not exhibit elevated levels of PCE (maximum concentration of 140 ug/kg). The area of significant contamination appears to be approximately 450 to 500 square feet.

As part of the RI, surface soil samples were also collected along the rear (eastern) portion of the building. Subsurface soil borings were constructed at nine of the surface soil sample locations. The borings were continuously sampled to a depth of approximately 20 feet below grade. Elevated levels of contamination (maximum PCE concentration of 280,000 ug/kg) appear to be limited to an area immediately adjacent to the back door of the former dry cleaning facility where dry cleaning fluid was evidently disposed. This area is approximately 250 to 300 square feet. Based on the subsurface sample results and the significant groundwater contamination associated with this site, elevated PCE contamination in these soils is likely to be present down to the depth of the water table (approximately 20 feet).

The results of the groundwater sampling conducted as part of the RI are summarized below.

#### Shallow Upper Glacial Aquifer

Elevated levels of PCE were detected in shallow/water table groundwater in the immediate vicinity of the Franklin Cleaners Site. The highest concentration detected was 1,502 ug/l in the well installed on site. The two shallow private wells sampled downgradient of the site showed PCE at 780 ug/l and 100 ug/l, respectively. VOC levels decrease in concentration in the shallow aquifer downgradient (south) of the site to below the groundwater standard of 5 ug/l approximately 3,000 feet downgradient of the site.

#### Intermediate Upper Glacial Aquifer

Elevated levels of VOCs were detected farther downgradient of the site in the intermediate depth samples (33 to 57 feet below the water table) collected from the Upper Glacial aquifer. Concentrations of PCE greater than 1,000 ug/l were detected approximately 1,000 feet downgradient of the site. Concentrations greater than 100 ug/l were detected at a distance of approximately 3,500 feet downgradient of the site in this zone.

#### Deep Upper Glacial Aquifer

Elevated levels of VOCs were detected in the deep Upper Glacial aquifer (49 to 87 feet below the water table) both upgradient and downgradient of the site. Concentrations in the immediate vicinity of the site in the deep zone exhibited slightly elevated VOC levels up to 72 ug/l. Overall, the deep aquifer data indicates a discontinuous plume/slug of highly contaminated groundwater (greater than 1,000 ug/l) migrating southerly from the site.

Concentrations greater than 100 ug/l have been detected in the deep Upper Glacial aquifer as far as 4,500 feet downgradient of the site.

#### General Conclusions Regarding Groundwater Contamination

Based on the results of the RI, the groundwater plume which emanates from the Franklin Cleaners Site can be traced to nearly 1 mile downgradient (south) of the site where it ends at the northern boundary of the Molloy College property and Mercy Hospital, just south of the Southern State Parkway (see Figure 1-2). The width of the plume remains narrow throughout its length, generally less than 500 feet. In comparing the contaminant levels in the shallow, intermediate and deep Upper Glacial aquifer, it is apparent that contamination migrates downward as it travels away from the site. Due to the presence of a low permeability unit at the interface of the Upper Glacial and Magothy aquifers, it is unlikely that significant contamination associated with the site has migrated into the Magothy aquifer.



# Section 2

#### 2.0 REMEDIAL PREDESIGN STUDIES

#### 2.1 Background/Purpose

The purpose of the predesign studies was to further delineate the groundwater contamination plume emanating from the Franklin Cleaners Site and to obtain the data necessary to characterize the aquifer for the design of the groundwater remediation system to effectively contain and treat the plume. The activities completed as part of the predesign studies included a groundwater sampling program and a pump test performed near the leading edge of the plume. Descriptions of each phase of the plume delineation program and pump test are presented below.

#### 2.2 Groundwater Contamination Plume Delineation Program

Several rounds of sample collection and analysis were required to delineate the horizontal and vertical extent of the groundwater contamination plume in the area of the planned groundwater extraction wells. Sample collection was performed along a line perpendicular to the flow path of the plume at a location which was believed to be near the leading edge of the plume and available for construction of the pump test well (see Figure 2-1).

A Geoprobe sampling system operated by Zebra Environmental Corp. was used for the initial phase of the sampling program. The Geoprobe sampling system consists of a groundwater sampling device mounted to the front of a skid steer loader. The sampling device is a 4-foot long screen point. The sampling device is threaded to the Geoprobe drive rods and driven into the water table to the desired sampling interval. When the desired depth is reached, the drive rods are retracted four feet, exposing approximately four feet of stainless steel screen. Dedicated polyethylene tubing fitted with a stainless steel check valve was inserted into the drive rods and used to extract a sample. Approximately three to five gallons of water were purged prior to sample collection.

The initial round of groundwater sampling was performed between July 29 and August 5, 1999. The program comprised collection of Geoprobe samples at six locations (GP-W1 through



GP-W6). At each probe location, samples were collected at depths of approximately 20, 50 and 84 feet below ground surface. Sample depths were based on depths established as part of the RI. The results of the Geoprobe program are presented in Table 2-1 and illustrated on Figure 2-2. As can be seen from the results, during the first round of sampling the highest concentrations of tetrachloroethene (PCE) were detected at probe points GP-W2 and GP-W3. PCE was detected at 460 ug/l and 770 ug/l, 84 feet below ground surface, at GP-W2 and GP-W3, respectively.

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The second round of groundwater sampling was performed between September 28 and 29, 1999. The program comprised collection of groundwater samples at five locations (GP-W7 through GP-W11) surrounding GP-W3. One groundwater sample was collected from each probe location. Samples were collected at depths ranging from 78 to 92 feet below ground surface. The results of this phase of the Geoprobe program are also presented in Table 2-1 and illustrated on Figure 2-2. As shown, the highest concentrations of PCE were detected at probe points GP-W7, GP-W8 and GP-W11. PCE was detected at concentrations of 210 ug/l and 430 ug/l in the samples collected at probe points GP-W7 and GP-W8, both advanced to 84 feet below ground surface. At probe point GP-W11, the western-most point advanced during the second round of groundwater sampling, PCE was found at a concentration of 1,200 ug/l at a depth of 92 feet below ground surface. At probe point GP-W10, the eastern-most point advanced during the second round of groundwater sampling, PCE was detected at 150 ug/l at 92 feet below ground surface. As a result, the second round of sampling indicated that the highest concentrations of PCE exist directly above the confining clay layer located approximately 95 feet below ground surface (see Section 2.3.1 below). The results of the second round of sampling also show that the plume extends further to the west than the initial round of sampling at shallower depths indicated.

The third round of groundwater sampling was performed on January 5, 2000. Collection of five Geoprobe groundwater samples at 92 feet below ground surface was planned, however, only one sample (GP-W12) was collected due to the equipment limitations. PCE was detected at a concentration of 960 ug/l at GP-W12 (see Table 2-1 and Figure 2-2).

#### TABLE 2-1 Franklin Cleaners Site Summary Of Groundwater Investigation Results Volatile Organic Compounds

	1										
SAMPLE IDENTIFICATION	GP-W 1	GP-W1	GP-W1	GP-W 2	GP-W 2	GP-W 2	GP-W 3	GP-W 3	GP-W 3	CONTRACT	NYSDEC CLASS GA
SAMPLE DEPTH	20'	50'	84'	21'	50'	84'	21'	50'	84'	REQUIRED	GROUNDWATER
DATE OF COLLECTION	07/29/99	07/29/99	07/29/99	08/04/99	08/04/99	07/29/99	08/04/99	08/04/99	08/04/99	DETECTION	STANDARD/
DILUTION FACTOR	1	1	1	1	1	1	1	1	1	LIMIT	GUIDELINE
VOLATILE ORGANICS	(ug/l)	(ug/l)									
			_								
Vinyl Chloride	U	U	U	U	U	U	U	U	U	1	2 ST
1,1-Dichloroethene	U	U	U	U	U	4	U	U	U	1	5 ST
Methylene Chloride	2 B	2 B	8	2 B	2 B	2 B	3 B	U	U	1	5 ST
t-1,2-Dichloroethene	U	U	U	U	U	U	U	U	U	1	5 ST
1,1-Dichloroethane	U	U	U	U	U	U	U	U	U	• 1	5 ST
1,1,1-Trichloroethane	U	1	U	U	U	8	U	1	21	1	5 ST
Carbon Tetrachloride	U	U	U	U	U	U	U	U	U	1	5 ST
1,2-Dichloroethane	U	U	U	U	U	U	U	U	U	1	0.6 ST
Trichloroethene	U	U	U	U	U	7	U	U	U	1	5 ST
Tetrachloroethene	U	1	U	U	U	460 D	2	16	770	1	5 ST
Chlorobenzene	U	U	U	U	U	U	U	U	U	1	5 ST
c-1,2-Dichloroethene	U	U	U	U	U	5	U	U	Ū	1	5 ST
Chloromethane	U	U	U	U	U	U	U	U	U	1	
Bromomethane	U	U	U	U	U	U	U	U	Ŭ	1	5 ST
Chloroethane	U	U	U	U	U	U	U	U	U	1	5 ST
Trichlorofluoromethane	U	U	2	U	U	U	U	U	Ū	1	5 ST
Chloroform	U	U	U	U	U	U	U	U	U	1	7 ST
1,2-Dichloropropane	U	U	U	U	U	U	U	U	Ŭ	1	1 ST
Bromodichloromethane	U	U	U	U	U	U	U	U	Ū	1	50 ST
2-Chloroethyl vinyl ether	U	U	U	U	U	U	U	U	U	1	
c-1,3-Dichloropropene	U	U	U	U	U	U	U	U	U	1	0.4 ST
t-1,3-Dichloropropene	U	U	U	U	U	U	U	U	U	1	0.4 ST
1,1,2-Trichloroethane	U	U	U	U	U	U	U	U	U	1	1 ST
Dibromochloromethane	U	U	U	U	U	U	U	Ū	Ŭ	1	50 ST
Bromoform	U	U	U	U	U	U	U	U	Ŭ	1	50 ST
1,3-Dichlorobenzene	U	U	U	U	U	U	U	U	U	1	3 ST
1,4-Dichlorobenzene	U	U	U	U	U	U	U	Ŭ	Ŭ	1	3 ST
1,2-Dichlorobenzene	U	U	U	U	U	U	U	Ū	Ŭ	1	3 ST
1,1,2,2-Tetrachloroethane	U	U	U	U	U	Ŭ	Ŭ	U	Ŭ	1	5 ST
TOTAL VOCs	2	4	10	2	2	486	5	17	791		

QUALIFIERS/ABBREVIATIONS:

U: Compound analyzed for but not detected

B: Indicates potential laboratory contamination

D: Compound Analyzed at Dilution

CRDL: Contract Required Detection Limit

ST: Standard

VOCs: Volatile Organic Compounds

#### 2/1 Woll To Microgram per liter

NOTES

1) Sample depth in feet below ground surface.

- Compound detected above Class GA Standards

#### 2-1 Continue Franklin Cleaners Site Summary Of Groundwater Investigation Results Volatile Organic Compounds

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SAMPLE IDENTIFICATION	GP-W4	GP-W4	GP-W 4	GP-W 5	GP-W 5	GP-W 5	GP-W 6	GP-W 6	GP-W 6	CONTRACT	NYSDEC CLASS GA
SAMPLE DEPTH	20'	50'	84'	21'	50'	84'	21'	50'	84'	REQUIRED	GROUNDWATER
DATE OF COLLECTION	08/04/99	08/04/99	08/04/99	08/05/99	08/05/99	08/05/99	08/05/99	08/05/99	08/05/99	DETECTION	STANDARD/
DILUTION FACTOR	1	1	1	1	1	1	1	1	1	LIMIT	GUIDELINE
VOLATILE ORGANICS	(ug/l)	(ug/l)									
Vinyl Chloride	U	U	U	U	U	U	U	U	U	1	2 ST
1,1-Dichloroethene	U	U	U	U	U	U	U	U	U	1	5 ST
Methylene Chloride	3 B	2 B	3 B	U	U	U	1	U	U	1	5 ST
t-1,2-Dichloroethene	U	U	U	U	U	U	U	U	U	1	5 ST
1,1-Dichloroethane	U	U	U	U	U	U	U	U	U	1	5 ST
1,1,1-Trichloroethane	U	U	U	U	U	U	U	U	U	1	5 ST
Carbon Tetrachloride	U	U	U	U	U	U	U	U	U	1	5 ST
1,2-Dichloroethane	U	U	U	U	U	U	U	U	U	1	0.6 ST
Trichloroethene	U	U	U	U	U	U	U	U	U	1	5 ST
Tetrachloroethene	U	U	5	U	6	2	U	U	U	1	5 ST
Chlorobenzene	U	U	U	U	U	U	U	U	U	1	5 ST
c-1,2-Dichloroethene	U	U	7	U	U	U	U	U	U	1	5 ST
Chloromethane	U	U	U	·U	U	U	U	U	U	1	
Bromomethane	U	U	U	U	U	U	U	U	U	1	5 ST
Chloroethane	U	U	U	U	U	U	U	U	U	1	5 ST
Trichlorofluoromethane	U	U	U	U	U	U	U	U	U	1	5 ST
Chloroform	U	U	U	U	U	U	U	U	U	1	7 ST
1,2-Dichloropropane	U	U	U	U	U	U	U	U	U	1	1 ST
Bromodichloromethane	U	U	U	U	U	U	U	U	U	1	50 ST
2-Chloroethyl vinyl ether	U	U	U	U	U	U	U	U	U	1	
c-1,3-Dichloropropene	U	U	U	U	U	U	U	U	U	1	0.4 ST
t-1,3-Dichloropropene	U	U	U	U	U	U	U	U	U	1	0.4 ST
1,1,2-Trichloroethane	U	U	U	U	U	U	U	U	U	1	1 ST
Dibromochloromethane	U	U	U	U	U	U	U	U	U	1	50 ST
Bromoform	U	U	U	U	U	U	U	U	U	1	50 ST
1,3-Dichlorobenzene	U	U	U	U	U	U	U	U	U	1	3 ST
1,4-Dichlorobenzene	U	U	U	U	1	U	U	U	U	1	3 ST
1,2-Dichlorobenzene	U	U	U	U	1	U	U	U	Ū	1	3 ST
1,1,2,2-Tetrachloroethane	U	U	U	U	2	U	U	U	U	1	5 ST
TOTAL VOCS	3	2	15	0	10	2	1	0	0		

#### QUALIFIERS/ABBREVIATIONS:

U: Compound analyzed for but not detected

B: Indicates potential laboratory contamination

D: Compound Analyzed at Dilution

**CRDL: Contract Required Detection Limit** 

ST: Standard

VOCs: Volatile Organic Compounds

02/14/2000 Microgram per liter

#### NOTES

1) Sample depth in feet below ground surface.

- Compound detected above Class GA Standard

#### TABLE 2-1 (Continued) Franklin Cleaners Site Summary Of Groundwater Investigation Results Volatile Organic Compounds

SAMPLE IDENTIFICATION	GP-W 7	GP-W 8	GP-W 9	GP-W 10	GP-W 11	GP-W 12	GP-W 13	GP-W 14	CONTRACT	NYSDEC CLASS GA
SAMPLE DEPTH	84'	84'	78'	92'	92'	92'	92'	92'	REQUIRED	GROUNDWATER
DATE OF COLLECTION	09/28/99	09/28/99	09/28/99	09/29/99	09/29/99	01/05/00	01/24/00	01/24/00	DETECTION	STANDARD/
DILUTION FACTOR	1	1	1	1	1	1	3	5	LIMIT	GUIDELINE
VOLATILE ORGANICS	(ug/l)	(ug/l)								
Vinvl Chloride	U	U	U	U	U	U	U	U	1	2 ST
1.1-Dichloroethene	U	U	10	Ū	Ŭ	Ŭ	Ŭ	Ŭ	1	5 ST
Methylene Chloride	U	U	U	U	U	2	U U		1	5.ST
t-1.2-Dichloroethene	U	Ŭ	Ŭ	Ŭ	Ŭ	Ū	U U	ŭ	1	5 ST
1.1-Dichloroethane	U	U	Ŭ	U	Ŭ	Ŭ	U U	2	1	5 ST
1.1.1-Trichloroethane	U	U	22	1 0	2	3	Ŭ	6	1 1	5 ST
Carbon Tetrachloride	U	U	U	Ū	Ū	U	Ŭ	U	1 1	5 ST
1.2-Dichloroethane	U	Ŭ	Ŭ	Ŭ	Ŭ	Ŭ	Ŭ	Ŭ	1	0.6.ST
Trichloroethene	2	1	1	2	2	2	U U	U U	1	5.ST
Tetrachloroethene	210 D	430 D	34	150	1.200 D	960 D	U U	26		5 ST
Chlorobenzene	U	U	U	U	U	U	Ū		1 1	5 ST
c-1,2-Dichloroethene	6	2	Ŭ	6	1 1	Ŭ	Ŭ	Ŭ	1	5 ST
Chloromethane	U	U	U	U	U U	Ŭ	U	Ŭ	1	
Bromomethane	U	Ū	U	Ŭ	Ŭ	Ŭ	Ŭ	Ŭ	1	5 ST
Chloroethane	U	U	U	U	Ŭ	Ŭ	Ŭ	Ŭ	1	5 ST
Trichlorofluoromethane	U	U	U	U	Ŭ	Ŭ	Ŭ	Ŭ	1	5 ST
Chloroform	U	U	U	U	Ŭ	Ŭ	1	Ŭ	1	7 ST
1,2-Dichloropropane	U	U	U	U	U	U	Ú	Ŭ	1	1 ST
Bromodichloromethane	U	U	U	U	U	U	Ū	Ŭ	1	50 ST
2-Chloroethyl vinyl ether	U	U	U	U	U	U	Ū	U	1	
c-1,3-Dichloropropene	U	U	U	U	U	U	U	U	1	0.4 ST
t-1,3-Dichloropropene	U	U	U	U	U	U	U	U	1	0.4 ST
1,1,2-Trichloroethane	U	U	U	U	U	1	U	U	1	1 ST
Dibromochloromethane	U	U	U	U	U	U	U	U	1	50 ST
Bromoform	U	U	U	U	U	U	Ŭ	Ŭ	1	50 ST
1,3-Dichlorobenzene	U	U	U	U	U	U	U	Ū	1	3 ST
1,4-Dichlorobenzene	4	2	2	1	2	U	Ū	U	1	3 ST
1,2-Dichlorobenzene	U	υ	U	U	U	U	U	U	1	3 ST
1,1,2,2-Tetrachloroethane	U	U	U	U	Ū	Ŭ	Ŭ	Ŭ	1	5 ST
TOTAL VOCs	222	435	69	159	1207	068	1	31		

QUALIFIERS/ABBREVIATIONS:

U: Compound analyzed for but not detected

D: Compound Analyzed at Dilution

CRDL: Contract Required Detection Limit

ST: Standard

VOCs: Volatile Organic Compounds

### ug/l= Microgram per liter

#### NOTES

1) Sample depth in feet below ground surface.

- Compound detected above Class GA Standard



1/DESIGN FILE: 1640-2-2 WM\_0

A hydropunch sampling system was used for the fourth sampling round to reach the desired sample depth. The hydropunch sampling system consists of a drill rig, small diameter augers and a groundwater sampling device. The augers are advanced to the top of the desired sample interval. The hydropunch sampler is then lowered inside the auger string and driven to the desired sampling interval. The sampling device is retracted to expose the hydropunch screen and allow groundwater to enter the sampler. The sample is forced by hydrostatic pressure into the sampler which is equipped with check valves on the top and bottom. The sampling device is retracted to the surface where the sample is collected for analysis.

The fourth round of groundwater sampling was performed on January 24, 2000 by Land, Air, Water Environmental Services, Inc. The program comprised collection of groundwater samples at two locations (GP-W13 and GP-W14). One groundwater sample was collected from each location at 92 feet below ground surface. The results of the hydropunch program are presented in Table 2-1 and illustrated on Figure 2-2. As can be seen from the results, although PCE was not detected in GP-W13, PCE was detected in groundwater at a concentration of 26 ug/l at GP-W14. Therefore, the results of the fourth round of sampling show that the western edge of the plume extends to probe point GP-W14.

In summary, the results of the plume delineation program indicate that the most elevated levels of PCE (i.e., greater than 1,000 ug/l) exist at depths of greater than 80 feet. Based on the results of the program, the groundwater contamination plume is concentrated at a depth of approximately 80 to 95 feet below ground surface, immediately above the clay layer. The RI/FS Report indicates that concentrations of greater than 1,000 ug/l were present approximately 1,200 feet upgradient of the Southern State Parkway at shallower depths (approximately 49 to 87 feet below ground surface) (see Figure 1-2). The results of the plume delineation program also indicate that the plume is slightly farther west (approximately 100 feet) than determined during the remedial investigation. It can be concluded from the plume delineation program that the groundwater contamination plume is centered in the vicinity of GP-W8 and GP-W9 and appears to be approximately 400 feet wide at this location (based on the standard of 5 ug/l for PCE). For the purpose of modeling the extraction well capture zone, a more conservative plume width of 450 feet will be used.

#### 2.3 Pump Test Field Program

Activities performed as part of the pump test included installation of three groundwater monitoring/observation wells, installation of a groundwater extraction well, measurement and recording of pre-test groundwater elevations, a pre-test and pump test, and measurement and recording of post-test groundwater elevations. Descriptions of the field activities, the data collected and an analysis of the pump test results are presented below.

#### 2.3.1 Monitoring Wells

Three monitoring wells (PTMW-1, PTMW-2 and PTMW-3) were installed by Uni-Tech Drilling Company, Inc., using the hollow stem auger and mud rotary techniques. Observation well PTMW-1 was installed on September 14, 1999, using the hollow stem auger technique. The hollow stem auger technique was used to facilitate split spoon sampling of the borehole. Observation wells PTMW-2 and PTMW-3 were installed between October 11 and October 13, 1999, using the mud rotary technique. Mud rotary technique was selected to facilitate installation of the 6" diameter extraction well (see further discussion below). The locations of the monitoring wells were selected based on the planned location for the pump test well (PTW-1) and anticipated drawdown (see Figure 2-3).

The observation wells were positioned at fixed distances from the planned location of the extraction well to gauge the variations in drawdown during the pump test. PTMW-1, located near probe point GP-W3, approximately 27 feet east of PTW-1, was advanced into the Gardiners Clay unit in order to determine the thickness and characteristics of the confining unit. The bore hole was sampled at 5-foot intervals beginning at ground surface to a depth of 50 feet using a 2-foot long 2-inch diameter split spoon. Below 50 feet the boring was sampled continuously at 2-foot intervals to 100 feet below ground surface. PTMW-2, located 12 feet west of PTW-1, was advanced to 92 feet below ground surface and was sampled continuously at 2-foot intervals beginning at 82 feet below surface to confirm the downhole information collected during the drilling of PTMW-1. PTMW-3, located 50 feet west of PTW-1, was advanced to 95 feet below



ground surface. Upon retrieval of each split spoon, the sample was logged in accordance with the Modified Burmeister Soil Classification System. The boring logs are provided in Appendix A. In general, the soils can be classified as fine to coarse sand from grade to 70 feet below ground surface and silty, fine to coarse sand with interbedded sandy-clay lenses to 95 feet, where a prominent clay layer at least 5 feet thick was encountered.

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Five split spoon samples were selected from PTMW-1 for grain size analysis to determine the appropriate screen slot size for the pump test well. The samples were selected from the planned depth interval for the pump test well screen (72 to 92 feet below surface). The results of the grain size analyses are provided in Appendix B. A discussion of the results is presented in Section 2.3.2.

The three observation wells were constructed with 2-inch diameter, Schedule 40, threaded flush joint PVC riser pipe and 20-foot long 10-slot, Schedule 40 PVC well screen. PTMW-1 and PTMW-3 were screened from 73 to 93 feet below ground surface and PTMW-2 was screened from 62 to 82 feet below ground surface. Each observation well was installed in approximately a 6.5-inch diameter borehole. Number 1 Grade gravel pack was tremied around the well screen beginning at two feet below the bottom of the well screen to two feet above the top of the well screen. A 2-foot thick bentonite seal was then placed above the sand pack. The remaining annular space was backfilled with a bentonite/cement grout mix prior to cementing a flush mounted monitoring well manhole to complete the installation. The well construction logs are provided in Appendix C. The wells were developed by pumping and surging to remove sediment from the well and to provide hydraulic connection to the surrounding formation on October 14, 1999.

#### 2.3.2 Extraction Well

The extraction well, PTW-1, was installed on October 12, 1999, using the mud rotary technique. The location of the pump test well and screened interval was based on the results of the plume delineation program (see Figure 2-3).

2-11

The results of the grain size analyses for the samples collected during drilling of PTMW-1 were provided to Uni-Tech Drilling Company, Inc., and a pumping rate of 150 gpm was specified. Based on the information provided, Uni-Tech recommended a 40-slot screen. As a result, the extraction well was constructed with 6-inch diameter, Schedule 80, threaded flush joint PVC riser pipe and 20-foot long 40-slot, continuous-slot stainless steel well screen installed at a depth of 73 to 93 feet below ground surface. The extraction well was constructed in a 14-inch diameter borehole. Number 2 Grade gravel pack was tremied around the well screen beginning at two feet below the bottom of the well screen to 9 feet above the top of the well screen. The gravel pack was tremied to 9 feet above the well screen to prevent settling and consolidation of the sealing and grouting material into the screen zone. A 2-foot thick bentonite seal was then placed above the sandpack. The remaining annular space was backfilled with a bentonite/cement grout mix prior to cementing a flush mounted monitoring well manhole to complete installation. The well construction log is provided in Appendix C. The well was developed by pumping and surging to remove sediment from the well and to provide hydraulic connection to the surrounding formation on October 14, 1999.

#### 2.3.3 Pre-test Data Logging and Recording

Prior to the start of the pump test, pressure transducers were installed to continuously collect background groundwater elevation data from the newly installed wells, PTMW-1, PTMW-2, PTMW-3, and existing well MW-4D (see Figures 1-2 and 2-3). Groundwater elevations were measured in each well continuously for 8 days at 10-minute intervals. The pressure transducers used were Troll 4,000s manufactured by In-Situ Inc. The Trolls are fully submersible, 1.5-inch diameter stainless steel pressure transducers capable of collecting water elevations and temperature measurements. The Trolls were installed at a depth of 50 feet below ground surface in each well and were pre-programmed using the vendor supplied *Win-Situ*<sup>TM</sup> software to digitally collect and store data. The data collected prior to the pump test to establish a baseline indicates a non-fluctuating groundwater-table.

Immediately prior to beginning the pump test, the Trolls were programmed via a laptop computer to collected data at 3-second intervals, therefore, capturing both the drawdown and recovery data. Upon completion of the tests, the Trolls were programmed to collect data at 10-minute intervals for the following 4 days.

#### 2.3.4 Pump Test

A pre-test and three (3) aquifer pump tests were conducted using extraction well PTW-1 and monitoring wells PTMW-1, PTMW-2, PTMW-3 and MW-4D on November 9 through November 11, 1999. Monitoring wells PTMW-1, PTMW-2 and PTMW-3, located around the pump test well at varying distances (27, 12 and 50 feet, respectively) (see Figure 2-3), were used to gauge water table drawdown as a function of distance during the test. MW-4D is located outside the expected zone of influence of the extraction well, and therefore, was used to monitor for background fluctuations in the water table.

A Grundfos pump (Model 135650-3) supplied by NYSDEC was installed in PTW-1 by Uni-Tech Drilling Co. on October 14, 1999, at a depth of 60 feet below ground surface. The pump plate indicated a flow rate of 75 to 189 gallons per minute (gpm) at a discharge head of 137 to 61 feet of water column. Two-inch ID polyethylene tubing extending from the pump to ground surface was installed to convey the pump discharge. Two-inch Schedule 40 PVC was used to connect the well head to the inline check valve, gate valve and flow totalizer and ultimately to the 3-inch discharge hose. Approximately 1,000 feet of hose was required to discharge into a Nassau County sanitary sewer system manhole located on Woodland Drive approximately 70 feet east of the intersection with Hempstead Avenue with County authorization. The inline totalizer was utilized to monitor the flow of groundwater discharged from the extraction well. The gate valve was used to regulate flow rate. A control panel was installed to control operation of the pump. A laptop computer was used to program and monitor the pressure transducers.

The pre-test was completed on November 9, 1999, starting at 14:35 and ending at 16:00. Prior to the start of the pretest, a pressure transducer was installed in the extraction well to collect drawdown data. The pre-test was performed to determine the maximum drawdown and maximum pumping rate of the pump under field conditions and to determine whether the observation wells were located within the zone of influence of the extraction well. Additionally, the pre-test was completed to establish the reliability of the equipment and ensure proper flow and discharge. During the pre-test, the pump was operated continuously at 92 gpm for two hours producing a drawdown of 34.5 feet in the extraction well. The flow rate produced drawdown in PTMW-1, PTMW-2 and PTMW-3 ranging from 1.8 ft to 3.5 ft, indicating usable data would be collected from the observation wells during the actual pump tests.

The first pump test was started on November 9, 1999, at 20:00. The test was performed at a flow rate of 80 gpm for approximately 8.3 hours prior to drawdown stabilization in all monitoring wells. Upon drawdown stabilization, the pump was shut down on November 10, 1999, at 4:14 and the aquifer was allowed to recover to pre-pumping conditions. The extraction well and all monitoring wells returned to pre-pumping conditions by 10:05 of the same day. Prior to shut down, a discharge sample was collected for analysis of chlorinated volatile organic compounds, dissolved iron and dissolved manganese by Methods 601, 236.1 and 243.2, respectively. The analyses for iron and manganese were performed to provide data needed for design of the treatment system (see Section 4.0). The results were 29.4 ug/l, 54 ug/l and 650 ug/l for dissolved iron, dissolved manganese and tetrachloroethene, respectively.

The second test was started upon full recovery of the extraction well and monitoring wells on November 10, 1999, at 10:05. The second test was performed for approximately 8.7 hours at a flow rate of 65 gpm, ending at 16:48 when drawdown conditions had stabilized. The recovery data was collected until 11:30 on November 11, 1999. An additional final test was run following full recovery for approximately 20 minutes at a constant flow rate of 62 gpm.

Post-test data was collected from November 11 to November 15, 1999. The Trolls were reprogrammed on November 11, 1999, to collect data at 10 minute intervals. The post-test was completed to detect any post-pump test trends or fluctuation in the water table. Over the course of the post-test, no fluctuations or trends were detected.

#### 2.4 Pump Test Results

#### 2.4.1 Methods of Analysis

The data from the pump test was analyzed using the Aquifer Test for Windows pumping test and slug test analysis software package furnished by Waterloo Hydrogeologic of Waterloo, Ontario. The software contains routines for estimation of transmissivity, hydraulic conductivity and storativity for confined and unconfined aquifers. Aquifer Test allows complete analysis of the pump test data via the Cooper and Jacob distance-drawdown method, time-drawdown method and distance-time-drawdown method. The recovery data for each well was analyzed using the Theis and Jacob recovery method. Appendix D provides the pump test data as well as graphical presentations of the result of each analysis.

The distance-drawdown method utilizes a minimum of three observation wells. The distance from each observation well to the extraction well is plotted versus the drawdown at a specified time during the pump test. A best fit straight line is drawn, yielding a slope that is used to calculate transmissivity. The hydraulic conductivity is then obtained by dividing the transmissivity by the aquifer thickness (72 ft).

The time-drawdown method uses the drawdown and time data obtained from an observation well, the distance from the extraction well and the pumping rate. The time is plotted versus the drawdown on a semi-logarithmic graph. A best fit straight line is drawn, yielding a slope that is used to calculate transmissivity. The hydraulic conductivity is then obtained by dividing the transmissivity by the aquifer thickness (72 ft).

The time-distance-drawdown method uses the drawdown and time data collected from an observation well, the distance from the extraction well and the pumping rate. The drawdown is plotted versus time divided by the distance squared on a semi-logarithmic graph. A best fit straight line is drawn, yielding a slope that is used to calculate transmissivity. The hydraulic conductivity is then obtained by dividing the transmissivity by the aquifer thickness (72 ft).

The recovery data for each well was analyzed using the Theis and Jacob recovery test method. The method uses the recovery data of an observation well, the distance from the extraction well and pumping duration. The drawdown is plotted versus the ratio of total time since pumping began and time since pumping ceased. A best fit straight line is drawn, yielding a slope that is used to calculate transmissivity. The hydraulic conductivity is then obtained by dividing the transmissivity by the aquifer thickness (72 ft).

#### 2.4.2 Analysis of Pump Test 1

The first pump test was started on November 9, 1999, at 20:00. The test was performed at a constant flow rate of 80 gpm. A maximum drawdown of 26.6 feet was measured in PTW-1. Maximum drawdowns measured in PTMW-1, PTMW-2 and PTMW-3 were 1.84, 3.86 and 1.87 feet, respectively, after approximately 8.3 hours of pump operation. A hydraulic conductivity was not calculated for PTMW-2 and a distance-drawdown analysis was not completed due to a malfunction of the transducer in PTMW-2. Data from the start of the test to approximately one hour into the test was lost due to the malfunction. The data collected from the test was analyzed using the Cooper and Jacob distance-time-drawdown and time-drawdown methods. The results reveal hydraulic conductivities of 19 ft/day and 21 ft/day for PTMW-1 and PTMW-3 as summarized in Table 2-2 below. The low hydraulic conductivities calculated for PTMW-1 may be due to incomplete development of the well. Graphical representations of the analyses are presented in Appendix D.

#### Table 2-2

#### Pump Test 1 Results of Analysis of Drawdown Data

Test 1 (80 gpm)	Hydraulic Conductivity (ft/day)					
Cooper and Jacob Method	PTMW-1	PTMW-2	PTMW-3			
Distance-Time-Drawdown	19	NA	21			
Time-Drawdown	19	NA	20			

Upon stabilization of drawdown during Test 1, the pump was turned off and the Trolls collected the recovery data. The data was analyzed using the Theis and Jacob recovery test method. Based on the results of the analysis the hydraulic conductivities are 24 ft/day, 11 ft/day and 27 ft/day, respectively, for PTMW-1, PTMW-2 and PTMW-3. The results are tabulated in Table 2-3 below.

#### Table 2-3

#### Pump Test 1 Results of Analysis of Recovery Data

Test 1 (80 gpm)	Hydraulic Conductivity (ft/day)					
Theis and Jacob Method	PTMW-1	PTMW-2	PTMW-3			
Recovery Test	24	11	27			

#### 2.4.3 Analysis of Pump Test 2

The second test was started upon full recovery of the extraction well and all monitoring wells on November 10, 1999, at 10:05. The test was performed at a constant flow rate of 65 gpm. A maximum drawdown of 20 feet was measured in PTW-1. Maximum drawdown measurements of 1.34, 3.01 and 1.38 feet were recorded in PTMW-1, PTMW-2 and PTMW-3, respectively, after approximately 8.7 hours of pump operation. Analysis of the maximum drawdown data for the three monitoring wells using the Cooper and Jacob distance-drawdown method indicated a hydraulic conductivity of 21 ft/day. The data collected from the test was also analyzed using the Cooper and Jacob distance-time-drawdown and time-drawdown methods. The results reveal hydraulic conductivities of 23 ft/day, 12 ft/day and 25 ft/day for PTMW-1, PTMW-2 and PTMW-3, respectively, as summarized in Table 2-4 below. Graphical representations of the analyses are presented in Appendix D.

#### Table 2-4

#### Pump Test 2 Results of Analysis of Drawdown Data

Test 2 (65 gpm)	Hydraulic Conductivity (ft/day)					
Cooper and Jacob Method	PTMW-1	PTMW-2	PTMW-3			
Distance-Time-Drawdown	23	12	25			
Time-Drawdown	23	12	25			

Upon stabilization of drawdown in each observation well during Test 2, the pump was turned off and the recovery data was collected. The data was analyzed using the Theis and Jacob recovery test method. Based on the results of the analysis the hydraulic conductivities are 23 ft/day, 12 ft/day and 21 ft/day, respectively, for PTMW-1, PTMW-2 and PTMW-3. The results are tabulated in Table 2-5 below.

#### Table 2-5

#### Pump Test 2 Results of Analysis of Recovery Data

Test 2 (65 gpm)	Hydraulic Conductivity (ft/day)					
Theis and Jacob Method	PTMW-1	PTMW-2	PTMW-3			
Recovery Test	23	12	21			

#### 2.4.4 Analysis of Pump Test 3

An additional pump test was completed on November 11, 1999. The test was run for a total of 20 minutes at a constant flow rate of 62 gpm. The test was completed to obtain additional data for the initial drawdown exhibited by the observation and extraction wells. The maximum drawdown in PTW-1 was recorded as 18.9 feet. Maximum drawdowns measured in PTMW-1, PTMW-2 and PTMW-3 were 1.28, 2.8 and 1.33 feet, respectively, after approximately 20 minutes of pump operation. Analysis of the maximum drawdown data for the three monitoring wells using the Cooper and Jacob distance-drawdown method indicated a

hydraulic conductivity of 21 ft/day. The data collected from the test was also analyzed using the Cooper and Jacob distance-time-drawdown and time-drawdown methods. The results indicate hydraulic conductivities of 22 ft/day, 11 to 12 ft/day and 22 ft/day for PTMW-1, PTMW-2 and PTMW-3, respectively, as summarized in Table 2-6 below. Graphical representations of the analyses are presented in Appendix D.

#### Table 2-6

Test 3 (62 gpm)	Hydraulic Conductivity (ft/day)		
Cooper and Jacob Method	PTMW-1	PTMW-2	PTMW-3
Distance-Time-Drawdown	21	12	22
Time-Drawdown	22	11	22

#### Pump Test 3 Results of Analysis of Drawdown Data

In summary, the results of the analyses of the pump test data indicate an aquifer hydraulic conductivity ranging from 11 ft/day to 27 ft/day. The analyses of the drawdown and recovery data collected from PTMW-1 and PTMW-3 exhibit fairly good correlation (results ranged from 19 ft/day to 27 ft/day). These results also correlate well with the results of the Cooper and Jacob distance-drawdown method analyses which utilize data from all monitoring wells concurrently (results were 21 ft/day for both Pump Tests 2 and 3).

The results obtained from the drawdown and recovery data for PTMW-2 do not correlate well with the results obtained for PTMW-1 and PTMW-3. The results obtained from PTMW-2 range from 11 ft/day to 12 ft/day. The difference may be the result of the shallower screen interval of PTMW-2 (62 to 82 feet bgs) as compared to PTMW-1 and PTMW-3 (73 to 93 feet bgs) that reflects the effect of a vertical anisotropy in hydraulic conductivity. The lower hydraulic conductivity in PTMW-2 indicates less permeable soil layers at the shallower depth, which is consistent with downhole observations recorded during well construction and sampling of nearby well PTMW-1. The soil found in the 65 to 85-foot depth interval contained a higher

percentage of finer sand and clay than the soil found at the deeper intervals (i.e., 85 to 95 foot bgs).

In conclusion, the results indicate a hydraulic conductivity for unconsolidated sands and silts at the site ranging from 11 ft/day to 27 ft/day. These rates are consistent with the range reported for silty sand to medium sand by Freeze and Cherry (1979) (3 to 28 ft/day). For the purposed of modeling the required extraction well capture zone, a more conservative hydraulic conductivity (30 ft/day) will be used.

# **Section 3**

#### 3.0 BASIS OF DESIGN

#### 3.1 Introduction

As discussed in Section 1.0, the objective of this Remedial Measure (RM) is to construct an extraction and treatment system to contain and treat the contaminated groundwater plume migrating from the Franklin Cleaners Site. Accordingly, using the plume delineation and pump test results presented in Section 2.0, the capture zone was modeled for multiple pumping well configurations and pumping rates to evaluate potential system configuration options. The objective is to capture the entire width of the plume at the planned location for construction of the extraction system. The plume has been defined as the zone of groundwater exhibiting greater than 5 ug/l of tetrachloroethene contamination (see Figure 2-2). Additionally, in this section site constraints, management of treated water and basic treatment system design data are addressed.

#### 3.2 Capture Zone Modeling

A simplified two-dimensional modeling analysis was performed to evaluate extraction well configurations and groundwater extraction rates. Capture zone estimates were calculated using  $WinFlow^{TM}$ , a 2-dimensional (2-D), steady-state groundwater flow model supplied by Environmental Simulations, Inc. The 2-D model simulates groundwater flow in a horizontal plane using analytical functions developed by Strack (1989). A range of groundwater extraction rates and extraction well locations were evaluated.

The aquifer characteristics input into the model were based on site-specific information obtained during the RI, the groundwater delineation program and the pump test. The input characteristics include the following:

- Hydraulic Conductivity 30 ft/day
- Storativity 0.2
- Transmissivity 2,160 ft<sup>2</sup>/day
- Horizontal Gradient 0.00017 ft/ft

3-1
- Porosity-0.2
- Saturated Aquifer Thickness 72 feet

The targeted area for location of the extraction well(s) is between the boundaries of the Molloy College and Mercy Hospital properties along the shoulder of the east bound Southern State Parkway. The location is downgradient of the Franklin Cleaners Site and upgradient of the Village of Rockville Centre public water supply wells and perpendicular to the flow path of the plume.

One and two well extraction scenarios were evaluated at cumulative extraction rates of 15, 20, 30 and 40 gpm. Existing extraction well PTW-1 was utilized in both the single extraction well and two well scenarios. For the two well scenario, a second extraction point with the same screen diameter as PTW-1 was modeled. The second well, PTW-2 was located approximately 120 feet west of PTW-1. The flow was distributed equally between the two wells (PTW-1 and PTW-2) when modeling the two well scenario. Figure 3-1 illustrates pre-pumping conditions using the aquifer characteristics described above.

The results of the single well capture zone modeling using flow rates of 15, 20, 30 and 40 gpm indicate capture zones of approximately 270, 490, 720 and 1,000 feet in width, respectively, at the point of extraction (see Figures 3-2, 3-3, 3-4 and 3-5). The results of the two well capture zone modeling using cumulative flow rates of 15, 20, 30 and 40 gpm indicate capture zones of approximately 350, 500, 720 and 990 feet in width, respectively (see Figures 3-6, 3-7, 3-8 and 3-9). As discussed above, a minimum plume width of 450 feet is recommended for determining the required capture zone width. Therefore, the results of the modeling indicate that the minimum required cumulative pumping rate for plume containment is 20 gpm. Based on the results of the modeling this conclusion applies to both the single well and two well scenarios.

Based on the results of the modeling, a one or two extraction well configuration may be used to contain the groundwater plume. Although one well would result in a savings in construction costs, the two well configuration provides operational flexibility which would not



75-	
73-	
WATER TABLE ELEVATION IN FEET FROM ASSUMED DATUM (I.e., TOP OF CLAY LAYER)	
0 300' 600 SCALE: 1"=300'	,



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75-
74
72
WATER TABLE ELEVATION IN FEET FROM   ASSUMED DATUM (i.e., TOP OF CLAY LAYER)   0 300'   500'   SCALE:
FIGURE 3-2



75-
74-
WATER TABLE ELEVATION IN FEET FROM
ASSUMED DATUM (I.e., TOP OF CLAY LAYER)
FIGURE 3-2





B

k

75-
74
72
ASSUMED DATUM (I.e., TOP OF CLAY LAYER)
0 300' 600' SCALE: 1"=300'
FIGURE 3-4





I I I

4







be provided by the one well configuration. For example, one well may be taken down for servicing without shutting down the entire system and maintaining containment of the plume. Also, flow rates can be increased or reduced in separate parts of the plume if a change in contaminant concentrations indicate such a change would be beneficial. The additional cost associated with one additional extraction well, including the pump and appurtenances, is estimated to be less than \$20,000. Therefore, a two well configuration is recommended.

Since the model is based on a simplification of actual site conditions and uses several assumptions, a factor of safety is recommended to provide a flow rate that captures the full width of the plume. It is recommended that the extraction system be designed for a cumulative flow rate of 70 gpm (i.e., two wells each extracting 35 gpm). The incremental cost increase for the higher flow rate would be minimal and would provide a margin of safety which accounts for potential effects of the heterogeneous nature of the aquifer and the simplifying assumptions of the model as well as providing the capability to extract greater quantities of groundwater, if required, and operate with a single well during servicing (as discussed above). Initially groundwater would be extracted at approximately 20 gpm to minimize unnecessary pumping and treatment of clean groundwater. The extraction rate would then be increased if necessary based on the results of downgradient groundwater monitoring.

#### 3.3 Site Constraints

The treatment system equipment will be housed in a small building within the limits of the wooded area, between the boundaries of Molloy College and Mercy Hospital, south of the east bound Southern State Parkway as shown on Drawing 1 presented in a map pocket at the back of this document. This property is owned by the New York State Office of Parks, Recreation and Historic Preservation (NYSOPR&HP). Presently, plans are to access the property for construction, operations and maintenance via the Molloy College property (see Drawing 1). As a result, agreements will be required with both NYSOPR&HP and Molloy College. Additionally, approval of the plans for clearing and landscaping will be required from NYSOPR&HP.

#### 3.4 Treated Water Discharge

Treated groundwater will be discharged to the existing Nassau County Department of Public Works (NCDPW) storm drain system. The closest storm drain manhole is located on Hempstead Avenue near the intersection with Woodland Drive (see Drawing 1). NCDPW has indicated that the storm drain system in this area could accept the additional flow (see Appendix E). However, the remediation system shall be designed to cease discharge during a large storm event which would result in an exceedence of the storm drain capacity.

In order to discharge treated groundwater to the storm drain system, piping will be installed from the treatment system to the storm drain manhole as shown on Drawing 1. The piping will be installed below grade on property owned by NYSOPR&HP, parallel to the Molloy College property boundary, prior to intersecting Hempstead Avenue.

The storm drain manhole located on Hempstead Avenue is connected to an 18-inch diameter reinforced concrete pipe (RCP). The flow along Hempstead Avenue is south. The 18-inch pipe expands to a 24-inch pipe at the intersection of Beech Street. At the intersection of Bulson Road, the flow heads west until the intersection of North Village Avenue where it connects to a 30-inch pipe and heads south. At the intersection of North Village Avenue and DeMott Avenue the 30-inch pipe expands to a 36-inch pipe. The flow then turns onto Lakeside Drive where the pipe is connected to a 42-inch pipe at the intersection of Maine Avenue. Lakeside Drive becomes North Centre Avenue and at the intersection of Maine Avenue the 42-inch pipe connects to a 48-inch pipe. At the intersection of Nassau Avenue and North Centre Avenue the storm drain flows west, until the intersection with Banks Avenue. On Banks Avenue the flow is south until Nassau Avenue, where flow is west along Nassau Avenue. The storm drain system ends at a headwall located on Nassau Avenue just south of Smith Pond, also known as Smith Lake, combines with the overflow from Smith Pond and discharges into the head of Mill River.

Mill River receives the discharge from the storm drain system in this area. Mill River is an existing stream that ultimately discharges into Reynolds Channel. Based on a discussion with James Beach (NYSDEC, Division of Water) Mill River is classified as a Class SC surface water body. NYSDEC regulations, 6 NYCRR 703 (Surface Water and Groundwater Quality Standards and Groundwater Effluent Limits), establish a guidance value of 1.0 ug/l for tetrachloroethene (PCE) in a Class SC water body.

Approvals to connect to the storm drain system will be required from the NCDPW. In order to install pipe along the Hempstead Avenue right-of-way and across Hempstead Avenue and connect to and use the storm drain system, NCDPW road opening and connection permits are required. Based on discussions with NYSDEC, a State Pollution Discharge Elimination System (SPDES) permit will not be required since this is a New York State Superfund project; however, compliance with the substantive requirements of the SPDES regulations is required.

#### 3.5 Design Data

It was anticipated that the major treatment system unit operations would include groundwater extraction, metals (Fe and Mn) removal, pH adjustment, removal of volatile organic compounds (VOCs) and vapor phase treatment. As a result, the key design data for the system includes anticipated concentrations of PCE, iron (Fe), manganese (Mn) and pH in the extracted groundwater. Table 3-1 summarizes the design data obtained during the groundwater plume delineation program and the pump test.

Iron and manganese were detected in the pump test discharge sample at concentrations of 29.4 ug/l and 54 ug/l, respectively. There are no standards or guidance values listed by the NYSDEC for discharge of iron and manganese to a Class SC water body, however, removal of iron and manganese may be required to avoid problems associated with operation of the air stripping system being considered for the removal of PCE and other volatile organic compounds in the groundwater contaminant plume.

As stated above, the NYSDEC guidance value is 1.0 ug/l for PCE for discharge to a Class SC water body. Most of the Geoprobe and hydropunch samples in the project area exhibited concentrations above this value (1,200 ug/l and 960 ug/l for GP-W11 and GP-W12,

# Table 3-1

3

# FRANKLIN CLEANERS SITE GROUNDWATER EXTRACTION AND TREATMENT REMEDIAL MEASURE ENGINEERING REPORT DESIGN DATA SUMMARY

# Concentration (ug/l) in Groundwater Samples

<u>Constituent</u>	Pump Test Discharge Sample <u>PT-GW</u>	Probe Point Sample Location <u>GP-W11</u>	Probe Point Sample Location <u>GP-W12</u>	NYSDEC Class SC Guidance <u>Value</u>
PCE	650	1,200	960	1
Iron (Fe)	29.4	NA	NA	NS
Manganese (Mn)	54	NA	NA	NS
pH	6.2	5.32	6.44	NS

## Notes:

1. All constituents analyzed for in laboratory except for pH, which is field measured.

2. See Figure 2-1 for probe locations and Figure 2-3 for well location.

NS - No standard

NA - Not analyzed

respectively). The treatment system will be designed to remove PCE at the maximum concentration of 1,200 ug/l detected to a concentration of 1.0 ug/l.

# **Section 4**

#### 4.0 EXTRACTION AND TREATMENT SYSTEM PROCESS DESIGN

#### 4.1 Introduction

As discussed in Section 3, the extraction system will be designed to remove the contaminated groundwater with two wells and the treatment system will be designed to reduce PCE from an inlet concentration of 1,200 ug/l to a discharge concentration of 1.0 ug/l at a maximum flow rate of 70 gpm. As described in the Remedial Investigation and Feasibility Study (RI/FS) Report and Record of Decision (ROD), air stripping is the treatment technology that has been selected for removal of VOCs from the groundwater. Additionally, as described in the RI/FS Report and ROD, granular activated carbon will be used to treat the exhaust gas from the air stripping process prior to discharge to the atmosphere.

#### 4.2 System Layout

Based on the flow path, plume width and chemical characteristics of the groundwater plume to be contained, the major treatment system equipment required will include two extraction wells, a low profile air stripper, two granular activated carbon (GAC) vessels for air stripper exhaust gas treatment and a lift station to convey the treated discharge to the storm water sewer system. A flow schematic of the treatment system is presented as Figure 4-1. The treatment system will be housed in a split-face concrete block building. Drawing 1 shows the proposed location of the extraction and treatment system, and the general arrangement of equipment is shown on Figure 4-2.

#### 4.3 Pre-Treatment

Based on review of data presented in Section 3 and the results of the groundwater sampling during the remedial investigation, as well as communications with system vendors, pretreatment, including iron and manganese removal and filtration are not required as part of the groundwater treatment process for this project. As shown in Table 3-1, concentrations of iron and manganese detected in the pump test discharge were 29.4 ug/l and 54 ug/l, respectively.



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Additionally, during completion of the RI, samples collected from MW-4I (screened at a depth of 38 to 53 feet below ground surface) and MW-4D (screened at a depth of 62 to 77 feet below ground surface) located approximately 1,100 feet upgradient of the planned extraction wells (see Figure 1-2), exhibited a maximum manganese concentration of 29.8 ug/l, while iron was not detected in either well. (The instrument detection limit for iron was 9.7 ug/l.) Similar concentrations of these constituents were also detected in groundwater monitoring wells further upgradient which were sampled during the RI. Typically, concentrations of iron and manganese below 1 mg/l indicate that these inorganic constituents will not pose any operations and maintenance concerns for an air stripping system.

## 4.4 Extraction Wells and Influent Piping

As indicated in Section 3, two extraction wells located on property which is part of the Southern State Parkway, pumping at a total maximum flow rate of 70 gpm, will be used to contain the groundwater plume. In addition to the existing extraction well (PTW-1), a second extraction well, PTW-2, located approximately 120 feet west of PTW-1 will be installed. The location of the extraction wells is shown on Drawing 1.

Based on the preliminary results of the pre-design study plume delineation program, PTW-1 was constructed to draw water from 73 to 93 feet below ground surface. As discussed in Section 2, the plume delineation program indicated that the groundwater contamination is concentrated at a depth of approximately 80 to 95 feet below ground surface, immediately above a confining layer.

#### 4.4.1 Screen Depth and Casing

Extraction well PTW-2 will be constructed with the same diameter and materials as PTW-1 as described in Section 3; however, the length and screen depth interval will differ. Well PTW-2 will be installed to a depth of 95 feet below ground surface. The riser will be 6-inch diameter, Schedule 80, threaded flush joint PVC. A 15-foot long, continuous-slot stainless steel well screen will be installed at a depth of 80 to 95 feet below ground surface. The extraction well

will be installed in a minimum 10-inch diameter borehole. Number 2 Grade gravel pack will be tremied around the well screen beginning at 2 feet below the bottom of the well screen to 10 feet above the top of the well screen. The gravel pack is tremied to 10 feet above the well screen to prevent settling, and consolidation of the sealing and grout material into the screen zone. The remaining annular space will be backfilled with a bentonite/cement grout mix prior to cementing a flush-mounted vault to complete the installation. The well head will be installed in a vault for reasons of safety since the wells will be located approximately 20 feet from the parkway on the shoulder of the roadway. Figure 4-3 illustrates the typical extraction well construction.

#### 4.4.2 Extraction Well Pumps

A submersible well pump will be installed in each extraction well approximately 5 feet above the top of the screen. Four-inch diameter pumps equipped with approximately two horsepower inverter duty rated motors will provide the required flow and discharge head. Each pump will be connected to a variable frequency drive (VFD) controller located in the main control panel. The VFD controllers will provide the capability to operate each pump individually at a flow rate ranging from approximately 5 to 35 gpm. Two-inch diameter PVC pipe will extend from each pump to convey the pump discharge to ground surface.

#### 4.4.3 Influent Piping

The discharge piping from each well will deliver the extracted groundwater to the treatment system. The piping will be 2-inch diameter PVC pipe. The piping will be installed below the frost line to prevent freezing and damage to the piping system. The general layout of the piping is shown on Drawing 1.



## 4.5 Air Stripping System

As previously discussed, the air stripping system will be designed to reduce PCE in the extracted groundwater from an inlet concentration of 1,200 ug/l to 1 ug/l at a maximum flow rate of 70 gpm. As shown in Table 4-1, a discharge concentration of less than 0.5 ug/l PCE is expected to be achievable with a low profile air stripper at 70 gpm. This provides a factor of safety with respect to the surface water discharge limit of 1 ug/l. Based on communications with system vendors, however, any significant increase in groundwater extraction rates would require a larger air stripper in order to achieve the required removal efficiency for PCE. Air stripper performance has also been evaluated with respect to the additional volatile organic compounds detected during the plume delineation program, as summarized in Table 4-1. The influent contaminant concentrations shown in Table 4-1 represent the highest concentration of each contaminant detected during the plume delineation program.

The air stripper specified for this project to meet the liquid phase discharge criteria will be a skid-mounted low-profile air stripper. The estimated dimensions of the air stripper are approximately 8 feet high, 6 feet long and 4 feet wide. The air stripper will be installed inside the treatment system building. Typically, low-profile air stripping systems operate by countercurrent flow through horizontally positioned aeration trays. The groundwater flows downward through small (approximately 3/16-inch) holes in the aeration trays, while at the same time clean air is pulled up through the same holes. As a result, VOCs are transferred from the liquid phase to the vapor phase. Tray cleanout and inspection ports will be specified, as well as the capability to easily remove each tray to facilitate more thorough inspections and cleaning.

The low-profile air stripper will include an integral approximately 20 HP blower capable of supplying approximately 600 scfm (air to water ratio of approximately 64 to 1). Ambient air is introduced to the air stripper through the bottom and exits from the top by means of an induced draft. A mist eliminator located on the exhaust port of the air stripper will remove water droplets entrained in the exhaust gas prior to exiting the air stripper. The blower will be sized to provide the discharge pressure required to convey the exhaust gas through the exhaust gas treatment system.

4-7

#### Table 4-1

	Influent Concentration (ppb)	Effluent Co	NYSDEC Class	
Contaminant		Liquid Phase (ppb)	Vapor Phase (ppmv)	SC Surface Water Standard/ Guidance Value (ppb)
Tetrachloroethene	1,200	0.23	2.7	1 ST
Trichloroethene	7	<1	0	40 GV
1,1-Dichloroethene	10	<1	0	_2
1,1,1-Trichloroethane	10	<1	0	_2
1,1,2-Trichloroethane	10	4	0	_2
1,2-Dichloroethane	7	3	0	_2

# FRANKLIN CLEANERS SITE SUMMARY OF EXPECTED AIR STRIPPER PERFORMANCE

<sup>1</sup>Based on modeling performed by North East Environmental Products, Inc. for a Model 2651 shallow tray low profile air stripper.

<sup>2</sup>NYSDEC regulations, 6 NYCRR 703.5 establish no discharge Standard or Guidance Value for this compound.

# Abbreviations:

ppb = Parts per billion ppmv = Parts per million volume ST = Standard GV = Guidance Value Influent to the low-profile air stripper will be pumped from the two extraction wells, to the top of the air stripper. Spray nozzles will break up the water flow into droplets as it enters the stripper and uniformly distribute flow across the surface area of the trays, thereby enhancing mass transfer. The treated effluent will discharge from the bottom of the air stripper to the lift station prior to discharge to the NCDPW storm drain system (see Figure 4-1).

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#### 4.6 Exhaust Gas Treatment System

#### 4.6.1 Exhaust Gas Characteristics

The design characteristics of the low-profile air stripper exhaust gas stream are based on the design liquid phase inlet and outlet concentrations of tetrachloroethene of 1,200 ug/l and 1.0 ug/l, respectively, a groundwater flow rate of 70 gpm and an air flow rate of 600 scfm at 50°F and 1 atm. This equates to a mass vapor phase exhaust rate of 0.04 lb/hr of PCE (2.7 ppm). The predicted mass vapor phase exhaust rate for the additional contaminants detected during the plume delineation program, as shown in Table 4-1, are expected to be insignificant.

An estimate of potential air impacts at a PCE exhaust rate of 0.04 lb/hr was calculated using the standard point source method in the NYSDEC Air Guide-1. Based on the calculations, a stack height of approximately 25 to 30 feet would be required for the uncontrolled emission in order to comply with the annual guideline concentration of 1.2 ug/m<sup>3</sup> for PCE. Since this would be inconsistent with the project objective of maintaining a low profile treatment system, granular activated carbon will be used for exhaust gas treatment, as described in the RI/FS Report and ROD. The treated exhaust gas will be discharged at a height of approximately 3 feet above the roof of the treatment system building.

#### 4.6.2 Carbon Adsorption System Design Parameters

The fixed bed granular activated carbon adsorption system will be designed to remove 99 percent of the PCE in the low-profile air stripping system exhaust gas. The system will consist of two granular activated carbon vessels in series, an exhaust discharge stack and associated piping, valves and controls as shown in the schematic on Figure 4-1. This configuration will result in a flow rate of approximately 600 scfm (at 50°F) to each vessel. The secondary vessel in the series serves as a backup to control emissions when breakthrough of the primary vessel occurs and allows for continuous operation without continuous monitoring.

Each carbon vessel will be charged with approximately 1,000 pounds of activated  $4 \times 10$ -mesh carbon. The overall height of each canister will be approximately 5 feet, the dimensions will be approximately 4 feet by 4 feet, and the weight of each loaded vessel will be approximately 1,600 pounds.

Flow will be redirected by valves from the primary vessel to the secondary vessel when breakthrough of the primary vessel occurs and replacement carbon will be added to the "new" secondary vessel. The secondary vessel will discharge to an exhaust stack. Sample ports will be provided on the influent and effluent points on both the primary and secondary vessels to monitor for breakthrough. In addition, pressure gauges will be provided for monitoring pressure drop across each vessel. As discussed above, a mass vapor phase exhaust rate of approximately 0.04 lb/hr of PCE is expected. Based on an estimated PCE to carbon use rate of 1:10 (weight to weight), the carbon use rate is estimated to be approximately 10 pounds per day. Therefore, changeout of the primary vessel (1,000 pounds of carbon) will be required at approximately 100-day intervals.

#### 4.7 Lift Station and Treated Effluent Discharge

#### 4.7.1 Lift Station

The lift station will consist of two discharge pumps (providing 100% redundancy), a clearwell and associated controls. The discharge pumps will be sump pumps, each with a design flow rate of 80 gpm. The clearwell will be sized to accommodate the air stripper volume during a general alarm condition, provide sufficient volume between the discharge pump on/off switches and maintain 1 foot of vertical head above the discharge pumps. As a result, the clearwell will be a pre-cast concrete tank approximately 6 feet in diameter and approximately 8 feet deep.

#### 4.7.2 Treated Effluent Discharge

As discussed in Section 3.4, a force main will be installed to convey the treated water from the lift station to the storm drain manhole located on Hempstead Avenue. The force main will be 3-inch (nominal) diameter PVC pipe buried below the frost line. The general layout of the piping is shown on Drawing 1.

As discussed in Section 3.4, the storm drain system is owned and maintained by the Nassau County Department of Public Works (NCDPW). The NCDPW has indicated that the storm system can accommodate the additional flow (see Appendix E). However, the remediation system will be designed to cease discharge during a large storm event, which would result in an exceedance of the storm drain capacity.

#### 4.8 Electrical

#### 4.8.1 Power Supply Source

Long Island Power Authority (LIPA) electric poles run along the west side of Hempstead Avenue. A 208 volt, 3 phase, 60 hertz service drop will provide the required electrical power. The secondary cable will run below grade from the service drop location to the inside of the treatment system building. Coordination with LIPA to provide this service will be the responsibility of the contractor constructing the treatment system.

#### 4.8.2 Electrical Equipment

A small electrical room will be constructed inside the treatment system building. This electrical room will provide protection for the service meter, voltage breakers, utility panel(s), motor control centers (MCC), and any other control panels and telemetry equipment required to operate the treatment system.

## 4.9 Control Systems

### 4.9.1 General Failure Alarms

Most equipment failure alarms will result in a single "general failure" alarm. A general failure alarm will automatically shut down all electrical equipment except the discharge pumps. The main control panel will include an alarm reset and an adjustable delay during plant startup.

#### 4.9.2 Extraction Wells

Each extraction well pump will be equipped with a high-pressure switch on the pump discharge. If the pump discharge pressure exceeds an adjustable preset value, a general failure alarm will be activated. A sensor will also be provided in each well to activate a general failure alarm if the water level drops below a preset value. The pumps will shut down based on a general failure alarm. The influent flow rate will be manually adjusted using the VFD pump controllers. A hand-off-auto switch will be provided for each well pump.

#### 4.9.3 Air Stripper System

The air stripper sump will be equipped with a high-level float switch, which will activate the general failure alarm. The blower will be equipped with a high-pressure switch on the discharge duct and a high-vacuum switch on the suction duct. These switches will activate a general failure alarm above preset values. In the event of a general failure, the blower will be shut off after a delay to provide for treatment of the groundwater in the stripper at the time of general failure. A local hand-off-auto switch will be provided for the blower. A relay at the blower will confirm operation. If the blower is not operating, a general failure alarm will be activated.

#### 4.9.4 Exhaust Gas Treatment System

In the event of plugging in the GAC vessels, a high-pressure condition would result at the blower discharge activating a general failure alarm.

#### 4.9.5 Lift Station

A high-level float switch located in the clearwell will activate the general failure alarm. Low-level float switches will control the discharge pumps. The discharge pumps will be equipped with a high-pressure switch on the discharge pipe that will activate the general failure alarm. A local hand-off-auto control switch will be provided for each pump.

#### 4.9.6 Storm Drain

The high pressure switch on the clearwell discharge pumps will activate the general failure alarm. This will eliminate discharge from the lift station to the storm drain system during a major storm event.

### 4.9.7 Startup Sequence

The main control panel will start up the air stripper blower first, followed by the two extraction wells. The discharge pumps will start and stop based on the level in the sump and, therefore, will not be controlled by the main control panel.

The main control panel will be equipped with a hand-off-auto switch. In the "hand" mode, all equipment will be operated with the local or hand switches. In the "off" mode, no equipment will operate. In the "auto" mode, the startup sequence will begin. All equipment will continue to operate until a general failure alarm is activated. An adjustable time delay will prevent the general failure alarm from activating at startup.

#### 4.9.8 Telemetry Panel

A telemetry panel will contact the treatment system operator's pager upon a general failure alarm.

#### 4.10 Groundwater Monitoring Well Network

A groundwater monitoring well network, consisting of a total of five wells, will be installed downgradient of the extraction system wells to evaluate the effectiveness of and optimize the operation of the system. Three wells, ASMW-1 through ASMW-3, will be installed south of the treatment system building on property which is part of the Southern State Parkway. ASMW-2 will be located between the two extraction wells and ASMW-1 and ASMW-3 will be located near the estimated western and eastern limits of the plume, respectively. The proposed locations for wells ASMW-1 through ASMW-3 are shown on Drawing 1. Wells ASMW-1 through ASMW-3 will be screened approximately 85 to 95 feet below ground surface.

Groundwater monitoring wells ASMW-4 and ASMW-5 will be installed further downgradient, on Molloy College property. ASMW-4 will be screened above the clay unit, approximately 85 to 95 feet below ground surface, and ASMW-5 will be screened directly below the clay unit, approximately 100 to 110 feet below ground surface.

During construction of wells ASMW-2, ASMW-4 and ASMW-5, soil samples will be collected and analyzed for grain size and permeability to determine the depth, thickness and characteristics of the clay unit and the appropriate well screen depths. A thin-walled tube sampler will be used to collect relatively undisturbed samples of the clay (according to ASTM D1587 or approved equal) for permeability tests. (Only the upper interval of the clay layer will be sampled during construction of ASMW-2.)

Each monitoring well will be constructed in an approximately 8-inch diameter borehole drilled using hollow stem augers. The wells will be constructed of 2-inch diameter threaded,

flush joint Schedule 40 PVC riser and 20-slot screen. The wells will be completed with a concrete flush-mounted surface casing with a steel access cover.

The annulus of the borehole in the area of the screen will be sand-packed to a height of 2 feet above the screened interval with No. 1 Grade clean silica sand. A finer grained No. 00 sand pack material (100 percent passing the No. 30 sieve and less than 2 percent passing the No. 200 sieve), 6 inches in thickness, will be placed on top of the sand pack between the sand and the bentonite seal. A 3-foot seal of bentonite pellets or slurry will be placed immediately above the filter material and 6 inches of No. 00 Grade silica sand pack will be placed above the bentonite seal. The remaining annulus will be grouted to the surface with cement/bentonite grout. The bentonite will be tested and/or warranteed to be free of organic and inorganic contaminants. All material placed in the annulus of the borehole will be installed using a tremie pipe.

# **Section 5**

#### 5.0 PROJECT COST

#### 5.1 Purpose

The purpose of this cost estimate is to provide a budgetary value for funding the construction of the Franklin Cleaners Site Groundwater Extraction and Treatment System. An engineer's cost estimate will be prepared for inclusion in the bid documents after the final design documents (i.e., drawings and specifications) are complete.

#### 5.2 Cost Estimate

This cost estimate presents capital costs based on the conceptual design developed and presented in this report and certain assumptions based on available information at this time. The unit costs are based on manufacturer's estimates, data from recently completed projects and published cost estimating information. A 20 percent estimating contingency has been added due to the limited detailed information available at this time.

Table 5-1 summarizes the cost estimate. As shown, the total estimated capital cost including startup and initial testing is \$494,000.

# Table 5-1

# FRANKLIN CLEANERS SITE GROUNDWATER EXTRACTION AND TREATMENT SYSTEM DESIGN REPORT

# COST ESTIMATE SUMMARY

Work Item	Estimated Cost	
Mob/Demob and Site Clearing	\$25,000	
Site Work	\$50,000	
Groundwater Extraction and Monitoring Wells	\$38,000	
Influent and Effluent Piping	\$38,000	
Treatment System Equipment, Controls and Instrumentation	\$105,000	
Building	\$70,000	
Utilities	\$68,000	
Initial Startup and Testing	\$18,000	14
Subtotal	\$412,000	
Estimating Contingency @ 20%	\$82,000	
GRAND TOTAL	\$494,000	

# Appendix A
# APPENDIX A BORING LOGS

Driller <u>Butc</u> inspector <u>U</u> Rig Type <u>C</u> Drilling Method Drive Hammer GROUNDWAT Water Lavel Time Date Casing Depth Sample Samp Depth Numb	h H / Un ayne Ma me-85 - Auger/ Worgm ER OBSER 23' 7/13 93' SPT	VATIONS	UHILLING LOG         PROJECT NAME Frank in Cleaners         PROJECT #       1640 =         LocationvAddress       Pole 216 Southern         State Park way       State Park way         Weether       Clear         10 w 80's       Date/Time Start         9/13/99       11:00         Date/Time Finish       9/14/99         FIELD IDENTIFICATION OF MATERIAL	BORING I Sheet Boring Loc  Plot Plan	NUMBER <u>P</u> <u>1</u> of _ cation <u>17.5</u> <u>276</u>	H H EFT Easto
Inspector <u>U</u> Rig Type <u>C</u> Drilling Method Drive Hammer GROUNDWAT Water Lavel Time Date Casing Depth Sample Sample Depth Numb 2- <u>2</u> <u>SS+</u>	Ayne M( ME - 85 Auger/ Wolgm ER OBSER 23' 1/13 93' SPT T	Ann Pr. // Rig Split Storm VATIONS CID/FID Reading	PROJECT NAME <u>Franklin Cleaners</u> PROJECT # <u>1640</u> = LocationvAddress <u>Pole 216 Southern</u> <u>State Parkway</u> Weather <u>Clear</u> <u>10w 80's</u> Date/Time Start <u>9//3/99 11:00</u> Date/Time Finish <u>9/14/99 18:30</u> FIELD IDENTIFICATION OF MATERIAL	Sheet Borting Loo  Plot Plan		H FF Easto
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ILLING CONTRACTOR Her <u>Butch H, Uni Tech</u> Dector <u>Wayne Mann</u>	ORILLING LOG PROJECT NAME <u>Franklin Cleaners</u>	BORING NUMBER <u>PTMW-1</u> Sheet <u>2</u> of <u>4</u> Boring Location <u>17.5 Ft east of</u> Role 2/6
TYDE CME-85 Drill Right Meno Method Auger/Splits	PROJECT # 1640 Location Address Pole 216 Southern	
ve Hammer Weight	- State Parkway	
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ater Level 23'	low 80 s	
me	Date/Time Start 9/1.3/17 11:00	
ate 19/13/99	Date/Time Finish ////////////////////////////////////	
asing Depth 931	THE STORATION OF MATERIAL	WELL SCHEMATIC COMMENTS
mole Samole SPT PID/F	FIELD IDENTIFICATION OF WAR CHINA	
eoth Number need	To II hr Brown Dense Medium to	
1-51 0-0	Coarse SAND Trace small founded	
louis 9 20 21.27	Gravel	
1, 10, 14		Benionite
1-53 0.0	) Same	Grout
covery 20"	-	
slows 17, 20, 22, 27	-	2" Puc sit
3-50	53-55 Same	Riser
CIONCE 24"		
Blow \$ 23,14, 14,18		
	CGS7 Sand With I put	
5-57	Libr Rrowin fino to coalse SAM	20 1
Recovery 4	Cigni Diown The rest	
T, 0,1, P1 - 2001 C		
57-589	57-59 Jan/Drange Brown measure De	
receivery 24"	Fine to Coarse SAND, Trace s	mail
Blows 11, 15, 15, 17	fine rounded Gravel. I" laye	
	of Gray Silty Clay in tipe 59t	
59-6/1	59-681 Tan/Orange Brown medium Den	nse l
recovery 20"	Fine to Coarse SAND Trace	
Blows 9,8, 17, 15	small rounded bravel	lau
	2" thick layer of Gray Saving 0	
	@ 60 FT.	
61-633	61-63 Tan/Orange Brown Dense Pine	
recovery 21's	Coarse SAND Trace Small // M	
Blows 13,25,31,26	Tourioeo (J lavei.	
	62-64 Some	
62-64		
Rlow 26.17.19.21		
Blows rejugitie		
64-66	64-66 Same	
recovery 14"		
1 - 1 1. 4 11 17		

a start of the second sec

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	ORIULING LOG	BORING NUMBER PTMW-1
PILLING CONTRACTOR	Unicelling Loud line Claures	sheet 3 of 11
mer Bulch r haileon	PROJECT NAME _PLANKING CLEARERS	Boring Location 17.5ft east of
spector Durgae Man	1/110 =	Pole 216
g Type (ME-85 Still Mg	PROJECT # 1640	
illing Method Auger 15011 2000	State Parkway	
tve Hammer Weight		Plot Plan
ROUNDWATER OBSERVATIONS	Weather <u>Ulcar</u>	
ater Lavel 23'	al.2/29 11:00	
	Date/Time Start 11/0/11 1/00	
ate 9/14/94	Date/Time Finish 9/19/11 10-30	
asing Depth 93'		WELL SCHEMATIC   COMMENTS
ample Sample SPT PID/Fill	FIELD IDENTIFICATION OF MATERIAL	Well Soneir
	11 17 Tas Brown dease fine to Coarse	
5-63 0.0	SAND Trace + Gravel	
1/11/5 9.14.18.22	67-68 From Fine CAND little A)	
nus argreges	City Sondy Char Lichnice conte	
	Sirry, Darloy Clay high miza conte	
8-70 0.0	68-70 Gray Fine to medium SAND	
ecovery 12"	little (+) Silty Sendy Clay, Organic	Bentonite Grou
lows 7,10,14,18	material visible in striation in 2"in	terves
	@ 68 +69 Ft. High mica content.	
771 0.0	70-72 Gray Dense Fine to Medium SAN.	
o-/ A bit	high Mica Content, very fine sana.	
Blows 21,77,31,28		Finil State 2 PVC riser
	7274 Low Dense Fine to Medium SAM	D
7-74 0.0	hip Mice content 4" Grou Kadu	1
ecovery 16"	Glau & 72 ft.	
3/000 4,9,13,11		in and collected
711-76 1 0.0	74-76 Top 8" Gray Sandy Clay. Block	+ L'
receivery 14"	Striations, high Sand content littleplo	STICI PTAWE-1(74-76)
Blows 5,10,13,12	Bottom 6" Gray Dense Fine To Med	111M - 11 - 1 - 1 07:50
	SAND little LA Silty Sand.	12/2/1-1-1-1-1-1
2, 29	74-78 Fran Dense Fine to Medium SA	ND , hit is somple collected
16-10 0.0	1:++1, () aray silt. 1" interval 6	ray for grain size on
Blow 5 10.10.19.21	Sadu The 6 70'	1- 1 P(mw-106-78)9
	Sanay ciay a 10 to mediu	n -:
78-80	78-80 Dark Gray Jense Fine With	
recovery 14"	SAND INTHE C-3 gray -	X
Blows 5,9,23,37		1111 345 5
	30-82 Refusal @ 80'11" + 1 marce SAN.	D. 1994
80-82	Gray Dense Fine To Course	
12/001 29 50/5		
01005 11 590	- Andrew Come to Medium S.	AND I' Sample collected
82-841	82-84 Gray Dense Vine 10 " layer of	grain Size analys
recovery 14"	nign mice conient, Black + ragere	1-1 1-1 19:10
Blours 6.14, 26, 47	un urganic morrer.	1

RILLING CONTRACTOR Driller Butch H / Uni Tech	ORILLING LOG PROJECT NAME <u>Franklin Cleaners</u>	BORING NUMBER <u>PTMW-1</u> Sheet <u>4</u> of <u>4</u> Boring Location <u>17.5 ft Fast</u>				
Alg Type <u>CME-85 Drill Rig</u> Drilling Method <u>Auger Isplitspo</u>	PROJECT # 1640 = MLOCAUDIVADDress Pole 246 Southern State Parkway					
	Weather <u>Clear</u> <u>10 w 80'3</u> Date/Time Start <u>9/13/49</u> 11:00 Date/Time Finish <u>9/14/49</u> 18:30	Plot Plan				
Sample Sample SPT PID/FID Depth Number Reeding	FIELD IDENTIFICATION OF MATERIAL	WELL SCHEMATIC COMMENTS				
14-86 ecovery 13" Slows 8,21,31,35	84-86 Gray Dense Fine to Medium SAND littlet) silt with & black striations	Sample collected for				
6-88 2 cover 4 12" 36ws 25, 50/5	86-88 REFUSALE OF II Bray Dense Fine to Medium SAND little G) Silt. Powder like. High Mica Content. 88-90 Gray Dense Fine to Medium SAN.	D				
recovery 16" Blow 9,16,34,34 10-92	little (-) Silt: Itigh Mica content. highpercentage fine SAND. 90-92 Dark Gray Dense to Fine to Mod	lion 2"PVC Scieen				
Recovery 22" Blows 23,22, 25,27 72-94 Recovery 22" Blows 11, 12,16,10	92-94 Dark Gray Dense Fine to Medium SAND, little (-) Sill. Bottom 3" brownish Tan Fine Sond.	-1 anolysis PTmw-1(90-9 91/4/49 10:15 7 1 93 ft below Grobe				
74-96 recovery Blow 3 3,9,7, 12	94-95.3Ft Brownish Gray Medium Dense fine to medium SAND. followed I" interval lignite.	bravelpack				
	95.3-96 9" Dask Dense Gray /Block Sill Clay, little moisture Dask Dense Gray /Black Sill	ty 25.3 Openninginto Clay filled with Bentonite water				
76-98 recovery 12" Blows 13,21,19,12	Clay, Clay appears competent.	dry Bentotte browthin mix				
98-\$100 Tecovery 24" 13/0ws 16,22,32,38	98-100 Dark Gray Polace Gray Sand /- Clay. no moisture. Gray Sand /- Striations opprox 1/8 inch thick	Silte				
	Boring Terminated. Clay layer filled w/ Bentonite mix. berehole Flushed to remove Bentonite/m	ud mix				
	2 ft gravel pack above clay then wellin	A5.[al]				

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Driller Joe Jester / Uni Tech       PROJECT NAME       Frank in Cleaners       Sh         Inspector       Wayne M.       PROJECT NAME       Frank in Cleaners       Sh         Big Type (MIC-85)       PROJECT NAME       Frank in Cleaners       Sh         Drilling Method       Mud Rotey       Location/Address       Bele 116       Southern       1         Drive Hammer Weight	eet of ring Location 22 Pole 216 Plan TN East bound Prow- tine & de ELL SCHEMATIC	Southern State R Southern State R Provi Rola 216 COMMENTS COMMENTS 2 Provi Rola 216
Date       Definition       PROJECT NAME       Prank in Clearces       Bit         PROJECT Wayne Minimum       PROJECT #       1640 - 2	Plan TN East bound. Prow time & &	Southern State P
Rig Type (M/E-85)       PROJECT # 1640 - 2	Plan TN East bound line add	Southern State M Pale 216 COMMENTS 2 <sup>11</sup> pvc Screen # 10
Image: Second	Plan TN East bound Fine & & ELL SCHEMATIC	Southern State M Pala 216 COMMENTS COMMENTS 2"PVC Screen # 10
Drive Hammer Weight	Plan TN East bound Fine & All	Southern State In Pale 216 COMMENTS 2"PVC Screen # 10
State particular         State particular         GROUNDWATER OBSERVATIONS         Weather Level       23'         Time       Date/Time Stat       10/1/19 12:00         Date       Date/Time Stat       10/1/19 6:10       Free         Casing Depth       Date/Time Finish       10/1/19 6:10       Free         Sample       Sample       Sample       Sample       Sample       Sample       Sample       Sample       Sample       PID/FID       FIELD IDENTIFICATION OF MATERIAL       We         Depth       Type       Reading       Doc       D-2 Organic material to .5'       Science SAND to 24         Depth       Tipe       0.0       D-2 Organic material to .5'       Science SAND to 24         Desch dig       Loose Medium to Coaise SAND to 24       Science SAND to 24       Science Sand Sand Sand Sand Sand Sand Sand Sand	Plan TN East bound. Pine & de ELL SCHEMATIC	Southern State In Pale 216 COMMENTS 2"PVC Screen # 10
GROUNDWATER OBSERVATIONS       Weather       Clear Cool = 60°F       Plot         Water Level       23'       Date/Time Start       10/1/199 12:00       Fige         Date       Date/Time Start       10/1/199 12:00       Fige       Fige         Date       Date/Time Start       10/1/199 12:00       Fige       Fige         Sample       Sample       SPT       PID/FID       FIELD IDENTIFICATION OF MATERIAL       WE         O-2       Image: Control of the start       0.0       0-2 Organic material to .5''       fige         0-2       Image: Control of the start       0.0       0-2 Organic material to .5''       fige         0-2       Image: Control of the start       0.0       0-2 Organic material to .5''       fige         0-2       Image: Control of the start       0.0       0-2 Organic material to .5''       fige         0-2       Image: Control of the start       0.0       0-2 Organic material to .5''       fige         100000       0-2       Organic material to .5''       fige       fige         2-4       0.0       Dotse Medium to Coaise SAND       fige       fige         10000       Begin       collecting       spoons       fige       fige         2-34       S       <	Plan TN East bound Planw Line Q. M ELL SCHEMATIC	Southern State I
Water Level       23'         Time       Date       Date/Time Start       10/1/199       12:00         Date       Date/Time Finish       10/1/199       6:10       Fige         Casing Depth       Date/Time Finish       10/1/199       6:10       Fige         Sample       Sample       Sample       Sample       SPT       PID/FID       FIELD IDENTIFICATION OF MATERIAL       WE         Oopth       Type       PID/FID       FIELD IDENTIFICATION OF MATERIAL       WE         Oopth       Type       O.O       O-2 Orgonic meterial to .5'       Start         Iccourty       none       headdig       Icourt Medium       to Conise SAND       Start         Q-2       O.O       Loose       Medium       to Conise SAND       To 14         Q-4       O.O       Loose       Medium       to Conise SAND       Material         Hand       dig       Dense       Gray, Fine to Medium       Sapons       Sapons         Begin       collect fing       Spoons       Sapons       Sapons         Begin       Collect fing       Spoons       Sapons       Sapons         Begin       Collect fing       Spoons       Sapons       Sapons <t< td=""><td>Pine Q de</td><td>COMMENTS Pala 216 COMMENTS 2"PVC SCREEN # 10</td></t<>	Pine Q de	COMMENTS Pala 216 COMMENTS 2"PVC SCREEN # 10
Time       Date       Date/Time Start       10/1/19 (1/20)         Date       Date/Time Finish       10/1/19 6:10       File         Casing Depth       Date/Time Finish       10/1/19 6:10       File         Sample       Sample       Sample       SPT       PID/FID       FIELD IDENTIFICATION OF MATERIAL       WE         Depth       Type       Peeding       FIELD IDENTIFICATION OF MATERIAL       WE         0-2       0.0       0-2 Organic meterial to .5'       S'         1/200/11       1000       0-2 Organic meterial to .5'       S'         1/200/11       0.0       0-2 Organic meterial to .5'       S'         1/200/11       0.0       1000       1000       1000         1/201/11       0.0       0.0       1000       1000         1/201/11       0.0       0.0       1000       1000         1/201/11       0.0       0.0       0.0       1000         1/201/11       0.0       0.0       0.0       1000<	Production of the second secon	2"PVC Screen # 10
Date       Date/Time Finish       10/1/174       6:10       Recipe         Casing Depth       Sample       Sample       SPT       PID/FID       FIELD IDENTIFICATION OF MATERIAL       WE         Depth       Type       P       Pielding       FIELD IDENTIFICATION OF MATERIAL       WE         Oppth       Type       P       0.0       0-2 Crgonic material to :5'       10         1       1       0.0       0-2 Crgonic material to :5'       10       10         1       1000       0-2 Crgonic material to :5'       10       10       10         2       0.0       0-2 Crgonic material to :5'       10       10       10         2       0.0       0-2 Crgonic material to :5'       10       10       10         2       0.0       10       0.0       10       10       10       10         1       10.00       10       10       10       10       10       10       10       10         2       0.0       10       0.0       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10       10<	LL SCHEMATIC	COMMENTS Pole 216 COMMENTS 2"pvc Screen # 10
Casing Depth       Y**         Sample Depth       SPT       PID/FID       FIELD IDENTIFICATION OF MATERIAL       WE         Depth       Tipe       O.O       O-2 Orgonic material to .5'       Standard to .5'         Iccourty none       hadedig       lossetMedium       to Coaise SAND to 24+         2-4       O.O       Loose Medium       to Coaise SAND       to 24+         2-4       O.O       Loose Medium       to Coaise SAND       to 24+         2-4       O.O       Loose Medium       to Coaise SAND       to 24+         2-4       O.O       Loose Medium       to Coaise SAND       to 24+         2-4       O.O       Loose Medium       to Coaise SAND       to 24+         2-4       O.O       Loose Medium       to Coaise SAND       to 24+         2-4       O.O       Loose Medium       to Coaise SAND       to 24+         2-4       O.O       Loose Medium       to Coaise SAND       to 24+         2-4       O.O       Loose Medium       to Coaise SAND       to 24+         2-4       O.O       Begin collecting Spoons       to 24+       to 24+         2-34       S       Dense Gray, Fine to Medium       to 34+       to 34+		COMMENTS COMMENTS
Sample Sample SPT PID/FID FIELD IDENTIFICATION OF MATERIAL WE Dopth Type PID/FID Reading FIELD IDENTIFICATION OF MATERIAL WE 0-2 1 0.0 0-2 Organic material to .5' recovery none handdig loss Medium to Coaise SAND to 247 2-4 0.0 Loose Modium to Coaise SAND to 247 2-4 0.0 Loose Modium to Coaise SAND Hand dig Tan light brown in color. no obol. Begin collecting Spoons Begin collecting Spoons Begin collecting Spoons Begin SAND, Fine to Medium SAND, Trace (A) Silty Sand no oder no steining 14-86 S 0.0 Gray fine SAND, little (A) Silty Sand, Trace (A) Silty Clay		2"pvc Screen # 10
0-2 0.0 0-2 Organic material to .5' 1000 1000 1000 1000 1000 10 1000 10 1000 10 1		2"pvc screen # 10
feccursy none       handdig       lose Medium       to Coaise SAND to 24+         2-4       0.0       Loose Medium to Coaise SAND       ND         Hand dig       Tan light brown in color.       noodol.         Hand dig       Tan light brown in color.       noodol.         Begin collecting spoons       Coase Section         Regin collectin spoons       Coase Section		2"pvc screen # 10
2-4       0.0       Loose Medium to Coaise SAND         Itand dig       Tan light brown in color. no odol.         Tan light brown in color. no odol.         Begin collecting spoons         Begin collecting spoons         Bestin collecting		2"pvc screen # 10
Hand dig tan light brown in colar. noodol. Begin collecting spoons Begin collecting spoons		2"pvc screen # 10
Begin collecting spoons Begin collecting spoo		2"pvc screen # 10
Begin collecting spoons Begin collecting spoo		2"pvc screen # 10
Begin collecting spoons Begin collecting spoo		2"PVC SCREEN # 10
Begin collecting spoons Begin collecting spoo		2"pVc Screen # 10
Begin collecting spoons Begin collecting spoons SAND, Fine to Medium SAND, Frace (4) Silty Sand Begin collecting spoons Begin collecting spoo		2"PVC SCREEN # 10
2-84 S Dense Gray, Fine to Medium SAND, Trace (A) Silty Sand no oder no steining 4-86 S Covery 18" Sand, Trace (A) Silty Clay		2"PVC Screen #10
22-84 S Dense Gray, Fine to Medium SAND, Trace (A) Silty Sand No oder no staining 14-86 S Covery 18" Sand, Trace (A) Silty Clay		Screen # 10
32-84 5 Dense Gray, Fine to Medium SAND, Tracz (A) Silty Sand in oder no steining 14-86 5 Ceovery 18" Sand, Trace (A) Silty Clay		
Arecovery = 16" SAND, Trace (4) Silty Sand No oder no steining 14-86 5 0.0 Gray fine SAND, little (4) Silty covery 18" Sand, Trace (4) Silty Clay		
310005 12,20,27,25 no oder no steining 14-86 5 0.0 Gray fine SAND, little (A) silty in ecovery 18" Sand, Trace (A) Silty Clay		
4-86 5 0.0 Gray fine SAND, little (+) silty is ecovery 18" Sand, Trace (+) Silty Clay	· · · · · · · ·	
14-86 5 0.0 Gray fine SAND, little (+) silty in ecovery 18" Sand, Trace (+) Silty Clay	121 181	
ecovery 18" Sand, Trace (4) Silty Clay	14.17	
News 7 18.25.33 Sand, Trace (7) Silty Clay		- Carl Park
	1.1.1.	Unever lach
	1	Trole to or
	-	
0-30 3 A.O Gray Fine To Medium SAND	1	
How's \$129. 33 20 little (-) Silty SAND. 2" layer	1: 1 1	
Cark Chay gray Clay @ 87.5'	1.1 ~	
noodd	1:1-	
18-90 S D.D Gray fine to Medium SAND .:	1 2 4	
Clovery H little (-) Silty S.AND. 5" Tanich .	17	
brown Coarse Gravely SAND@ 89.5	5	
	1 1	
10-92 S 0.0 Gray fine to Medium SAND	12212	
ecovery 10" littlets Silt, SAAN 1" 1 11		
Slows of derk arey cand. 11 loyer/lense	2:1-1	
no odor y cray		

DRILLCON.PM4

# Appendix B

# **APPENDIX B**

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# **GRAIN SIZE ANALYSIS RESULTS**

Analytical Data Package for Dvirka & Bartilucci

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Client Project: Franklin Cleaners/1640-2

SDG# 61787

Mitkem Project ID: 61787

October 14, 1999

#### **SDG** Narrative

Mitkem Corporation submits the enclosed data package in response to Dvirka & Bartilucci's Franklin Cleaners project. Under this deliverable, analysis results are presented for five soil samples that were received on September 15, 1999. Analyses were performed per specifications in the chain of custody forms.

The following samples are submitted in this data package:

Client ID	Lab ID	Analysis
PTMW-1(74-76)	61787001	G
PTMW-1(76-78)	61787002	G
PTMW-1(82-84)	61787003	G
PTMW-1(86-88)	61787004	G
PTMW-1(90-92)	61787005	G

G = Grain Size - ASTM D422

The analyses were performed according to ASTM protocols. The analyses were subcontracted to Rhode Island Analytical Laboratories (RIAL) for performance of the requested tests, which are not performed by Mitkem. A copy of the RIAL report is attached.

No unusual observation was made for the analysis.

If you have any questions, please do not hesitate to call me.

Sincerely,

drad a fash

Edward A. Lawler Laboratory Operations Manager 10/15/99

110001

CHAIN-OF-CUSTODY RECORD
<u>emmi or cobrodi kecold</u>

Page \_\_\_\_ of \_\_\_\_

	REPOI	RT TO		1.1.1.									14	INV	OICE	то			25-11-1					
COMPANY Duicka	tot Bartila	ice i			PHON	SIA	364-9890	СОМ	PANY	Du	ich	4 4	B	rti	100	ci'		PHON	512	).364	-929	a LA	ABPRC	DJECT #:
NAME Robbin Pr	Trella				FAX	203	64-9045	NAM	EJ	ave	6	-/05	5	<u>u iri</u>		-		FAX	ELD)	264-	904	5 (	61	787
ADDRESS 333 Cru	ssways Park	.7	Dri	10		S. C.		ADD	RESS	33/		0551	1011	s P	2.1	Dri		e	191.		101	TL	JRNAR	OUND TIME:
CITY/ST/ZIP Woodb	un NU		117	77				CITY	/ST/ZI	P/1	lad		N	2	117	97	and the second s						72h	~
CLIENT PROJECT NAME:	9	CLIEN	IT PRO	DJECT	r #:		CLIENT P.O.#:			-w	1000	uig	ush	)			CATED		VOD				- 111	
Franklin Cleaners 1640-2 1640-2					1640-2					18th	/	/	/				LYSE.	. /	1	/	/			
SAMPLE IDENTIFICATION	DATE/TIME SAMPLED	COMPOSITE	GRAB	WATER	SOIL	OTHER	LAB ID	# OF CONTAINERS		paula	eliste												COMN	MENTS
PIMW-1(74-76)	9/14/19 07:50		×		X		01	2	$\propto$												(2)	803	jors	(gloss)
PFmw-1(82-84)	9/14/99 07:50		×		X													-	-					
PT MW-1 (76-78)	9/14/19/07:50		×		X		02	2	X												(2)	807	101.50	(aloss)
PTMW-1(82-84)	9/14/97 19:10		X		x		03	2	X												(2)	807	lers	(alass)
PTMW-1(86-58)	9/14/9919:30		×		X		04	2	X												28	07	iars	Celass
TMW-1(90-92)	9/14/99 10:15	-	$\propto$		X		05	2	X												111	11	"	11
5	1																				11 11	"	~	"
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30°5			1										1										/	

WHITE: LABORATORY COPY

MITKEM

CORPORATION

175 Metro Center Boulevard Warwick, Rhode Island 02886-1755

(401) 732-3400 • Fax (401) 732-3499

email: mitkem@mitkem.com

PINK: CLIENT'S COPY

# **MITKEM CORPORATION**

Page 1 of 1

#### 09/15/99 05:26 PM

Client:

#### **R0** 61787 Lab Workorder Dvirka & Bartilucci Lab Workorder ID: Franklin Cleaners/1640-2 Client Proj ID:

Client PO #: 1640-2 Project / Profile Name: Franklin Cleaners Date Due: 09/20/99 \* Customer Service: Del Req'd: ASP B (2 copies) Completed?: Profile Notes:

Voas are unpreserved;7 Day Holding Time Project Notes: SAMPLES SUBBED TO RIAL

Original



Lab Workorder #: 61787

3

Date Opened: 09/15/99 11:46 Date Closed: 09/15/99 17:26

Project Status: WP

Lab ID 61787001	<u>Client ID</u> PTMW-1(74-76)	<u>Matrix</u> S	<u>Type</u> SAMPLE	<u>Analysis Code</u> A19-D422Gr DRY WEIGHT	Collected 09/14/99 07:50	Received 09/15/99	<u>Due</u> 09/20/99	<u>Notes</u> PTMW17476SEIVE & HYDROMETER
61787002	PTMW-1(76-78)	S	SAMPLE	A19-D422Gr DRY WEIGHT	09/14/99 07:50	09/15/99	09/20/99	PTMW17678SEIVE & HYDROMETER
61787003	PTMW-1(82-84)	S	SAMPLE	A19-D422Gr DRY WEIGHT	09/14/99 09:10	09/15/99	09/20/99	PTMW18284SEIVE & HYDROMETER
61787004	PTMW-1(86-88)	S	SAMPLE	A19-D422Gr DRY WEIGHT	09/14/99 09:30	09/15/99	09/20/99	PTMW18688SEIVE & HYDROMETER
61787005	PTMW-1(90-92)	S	SAMPLE	A19-D422Gr DRY WEIGHT	09/14/99 10:15	09/15/99	09/20/99	PTMW19092SEIVE & HYDROMETER

#### **INVOICE AND REPORT GO TO:**

**Robbin Petrella** Dvirka & Bartilucci 330 Crossways Park Drive Woodbury, NY, 11797 W: 516-364-9890 F : 516-364-9045

C0003

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	MITK	EM	CORPORA	TIC	NC			~
	Sam	ple	Condition F	orn	1			Page_of
Received By: NP	Reviewed By:	A	Date: 9115 90				мітке	EM Project: 61787
Client Project: FRAN	KIN CLEANER	5	Client: DURKA	ŧ.	BART	inc	xcl	0
		-	Sample ID	P	reserva	ation (	pH)	Comments/Remarks
Condition:		Lab	Client	HNU.	12304	nu	Naun	corrective Action"
	$\sim$	01	PTMW-1(74-76)					
1) Custody Seal(s)	Present/Absent	02	-1 (76-78)					
	Coole)s/Bottles	03	-1 (82-84)					
	Intac/Broken	04	-1(86-88)					
1		in	(go-g)					
1		05	V I Co Ia					4
2) Custody Seal Number(s	) <u>N</u>  A	-						
		-						/
								/
Chain-of-Custody	Present/Absent							
s.	$\bigcirc$						1	
	70						-	
() Cooler Temperature						-	- :	
Coolant Condition	<u>LCE</u>							/
	0							/
i) Aichill(s)	Present/Absent						-/1	
Airbill Number(s)	FED-EX							
	511368228134					4		
	<u>.</u>						2	
	Internet						1	•
) Sample Bolles	milace			/				
	Broken			1				
	Leaking		/					
) Date Received	9/15/99							•
) Time Received	09:00							
			/				-	
	71 1100		/					
Project Due Date	12 MKS	1						

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#### R.I. Analytical Laboratories, Inc.

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	CER	TIFICATE	OF ANALYS	SIS	1 1 1	1/,
Mitkem Corpora Date Received: Work Order #	tion 9/15/99 9909-08765		Ар	proved by: R.J. Analy	vida //	1/2
Sample #: 0 SAMPLE DESC	001 CRIPTION: 61787-01 0	9/14/99 @0	)750		l	
PARAMETER	SAMPLE RESULTS	DET. LIMIT	UNITS	METHOD	ANALYZED DATE/TIME	ANALYST
SIEVE ANALYSIS HYDROMETER	*		%	ASTM	9/20/99 10:00 10/05/99 16:27	SB SB
* See Attached for Si	ieve Analysis					
Sample #: 0 SAMPLE DESC	02 RIPTION: 61787-02 0	9/14/99 @0	750			
PARAMETER	SAMPLE RESULTS	DET. LIMIT	UNITS	METHOD	ANALYZED DATE/TIME	ANALYST
SIEVE ANALYSIS HYDROMETER	*		%	ASTM	9/20/99 10:00 10/05/99 16:27	SB SB
* See Attached for Sid	eve Analysis					
Sample #: 00 SAMPLE DESCI	03 RIPTION: 61787-03 09	9/14/99 @09	910			
PARAMETER	SAMPLE RESULTS	DET. LIMIT	UNITS	METHOD	ANALYZED DATE/TIME	ANALYST
SIEVE ANALYSIS HYDROMETER	*		%	ASTM	9/20/99 10:00 10/05/99 16:27	SB SB
* See Attached for Sie	eve Analysis					
Sample #: 00 SAMPLE DESCR	4 RIPTION: 61787-04 09	/14/99 @09	30			1- Ø
PARAMETER	SAMPLE RESULTS	DET. LIMIT	UNITS	METHOD	ANALYZED DATE/TIME	ANALYST
SIEVE ANALYSIS HYDROMETER	*		%	ASTM	9/20/99 10:00 10/05/99 16:27	SB SB

\* See Attached for Sieve Analysis

Page 3 of 3

# R.I. Analytical Laboratories, Inc.

#### CERTIFICATE OF ANALYSIS

Mitkem Corporation Date Received: 9/15/99 Work Order # 9909-08765

LYSIS	s , //	
Approved by:	Inm.M.	
Ŕ	.I. Analytical	

Sample #: 005

SAMPLE DESCRIPTION: 61787-05 09/14/99 @1015

PARAMETER	SAMPLE RESULTS	DET. LIMIT	UNITS	METHOD	ANALYZED DATE/TIME	ANALYST
SIEVE ANALYSIS	*		9%	A CTD 4		
HYDROMETER	*		10	ASTM	9/20/99 10:00	SB
					10/05/99 16:27	SB

\* See Attached for Sieve Analysis

#### -Sieve Analysis-

Company:Mitkem Corp.Analysis(s):S.B.Date:9/20/99

Sieve #	Sieve &	Sieve &	Sample (g)	%	%
	Cardboard	Cardboard&		Retained	Passing
	(g)	Sample (g)			
40	426.65	433.44	6.79	5.59	94.41
60	388.48	422.04	33.56	27.36	66.78
120	458.71	515.72	57.01	46.94	19.84
200	375.95	383.73	7.78	6.41	13.43
270	423.64	431.87	8.23	6.78	6.65
325	423.63	425.44	1.81	1.49	5.16
400	432.78	435.96	3.18	2.62	2.54
PAN	391.64	394.72	3.08	2.54	0.00

#### Sample #: 8765-1 Initial Mass: 122.12

Total = 121.44

Sieve #	Sieve &	Sieve &	Sample (g)	%	%
	Cardboard	Cardboard&		Retained	Passing
	(g)	Sample (g)			
40	426.72	487.37	60.65	27.67	72.33
60	387.76	490.08	102.32	46.68	25.65
120	458.60	502.10	43.50	19.85	5.80
200	375.85	381.21	5.36	2.45	3.35
270	423.48	424.09	0.61	0.28	3.07
325	423.43	424.70	1.27	0.58	2.49
400	432.55	433.72	1.17	0.53	1.96
PAN	391.50	395.80	4.30	1.96	0.00

#### Sample #: 8765-2 Initial Mass: 219.82

Total = 219.18

1.5

#### -Sieve Analysis-

Company:Mitkem Corp.Analysis(s):S.B.Date:9/20/99

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#### Sample #: 8765-3 Initial Mass: 179.84

Sieve #	Sieve &	Sieve &	Sample (g)	%	%
	Cardboard	Cardboard&		Retained	Passing
	(g)	Sample (g)			
40	426.69	453.11	26.42	14.96	85.04
60	387.76	496.25	108.49	61.44	23.60
120	458.5	486.15	27.65	15.66	7.94
200	375.77	380.88	5.11	2.89	5.05
270	423.38	424.46	. 1.08	0.61	4.44
325	423.48	424.74	1.26	0.71	3.73
400	432.78	434.02	1.24	0.70	3.03
PAN	391.58	396.93	5.35	3.03	0.00

Total = 176.60

#### Sample #: 8765-4 Initial Mass: 202.33

Sieve #	Sieve &	Sieve &	Sample (g)	%	%
	Cardboard	Cardboard&	Cardboard&		Passing
	(g)	Sample (g)			
40	426.84	428.67	1.83	0.91	99.09
60	387.76	520.09	132.33	65.59	33.50
120	458.46	500.81	42.35	20.99	12.51
200	375.72	384.65	8.93	4.43	8.08
270	423.52	428.25	4.73	2.34	5.74
325	423.53	424.90	1.37	0.68	5.06
400	432.56	435.45	2.89	1.43	3.63
PAN	391.51	398.83	7.32	3.63	0.00

Total = 201.75

## -Sieve Analysis-

Company:Mitkem Corp.Analysis(s):S.B.Date:9/20/99

- 140

#### Sample #: 8765-5 Initial Mass: 251.97

Sieve #	Sieve &	Sieve &	Sample (g)	%	%
	Cardboard	Cardboard&		Retained	Passing
	(g)	Sample (g)			
40	426.59	441.94	15.35	6.13	93.87
60	387.90	545.35	157.45	62.90	30.97
120	458.45	506.62	48.17	19.24	11.73
200	375.81	387.43	11.62	4.64	7.09
270	423.45	429.60	6.15	2.46	4.63
325	423.46	423.56	0.10	0.04	4.59
400	432.64	435.42	2.78	1.11	3.48
PAN	391.50	400.20	8.7	3.48	0.00

Total = 250.32

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# MITKEM Corporation

175 Metro Center Boulevard Warwick, Rhode Island 02886-1755 (401) 732-3400 • Fax (401) 732-3499 email: mitkem@mitkem.com

# **CHAIN-OF-CUSTODY RECORD**

Page of

	REPO	RT TO	j. j. j.									3	INV	OICE	то								
COMPANY				PHO	NE		COM	IPANY								PH	ONE			L	AB PRO	JECT #:	
NAME Date	1 Report.	3		FAX			NAM	IE	Problemania	C	en	Ra	na	Ui	LL FAX					870	05		
ADDRESS		/					ADD	RESS												Т	URNAR	OUND T	ME:
CITY/ST/ZIP	*						CITY	/ST/ZI	Р												12h	9-11	7
CLIENT PROJECT NAME:		CLIEN	T PROJE	CT #:		CLIENT P.O.#:		Γ			0	422									000	1 d	-
	=		617	87		996178	7A				Agent	/	/	/	LEQUES /		ALYS	ES /	1 /	1	/		
SAMPLE	DATE/TIME SAMPLED	COMPOSITE	GRAB WATER	Soil	OTHER	LAB ID	# OF CONTAINERS	(	Grain	malus											СОММ	1ENTS	
61787-01	9/14/99/07:50			¥			2	X															
- 02	1 107:50			×			2	X															
-03	1 9:10			×			2	X															
-04	1 9:30			X	-		2	X															
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PINK: CLIENT'S COPY

Mitkem Corporation Attn: Data Reporting 175 Metro Center Blvd. Warwick, RI 02886-1755 Date Received:9/15/99Date Reported:10/06/99P.O.#:9961787AWork Order #:9909-08765

#### PARTICLE SIZE

**ASTM METHOD D422** 

RIAL SAMPLE ID 8765-1

Gravel	0.00%
Course Sand	0.00%
Medium Sand	5.59%
Fine Sand	80.98%
Silt size, 0.074 to 0.005 mm	10.63%
Clay size, smaller than 0.005 mm	2.80%
Colloids, smaller than 0.001 mm	0.00%

#### **ASTM METHOD D422**

.

#### RIAL SAMPLE ID 8765-2

Gravel	0.00%
Course Sand	0.00%
Medium Sand	27.67%
Fine Sand	68.98%
Silt size, 0.074 to 0.005 mm	2.93%
Clay size, smaller than 0.005 mm	0.42%
Colloids, smaller than 0.001 mm	0.00%

#### ASTM METHOD D422

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#### **RIAL SAMPLE ID 8765-3**

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Gravel	<u> </u>
Course Sand	0.00%
Medium Sand	<u>_14.96%</u>
Fine Sand	_79.99%
Silt size, 0.074 to 0.005 mm	_4.43%
Clay size, smaller than 0.005 mm	0.62%
Colloids, smaller than 0.001 mm	0.00%

#### ASTM METHOD D422

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#### RIAL SAMPLE ID 8765-4

Gravel	0.00%
Course Sand	0.00%
Medium Sand	0.91%
Fine Sand	_91.01%
Silt size, 0.074 to 0.005 mm	
Clay size, smaller than 0.005 mm	0.86%
Colloids, smaller than 0.001 mm	0.00%

#### ASTM METHOD D422

#### RIAL SAMPLE ID 8765-5

Gravel	0.00%
Course Sand	0.00%
Medium Sand	<u> </u>
Fine Sand	86.78%
Silt size, 0.074 to 0.005 mm	6.29%
Clay size, smaller than 0.005 mm	0.80%
Colloids, smaller than 0.001 mm	0.00%



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James EAMs

Vice President

hc: Chain of Custody

**R.I.** Analytical

Specialists in Environmental Services

#### **CERTIFICATE OF ANALYSIS**

Mitkem Corporation Attn: Data Reporting 175 Metro Center Blvd. Warwick, RI 02886-1755

 Date Received:
 9/15/99

 Date Reported:
 10/06/99

 P.O. #:
 9961787A

 Work Order #:
 9909-08765

#### **DESCRIPTION:** PROJECT #61787 (FIVE SOIL SAMPLES)

Subject sample(s) has/have been analyzed by our laboratory with the attached results.

Reference: All parameters were analyzed by U.S. EPA approved methodologies. The specific methodologies are listed in the methods column of the Certificate Of Analysis.

you have any questions regarding this work, or if we may be of further assistance, please contact us.

Michael J. Hobin

Quality Control Coordinator

41 Illinois Avenue, Warwick, RI 02888 Tel: (401) 737-8500 Fax: (401) 738-1970 950 Boylston Street, Unit 102, Newton Highlands, MA 02461 Tel: (617) 965-5133 Fax: (617) 965-5624

Last Page of Data Report

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Appendix C	

# **APPENDIX C**

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# WELL CONSTRUCTION LOGS

CONSULTING ENGINEERS	WELL CONSTR	UCTION LOG	
SITE Fran	klin Cleaners	JOB NO WELL	NO. <u>PTW-1</u>
TOTAL DEPTH	35 SURFACE ELEV	TOP RISER ELEV	<i></i>
WATER LEVELS (D	EPTH, DATE, TIME)	DATE INSTALLED	10/12/99
RISER C SCREEN C	IA <u>6</u> " MATERIAL <u>PVC</u> , <u>Schedal</u> IA <u>6</u> " MATERIAL <u>Stainlessstee</u>	<i>e 30</i> L <b>ENGTH <u>73'</u> ∉/ LENGTH <u>20'</u> SL</b>	OT SIZE
	SCH	IEMATIC	
Surface Seal Ty Pertland Ce	pe vient		Ground Surfa ————————————————————————————————————
Grout Type	<u>Bentonite / Poitland</u> <u>Cement Mix</u>	62 TOP Se	al
Seal Type	Enviroplug Besterite	<u>64</u> Top Sa 7.3 Top Sc	nd Pack
Sand Pack Type Size <u>#2</u>	Silica Questz	<u>93</u> Botton 95 Total	n Screen Depth of Boring

CONSULTING ENGINEERS	WELL	CONSTRUCTION LOG	
r. 1	h. cl		DEMON
SITE <u>Frank</u>	VIA Cleaners	JOB NO. <u>1640</u> WELL NO.	<u>  mw= </u>
TOTAL DEPTH	100' SURFACE ELEV.	TOP RISER ELEV	
WATER LEVELS	DEPTH, DATE, TIME: 23	DATE INSTALLED	1/14/99
R I SER SCREEN	DIA $\frac{2^{*}}{2^{*}}$ MATERIAL $P_{VC}$ Solution $\frac{2^{*}}{2^{*}}$ MATERIAL $P_{VC}$ Solution	chedule 40 LENGTH 73' chedule 40 LENGTH 20' SLOT	SIZE <u>#10</u>
	\$	SCHEMATIC	
			Ground Su
Surface Seal T Portland Ce	ype ment		Riser Elevation
	_		
Grout Type	Bentonite / Portland	_ ////	
	Cement Mir.	- ////	
		69 Top Seal	
	Enical Ptita		
Seel Tree	Phonophia Destosite	- <u>7/</u> Top Sand P	ack
Se <b>al</b> Typ <b>e</b>		beeseed beeseed	
Se <b>al</b> Typ <b>e</b>		73' Top Screen	
Seal Type		<u>73</u> Top Screen	
Seal Type		73 <sup>'</sup> Top Screen	
Seal Type Sand Pack Type	Silica Quartz	73'Top Screen	
Seal Type Sand Pack Type Size <u>#1</u>	Silica Quaitz	73'Top Screen	
Seal Type Sand Pack Type Size <u>#1</u>	Silica Quartz	73' Top Screen	

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CONSULTING ENGINEERS		TOUCTION LOC	
	WELL CONS	TRUCTION LUG	
SITE Franklin	n Cleaners	JOB NO. 1640	WELL NO. <u>PTMW-2</u>
TOTAL DEPTH	JZ' SURFACE ELEV.	TOP RI	SER ELEV.
WATER LEVELS (DE	EPTH, DATE, TIME) ~23'	DATE I	NSTALLED _10/11/99
RISER DI SCREEN DI	A <u>2"</u> MATERIAL <u>PUC Sche</u> A <u>2"</u> MATERIAL <u>PUC, Sche</u>	dule 40 LENGTH <u>63</u> dule 40 LENGTH <u>20</u>	SLOT SIZE 10
	SC	HEMATIC	
			Ground Surfa
Surface Seal Typ	e <b>distribution</b>		Riser Elevation Bottom Surface Set
Grout Type	Bentonite I Postland Cement Mix	5	Top Seal
Seal Type	Enviroplus Bentenite	AF AF	Top Sand Back
		62	Top Screen
Sand Pack Type _ Size#/	Silica Quei Tz		
		terres presses	Babban Canaan

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# Appendix D

# APPENDIX D

# PUMP TEST DATA

PUMP TEST 1



Transmissivity [ft²/min]: 9.43 x 10<sup>-1</sup>

Hydraulic conductivity [ft/min]: 1.31 x 10<sup>-2</sup>

Aquifer thickness [ft]: 72.00
Dvirka and Bartilucci		Pumping test analysis		Date: 04.01.200	Date: 04.01.2000 Page 2		
330 Cros	Jou Crossways Park Drive         Time-Drawdown-method a           Noodbury N.Y. 11797         COOPER & JACOB		nod after	Project: FRANK	LIN CLEANERS		
ph.(516)364	4-9890	Unconfined aquifer		Evaluated by: V	VM		
Pumping	Test No. 1		Test conducted	d on: 11/09/99			
PTMW-1			PTMW-1				
Discharg	e 80.00 U.S.gal/min		Distance from	the pumping well 27.00	ft		
Static wa	ater level: 0.00 ft below datum						
	Pumping test duration	Water level	D	rawdown	Corrected		
					drawdown		
	[min]	[ft]		[ft]	[ft]		
2	0.05	0.01		0.01	0.01		
3	0.10	0.02		0.02	0.02		
4	0.15	0.03		0.03	0.03		
5	0.20	0.07		0.07	0.07		
6	0.25	0.13		0.13	0.13		
7	0.30	0.19		0.19	0.19		
8	0.35	0.27		0.27	0.27		
9	0.40	0.34		0.34	0.34		
11	0.40	0.43		0.43	0.43		
12	0.55	0.50		0.58	0.50		
13	0.60	0.67		0.67	0.67		
14	0.65	0.73		0.73	0.73		
15	0.70	0.81		0.81	0.81		
16	0.75	0.87		0.87	0.86		
17	0.80	0.94		0.94	0.93		
18	0.85	1.00		1.00	0.99		
19	0.90	1.05		1.05	1.04		
20	0.95	1.11		1.11	1.10		
21	1.00	1.15		1.15	1.14		
22	1.05	1.20		1.20	1.19		
24	1 15	1.24		1.24	1.23		
25	1.20	1.20		1.31	1.30		
26	1.25	1.35		1.35	1.34		
27	1.30	1.39		1.39	1.38		
28	1.35	1.41		1.41	1.40		
29	1.40	1.43		1.43	1.42		
30	1.45	1.46		1.46	1.45		
31	1.50	1.47		1.47	1.45		
32	1.55	1.49		1.49	1.47		
33	1.60	1.51		1.51	1.49		
35	1.00	1.53		1.55	1.51		
36	1.75	1.55		1.57	1.55		
37	1.80	1.58		1.58	1.56		
38	1.85	1.58		1.58	1.56		
39	1.90	1.60		1.60	1.58		
40	1.95	1.61		1.61	1.59		
41	2.00	1.62		1.62	1.60		
42	2.05	1.63		1.63	1.61		
43	2.10	1.64		1.64	1.62		
44	2.15	1.65		1.65	1.63		
45	2.20	1.66		1.66	1.64		
40	2.25	1.67		1.67	1.65		
47		1.07			1.05		

854×55



2.00 <sub>o</sub> PTMW-1

1.80

Transmissivity [ft²/min]: 9.75 x 10<sup>-1</sup>

Hydraulic conductivity [ft/min]: 1.35 x 10<sup>-2</sup>

11

Dvirka a	and Bartilucci	Pumping test analysis	Pumping test analysis Distance-Time-Drawdown-method after COOPER & JACOB		Date: 04.01.2000 Page 2		
330 Cros Noodbury N	sways Park Drive	Distance-Time-Drawd after COOPER & JAC			LIN CLEANERS		
oh.(516)364	1-9890	Unconfined aquifer	-	Evaluated by: W	Μ (M		
Pumping Test No. 1			Test conducted o	n: 11/09/99			
PTMW-1			PTMW-1				
Discharge	e 80.00 U.S.gal/min		Distance from the	e pumping well 27.00 f	t		
Static wa	ter level: 0.00 ft below datum				and the second		
	Pumping test duration	Water level	Drav	vdown	Corrected drawdown		
	[min]	[ft]		[ft]	[ft]		
2	0.05	0.01		0.01	0.01		
3	0.10	0.02		0.02	0.02		
4	0.15	0.03		0.03	0.03		
5	0.20	0.07		0.07	0.07		
6	0.25	0.13		0.13	0.13		
7	0.30	0.19		0.19	0.19		
8	0.35	0.27		0.27	0.27		
9	0.40	0.34		0.34	0.34		
10	0.45	0.43		0.43	0.43		
12	0.50	0.50		0.50	0.50		
12	0.00	0.58		0.50	0.56		
14	0.65	0.07		0.73	0.73		
15	0.70	0.75		0.81	0.81		
16	0.75	0.87		0.87	0.86		
17	0.80	0.94		0.94	0.93		
18	0.85	1.00		1.00	0.99		
19	0.90	1.05		1.05	1.04		
20	0.95	1.11		1.11	1.10		
21	1.00	1.15		1.15	1.14		
22	1.05	1.20		1.20	1.19		
23	1.10	1.24		1.24	1.23		
24	1.15	1.28		1.28	1.27		
25	1.20	1.31		1.31	1.30		
27	1.20	1.35		1.30	1.34		
28	1.35	1.35		1.41	1.40		
29	1.40	1.43		1.43	1.42		
30	1.45	1.46		1.46	1.45		
31	1.50	1.47		1.47	1.45		
32	1.55	1.49		1.49	1.47		
33	1.60	1.51		1.51	1.49		
34	1.65	1.53		1.53	1.51		
35	1.70	1.55		1.55	1.53		
36	1.75	1.57		1.57	1.55		
38	1.80	1.58		1.50	1.50		
39	1 90	1.50		1.60	1.50		
40	1.95	1.61		1.61	1.59		
41	2.00	1.62		1.62	1.60		
42	2.05	1.63		1.63	1.61		
43	2.10	1.64		1.64	1.62		
44	2.15	1.65		1.65	1.63		
45	2.20	1.66		1.66	1.64		
46	2.25	1.67		1.67	1.65		
47	2.30	1.67		1.67	1.65		



Transmissivity [ft²/min]: 1.03 x 10<sup>0</sup>

Hydraulic conductivity [ft/min]: 1.43 x 10<sup>-2</sup>

330 Cross		Pumping test analysis		Date. 04.01.2000	J Page 2
330 Crossways Park Drive T Woodbury N X 11797		Time-Drawdown-meth COOPER & JACOB	nod after	Project: FRANKI	LIN CLEANERS
ph.(516)364-9	3890	Unconfined aquifer		Evaluated by: W	М
Pumping T	est No. 1		Test conducte	ed on: 11/09/99	
PTMW-3			PTMW-3		
Discharge	80.00 U.S.gal/min		Distance from	the pumping well 50.00 f	t
Static wate	er level: 0.00 ft below datum				
	Pumping test duration	Water level	C	Drawdown	Corrected
	[min]	[ft]		[ft]	drawdown [ft]
2	0.05	0.00		0.00	
3	0.10	0.01		0.01	
4	0.15	0.02		0.02	
5	0.20	0.03		0.03	
6	0.25	0.06		0.06	
7	0.30	0.11		0.11	
8	0.35	0.16		0.16	
9	0.40	0.23		0.23	
10	0.45	0.29		0.29	
12	0.55	0.30		0.44	
13	0.60	0.51		0.51	
14	0.65	0.57		0.57	
15	0.70	0.63		0.63	
16	0.75	0.70		0.70	
17	0.80	0.76		0.76	
18	0.85	0.82		0.82	
20	0.90	0.87		0.87	
20	1.00	0.92		0.92	
22	1.05	1.01		1.01	
23	1.10	1.06		1.06	
24	1.15	1.10		1.10	
25	1.20	1.14		1.14	
26	1.25	1.17		1.17	
27	1.30	1.21		1.21	
20	1.35	1.23		1.23	
30	1.45	1.30		1.30	
31	1.50	1.32		1.32	
32	1.55	1.34		1.34	
33	1.60	1.37		1.37	
34	1.65	1.39		1.39	
35	1.70	1.41		1.41	
37	1.80	1.43		1.45	
38	1.85	1.46		1.46	
39	1.90	1.48		1.48	
40	1.95	1.50		1.50	
41	2.00	1.51		1.51	
42	2.05	1.52		1.52	
43	2.10	1.54		1.54	
44	2.15	1.55		1.55	
46	2.25	1.57		1.58	
40 1					
47	2.30	1.58		1.58	
47 48	2.30 2.35	1.58 1.59		1.58 1.59	

Dvirka	and Bartilucci	Pumping test analysis		Date: 04.01.200	0 Page 3
330 Cros Woodbury	330 Crossways Park Drive     Time-Drawdown-meth       Woodbury N.Y. 11797     COOPER & JACOB       ph.(516)364-9890     Unconfined aquifer		od after	Project: FRANK	LIN CLEANERS
ph.(516)36				Evaluated by: W	М
Pumping	g Test No. 1		Test conducted	on: 11/09/99	
PTMW-3	3		PTMW-3		
Discharg	ge 80.00 U.S.gal/min		Distance from th	e pumping well 50.00 f	t
Static wa	ater level: 0.00 ft below datum				
	Pumping test duration	Water level	Dra	awdown	Corrected drawdown
51	2.50	[II] 1.61		1.61	[π] 1.5
52	2.55	1.62		1.62	1.6
53	2.60	1.63		1.63	1.6
54	2.65	1.63		1.63	1.6
55	2.70	1.64		1.64	1.6
57	2.75	1.64		1.64	1.6
58	2.85	1.64		1.04	1.6
59	2.90	1.65		1.65	1.6
60	2.95	1.65		1.65	1.6



Transmissivity [ft²/min]: 1.04 x 10<sup>0</sup>

Hydraulic conductivity [ft/min]: 1.45 x 10<sup>-2</sup>

Dvirka and Bartilucci		Pumping test analysis		Date: 04.01.200	00 Page 2
330 Cros Woodbury	ssways Park Drive N.Y. 11797	Distance-Time-Drawd after COOPER & JAC	Distance-Time-Drawdown-method after COOPER & JACOB		LIN CLEANERS
ph.(516)36	64-9890	Unconfined aquifer		Evaluated by: V	VM
Pumping	J Test No. 1		Test conducted of	on: 11/09/99	
PTMW-3	3		PTMW-3		
Discharg	ge 80.00 U.S.gal/min		Distance from the	e pumping well 50.00	ft
Static wa	ater level: 0.00 ft below datum				
	Pumping test duration	Water level	Drav	wdown	Corrected
					drawdown
	[min]	[ft]		[ft]	[ft]
2	0.05	0.00		0.00	0.00
3	0.10	0.01		0.01	0.01
4	0.15	0.02		0.02	0.02
5	0.20	0.03		0.03	0.03
6	0.25	0.06		0.06	0.06
8	0.30	0.11		0.11	0.11
9	0.35	0.16		0.16	0.16
10	0.45	0.23		0.23	0.23
11	0.50	0.36		0.36	0.25
12	0.55	0.44		0.44	0.44
13	0.60	0.51		0.51	0.51
14	0.65	0.57		0.57	0.57
15	0.70	0.63		0.63	0.63
16	0.75	0.70		0.70	0.70
1/	0.80	0.76		0.76	0.76
10	0.85	0.82		0.82	0.82
20	0.95	0.87		0.87	0.86
21	1.00	0.92		0.92	0.91
22	1.05	1.01		1.01	1.00
23	1.10	1.06		1.06	1.05
24	1.15	1.10		1.10	1.09
25	1.20	1.14		1.14	1.13
26	1.25	1.17		1.17	1.16
27	1.30	1.21		1.21	1.20
20	1.35	1.23		1.23	1.22
30	1.40	1.27		1.2/	1.26
31	1.50	1.30		1.30	1.29
32	1.55	1.34		1.34	1.31
33	1.60	1.37		1.37	1.36
34	1.65	1.39		1.39	1.38
35	1.70	1.41		1.41	1.40
36	1.75	1.43		1.43	1.42
38	1.80	1.45		1.45	1.44
39	1.00	1.46		1.46	1.45
40	1.95	1.40		1.40	1.46
41	2.00	1.51		1.51	1.40
42	2.05	1.52		1.52	1.50
43	2.10	1.54		1.54	1.52
44	2.15	1.55		1.55	1.53
45	2.20	1.57		1.57	1.55
46	2.25	1.58		1.58	1.56
41	2.30	1.58		1.58	1.56
40	2.35	1.59		1.59	1.57
TJ	2.40	1.60		1.60	1.58

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Dvirka and	Bartilucci	Pumping test analysis		Date: 04.01.200	0 Page 3	
330 Crossways Park Drive         Distance-Time-I           Woodbury N.Y. 11797         after COOPER		Distance-Time-Drawd after COOPER & JAC	own-method OB	Project: FRANK	Project: FRANKLIN CLEANERS	
ph.(516)364-989	90	Unconfined aquifer		Evaluated by: W	M	
Pumping Tes	st No. 1		Test conducted	on: 11/09/99		
PTMW-3			PTMW-3			
Discharge 80	0.00 U.S.gal/min		Distance from th	ne pumping well 50.00 f	t	
Static water	level: 0.00 ft below datum					
F	Pumping test duration	Water level	Dra	awdown [ft]	Corrected drawdown [ft]	
51	2.50	1.61		1.61	1	
52	2.55	1.62		1.62	1	
53	2.60	1.63		1.63	1	
54	2.65	1.63		1.63	1	
55	2.70	1.64		1.64	1	
56	2.75	1.64		1.64	1	
57	2.80	1.64		1.64	1	
58	2.85	1.65		1.65	1	
59	2.90	1.65		1.65	1	
61	2.95	1.05		1.05	1	
		a martinite and a second s				



Transmissivity [ft²/min]: 9.78 x 10<sup>-2</sup>

Hydraulic conductivity [ft/min]: 1.35 x 10<sup>-3</sup>

Dvirka and Bartilucci		Pumping test analysis		Date: 21.01.200	00 Page 2
330 Crossways Park Drive Woodbury N.Y. 11797		Recovery method after THEIS & JACOB		Project: FRANK	LIN CLEANERS
ph.(516)364	4-9890	Unconfined aquifer		Evaluated by: W	VM
Pumping	Test No. 1	Test conducted on: 11	/09/99 - 11/10/99	9	
PTW-1			PTW-1		
Discharo	e 80.00 U.S.gal/min				
Static wa	ter level: 0.00 ft below datum		Pumping test duration:	499 80 min	
		) M/star Jawal	Pumping test duration.	499.00 mm	Corrected
		vvater level	Residual		Corrected
	end of pumping		drawdow	n	drawdown
	[min]	[ft]	[ft]		[ft]
1	0.05	26.10		26.10	21.37
2	0.10	22.92		22.92	19.27
3	0.15	20.04		20.04	17.25
4 E	0.20	17.48		17.48	15.36
0	0.25	15.22		12.22	13.01
7	0.30	13.24		11.50	12.02
- / 	0.30	0.00		9.00	0.00
0	0.40	9.99		8.67	9.30
10	0.40	0.07		7.55	0.15
11	0.50	6.53		6.53	01.1 20 A
12	0.00	5.72		5.72	5.40
13	0.65	4 99		4.99	4.82
14	0.00	4.36		4.36	4 23
15	0.75	3.81		3.81	3.71
16	0.80	3.36		3.36	3.28
17	0.85	2.97		2.97	2.91
18	0.90	2.64		2.64	2.59
19	0.95	2.34		2.34	2.30
20	1.00	2.10		2.10	2.07
21	1.05	1.89		1.89	1.87
22	1.10	1.70		1.70	1.68
23	1.15	1.55		1.55	1.53
24	1.20	1.41		1.41	1.40
25	1.25	1.29		1.29	1.28
26	1.30	1.18		1.18	1.17
27	1.35	1.10		1.10	1.09
28	1.40	1.02		1.02	1.01
29	1.45	0.95		0.95	0.94
30	1.50	0.90		0.90	0.89
31	1.55	0.84		0.84	0.84
32	1.60	0.79		0.79	0.79
34	1.00	0.75		0.75	0.75
35	1.70	0.72		0.72	0.72
36	1.75	0.00		0.65	0.00
37	1.85	0.63		0.63	0.63
38	1.90	0.60		0.60	0.60
39	1.95	0.58		0.58	0.58
40	2.00	0.56		0.56	0.56
41	2.05	0.54		0.54	0.54
42	2.10	0.52		0.52	0.52
43	2.15	0.51		0.51	0.51
44	2.20	0.50		0.50	0.50
45	2.25	0.51		0.51	0.51
46	2.30	0.47		0.47	0.47
47	2.35	0.46		0.46	0.46
48	2.40	0.45		0.45	0.45
49	2.45	0.45		0.45	0.45
50	2.50	0.43		0.43	0.43

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Dvirka and Bartilucci		Pumping test analysis		Date: 21.01.200	0 Page 3	
330 Crossways Park Drive Woodbury N.Y. 11797		Recovery method after THEIS & JACOB	Recovery method after THEIS & JACOB		Project: FRANKLIN CLEANERS	
ph.(516)364	-9890	Unconfined aquifer		Evaluated by: W	/M	
Pumping	Test No. 1		Test conducted	on: 11/09/99 - 11/10/99	)	
PTW-1	PTW-1		PTW-1			
Discharge	e 80.00 U.S.gal/min					
Static wat	ter level: 0.00 ft below datum		Pumping test du	uration: 499.80 min		
	Time from	Water level	R	esidual	Corrected	
	end of pumping		dra	awdown	drawdown	
	[min]	[ft]		[ft]	[ft]	
51	2.55	0.42		0.42	0.42	
52	2.60	0.42		0.42	0.42	
53	2.65	0.41		0.41	0.41	
54	2.70	0.40		0.40	0.40	
55	2.75	0.39		0.39	0.39	
57	2.80	0.39		0.39	0.39	
58	2.00	0.38		0.38	0.38	
59	2.50	0.30		0.30	0.38	
60	3.00	0.37		0.37	0.38	
61	3.05	0.36		0.36	0.36	
62	3.10	0.36		0.36	0.36	
63	3.15	0.35		0.35	0.35	
64	3.20	0.35		0.35	0.35	
65	3.25	0.34		0.34	0.34	
66	3.30	0.34		0.34	0.34	
67	3.35	0.34		0.34	0.34	
68	3.40	0.33		0.33	0.33	
69	3.45	0.33		0.33	0.33	
70	3.50	0.32		0.32	0.32	
72	3.55	0.32		0.32	0.32	
73	3.65	0.32		0.32	0.32	
74	3.70	0.32		0.32	0.32	
75	3.75	0.32		0.32	0.32	
76	3.80	0.31		0.31	0.31	
77	3.85	0.31		0.31	0.31	
78	3.90	0.31		0.31	0.31	
79	3.95	0.31		0.31	0.31	
80	4.00	0.31		0.31	0.31	
81	4.05	0.30		0.30	0.30	
82	4.10	0.30		0.30	0.30	
84	4.15	0.29		0.29	0.29	
85	4.20	0.30		0.30	0.30	
86	4.30	0.29		0.29	0.29	
87	4.35	0.29		0.29	0.29	
88	4.40	0.29		0.29	0.29	
89	4.45	0.29		0.29	0.29	
90	4.50	0.28		0.28	0.28	
91	4.55	0.28		0.28	0.28	
92	4.60	0.29		0.29	0.29	
93	4.65	0.28		0.28	0.28	
94	4.70	0.28		0.28	0.28	
95	4.75	0.28		0.28	0.28	
90	4.80	0.28		0.28	0.28	
97	4.85	0.27		0.27	0.27	
99	4.90	0.27		0.27	0.27	
100	5.00	0.27		0.27	0.27	

Dvirka and	Bartilucci	Pumping test analysis		Date: 21.01.2000	Page 4
330 Crosswa Woodbury N.Y. 1	ys Park Drive	Recovery method after THEIS & JACOB		Project: FRANKLIN	N CLEANERS
ph.(516)364-989	D	Unconfined aquifer		Evaluated by: WM	
Pumping Tes	t No. 1		Test conducted on:	11/09/99 - 11/10/99	
PTW-1			PTW-1		
Discharge 80	.00 U.S.gal/min				
Static water le	evel: 0.00 ft below datum		Pumping test duration	on: 499.80 min	
	Time from end of pumping	Water level	Resid drawd	lual own	Corrected drawdown
101	[min]	[ft]	[ft]	0.07	[ft]
102	5.10	0.27		0.27	
103	5.15	0.27		0.27	
104	5.20	0.26		0.26	
				the second	



Transmissivity [ft²/min]: 1.18 x 10<sup>0</sup>

Hydraulic conductivity [ft/min]: 1.64 x 10<sup>-2</sup>

Dvirka and Bartilucci		Pumping test analysis		Date: 04.01.2000 Page 2		
330 Cross Woodbury N	ways Park Drive Y. 11797	Recovery method after THEIS & JACOB	er	Project: FRANKI	LIN CLEANERS	
ph.(516)364-	9890	Unconfined aquifer		Evaluated by: W	M	
Pumping	Fest No. 1		Test conducted o	n: 11/09/99		
PTMW-1			PTMW-1			
Discharge	80.00 U.S.gal/min		Distance from the	pumping well 27.00 fl		
Static wate	er level: 0.00 ft below datum		Pumping test dur	ation: 499 90 min		
	Time from	Water level	Por	sidual	Corrected	
	end of pumping	water lever	draw	Ndown	drawdown	
		[#1	ulav	r#1	urawuown (#1	
1	0.05			1.81	[II] 1 79	
2	0.10	1.78		1.78	1.76	
3	0.15	1.74		1.74	1.72	
4	0.20	1.69		1.69	1.67	
5	0.25	1.63		1.63	1.61	
6	0.30	1.57		1.57	1.55	
7	0.35	1.51		1.51	1.49	
8	0.40	1.45		1.45	1.44	
9	0.45	1.38		1.38	1.37	
10	0.50	1.32		1.32	1.31	
11	0.55	1.25		1.25	1.24	
12	0.60	1.19		1.19	1.18	
13	0.65	1.13	-	1.13	1.12	
14	0.70	1.08		1.08	1.07	
15	0.75	1.02		1.02	1.01	
16	0.80	0.97		0.97	0.96	
17	0.85	0.92		0.92	0.91	
18	0.90	0.87		0.87	0.86	
19	0.95	0.82		0.82	0.82	
20	1.00	0.79		0.79	0.79	
21	1.05	0.75		0.75	0.75	
22	1.10	0.72		0.72	0.72	
24	1.13	0.09		0.66	0.69	
25	1.25	0.63		0.63	0.00	
26	1.30	0.61		0.61	0.03	
27	1.35	0.58		0.58	0.58	
28	1.40	0.56		0.56	0.56	
29	1.45	0.54		0.54	0.54	
30	1.50	0.52		0.52	0.52	
31	1.55	0.51		0.51	0.51	
32	1.60	0.49		0.49	0.49	
33	1.65	0.48		0.48	0.48	
34	1.70	0.47		0.47	0.47	
35	1.75	0.45		0.45	0.45	
36	1.80	0.44		0.44	0.44	
3/	1.85	0.43		0.43	0.43	
30	1.90	0.42		0.42	0.42	
40	1.95	0.41		0.41	0.41	
40	2.00	0.41		0.20	0.41	
42	2.05	0.39		0.39	0.39	

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Transmissivity [ft²/min]: 5.52 x 10<sup>-1</sup>

Hydraulic conductivity [ft/min]: 7.68 x 10<sup>-3</sup>

Dvirka a	and Bartilucci	Pumping test analysis	Pumping test analysis		0 Page 2
330 Cross	sways Park Drive	Recovery method after THEIS & JACOB	er	Project: FRANK	LIN CLEANERS
ph.(516)364	4-9890	Unconfined aquifer		Evaluated by: W	M
Pumping	Test No. 1		Test conducted c	on: 11/09/99	
PTMW-2			PTMW-2		
Discharg	je 80.00 U.S.gal/min		Distance from the	e pumping well 12.00 f	t
Static wa	ater level: 0.00 ft below datum		Pumping test dur	ation: 500.00 min	
	Time from	Water level	Re	eidual	Corrected
	end of numning	Water ione.	drav	vdown	drawdown
	[min]	[ft]	-	[ft]	[ft]
2	0.05	3.87		3.87	3.77
3	0.10	3.76		3.76	3.66
4	0.15	3.57		3.57	3.48
5	0.20	3.36		3.36	3.28
6	0.25	3.14		3.14	3.07
7	0.30	2.93		2.93	2.87
8	0.35	2.72		2.72	2.67
9	0.40	2.52		2.52	2.47
10	0.45	2.33		2.33	2.29
11	0.50	2.15		2.15	2.12
12	0.55	1.99		1.99	1.96
13	0.60	1.84		1.84	1.82
14	0.65	1.70		1.70	1.68
16	0.75	1.50		1.50	1.50
17	0.80	1.40		1.40	1.43
18	0.85	1.26		1.26	1.25
19	0.90	1.18		1.18	1.17
20	0.95	1.10		1.10	1.09
21	1.00	1.03		1.03	1.02
22	1.05	0.97		0.97	0.96
23	1.10	0.91		0.91	0.91
24	1.15	0.86		0.86	0.86
25	1.20	0.81		0.81	0.81
26	1.25	0.77		0.77	0.77
27	1.30	0.74		0.74	0.73
20	1.35	0.70		0.70	0.70
30	1.45	0.65		0.65	0.64
31	1.50	0.62		0.62	0.62
32	1.55	0.60		0.60	0.59
33	1.60	0.57		0.57	0.57
34	1.65	0.56		0.56	0.55
35	1.70	0.54		0.54	0.54
36	1.75	0.52		0.52	0.52
37	1.80	0.50		0.50	0.50
38	1.85	0.49		0.49	0.49
40	1.90	0.48		0.48	0.47
41	2 00	0.47		0.47	0.40
42	2.05	0.44		0.44	0.44
43	2.10	0.43		0.43	0.43
44	2.15	0.42		0.42	0.42
45	2.20	0.41		0.41	0.41
46	2.25	0.41		0.41	0.40
47	2.30	0.40		0.40	0.40
48	2.35	0.39		0.39	0.39
49	2.40	0.38		0.38	0.38
50	2.45	0.38		0.38	0.38

Dvirka and Bartilucci 330 Crossways Park Drive		Pumping test analysis	Pumping test analysis		DO Page 3
Woodbury N	N.Y. 11797	THEIS & JACOB	r	Project: FRANKLIN CL	
ph.(516)364	-9890	Unconfined aquifer		Evaluated by: V	VM
Pumping	Test No. 1		Test conducted of	on: 11/09/99	
PTMW-2 PTMW-2			PTMW-2		
Discharge	e 80.00 U.S.gal/min		Distance from the	e pumpina well 12 00	ft
Static wat	ter level: 0.00 ft below datum		Pumping test dur	ration: 500 00 min	
	Time from	Water level		aidual	
	end of pumping	vvater lever	Re	wdown	Corrected
	[min]	[ft]	ura	(ff)	drawdown
51	2.50	0.37		0.37	[π]
52	2.55	0.36		0.37	0.3
53	2.60	0.36		0.36	0.3
54	2.65	0.36		0.36	0.3
55	2.70	0.35		0.35	0.3
56	2.75	0.34		0.34	0.3
57	2.80	0.34		0.34	0.3
58	2.85	0.34		0.34	0.3
59	2.90	0.33		0.33	0.3
61	2.95	0.33		0.33	0.3
62	3.00	0.32		0.32	0.3
63	3.00	0.32		0.32	0.3
64	3.15	0.32		0.32	0.3
65	3.20	0.31		0.31	0.3
66	3.25	0.31		0.31	0.3
67	3.30	0.30		0.30	0.3
68	3.35	0.30		0.30	0.3
69	3.40	0.30		0.30	0.3
70	3.45	0.30		0.30	0.3
71	3.50	0.30		0.30	0.3
72	3.55	0.29		0.29	0.2
73	3.60	0.29		0.29	0.29
75	3.05	0.29		0.29	0.29
76	3.75	0.29		0.29	0.29
77	3.80	0.28		0.28	0.28
78	3.85	0.28		0.28	0.28
79	3.90	0.28		0.28	0.28
80	3.95	0.28		0.28	0.20
81	4.00	0.28		0.28	0.27
82	4.05	0.28		0.28	0.27
83	4.10	0.28		0.28	0.27
84	4.15	0.27		0.27	0.27
86	4.20	0.27		0.27	0.27
87	4.25	0.27		0.27	0.27
88	4.30	0.27		0.27	0.27
89	4.40	0.26		0.26	0.26
90	4.45	0.20		0.20	0.26
91	4.50	0.26		0.26	0.26
92	4.55	0.26		0.26	0.26
93	4.60	0.26		0.26	0.26
94	4.65	0.26		0.26	0.26
95	4.70	0.26		0.26	0.26
96	4.75	0.26		0.26	0.26
97	4.80	0.26		0.26	0.25
98	4.85	0.25		0.25	0.25
33	4.90	0.25		0.25	0.25

Dvirka and Bartilucci 330 Crossways Park Drive Woodbury N.Y. 11797		Pumping test analysis		Date: 13.01.20	00 Page 4
		Recovery method after THFIS & JACOB	Recovery method after THEIS & JACOB		Project: FRANKLIN CLEANERS
ph.(516)364-9	890	Unconfined aquifer	r Evaluated by: WM		νM
Pumping Test No. 1			Test conducte	ed on: 11/09/99	3
PTMW-2			PTMW-2		
Discharge	80.00 U.S.gal/min		Distance from	n the pumping well 12.00	ft
Static wate	r level: 0.00 ft below datum		Pumpina test	duration: 500.00 min	1
	Time from	Water level		Pesidual	Corrected
	and of pumping	vvaler lever		drawdawn	drawdown
	end of pumping	(4)			Ulawuowii
101	[min]	[II]		0.25	[II]
101	5.00	0.20		0.25	0.25
102	5.05	0.23		0.25	0.25
103	5.10	0.25		0.25	0.25
105	5.15	0.20		0.25	0.20
106	5.20	0.24		0.24	0.24
107	5.20	0.24		0.24	0.24
108	5.30	0.24		0.24	0.24
100	5.35	0.24		0.24	0.24
110	5.40	0.24		0.24	0.24
111	5.40	0.24		0.24	0.24
112	5.50	0.24		0.24	0.24
112	5.55	0.24		0.24	0.24
114	5.65	0.24		0.24	0.24
115	5.05	0.23		0.23	0.23
116	5.75	0.23		0.23	0.23
117	5.80	0.23		0.23	0.23
118	5.85	0.23		0.23	0.23
110	5.00	0.23		0.23	0.23
120	5.00	0.23		0.23	0.23
121	6.00	0.20		0.23	0.23
122	6.05	0.23		0.23	0.23
123	6.10	0.23		0.23	0.23
124	6.15	0.23		0.23	0.23
125	6.20	0.22		0.22	0.22
126	6.25	0.22		0.22	0.22
127	6.30	0.22		0.22	0.22
128	6.35	0.22		0.22	0.22
129	6.40	0.22		0.22	0.22
130	6.45	0.22		0.22	0.22
131	6.50	0.22		0.22	0.22
132	6.55	0.22		0.22	0.22
133	6.60	0.22		0.22	0.22
134	6.65	0.22		0.22	0.22
135	6.70	0.22		0.22	0.22
136	6.75	0.22		0.22	0.22
137	6.80	0.22		0.22	0.22
138	6.85	0.22		0.22	0.22
139	6.90	0.22		0.22	0.22
140	6.95	0.21		0.21	0.21
141	7.00	0.21		0.21	0.21
142	7.05	0.21		0.21	0.21
143	7.10	0.21		0.21	0.21
144	7.15	0.21		0.21	0.21
145	7.20	0.21		0.21	0.21
146	7.25	0.21		0.21	0.21
147	7.30	0.21		0.21	0.21
148	7.35	0.21		0.21	0.21
149	7.40	0.21		0.21	0.21
150	7.45	0.21		0.21	0.21

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Dvirka and Bartilucci		Pumping test analysis		Date: 13.01.2000	Page 5	
330 Crossways Park Drive Woodbury N.Y. 11797		Recovery method after THEIS & JACOB	r	Project: FRANKLIN CLEANERS		
ph.(516)364-9	890	Unconfined aquifer		Evaluated by: WM		
Pumping T	est No. 1		Test conducted of	on: 11/09/99	1	
PTMW-2			PTMW-2			
Discharge	80.00 U.S.gal/min		Distance from the	e pumping well 12.00 ft		
Static wate	r level: 0.00 ft below datum		Pumping test dur	ation: 500.00 min		
	Time from	Water level	Re	sidual	Corrected	
	end of pumping		drav	wdown	drawdown	
	[min]	[ft]		[ft]	[ft]	
151	7.50	0.21		0.21	0.21	
152	7.55	0.21		0.21	0.21	
153	7.60	0.21		0.21	0.21	
154	7.65	0.21		0.21	0.21	
155	7.70	0.21		0.21	0.21	
157	7.15	0.21		0.21	0.21	
158	7.85	0.21		0.21	0.21	
159	7.90	0.21		0.21	0.21	
160	7.95	0.21		0.21	0.21	
161	8.00	0.21	-	0.21	0.21	
162	8.05	0.20		0.20	0.20	
163	8.10	0.20		0.20	0.20	
164	8.15	0.20		0.20	0.20	
165	8.20	0.20		0.20	0.20	
166	8.25	0.20		0.20	0.20	
167	8.30	0.20		0.20	0.20	
168	8.35	0.20		0.20	0.20	
169	8.40	0.20		0.20	0.20	
170	8.50	0.20		0.20	0.20	
172	8.55	0.20		0.20	0.20	
173	8.60	0.20		0.20	0.20	
174	8.65	0.20		0.20	0.20	
175	8.70	0.20		0.20	0.20	
176	8.75	0.20		0.20	0.20	
177	8.80	0.20		0.20	0.20	
178	8.85	0.20		0.20	0.20	
179	8.90	0.20		0.20	0.20	
180	8.95	0.20		0.20	0.20	
181	9.00	0.20		0.20	0.20	
183	9.05	0.20		0.20	0.20	
184	9.10	0.20		0.20	0.20	
185	9.20	0.19		0.19	0.19	
186	9.25	0.20		0.20	0.20	
187	9.30	0.19		0.19	0.19	
188	9.35	0.19		0.19	0.19	
189	9.40	0.19		0.19	0.19	
190	9.45	0.19		0.19	0.19	
191	9.50	0.19		0.19	0.19	
192	9.55	0.19		0.19	0.19	
193	9.60	0.19		0.19	0.19	
194	9.65	0.19		0.19	0.19	
196	9.70	0.19		0.19	0.19	
197	9.75	0.19		0.19	0.19	
198	9.85	0.19		0.19	0.19	
199	9.90	0.19		0.19	0.19	
200	9.95	0.19		0.19	0.19	

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Dvirka and BartilucciPumpin330 Crossways Park DriveRecoverWoodbury N.Y. 11797THEISph.(516)364-9890Uncomp		Pumping test analysis		Date: 13.01.2000 Page 6	
		Recovery method after THEIS & JACOB	r	Project: FRANKL	IN CLEANERS
		Unconfined aquifer	confined aquifer		Evaluated by: WM
Pumping Test No. 1			Test conducted on:	: 11/09/99	L
PTMW-2	2		PTMW-2		
Discharc	ge 80.00 U.S.gal/min		Distance from the p	oumping well 12.00 ft	- 1
Static wa	ater level: 0.00 ft below datum		Pumping test durat	ion: 500.00 min	
	Time from	Water level	Resid	dual	Corrected
1	end of pumping		drawo	down	drawdown
	[min]	[ft]	[ft	:]	[ft]
201	10.00	0.19		0.19	0.19
					and a state of a second
			-		
	4				
					The second se



Transmissivity [ft²/min]: 1.37 x 10<sup>0</sup>

Hydraulic conductivity [ft/min]: 1.90 x 10<sup>-2</sup>

Dvirka and BartilucciPumping test330 Crossways Park DriveRecovery meWoodbury N.Y. 11797THEIS & JACph.(516)364-9890Unconfined and		Pumping test analysis Recovery method after THEIS & JACOB		Date: 10.01.2000 Page 2 Project: FRANKLIN CLEANERS		
		Pumping 1	Pumping Test No. 1			n: 11/09/99
PTMW-3			PTMW-3			
Discharge	80.00 U.S.gal/min		Distance from the	pumping well 50.00 f	t	
Static wate	er level: 0.00 ft below datum		Pumping test dura	ation: 500.00 min		
	Time from	Water level	Res	sidual	Corrected	
	end of pumping		draw	vdown	drawdown	
	[min]	[ft]		ft]	[ft]	
1	0.05	1.82		1.82	1.80	
2	0.10	1.79		1.79	1.77	
3	0.15	1.75		1.75	1.73	
4	0.20	1.70		1.70	1.68	
5	0.25	1.65		1.65	1.63	
6	0.30	1.60		1.60	1.58	
7	0.35	1.54		1.54	1.52	
8	0.40	1.48		1.48	1.46	
9	0.45	1.43		1.43	1.42	
10	0.50	1.37		1.37	1.36	
12	0.55	1.32		1.32	1.31	
13	0.65	1.20		1.20	1.25	
14	0.70	1.16		1.16	1.15	
15	0.75	1.10		1.12	1.10	
16	0.80	1.07		1.07	1.06	
17	0.85	1.03		1.03	1.02	
18	0.90	0.99		0.99	0.98	
19	0.95	0.95		0.95	0.94	
20	1.00	0.92		0.92	0.91	
21	1.05	0.88		0.88	0.87	
22	1.10	0.85		0.85	0.84	
23	1.15	0.82		0.82	0.82	
24	1.20	0.79		0.79	0.79	
25	1.25	0.77		0.77	0.77	
20	1.30	0.74		0.74	0.74	
28	1.00	0.72		0.72	0.72	
29	1.45	0.68		0.68	0.68	
30	1.50	0.66		0.66	0.66	
31	1.55	0.64		0.64	0.64	
32	1.60	0.63		0.63	0.63	
33	1.65	0.61		0.61	0.61	
34	1.70	0.59		0.59	0.59	
35	1.75	0.58		0.58	0.58	
36	1.80	0.56		0.56	0.56	
3/	1.85	0.55		0.55	0.55	
39	1.90	0.54		0.54	0.54	
40	2 00	0.53		0.52	0.53	

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PUMP TEST 2



Transmissivity [ft²/min]: 1.05 x 10<sup>0</sup>

Hydraulic conductivity [ft/min]: 1.46 x 10<sup>-2</sup>



Transmissivity [ft²/min]: 1.14 x 10<sup>0</sup>

Hydraulic conductivity [ft/min]: 1.58 x 10<sup>-2</sup>

Dvirka and Bartilucci 330 Crossways Park Drive Woodbury N.Y. 11797		Pumping test analysis		Date: 06.01.2000 Page 2	
		Time-Drawdown-metho COOPER & JACOB	od after	Project: FRANKLIN CLEANERS	
ph.(516)364-9	9890	Unconfined aquifer		Evaluated by: W	М
Pumping Test No. 2		Test conducted	on: 11/10/99		
PTMW-1			PTMW-1		
Discharge	65.00 U.S.gal/min		Distance from th	ne pumping well 27.00 ft	
Static wate	er level: 0.00 ft below datum				
	Pumping test duration	Water level	Dra	awdown	Corrected
	[min]	[ft]	_	[ft]	[ft]
1	0.20	0.01		0.01	0.01
2	0.25	0.02		0.02	0.02
3	0.30	0.02		0.02	0.02
5	0.35	0.04		0.04	0.04
6	0.45	0.04		0.04	0.04
7	0.50	0.05		0.05	0.05
8	0.55	0.06		0.06	0.05
9	0.60	0.07		0.07	0.07
10	0.65	0.09		0.09	0.09
11	0.70	0.11		0.11	0.11
12	0.75	0.11		0.11	0.11
13	0.80	0.14		0.14	0.14
15	0.85	0.15		0.15	0.15
16	0.90	0.17		0.17	0.17
17	1.00	0.19		0.19	0.19
18	1.05	0.23		0.21	0.21
19	1.10	0.26		0.26	0.26
20	1.15	0.28		0.28	0.28
21	1.20	0.30		0.30	0.30
22	1.25	0.32		0.32	0.32
23	1.30	0.35		0.35	0.35
24	1.35	0.37		0.37	0.37
26	1.40	0.39		0.39	0.39
27	1.50	0.41		0.41	0.41
28	1.55	0.45		0.45	0.43
29	1.60	0.47		0.47	0.43
30	1.65	0.49		0.49	0.49
31	1.70	0.50		0.50	0.50
32	1.75	0.52		0.52	0.52
33	1.80	0.53		0.53	0.53
35	1.85	0.57		0.57	0.57
36	1.95	0.57		0.57	0.57
37	2.00	0.61		0.00	0.60
38	2.05	0.62		0.62	0.62
39	2.10	0.64		0.64	0.64
40	2.15	0.66		0.66	0.66
41	2.20	0.67		0.67	0.67
42	2.25	0.68		0.68	0.68
43	2.30	0.70		0.70	0.70
44	2.35	0.71		0.71	0.71
46	2.40	0.72		0.72	0.72
47	2.50	0.73		0.73	0.73
48	2.55	0.76		0.74	0.74
49	2.60	0.78		0.78	0.78
50	2.65	0.79		0.79	0.79

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Dvirka and Bartilucci 330 Crossways Park Drive Woodbury N.Y. 11797 ph.(516)364-9890		Pumping test analysis		Date: 06.01.200	0 Page 3	
		Time-Drawdown-meth COOPER & JACOB	Time-Drawdown-method after COOPER & JACOB Unconfined aquifer		Project: FRANKLIN CLEANERS	
		Unconfined aquifer			Evaluated by: WM	
Pumping Test No. 2			Test conducted of	on: 11/10/99		
PTMW-1			PTMW-1			
Discharge	e 65.00 U.S.gal/min		Distance from the	e pumping well 27.00 f	t	
Static wat	er level: 0.00 ft below datum					
	Pumping test duration	Water level	Dra	wdown	Corrected drawdown	
	[min]	[ft]		[ft]	[ft]	
51	2.70	0.83		0.83	0.83	
52	2.75	0.84		0.84	0.84	
53	2.80	0.87		0.87	0.86	
54	2.85	0.90		0.90	0.89	
56	2.90	0.92		0.92	0.91	
57	3.00	0.94		0.96	0.95	
58	3.05	0.98		0.98	0.97	
59	3.10	1.00		1.00	0.99	
60	3.15	1.02		1.02	1.01	
61	3.20	1.04		1.04	1.03	
62	3.25	1.05		1.05	1.04	
63	3.30	1.07		1.07	1.06	
64	3.35	1.08		1.08	1.07	
65	3.40	1.09		1.09	1.08	
67	3.45	1.10		1.10	1.09	
68	3.50	1.11		1.11	1.10	
69	3.60	1.12		1.12	1.11	
70	3.65	1.14		1.14	1.13	
71	3.70	1.14		1.14	1.13	
72	3.75	1.15		1.15	1.14	
73	3.80	1.17		1.17	1.16	
74	3.85	1.17		1.17	1.16	
75	3.90	1.18		1.18	1.17	
76	<u>3.95</u> 4.00	<u>1.18</u> 1.19		1.18	<u> </u>	



Transmissivity [ft²/min]: 1.13 x 10<sup>0</sup>

Hydraulic conductivity [ft/min]: 1.57 x 10<sup>-2</sup>

Dvirka and Bartilucci 330 Crossways Park Drive Woodbury N.Y. 11797		Pumping test analysis Distance-Time-Drawdown-method after COOPER & JACOB		Date: 06.01.2000 Page 2 Project: FRANKLIN CLEANERS			
							ph.(516)36
Pumping	g Test No. 2		Test conducted of	on: 11/10/99			
PTMW-1	I		PTMW-1				
Discharg	ge 65.00 U.S.gal/min		Distance from the	e pumping well 27.00	ft		
Static wa	ater level: 0.00 ft below datum						
	Pumping test duration	Water level	Dra	wdown	Corrected		
					drawdown		
	[min]	[ft]		[ft]	[ft]		
1	0.20	0.01		0.01	0.01		
2	0.25	0.02		0.02	0.02		
3	0.30	0.02	1.	0.02	0.02		
4	0.35	0.04		0.04	0.04		
5	0.40	0.04		0.04	0.04		
7	0.45	0.05		0.05	0.05		
8	0.50	0.05		0.05	0.05		
9	0.55	0.00		0.00	0.00		
10	0.65	0.07		0.09	0.09		
11	0.70	0.11		0.11	0.11		
12	0.75	0.11		0.11	0.11		
13	0.80	0.14		0.14	0.14		
14	0.85	0.15		0.15	0.15		
15	0.90	0.17		0.17	0.17		
16	0.95	0.19		0.19	0.19		
17	1.00	0.21		0.21	0.21		
18	1.05	0.23		0.23	0.23		
19	1.10	0.26		0.26	0.26		
20	1.15	0.28		0.28	0.28		
21	1.20	0.30		0.30	0.30		
22	1.25	0.32		0.32	0.32		
23	1.30	0.35		0.35	0.35		
24	1.55	0.37		0.37	0.37		
26	1.40	0.39		0.33	0.41		
27	1.50	0.43		0.43	0.43		
28	1.55	0.45		0.45	0.45		
29	1.60	0.47		0.47	0.47		
30	1.65	0.49		0.49	0.49		
31	1.70	0.50		0.50	0.50		
32	1.75	0.52		0.52	0.52		
33	1.80	0.53		0.53	0.53		
34	1.85	0.57		0.57	0.57		
35	1.90	0.57		0.57	0.57		
30	1.95	0.60		0.60	0.60		
38	2.00	0.61		0.62	0.61		
39	2.00	0.62		0.64	0.02		
40	2.15	0.66		0.66	0.66		
41	2.20	0.67		0.67	0.67		
42	2.25	0.68		0.68	0.68		
43	2.30	0.70		0.70	0.70		
44	2.35	0.71		0.71	0.71		
45	2.40	0.72		0.72	0.72		
46	2.45	0.73		0.73	0.73		
47	2.50	0.74		0.74	0.74		
48	2.55	0.76		0.76	0.76		
49	2.60	0.78		0.78	0.78		
50	2.65	0.79		0.79	0.79		

Dvirka	and Bartilucci	Pumping test analysis		Date: 06.01.200	00 Page 3
330 Crossways Park Drive     Distance-Time-Drawc       Woodbury N.Y. 11797     after COOPER & JAC       ph.(516)364-9890     Unconfined aquifer       Pumping Test No. 2     2		Distance-Time-Drawdown	n-method	Project: FRANKLIN CLEANERS	
		Unconfined aquifer		Evaluated by: V	VM
		т	est conducted o	on: 11/10/99	
PTMW-1					
Discharc	ne 65.00 U.S.gal/min		listance from the		4
Static wa	ater level: 0.00 ft below datum			e pumping weil 27.00	n
	Pumping test duration	Water level	Dra	udown	Corrected
		Water level	Dia	wdown	drawdown
51	[min] 2 70	[ft]0.83		[ft]	[ft]
52	2.75	0.84		0.84	0.8
53	2.80	0.87		0.87	0.8
54	2.85	0.90		0.90	0.8
55	2.90	0.92		0.92	0.9
56	2.95	0.94		0.94	0.9
59	3.00	0.96		0.96	0.9
59	3.05	0.98		0.98	0.9
60	3.15	1.00		1.00	0.99
61	3.20	1.02		1.02	1.0
62	3.25	1.05		1.05	1.04
63	3.30	1.07		1.07	1.00
64	3.35	1.08		1.08	1.0
65	3.40	1.09		1.09	1.08
67	3.45	1.10		1.10	1.09
68	3.55	1.11		1.11	1.10
69	3.60	1.12		1.12	1.11
70	3.65	1.14		1.14	1.12
71	3.70	1.14		1.14	1.13
72	3.75	1.15		1.15	1.14
73	3.80	1.17		1.17	1.16
75	3.85	1.17		1.17	1.16
76	3.90	1.18		1.18	1.17
77	4.00	1.10		1.18	1.17

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Transmissivity [ft²/min]: 6.06 x 10<sup>-1</sup>

Hydraulic conductivity [ft/min]: 8.42 x 10<sup>-3</sup>

Dvirka and Bartilucci Pumping test analysis			Date: 06.01.200	00 Page 2	
330 Cros Woodbury	330 Crossways Park Drive     Time-Drawdown-me       Woodbury N.Y. 11797     COOPER & JACOE		od after	Project: FRANK	LIN CLEANERS
ph.(516)36	34-9890	Unconfined aquifer		Evaluated by: V	VM
Pumping	g Test No. 2		Test conducte	ed on: 11/10/99	
PTMW-2	2		PTMW-2		
Dischar	ge 65.00 U.S.gal/min		Distance from	the pumping well 12.00	ft
Static wa	ater level: 0.00 ft below datum				
	Pumping test duration	Water level		Drawdown	Corrected
	[min]	[ft]		[ft]	drawdown [ft]
2	0.05	0.03		0.03	0.
3	0.10	0.06		0.06	0.
4	0.15	0.09		0.09	0.
5	0.20	0.12		0.12	0.
7	0.30	0.14		0.14	0.
8	0.35	0.18		0.18	0.
9	0.40	0.20		0.20	0.
10	0.45	0.22		0.22	0.
11	0.50	0.25		0.25	0.
13	0.55	0.30		0.30	0.
14	0.65	0.42		0.42	0.
15	0.70	0.48		0.48	0.
16	0.75	0.53		0.53	0.
17	0.80	0.58		0.58	0.
19	0.90	0.03		0.69	0.
20	0.95	0.76		0.76	0.
21	1.00	0.82		0.82	0.
22	1.05	0.88		0.88	0.
23	1.10	0.94		0.94	0.
24	1.15	0.99 1.05	_	0.99	0.
26	1.25	1.10		1.10	1.
27	1.30	1.15		1.15	1.
28	1.35	1.19		1.19	1.
29	1.40	1.23		1.23	1.
30	1.45	1.2/		1.27	1.
32	1.55	1.33		1.30	1.
33	1.60	1.38		1.38	1.
34	1.65	1.42		1.42	1.
35	1.70	1.47		1.47	1.
36	1.75	1.51		1.51	1.
38	1.85	1.58		1.55	1.
39	1.90	1.61		1.61	1.
40	1.95	1.65		1.65	1.
41	2.00	1.67		1.67	1.
42	2.05	1.70		1.70	1.
43	2.10	1.72		1.72	1.
45	2.20	1.75		1.75	1.
46	2.25	1.77		1.77	1.
47	2.30	1.78		1.78	1.
48	2.35	1.81		1.81	1.
49	2.40	1.07		1.87	1.

Dvirka and	d Bartilucci	Pumping test analysis	3	Date: 06.01.200	0 Page 3	
330 Crossw Woodbury N.Y.	ays Park Drive	Time-Drawdown-meth COOPER & JACOB	nod after	Project: FRANK	Project: FRANKLIN CLEANERS	
pn.(516)364-98	90	Uncommed aquiter		Evaluated by: W	M	
Pumping Test No. 2			Test conducted	on: 11/10/99		
PTMW-2			PTMW-2			
Discharge 6	5.00 U.S.gal/min		Distance from t	he pumping well 12.00 f	t	
Static water	level: 0.00 ft below datum					
F	Pumping test duration	Water level	Dr	awdown	Corrected drawdown	
	[min]	[ft]		[ft]	[ft]	
51	2.50	2.00		2.00	1.9	
52	2.55	2.08	6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2.08	2.0	
53	2.60	2.15		2.15	2.1	
55	2.65	2.21		2.21	2.1	
56	2.70	2.28		2.20	2.2	
57	2.10	2.33		2.00	2.2	
58	2.00	2.38		2.30	2.3	
59	2.00	2.43		2.47	2.0	
60	2.95	2.50		2.50	2.4	
61	3.00	2.53		2.53	2.4	
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Transmissivity [ft²/min]: 5.90 x 10<sup>-1</sup>

Hydraulic conductivity [ft/min]: 8.19 x 10<sup>-3</sup>

Dvirka and Bartilucci 330 Crossways Park Drive Woodbury N.Y. 11797		Pumping test analysis	5	Date: 06.01.2000 Page 2			
		Distance-Time-Drawo after COOPER & JAC	Distance-Time-Drawdown-method after COOPER & JACOB		Project: FRANKLIN CLEANERS		
ph.(516)36	54-9890	Unconfined aquifer		Evaluated by: WM			
Pumping Test No. 2			Test conducted on: 11/10/99				
PTMW-2	2		PTMW-2				
Discharg	ge 65.00 U.S.gal/min		Distance from the	e pumping well 12.00 f	t		
Static wa	ater level: 0.00 ft below datum						
	Pumping test duration	Water level	Drav	wdown	Corrected		
					drawdown		
	[min]	[ft]		[ft]	[ft]		
2	0.05	0.03		0.03	0.03		
3	0.10	0.06		0.06	0.06		
4	0.15	0.09		0.09	0.09		
5	0.20	0.12		0.12	0.12		
6	0.25	0.14		0.14	0.14		
7	0.30	0.16		0.16	0.16		
8	0.35	0.18		0.18	0.18		
10	0.40	0.20		0.20	0.20		
11	0.45	0.22		0.22	0.22		
12	0.50	0.25		0.25	0.25		
13	0.60	0.37		0.37	0.37		
14	0.65	0.42		0.42	0.42		
15	0.70	0.48		0.48	0.48		
16	0.75	0.53		0.53	0.53		
17	0.80	0.58		0.58	0.58		
18	0.85	0.63		0.63	0.63		
19	0.90	0.69		0.69	0.69		
20	0.95	0.76		0.76	0.76		
21	1.00	0.82		0.82	0.82		
22	1.05	0.88		0.88	0.87		
23	1.10	0.94		0.94	0.93		
25	1.15	0.99		0.99	0.98		
26	1.20	1.05		1.05	1.04		
27	1.30	1.10		1.10	1.09		
28	1.35	1.19		1.19	1.14		
29	1.40	1.23		1.23	1.22		
30	1.45	1.27		1.27	1.26		
31	1.50	1.30		1.30	1.29		
32	1.55	1.33		1.33	1.32		
33	1.60	1.38		1.38	1.37		
34	1.65	1.42		1.42	1.41		
36	1./0	1.47		1.4/	1.45		
37	1.75	1.51		1.51	1.49		
38	1.85	1.58		1.58	1.55		
39	1.90	1.61		1.61	1.59		
40	1.95	1.65		1.65	1.63		
41	2.00	1.67		1.67	1.65		
42	2.05	1.70		1.70	1.68		
43	2.10	1.72		1.72	1.70		
44	2.15	1.74		1.74	1.72		
45	2.20	1.75		1.75	1.73		
40	2.25	1.77		1.77	1.75		
47	2.30	1.78		1.78	1.76		
49	2.35	1.01		1.87	1.79		
50	2.40	1.07		1.07	1.00		
Dvirka and Bartilucci		Pumping test analysis		Date: 06.01.2000 Page 3			
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330 Crossways Park Drive Woodbury N.Y. 11797		Sways Park Drive         Distance-Time-Drawdown-method           I.Y. 11797         after COOPER & JACOB		Project: FRANKLIN CLEANERS			
ph.(516)36	4-9890	Unconfined aquifer	Evaluated by: WM		M		
Pumping	Test No. 2		Test conducted	on: 11/10/99			
PTMW-2	2		PTMW-2				
Discharg	ge 65.00 U.S.gal/min		Distance from th	e pumping well 12.00 ft			
Static wa	ater level: 0.00 ft below datum						
	Pumping test duration	Water level	Dra	awdown	Corrected drawdown		
	[min]	[ft]		[ft]	[ft]		
51	2.50	2.00		2.00	1.97		
52	2.55	2.08		2.08	2.05		
54	2.00	2.15		2.15	2.12		
55	2.70	2.21		2.21	2.18		
56	2.75	2.33		2.33	2.24		
57	2.80	2.38		2.38	2.34		
58	2.85	2.43		2.43	2.39		
59	2.90	2.47		2.47	2.43		
60	2.95	2.50		2.50	2.46		
01	3.00	2.53		2.53	2.49		
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Transmissivity [ft²/min]: 1.26 x 10<sup>0</sup>

Hydraulic conductivity [ft/min]: 1.76 x 10<sup>-2</sup>

330 Crossways Park Drive worktay, NY, 1797 pt.(519)54-8890         Time-Drawdown-method after Quiconfined aquifer         Priject: FRANKLIN CLEANERS Evaluated by: WM           Pumping Test No. 2         Test conducted on: 11/10/99         Evaluated by: WM           PTMW-3         PTMW-3         PTMW-3           Distance from the pumping well 50.00 ft         Static water level: 0.00 ft below datum         Distance from the pumping well 50.00 ft           Static water level: 0.00 ft below datum         [ft]         [ft]         [ft]         [ft]           2         0.05         0.01         0.01         0.01           3         0.10         0.00         0.00         0.02           4         0.15         0.01         0.01         0.01           3         0.10         0.00         0.00         0.02           6         0.25         0.02         0.02         0.02           7         0.30         0.03         0.03         0.03           8         0.35         0.04         0.04         0.04           10         0.45         0.05         0.05         0.05           11         0.50         0.06         0.07         1.1         1.1           13         0.66         0.10         0.17	Dvirka and Bartilucci		Pumping test analysis		Date: 06.01.20	00 Page 2	
ph(\$15)836+880         Unconfined aquifer         Evaluated by: WM           Pumping Test No. 2         Test conducted on: 11/10/99           PTMW-3         Discharge 65.00 U.S.galmin         Distance from the pumping well 50.00 ft           Static water level: 0.00 ft below datum         Test conducted on: 11/10/99         Correct           Pumping test duration         Water level         Drawdown         Correct           gram         [ft]         [ft]         [ft]         [ft]           2         0.05         0.01         0.01         3           4         0.15         0.01         0.01         0.01           5         0.20         0.02         0.02         0.02           7         0.30         0.03         0.03         0.03           9         0.40         0.04         0.04         0.04           9         0.40         0.04         0.04         0.04           10         0.45         0.07         0.07         1.1           11         0.50         0.03         0.03         1.1           13         0.60         0.08         0.08         1.1           14         0.65         0.12         0.12         1.12	330 Crossways Park Drive		Time-Drawdown-meth	Time-Drawdown-method after COOPER & JACOB		Project: FRANKLIN CLEANERS	
Pumping Test No. 2         Test conducted on: 11/10/99           PTMW-3         Distance from the pumping well 50.00 f.           Distance from the pumping well 50.00 f.         Distance from the pumping well 50.00 f.           Static water level: 0.00 ft below datum         Distance from the pumping well 50.00 f.           Static water level: 0.00 ft below datum         Distance from the pumping well 50.00 f.           Imping test duration         Water level         Drawdown         Correct           Imping test duration         Water level         Drawdown         Correct           3         0.10         0.001         0.01         Correct           4         0.15         0.011         0.01         0.01           5         0.20         0.02         0.02         0.02           7         0.30         0.03         0.03         0.03           9         0.40         0.04         0.04         0.04           9         0.40         0.04         0.04         0.04           9         0.40         0.04         0.04         0.04           9         0.40         0.04         0.04         0.04           9         0.40         0.04         0.04         0.04           10	ph.(516)364	4-9890	Unconfined aquifer	Evaluated by: WM		VM	
PTMW-3         PTMW-3           Discharge 65.00 U.S.galmin         Distance from the pumping well 50.00 ft           Static water level: 0.00 ft below datum         Usance from the pumping well 50.00 ft           Static water level: 0.00 ft below datum         Usance from the pumping well 50.00 ft           generating the staturation         Water level         Drawdown         Correct drawdown           generating the staturation         Water level         Drawdown         Correct drawdown           generating the staturation         Water level         Drawdown         Correct drawdown           generating the staturation         (fi)         (fi)         (fi)         (fi)           generating the staturation         (fi)         (fi)         (fi)         (fi)           generating the staturation         0.05         0.001         0.001         (fi)           generating the staturation         0.03         0.03         0.03         (fi)           generating the staturation         0.04         0.04         0.04         (fi)           generating the staturation         0.05         0.06         0.06         (fi)           generating the staturation         0.05         0.06         0.06         (fi)           geneatin staturation         0.05 <td< td=""><td>Pumping</td><td>Test No. 2</td><td></td><td>Test conducted</td><td>on: 11/10/99</td><td></td></td<>	Pumping	Test No. 2		Test conducted	on: 11/10/99		
Distance from the pumping well 50.00 ft           State         Pumping test duration         Water level         Drawdown         Correct drawdo           [min]         [ft]         [ft]         [ft]         [ft]         [ft]           2         0.05         0.01         0.01         [ft]         [ft]         [ft]           3         0.10         0.00         0.00         [ft]         [ft]         [ft]           4         0.15         0.01         0.01         0.01         [ft]         [ft]           5         0.20         0.02         0.02         [ft]         [ft]         [ft]           6         0.25         0.02         0.02         [ft]         [ft]         [ft]           7         0.30         0.03         0.03         [ft]         [ft]         [ft]           8         0.35         0.04         0.04         [ft]         [ft]         [ft]           10         0.46         0.05         [ft]         [ft]         [ft]         [ft]           11         0.50         0.06         0.06         [ft]         [ft]         [ft]           12         0.55         0.17         0.17         [ft]	PTMW-3			PTMW-3			
Static water level:         Pumping test duration         Water level         Drawdown         Correct drawdo           [min]         [ft]	Discharg	e 65.00 U.S.gal/min		Distance from th	ne pumping well 50.00	ft	
Pumping test duration         Water level         Drawdown         Correct drawdo           [min]         [ft]         [ft] <td>Static wa</td> <td>ter level: 0.00 ft below datum</td> <td></td> <td></td> <td></td> <td></td>	Static wa	ter level: 0.00 ft below datum					
Imin         (f)         (f) </td <td></td> <td>Pumping test duration</td> <td>Water level</td> <td>Dra</td> <td>awdown</td> <td>Corrected</td>		Pumping test duration	Water level	Dra	awdown	Corrected	
Imin         Iff         Iff <thiff< th=""> <thiff< th=""></thiff<></thiff<>						drawdown	
2         0.05         0.01         0.01           3         0.10         0.00         0.00           4         0.15         0.01         0.01           5         0.20         0.02         0.02           6         0.25         0.02         0.02           7         0.30         0.03         0.03           8         0.35         0.04         0.04           9         0.40         0.04         0.04           10         0.45         0.05         0.05           11         0.50         0.06         0.06           12         0.55         0.07         0.07           13         0.60         0.08         0.08           14         0.65         0.10         0.10           15         0.12         0.12         1.12           16         0.75         0.13         0.13           17         0.80         0.15         0.15           18         0.85         0.17         0.17           19         0.90         0.18         0.22           22         1.05         0.23         0.23           23         1.10		[min]	[ft]		[ft]	[ft]	
3         0.10         0.00         0.00           4         0.15         0.01         0.01           5         0.20         0.02         0.02           6         0.25         0.02         0.02           7         0.30         0.03         0.03           8         0.35         0.04         0.04           9         0.40         0.04         0.04           10         0.45         0.05         0.06           11         0.50         0.06         0.06           12         0.55         0.07         0.07           13         0.60         0.08         0.08           14         0.65         0.10         0.10           15         0.70         0.12         0.12           16         0.75         0.13         0.13           17         0.80         0.15         0.16           18         0.85         0.17         0.17           19         0.90         0.18         0.18           20         0.95         0.20         0.22           21         1.00         0.25         0.28           22         1.05	2	0.05	0.01		0.01	0.01	
4 $0.15$ $0.01$ $0.01$ 5 $0.20$ $0.02$ $0.02$ 6 $0.25$ $0.02$ $0.02$ 7 $0.30$ $0.03$ $0.03$ 8 $0.35$ $0.04$ $0.04$ 9 $0.40$ $0.04$ $0.04$ 10 $0.45$ $0.05$ $0.06$ 11 $0.50$ $0.06$ $0.06$ 12 $0.55$ $0.07$ $0.07$ 13 $0.60$ $0.08$ $0.08$ 14 $0.65$ $0.10$ $0.10$ 15 $0.70$ $0.12$ $0.12$ 16 $0.75$ $0.13$ $0.13$ 17 $0.80$ $0.15$ $0.18$ 20 $0.95$ $0.20$ $0.20$ 21 $1.00$ $0.22$ $0.22$ 22 $1.05$ $0.23$ $0.23$ 23 $1.10$ $0.25$ $0.26$ 24 $1.15$ <td>3</td> <td>0.10</td> <td>0.00</td> <td></td> <td>0.00</td> <td>0.00</td>	3	0.10	0.00		0.00	0.00	
5 $0.20$ $0.02$ $0.02$ 6 $0.25$ $0.02$ $0.02$ 7 $0.30$ $0.03$ $0.03$ 8 $0.35$ $0.04$ $0.04$ 9 $0.40$ $0.04$ $0.04$ 10 $0.45$ $0.06$ $0.06$ 11 $0.50$ $0.06$ $0.06$ 12 $0.55$ $0.07$ $0.07$ 13 $0.60$ $0.08$ $0.08$ 14 $0.65$ $0.10$ $0.10$ 15 $0.70$ $0.12$ $0.12$ 16 $0.75$ $0.13$ $0.13$ 17 $0.80$ $0.15$ $0.15$ 18 $0.85$ $0.17$ $0.17$ 19 $0.90$ $0.18$ $0.18$ 20 $0.95$ $0.20$ $0.22$ 21 $1.05$ $0.23$ $0.23$ 23 $1.10$ $0.25$ $0.25$ 24 $1.15$ <td>4</td> <td>0.15</td> <td>0.01</td> <td></td> <td>0.01</td> <td>0.01</td>	4	0.15	0.01		0.01	0.01	
6 $0.25$ $0.02$ $0.02$ 7 $0.30$ $0.03$ $0.03$ 8 $0.35$ $0.04$ $0.04$ 9 $0.40$ $0.04$ $0.04$ 10 $0.455$ $0.05$ $0.06$ 11 $0.50$ $0.06$ $0.06$ 12 $0.55$ $0.07$ $0.07$ 13 $0.60$ $0.08$ $0.08$ 14 $0.65$ $0.10$ $0.10$ 15 $0.70$ $0.12$ $0.12$ 16 $0.75$ $0.13$ $0.15$ 17 $0.80$ $0.15$ $0.15$ 18 $0.85$ $0.17$ $0.17$ 19 $0.90$ $0.18$ $0.18$ 20 $0.95$ $0.20$ $0.20$ 21 $1.00$ $0.22$ $0.22$ 22 $1.05$ $0.25$ $0.25$ 23 $1.10$ $0.25$ $0.25$ 24 $1.15$ <	5	0.20	0.02		0.02	0.02	
i       0.03       0.03       0.03         8       0.35       0.04       0.04         9       0.40       0.04       0.04         10       0.45       0.05       0.05         11       0.50       0.06       0.06         12       0.55       0.07       0.07         13       0.60       0.08       0.08         14       0.65       0.10       0.10         15       0.70       0.12       0.12         16       0.75       0.13       0.13         17       0.80       0.15       0.15         18       0.85       0.17       0.17         19       0.90       0.18       0.18         20       0.95       0.20       0.20         21       1.00       0.22       0.23         22       1.05       0.23       0.23         23       1.10       0.25       0.26         24       1.15       0.28       0.28         25       1.20       0.30       0.30         26       1.25       0.32       0.32         27       1.30       0.34       0.43 <td>6</td> <td>0.25</td> <td>0.02</td> <td></td> <td>0.02</td> <td>0.02</td>	6	0.25	0.02		0.02	0.02	
0 $0.33$ $0.04$ $0.04$ 9 $0.40$ $0.04$ $0.04$ 10 $0.45$ $0.06$ $0.06$ 11 $0.50$ $0.06$ $0.06$ 12 $0.55$ $0.07$ $0.07$ 13 $0.60$ $0.08$ $0.08$ 14 $0.65$ $0.10$ $0.10$ 15 $0.70$ $0.12$ $0.13$ 16 $0.75$ $0.13$ $0.13$ 17 $0.80$ $0.15$ $0.15$ 18 $0.85$ $0.17$ $0.17$ 19 $0.90$ $0.18$ $0.18$ 20 $0.95$ $0.20$ $0.22$ 21 $1.00$ $0.23$ $0.23$ 22 $1.05$ $0.23$ $0.23$ 23 $1.10$ $0.25$ $0.25$ 24 $1.15$ $0.28$ $0.28$ 25 $1.20$ $0.30$ $0.30$ 26 $1.2$	7	0.30	0.03		0.03	0.03	
3 $0.04$ $0.04$ $0.04$ 10 $0.45$ $0.05$ $0.05$ 11 $0.50$ $0.06$ $0.06$ 12 $0.55$ $0.07$ $0.07$ 13 $0.60$ $0.08$ $0.08$ 14 $0.65$ $0.10$ $0.10$ 15 $0.70$ $0.12$ $0.12$ 16 $0.75$ $0.13$ $0.13$ 17 $0.80$ $0.15$ $0.15$ 18 $0.85$ $0.17$ $0.17$ 19 $0.90$ $0.18$ $0.18$ 20 $0.955$ $0.20$ $0.20$ 21 $1.00$ $0.22$ $0.22$ 22 $1.05$ $0.23$ $0.23$ 23 $1.10$ $0.25$ $0.28$ 24 $1.15$ $0.28$ $0.28$ 25 $1.20$ $0.30$ $0.30$ 26 $1.25$ $0.32$ $0.32$ 27 $1$	8	0.35	0.04		0.04	0.04	
11 $0.03$ $0.03$ $0.03$ $11$ $0.50$ $0.06$ $0.06$ $12$ $0.55$ $0.07$ $0.07$ $13$ $0.60$ $0.08$ $0.08$ $14$ $0.65$ $0.10$ $0.10$ $15$ $0.70$ $0.12$ $0.12$ $16$ $0.75$ $0.13$ $0.13$ $17$ $0.80$ $0.15$ $0.17$ $18$ $0.85$ $0.17$ $0.17$ $19$ $0.90$ $0.18$ $0.18$ $20$ $0.95$ $0.20$ $0.20$ $21$ $1.00$ $0.22$ $0.23$ $22$ $1.05$ $0.23$ $0.23$ $23$ $1.10$ $0.25$ $0.25$ $24$ $1.15$ $0.28$ $0.28$ $25$ $1.20$ $0.30$ $0.30$ $26$ $1.25$ $0.32$ $0.32$ $27$ $1.30$ $0.34$ $0.34$ $28$ $1.35$ $0.36$ $0.36$ $30$ <td< td=""><td>10</td><td>0.40</td><td>0.04</td><td></td><td>0.04</td><td>0.04</td></td<>	10	0.40	0.04		0.04	0.04	
12 $0.55$ $0.07$ $0.07$ 13 $0.60$ $0.08$ $0.08$ 14 $0.65$ $0.10$ $0.10$ 15 $0.70$ $0.12$ $0.12$ 16 $0.75$ $0.13$ $0.13$ 17 $0.80$ $0.15$ $0.15$ 18 $0.85$ $0.17$ $0.17$ 19 $0.90$ $0.18$ $0.18$ 20 $0.95$ $0.20$ $0.20$ 21 $1.00$ $0.22$ $0.22$ 22 $1.05$ $0.23$ $0.23$ 23 $1.10$ $0.25$ $0.25$ 24 $1.15$ $0.28$ $0.28$ 25 $1.20$ $0.30$ $0.30$ 26 $1.25$ $0.32$ $0.32$ 27 $1.30$ $0.34$ $0.34$ 28 $1.35$ $0.36$ $0.38$ 30 $1.45$ $0.39$ $0.39$ 31 $1.5$	11	0.50	0.05		0.05	0.05	
13 $0.60$ $0.08$ $0.08$ 14 $0.65$ $0.10$ $0.10$ 15 $0.70$ $0.12$ $0.12$ 16 $0.75$ $0.13$ $0.13$ 17 $0.80$ $0.15$ $0.15$ 18 $0.85$ $0.17$ $0.17$ 19 $0.90$ $0.18$ $0.18$ 20 $0.95$ $0.20$ $0.20$ 21 $1.00$ $0.22$ $0.22$ 22 $1.05$ $0.23$ $0.23$ 23 $1.10$ $0.25$ $0.25$ 24 $1.15$ $0.28$ $0.28$ 25 $1.20$ $0.30$ $0.30$ 26 $1.25$ $0.32$ $0.32$ 27 $1.30$ $0.34$ $0.34$ 28 $1.35$ $0.36$ $0.36$ 29 $1.40$ $0.38$ $0.33$ 30 $1.45$ $0.39$ $0.39$ 33 $1.6$	12	0.55	0.07		0.00	0.00	
14 $0.65$ $0.10$ $0.10$ 15 $0.70$ $0.12$ $0.12$ 16 $0.75$ $0.13$ $0.13$ 17 $0.80$ $0.15$ $0.15$ 18 $0.95$ $0.17$ $0.17$ 19 $0.90$ $0.18$ $0.18$ 20 $0.95$ $0.20$ $0.20$ 21 $1.00$ $0.22$ $0.22$ 22 $1.05$ $0.23$ $0.23$ 23 $1.10$ $0.25$ $0.25$ 24 $1.15$ $0.28$ $0.28$ 25 $1.20$ $0.30$ $0.30$ 26 $1.25$ $0.32$ $0.32$ 27 $1.30$ $0.34$ $0.34$ 28 $1.35$ $0.36$ $0.38$ 30 $1.45$ $0.39$ $0.39$ 31 $1.50$ $0.41$ $0.41$ 32 $1.55$ $0.43$ $0.43$ 33 $1.60$ $0.45$ $0.45$ 34 $1.65$ $0.56$	13	0.60	0.08		0.08	0.08	
15 $0.70$ $0.12$ $0.12$ $0.12$ $16$ $0.75$ $0.13$ $0.13$ $17$ $0.80$ $0.15$ $0.13$ $18$ $0.85$ $0.17$ $0.17$ $19$ $0.90$ $0.18$ $0.18$ $20$ $0.95$ $0.20$ $0.20$ $21$ $1.00$ $0.22$ $0.22$ $22$ $1.05$ $0.23$ $0.23$ $23$ $1.10$ $0.25$ $0.25$ $24$ $1.15$ $0.28$ $0.28$ $25$ $1.20$ $0.30$ $0.30$ $26$ $1.25$ $0.32$ $0.32$ $27$ $1.30$ $0.34$ $0.34$ $28$ $1.35$ $0.36$ $0.36$ $29$ $1.40$ $0.38$ $0.38$ $30$ $1.45$ $0.39$ $0.39$ $31$ $1.50$ $0.41$ $0.41$ $32$ $1.55$ $0.43$ $0.43$ $33$ $1.60$ $0.45$ $0.45$ $34$ $1.65$ $0.46$ $0.46$ $35$ $1.70$ $0.48$ $0.48$ $36$ $1.75$ $0.50$ $0.50$ $37$ $1.80$ $0.51$ $0.51$ $38$ $1.85$ $0.53$ $0.53$ $41$ $2.00$ $0.58$ $0.56$ $42$ $2.05$ $0.60$ $0.60$ $44$ $2.15$ $0.62$ $0.62$	14	0.65	0.10		0.10	0.10	
16 $0.75$ $0.13$ $0.13$ $17$ $0.80$ $0.15$ $0.15$ $18$ $0.85$ $0.17$ $0.17$ $19$ $0.90$ $0.18$ $0.18$ $20$ $0.95$ $0.20$ $0.20$ $21$ $1.00$ $0.22$ $0.22$ $22$ $1.05$ $0.23$ $0.23$ $23$ $1.10$ $0.25$ $0.26$ $24$ $1.15$ $0.28$ $0.28$ $25$ $1.20$ $0.30$ $0.30$ $26$ $1.25$ $0.32$ $0.32$ $27$ $1.30$ $0.34$ $0.34$ $28$ $1.35$ $0.36$ $0.36$ $29$ $1.40$ $0.38$ $0.38$ $30$ $1.45$ $0.39$ $0.39$ $31$ $1.50$ $0.41$ $0.41$ $32$ $1.55$ $0.43$ $0.43$ $34$ $1.65$ $0.46$ $0.46$ $34$ $1.65$ $0.56$ $0.56$ $37$ <td< td=""><td>15</td><td>0.70</td><td>0.12</td><td></td><td>0.12</td><td>0.12</td></td<>	15	0.70	0.12		0.12	0.12	
17 $0.80$ $0.15$ $0.15$ 18 $0.85$ $0.17$ $0.17$ 19 $0.90$ $0.18$ $0.18$ 20 $0.95$ $0.20$ $0.20$ 21 $1.00$ $0.22$ $0.22$ 22 $1.05$ $0.23$ $0.23$ 23 $1.10$ $0.25$ $0.25$ 24 $1.15$ $0.28$ $0.28$ 25 $1.20$ $0.30$ $0.30$ 26 $1.25$ $0.32$ $0.32$ 27 $1.30$ $0.34$ $0.34$ 28 $1.35$ $0.36$ $0.36$ 29 $1.40$ $0.38$ $0.38$ 30 $1.45$ $0.39$ $0.39$ 31 $1.50$ $0.41$ $0.41$ 32 $1.55$ $0.43$ $0.43$ 33 $1.60$ $0.45$ $0.45$ 34 $1.65$ $0.46$ $0.46$ 35 $1.70$ $0.48$ $0.48$ 36 $1.75$ $0.50$ $0.50$ 37 $1.80$ $0.51$ $0.51$ 38 $1.85$ $0.53$ $0.55$ 40 $1.95$ $0.56$ $0.56$ 41 $2.00$ $0.58$ $0.58$ 42 $2.05$ $0.60$ $0.60$	16	0.75	0.13		0.13	0.13	
18 $0.85$ $0.17$ $0.17$ 19 $0.90$ $0.18$ $0.18$ 20 $0.95$ $0.20$ $0.20$ 21 $1.00$ $0.22$ $0.22$ 22 $1.05$ $0.23$ $0.23$ 23 $1.10$ $0.25$ $0.25$ 24 $1.15$ $0.28$ $0.28$ 25 $1.20$ $0.30$ $0.30$ 26 $1.25$ $0.32$ $0.32$ 27 $1.30$ $0.34$ $0.34$ 28 $1.35$ $0.36$ $0.36$ 29 $1.40$ $0.38$ $0.38$ 30 $1.45$ $0.39$ $0.39$ 31 $1.50$ $0.41$ $0.41$ 32 $1.55$ $0.43$ $0.43$ 33 $1.60$ $0.45$ $0.45$ 34 $1.65$ $0.46$ $0.46$ 35 $1.70$ $0.48$ $0.48$ 36 $1.75$ $0.50$ $0.50$ 37 $1.80$ $0.51$	17	0.80	0.15		0.15	0.15	
19 $0.90$ $0.18$ $0.18$ 20 $0.95$ $0.20$ $0.20$ 21 $1.00$ $0.22$ $0.22$ 22 $1.05$ $0.23$ $0.23$ 23 $1.10$ $0.25$ $0.25$ 24 $1.15$ $0.28$ $0.28$ 25 $1.20$ $0.30$ $0.30$ 26 $1.25$ $0.32$ $0.32$ 27 $1.30$ $0.34$ $0.34$ 28 $1.35$ $0.36$ $0.36$ 29 $1.40$ $0.38$ $0.38$ 30 $1.45$ $0.39$ $0.39$ 31 $1.50$ $0.41$ $0.41$ 32 $1.55$ $0.43$ $0.43$ 33 $1.60$ $0.45$ $0.45$ 34 $1.65$ $0.46$ $0.46$ 35 $1.70$ $0.48$ $0.48$ 36 $1.75$ $0.50$ $0.50$ 37 $1.80$ $0.51$ $0.51$ 38 $1.85$ $0.53$ $0.53$ 40 $1.95$ $0.56$ $0.56$ 41 $2.00$ $0.58$ $0.58$ 42 $2.05$ $0.60$ $0.60$	18	0.85	0.17		0.17	0.17	
21 $0.93$ $0.20$ $0.20$ 21 $1.00$ $0.22$ $0.22$ 22 $1.05$ $0.23$ $0.23$ 23 $1.10$ $0.25$ $0.25$ 24 $1.15$ $0.28$ $0.28$ 25 $1.20$ $0.30$ $0.30$ 26 $1.25$ $0.32$ $0.32$ 27 $1.30$ $0.34$ $0.34$ 28 $1.35$ $0.36$ $0.36$ 29 $1.40$ $0.38$ $0.38$ 30 $1.45$ $0.39$ $0.39$ 31 $1.50$ $0.41$ $0.41$ 32 $1.55$ $0.43$ $0.43$ 33 $1.60$ $0.45$ $0.45$ 34 $1.65$ $0.46$ $0.46$ 35 $1.70$ $0.48$ $0.48$ 36 $1.75$ $0.50$ $0.50$ 37 $1.80$ $0.51$ $0.51$ 39 $1.90$ $0.55$ $0.55$ 40 $1.95$ $0.56$	19	0.90	0.18		0.18	0.18	
1100 $0.22$ $0.22$ $22$ $1.05$ $0.23$ $0.23$ $23$ $1.10$ $0.25$ $0.25$ $24$ $1.15$ $0.28$ $0.28$ $25$ $1.20$ $0.30$ $0.30$ $26$ $1.25$ $0.32$ $0.32$ $27$ $1.30$ $0.34$ $0.34$ $28$ $1.35$ $0.36$ $0.36$ $29$ $1.40$ $0.38$ $0.38$ $30$ $1.45$ $0.39$ $0.39$ $31$ $1.50$ $0.41$ $0.41$ $32$ $1.55$ $0.43$ $0.43$ $33$ $1.60$ $0.45$ $0.45$ $34$ $1.65$ $0.46$ $0.46$ $35$ $1.70$ $0.48$ $0.48$ $36$ $1.75$ $0.50$ $0.50$ $37$ $1.80$ $0.51$ $0.51$ $38$ $1.85$ $0.53$ $0.53$ $39$ $1.90$ $0.56$ $0.56$ $41$ $2.00$ <	20	1.00	0.20		0.20	0.20	
100 $0.25$ $0.25$ $23$ $1.10$ $0.25$ $0.25$ $24$ $1.15$ $0.28$ $0.28$ $25$ $1.20$ $0.30$ $0.30$ $26$ $1.25$ $0.32$ $0.32$ $27$ $1.30$ $0.34$ $0.34$ $28$ $1.35$ $0.36$ $0.36$ $29$ $1.40$ $0.38$ $0.38$ $30$ $1.45$ $0.39$ $0.39$ $31$ $1.50$ $0.41$ $0.41$ $32$ $1.55$ $0.43$ $0.43$ $33$ $1.60$ $0.45$ $0.45$ $34$ $1.65$ $0.46$ $0.46$ $35$ $1.70$ $0.48$ $0.48$ $36$ $1.75$ $0.50$ $0.50$ $37$ $1.80$ $0.51$ $0.51$ $38$ $1.85$ $0.53$ $0.53$ $39$ $1.90$ $0.55$ $0.56$ $41$	22	1.05	0.22		0.22	0.22	
24 $1.15$ $0.28$ $0.28$ $25$ $1.20$ $0.30$ $0.30$ $26$ $1.25$ $0.32$ $0.32$ $27$ $1.30$ $0.34$ $0.34$ $28$ $1.35$ $0.36$ $0.36$ $29$ $1.40$ $0.38$ $0.38$ $30$ $1.45$ $0.39$ $0.39$ $31$ $1.50$ $0.41$ $0.41$ $32$ $1.55$ $0.43$ $0.43$ $33$ $1.60$ $0.45$ $0.45$ $34$ $1.65$ $0.46$ $0.46$ $35$ $1.70$ $0.48$ $0.48$ $36$ $1.75$ $0.50$ $0.50$ $37$ $1.80$ $0.51$ $0.51$ $38$ $1.85$ $0.53$ $0.53$ $39$ $1.90$ $0.55$ $0.55$ $40$ $1.95$ $0.56$ $0.56$ $41$ $2.00$ $0.58$ $0.58$ $42$ $2.05$ $0.60$ $0.60$ $43$ $2.10$ $0.61$ $0.61$	23	1.10	0.25		0.25	0.25	
251.200.300.30 $26$ 1.250.320.32 $27$ 1.300.340.34 $28$ 1.350.360.36 $29$ 1.400.380.39 $30$ 1.450.390.39 $31$ 1.500.410.41 $32$ 1.550.430.43 $33$ 1.600.450.45 $34$ 1.650.460.46 $35$ 1.700.480.48 $36$ 1.750.500.50 $37$ 1.800.510.51 $38$ 1.850.530.53 $39$ 1.900.550.55 $40$ 1.950.560.56 $41$ 2.000.580.58 $42$ 2.050.600.60 $44$ 2.150.620.62	24	1.15	0.28		0.28	0.28	
26 $1.25$ $0.32$ $0.32$ $27$ $1.30$ $0.34$ $0.34$ $28$ $1.35$ $0.36$ $0.36$ $29$ $1.40$ $0.38$ $0.38$ $30$ $1.45$ $0.39$ $0.39$ $31$ $1.50$ $0.41$ $0.41$ $32$ $1.55$ $0.43$ $0.43$ $33$ $1.60$ $0.45$ $0.45$ $34$ $1.65$ $0.46$ $0.46$ $35$ $1.70$ $0.48$ $0.48$ $36$ $1.75$ $0.50$ $0.50$ $37$ $1.80$ $0.51$ $0.51$ $38$ $1.85$ $0.53$ $0.53$ $39$ $1.90$ $0.55$ $0.55$ $40$ $1.95$ $0.56$ $0.56$ $41$ $2.00$ $0.58$ $0.58$ $42$ $2.05$ $0.60$ $0.60$ $44$ $2.15$ $0.62$ $0.62$	25	1.20	0.30		0.30	0.30	
271.300.340.34 $28$ 1.350.360.36 $29$ 1.400.380.38 $30$ 1.450.390.39 $31$ 1.500.410.41 $32$ 1.550.430.43 $33$ 1.600.450.45 $34$ 1.650.460.46 $35$ 1.700.480.48 $36$ 1.750.500.50 $37$ 1.800.510.51 $38$ 1.850.530.55 $40$ 1.950.560.56 $41$ 2.000.580.58 $42$ 2.050.600.60 $43$ 2.100.620.62	26	1.25	0.32		0.32	0.32	
28 $1.35$ $0.36$ $0.36$ $29$ $1.40$ $0.38$ $0.38$ $30$ $1.45$ $0.39$ $0.39$ $31$ $1.50$ $0.41$ $0.41$ $32$ $1.55$ $0.43$ $0.43$ $33$ $1.60$ $0.45$ $0.45$ $34$ $1.65$ $0.46$ $0.46$ $35$ $1.70$ $0.48$ $0.48$ $36$ $1.75$ $0.50$ $0.50$ $37$ $1.80$ $0.51$ $0.51$ $38$ $1.85$ $0.53$ $0.53$ $39$ $1.90$ $0.55$ $0.55$ $40$ $1.95$ $0.56$ $0.56$ $41$ $2.00$ $0.58$ $0.58$ $42$ $2.05$ $0.60$ $0.60$ $43$ $2.10$ $0.61$ $0.61$	27	1.30	0.34		0.34	0.34	
291.400.380.38301.450.390.39311.500.410.41321.550.430.43331.600.450.45341.650.460.46351.700.480.48361.750.500.50371.800.510.51381.850.530.53391.900.550.55401.950.560.56412.000.580.58422.050.600.60432.100.610.61	28	1.35	0.36		0.36	0.36	
31 $1.45$ $0.39$ $0.39$ $31$ $1.50$ $0.41$ $0.41$ $32$ $1.55$ $0.43$ $0.43$ $33$ $1.60$ $0.45$ $0.45$ $34$ $1.65$ $0.46$ $0.46$ $35$ $1.70$ $0.48$ $0.48$ $36$ $1.75$ $0.50$ $0.50$ $37$ $1.80$ $0.51$ $0.51$ $38$ $1.85$ $0.53$ $0.53$ $39$ $1.90$ $0.55$ $0.55$ $40$ $1.95$ $0.56$ $0.56$ $41$ $2.00$ $0.58$ $0.58$ $42$ $2.05$ $0.60$ $0.60$ $43$ $2.10$ $0.61$ $0.61$	29	1.40	0.38		0.38	0.38	
32 $1.50$ $0.41$ $0.41$ $32$ $1.55$ $0.43$ $0.43$ $33$ $1.60$ $0.45$ $0.45$ $34$ $1.65$ $0.46$ $0.46$ $35$ $1.70$ $0.48$ $0.48$ $36$ $1.75$ $0.50$ $0.50$ $37$ $1.80$ $0.51$ $0.51$ $38$ $1.85$ $0.53$ $0.53$ $39$ $1.90$ $0.55$ $0.55$ $40$ $1.95$ $0.56$ $0.56$ $41$ $2.00$ $0.58$ $0.58$ $42$ $2.05$ $0.60$ $0.60$ $43$ $2.10$ $0.61$ $0.61$	31	1.45	0.39		0.39	0.39	
33 $1.60$ $0.45$ $0.45$ $34$ $1.65$ $0.46$ $0.46$ $35$ $1.70$ $0.48$ $0.48$ $36$ $1.75$ $0.50$ $0.50$ $37$ $1.80$ $0.51$ $0.51$ $38$ $1.85$ $0.53$ $0.53$ $39$ $1.90$ $0.55$ $0.55$ $40$ $1.95$ $0.56$ $0.56$ $41$ $2.00$ $0.58$ $0.58$ $42$ $2.05$ $0.60$ $0.60$ $43$ $2.10$ $0.61$ $0.62$	32	1.55	0.41		0.41	0.41	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	33	1.60	0.45		0.45	0.45	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	34	1.65	0.46		0.46	0.46	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	35	1.70	0.48		0.48	0.48	
37       1.80       0.51       0.51         38       1.85       0.53       0.53         39       1.90       0.55       0.55         40       1.95       0.56       0.56         41       2.00       0.58       0.58         42       2.05       0.60       0.60         43       2.10       0.61       0.61	36	1.75	0.50		0.50	0.50	
38       1.85       0.53       0.53         39       1.90       0.55       0.55         40       1.95       0.56       0.56         41       2.00       0.58       0.58         42       2.05       0.60       0.60         43       2.10       0.61       0.61	37	1.80	0.51		0.51	0.51	
39         1.90         0.55         0.55           40         1.95         0.56         0.56           41         2.00         0.58         0.58           42         2.05         0.60         0.60           43         2.10         0.61         0.61	38	1.85	0.53		0.53	0.53	
41     2.00     0.56     0.56       42     2.05     0.60     0.60       43     2.10     0.61     0.61	40	1.90	0.55		0.55	0.55	
42         2.05         0.60         0.56           43         2.10         0.61         0.61	41	2.00	0.56		0.56	0.56	
43         2.10         0.61         0.61           44         2.15         0.62         0.62	42	2.05	0.60		0.60	0.58	
44 2.15 0.62 0.62	43	2.10	0.61		0.61	0.61	
0.02 0.02	44	2.15	0.62		0.62	0.62	
45 2.20 0.63 0.63	45	2.20	0.63		0.63	0.63	
46 2.25 0.65 0.65	46	2.25	0.65		0.65	0.65	
47 2.30 0.65 0.65	47	2.30	0.65		0.65	0.65	
<u>48</u> 2.35 0.67 0.67	48	2.35	0.67		0.67	0.67	
<u>49</u> <u>2.40</u> <u>0.68</u> <u>0.68</u> <u>50</u> <u>2.45</u> <u>0.70</u> <u>0.70</u>	49	2.40	0.68		0.68	0.68	

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Dvirka and Bartilucci		Pumping test analysis		Date: 06.01.200	0 Page 3	
330 Crossways Park Drive Woodbury N.Y. 11797		Time-Drawdown-meth COOPER & JACOB	nod after	Project: FRANKLIN CLEANERS		
ph.(516)364	4-9890	Unconfined aquifer		Evaluated by: WM		
Pumping	Test No. 2		Test conducted of	on: 11/10/99		
PTMW-3			PTMW-3			
Discharg	e 65.00 U.S.gal/min		Distance from the	e pumping well 50.00 f	ft	
Static wa	ter level: 0.00 ft below datum					
	Pumping test duration	Water level	Dra	wdown	Corrected	
	[min]	[ft]		[ft]	[ft]	
51	2.50	0.72		0.72	0.72	
52	2.55	0.74		0.74	0.74	
53	2.60	0.76		0.76	0.76	
54	2.65	0.78		0.78	0.78	
55	2.70	0.81		0.81	0.81	
50	2.75	0.82		0.82	0.82	
58	2.80	0.85		0.85	0.84	
59	2.00	0.07		0.89	0.00	
60	2.95	0.91		0.91	0.90	
61	3.00	0.93		0.93	0.92	
62	3.05	0.94		0.94	0.93	
63	3.10	0.96		0.96	0.95	
64	3.15	0.98		0.98	0.97	
65	3.20	0.99		0.99	0.98	
66	3.25	1.00		1.00	0.99	
68	3.30	1.02		1.02	1.01	
69	3.40	1.03		1.05	1.02	
70	3.45	1.05		1.05	1.04	
71	3.50	1.07		1.07	1.06	
72	3.55	1.08		1.08	1.07	
73	3.60	1.09		1.09	1.08	
74	3.65	1.09		1.09	1.08	
75	3.70	1.10		1.10	1.09	
76	3.75	1.12		1.12	1.11	
78	3.80	1.12		1.12	1.11	
79	3.90	1.13		1 13	1.12	
80	3.95	1.13		1.14	1.12	
81	4.00	1.14		1.14	1.13	
	······					



Transmissivity [ft²/min]: 1.27 x 10<sup>0</sup>

Hydraulic conductivity [ft/min]: 1.76 x 10<sup>-2</sup>

Aquifer thickness [ft]: 72.00

Dvirka and Bartilucci		Pumping test analysis		Date: 06.01.2000 Page 2		
330 Cross	ways Park Drive	Distance-Time-Drawdown-method after COOPER & JACOB		Project: FRANKLIN CLEANERS		
ph.(516)364-	9890	Unconfined aquifer		Evaluated by: WM		
Pumping T	Fest No. 2		Test conducted of	on: 11/10/99		
PTMW-3			PTMW-3			
Discharge	65.00 U.S.gal/min		Distance from the	e pumping well 50.00 ft		
Static wate	er level: 0.00 ft below datum		L			
	Pumping test duration	Water level	Dra	wdown	Corrected	
					drawdown	
	[min]	[ft]		[ft]	[ft]	
2	0.05	0.01		0.01	0.01	
3	0.10	0.00		0.00	0.00	
4	0.15	0.01		0.01	0.01	
5	0.20	0.02		0.02	0.02	
6	0.25	0.02		0.02	0.02	
7	0.30	0.03		0.03	0.03	
8	0.35	0.04	+	0.04	0.04	
9	0.40	0.04		0.04	0.04	
10	0.45	0.05		0.05	0.05	
11	0.50	0.06		0.06	0.06	
12	0.55	0.07		0.07	0.07	
13	0.60	0.08		0.08	0.08	
14	0.65	0.10		0.10	0.10	
15	0.70	0.12		0.12	0.12	
16	0.75	0.13		0.13	0.13	
17	0.80	0.15		0.15	0.15	
18	0.85	0.17		0.17	0.17	
19	0.90	0.18		0.18	0.18	
20	0.95	0.20		0.20	0.20	
21	1.00	0.22		0.22	0.22	
22	1.05	0.23		0.23	0.23	
23	1.10	0.25		0.25	0.25	
24	1.15	0.20		0.20	0.20	
25	1.20	0.30		0.30	0.30	
20	1.20	0.32		0.34	0.32	
28	1.30	0.34		0.34	0.34	
29	1.35	0.30		0.38	0.30	
30	1.45	0.30		0.39	0.39	
31	1.50	0.41		0.41	0.41	
32	1.55	0.43		0.43	0.43	
33	1.60	0.45		0.45	0.45	
34	1.65	0.46		0.46	0.46	
35	1.70	0.48		0.48	0.48	
36	1.75	0.50		0.50	0.50	
37	1.80	0.51		0.51	0.51	
38	1.85	0.53		0.53	0.53	
39	1.90	0.55		0.55	0.55	
40	1.95	0.56		0.56	0.56	
41	2.00	0.58		0.58	0.58	
42	2.05	0.60		0.60	0.60	
43	2.10	0.61		0.61	0.61	
44	2.15	0.62		0.62	0.62	
45	2.20	0.63		0.65	0.63	
40	2.25	0.65		0.05	0.05	
4/	2.30	0.65		0.05	0.00	
40	2.30	0.07		0.68	0.67	
49	2.40	0.08		0.00	0.00	

Dvirka and Bartilucci		Pumping test analysis		Date: 06.01.200	0 Page 3		
330 Crossways Park Drive		Distance-Time-Drawd	Distance-Time-Drawdown-method after COOPER & JACOB		Project: FRANKLIN CLEANERS		
ph.(516)36	64-9890	Unconfined aquifer		Evaluated by: WM			
Pumping	Test No. 2		Test conducted	on: 11/10/99			
PTMW-3	3		PTMW-3				
Discharg	ge 65.00 U.S.gal/min		Distance from th	e pumping well 50.00	ft		
Static wa	ater level: 0.00 ft below datum						
	Pumping test duration	Water level	Dra	awdown	Corrected		
					drawdown		
= 4	[min]	[ft]		[ft]	[ft]		
51	2.50	0.72		0.72	0.72		
53	2.55	0.74		0.74	0.74		
54	2.65	0.78		0.78	0.78		
55	2.70	0.81		0.81	0.81		
56	2.75	0.82		0.82	0.82		
57	2.80	0.85		0.85	0.84		
58	2.85	0.87		0.87	0.86		
59	2.90	0.89		0.89	0.88		
61	3.00	0.91		0.91	0.90		
62	3.05	0.94		0.94	0.93		
63	3.10	0.96		0.96	0.95		
64	3.15	0.98		0.98	0.97		
65	3.20	0.99		0.99	0.98		
66	3.25	1.00		1.00	0.99		
68	3.30	1.02		1.02	1.01		
69	3.40	1.05		1.05	1.02		
70	3.45	1.05		1.05	1.04		
71	3.50	1.07		1.07	1.06		
72	3.55	1.08		1.08	1.07		
73	3.60	1.09		1.09	1.08		
75	3.65	1.09		1.09	1.08		
76	3.70	1.10		1.10	1.09		
77	3.80	1.12		1.12	1.11		
78	3.85	1.13		1.13	1.12		
79	3.90	1.13		1.13	1.12		
80	3.95	1.14		1.14	1.13		
81	4.00	1.14		1.14	1.13		
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Transmissivity [ft²/min]: 8.29 x 10<sup>-2</sup>

Hydraulic conductivity [ft/min]: 1.15 x 10<sup>-3</sup>

Dvirka and Bartilucci		Pumping test analysis		Date: 06.01.200	00 Page 2
Woodbury N.Y. 11797		Recovery method after THEIS & JACOB	r	Project: FRANKLIN CLEANERS	
ph.(516)364	-9890	Unconfined aquifer		Evaluated by: V	VM
Pumping	Test No. 2		Test conducted on:	11/10/99	
PTW-1			PTW-1		
Discharge	e 65.00 U.S.gal/min				
Static wa	ter level: 0.00 ft below datum		Pumping test duration	on: 400.00 min	
	Time from	Water level	Resid	ual	Corrected
	end of pumping		drawdo	own	drawdown
	[min]	[ft]	[ft]		[ft]
1	0.10	20.33		20.33	17.46
2	0.15	18.30		18.30	15.97
4	0.20	15.91		15.91	14.15
5	0.30	13.80		13.80	12.48
6	0.35	10.36	-	10.36	11.01
7	0.40	8.97		8.97	9.01
8	0.45	7.78		7.78	7.36
9	0.50	6.74		6.74	6.42
10	0.55	5.85		5.85	5.61
11	0.60	5.09		5.09	4.91
12	0.65	4.43		4.43	4.29
13	0.70	3.86		3.86	3.76
15	0.75	3.38		3.38	3.30
16	0.85	2.97		2.97	2.91
17	0.90	2.02		2.02	2.57
18	0.95	2.06		2.02	2.20
19	1.00	1.84		1.84	1.82



Transmissivity [ft²/min]: 1.16 x 10<sup>0</sup>

Hydraulic conductivity [ft/min]: 1.62 x 10<sup>-2</sup>

Dvirka and Bartilucci		Pumping test analysis		Date: 06.01.200	0 Page 2
330 Crossways Park Drive Woodbury N.Y. 11797		Recovery method afte THEIS & JACOB	r	Project: FRANK	LIN CLEANERS
ph.(516)364	1-9890	Unconfined aquifer	Evaluated by: WM		/M
Pumping	Test No. 2		Test conducted on:	11/10/99	
PTMW-1			PTMW-1		
Discharge	e 65.00 U.S.gal/min		Distance from the p	umping well 27.00 f	t
Static wa	ter level: 0.00 ft below datum		Pumping test duration	on: 500.00 min	
	Time from	Water level	Resid	lual	Corrected
	end of pumping		drawd	own	drawdown
	[min]	[ft]	[ft]		[ft]
2	0.05	4.40			
3	0.05	1.48		1.48	1.46
4	0.15	1.47		1.47	1.45
5	0.20	1.41		1.41	1.42
6	0.25	1.38		1.38	1.36
7	0.30	1.32		1.32	1.31
8	0.35	1.28		1.28	1.27
9	0.40	1.23		1.23	1.22
10	0.45	1.17		1.17	1.16
11	0.50	1.11		1.11	1.11
12	0.55	1.06		1.06	1.06
14	0.65	0.96		1.01	1.01
15	0.70	0.92		0.90	0.95
16	0.75	0.88		0.88	0.87
17	0.80	0.82		0.82	0.82
18	0.85	0.78		0.78	0.77
19	0.90	0.74		0.74	0.74
20	0.95	0.70		0.70	0.70
21	1.00	0.67		0.67	0.66
22	1.05	0.64		0.64	0.64
23	1.10	0.61		0.61	0.60
25	1.13	0.56		0.58	0.58
26	1.25	0.53		0.53	0.50
27	1.30	0.52		0.52	0.51
28	1.35	0.49		0.49	0.49
29	1.40	0.48		0.48	0.48
30	1.45	0.45		0.45	0.45
31	1.50	0.44		0.44	0.44
32	1.55	0.43		0.43	0.43
34	1.60	0.42		0.42	0.42
35	1.70	0.39		0.39	0.40
36	1.75	0.39		0.39	0.39
37	1.80	0.38		0.38	0.38
38	1.85	0.36		0.36	0.36
39	1.90	0.36		0.36	0.36
40	1.95	0.35		0.35	0.35
41	2.00	0.34		0.34	0.34
42	2.05	0.34		0.34	0.34
44	2.10	0.33	-	0.33	0.33
45	2.20	0.32		0.32	0.32
46	2.25	0.31		0.31	0.33
47	2.30	0.31		0.31	0.31
48	2.35	0.31		0.31	0.31
49	2.40	0.29		0.29	0.29
50	2.45	0.29		0.29	0.29

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Dvirka and Bartilucci		Pumping test analysis		Date: 06.01.2000 Page 3			
330 Crossways Park Drive		330 Crossways Park Drive Rec Woodbury N.Y. 11797 THE		Recovery method after THEIS & JACOB	er	Project: FRANK	LIN CLEANERS
oh.(516)364	-9890	Unconfined aquifer		Evaluated by: WM			
Pumping Test No. 2			Test conducted	on: 11/10/99			
PTMW-1			PTMW-1	-			
Discharge	e 65.00 U.S.gal/min		Distance from th	e pumping well 27.00	ft		
Static wat	er level: 0.00 ft below datum		Pumping test du	ration: 500.00 min			
	Time from	Water level	Re	esidual	Corrected		
	end of pumping		dra	wdown	drawdown		
	[min]	[ft]		[ft]	[ft]		
51	2.50	0.29		0.29	0.29		
52	2.55	0.29		0.29	0.29		
53	2.60	0.29		0.29	0.29		
54	2.65	0.26		0.26	0.26		
55	2.70	0.27		0.27	0.27		
56	2.75	0.27		0.27	0.27		
57	2.80	0.27		0.27	0.27		
58	2.85	0.27		0.27	0.27		
59	2.90	0.27		0.27	0.27		
60	2.95	0.26		0.26	0.26		
61	3.00	0.26		0.26	0.26		



Transmissivity [ft²/min]: 6.14 x 10<sup>-1</sup>

Hydraulic conductivity [ft/min]:  $8.53 \times 10^{-3}$ 

Dvirka and Bartilucci		Pumping test analysis		Date: 06.01.2000 Page 2		
330 Crossways Park Drive Woodbury N.Y. 11797		ry N.Y. 11797 Recovery method after THEIS & JACOB		Project: FRANKLIN CLEANERS		
ph.(516)364	-9890	Unconfined aquifer		Evaluated by: WM		
Pumping	Test No. 2		Test conducted of	on: 11/10/99		
PTMW-2			PTMW-2			
Discharge	e 65.00 U.S.gal/min		Distance from the	e pumping well 12.00 ft	1	
Static wat	er level: 0.00 ft below datum		Pumping test dur	ration: 400.00 min		
	Time from	Water level	Re	esidual	Corrected	
	end of pumping		dra	wdown	drawdown	
	[min]	[ft]		[ft]	[ft]	
	0.05	2.07		2.07	2.00	
2	0.05	3.07		2.07	2.87	
4	0.15	2.75		2.75	2.70	
5	0.20	2.56		2.56	2.51	
6	0.25	2.38		2.38	2.34	
7	0.30	2.21		2.21	2.18	
8	0.35	2.04		2.04	2.01	
9	0.40	1.89		1.89	1.87	
10	0.45	1.74		1.74	1.72	
11	0.50	1.60		1.60	1.58	
12	0.55	1.48		1.48	1.46	
13	0.60	1.37		1.37	1.36	
14	0.65	1.27		1.27	1.26	
15	0.70	1.18		1.18	1.17	
17	0.75	1.09		1.09	1.00	
18	0.85	0.95		0.95	0.94	
19	0.90	0.89		0.89	0.88	
20	0.95	0.84		0.84	0.84	
21	1.00	0.79		0.79	0.79	
22	1.05	0.74		0.74	0.74	
23	1.10	0.70		0.70	0.70	
24	1.15	0.67		0.67	0.67	
25	1.20	0.64		0.64	0.64	
26	1.25	0.60		0.60	0.60	
27	1.30	0.58		0.58	0.58	
28	1.35	0.55		0.55	0.55	
30	1.40	0.53		0.53	0.53	
31	1.45	0.51		0.51	0.51	
32	1.55	0.48		0.48	0.48	
33	1.60	0.46		0.46	0.46	
34	1.65	0.45		0.45	0.45	
35	1.70	0.44		0.44	0.44	
36	1.75	0.42		0.42	0.42	
37	1.80	0.41		0.41	0.41	
38	1.85	0.40		0.40	0.40	
39	1.90	0.39		0.39	0.39	
40	1.95	0.38		0.38	0.38	



Transmissivity [ft²/min]: 1.06 x 10<sup>0</sup>

Hydraulic conductivity [ft/min]: 1.48 x 10<sup>-2</sup>

Dvirka and Bartilucci		Bartilucci Pumping test analysis		Date: 13.01.2000 Page 2		
330 Crossways Park Drive		Recovery method after THEIS & JACOB	er	Project: FRANK	LIN CLEANERS	
ph.(516)364-989	0	Unconfined aquifer		Evaluated by: WM		
Pumping Tes	t No. 2		Test conducted on: 11/10/99			
PTMW-3			PTMW-3			
Discharge 65	.00 U.S.gal/min		Distance from the	e pumping well 50.00 f	t	
Static water k	aval: 0.00 ft balaw datum		Pumping toot dur	ation: 500.00 min		
		Water laval		aidual	Corrected	
		vvater level	Re	sidual	Corrected	
		[4]	drav	WOOWN	diawdown	
	lminj	נתן			្រា	
2	0.15	1.51		1.51	1.50	
3	0.20	1.50		1.50	1.49	
4	0.25	1.49		1.49	1.47	
5	0.30	1.46		1.46	1.44	
6	0.35	1.42		1.42	1.41	
7	0.40	1.39		1.39	1.38	
8	0.45	1.34		1.34	1.33	
9	0.50	1.30		1.30	1.29	
10	0.55	1.26		1.26	1.25	
12	0.60	1.21		1.21	1.20	
13	0.05	1.17		1.17	1.10	
14	0.75	1.12		1.12	1.11	
15	0.80	1.03		1.03	1.02	
16	0.85	0.99		0.99	0.98	
17	0.90	0.95		0.95	0.94	
18	0.95	0.91		0.91	0.91	
19	1.00	0.88		0.88	0.87	
20	1.05	0.84		0.84	0.84	
21	1.10	0.81		0.81	0.81	
22	1.15	0.78		0.78	0.77	
23	1.20	0.75	<u></u>	0.75	0.75	
24	1.25	0.72		0.72	0.72	
25	1.30	0.70		0.70	0.70	
20	1.35	0.68		0.68	0.67	
28	1.40	0.02		0.05	0.65	
29	1.50	0.03		0.61	0.63	
30	1.55	0.60		0.60	0.59	
31	1.60	0.58		0.58	0.58	
32	1.65	0.57		0.57	0.56	
33	1.70	0.55		0.55	0.54	
34	1.75	0.53		0.53	0.53	
35	1.80	0.52		0.52	0.52	
30	1.85	0.51		0.51	0.51	
38	1.90	0.49		0.49	0.49	
39	2.00	0.48		0.40	0.48	
40	2.05	0.46		0.46	0.47	
41	2.10	0.45		0.45	0.45	
42	2.15	0.45		0.45	0.45	
43	2.20	0.44		0.44	0.44	
44	2.25	0.43		0.43	0.43	
45	2.30	0.42		0.42	0.42	
46	2.35	0.41		0.41	0.41	
47	2.40	0.41		0.41	0.40	
48	2.45	0.40		0.40	0.40	
49	2.50	0.39		0.39	0.39	
50	2.55	0.39		0.39	0.39	

Dvirka and Bartilucci		Pumping test analysis		Date: 13.01.200	00 Page 3
330 Crossways Park Drive Woodbury N.Y. 11797		Recovery method afte THEIS & JACOB	r	Project: FRAN	LIN CLEANERS
ph.(516)364	1-9890	Unconfined aquifer	nfined aquifer Evalu		VM
Pumping	Test No. 2		Test conducted	on: 11/10/99	
PTMW-3			PTMW-3		
Discharge	e 65.00 U.S.gal/min		Distance from th	e pumping well 50.00	ft
Static wa	ter level: 0.00 ft below datum		Pumping test du	ration: 500.00 min	
	Time from	Water level	Re	esidual	Corrected
	end of pumping		dra	wdown	drawdown
	[min]	[ft]		[ft]	[ft]
51	2.60	0.38		0.38	0.38
52	2.65	0.37		0.37	0.37
53	2.70	0.37		0.37	0.37
55	2.80	0.36		0.36	0.36
56	2.85	0.35		0.35	0.30
57	2.90	0.35		0.35	0.35
58	2.95	0.35		0.35	0.3
59	3.00	0.34		0.34	0.34
			-		
					and the second sec

PUMP TEST 3



₀ PTMW-1 □ PTMW-2

₄ PTMW-3

Transmissivity [ft²/min]: 1.05 x 10<sup>0</sup>

Hydraulic conductivity [ft/min]: 1.47 x 10<sup>-2</sup>

Aquifer thickness [ft]: 72.00

3.00



Transmissivity [ft²/min]: 1.09 x 10<sup>0</sup>

Hydraulic conductivity [ft/min]: 1.51 x 10<sup>-2</sup>

ways Park Drive Y. 11797 1890 est No. 3	Time-Drawdown-metho COOPER & JACOB Unconfined aquifer	od after	Project: FRANKI	IN CLEANERS
iest No. 3	Unconfined aquifer			
est No. 3			Evaluated by: WM	
		Test conducted or	n: 11/11/99	
		PTMW-1		
62.00 U.S.gal/min		Distance from the	pumping well 27.00 f	t
r level: 0.00 ft below datum				
Pumping test duration	Water level	Draw	vdown	Corrected
				drawdown
[min]	[ft]	[	ft]	[ft]
0.05	-0.01		-0.01	-0.0
0.10	0.01		0.01	0.0
0.15	0.03		0.03	0.0
0.20	0.05		0.05	0.0
0.25	0.10		0.10	0.1
0.30	0.14		0.14	0.1
0.35	0.20		0.20	0.2
0.45	0.24		0.31	0.2
0.50	0.37		0.37	0.3
0.55	0.43		0.43	0.4
0.60	0.48		0.48	0.4
0.65	0.54		0.54	0.5
0.70	0.59		0.59	0.5
0.75	0.64		0.64	0.6
0.80	0.68		0.68	0.6
0.85	0.72		0.72	0.7
0.90	0.77		0.77	0.7
0.95	0.79		0.79	0.7
1.00	0.86		0.86	0.8
1.10	0.89		0.89	0.0
1.15	0.90		0.90	0.9
1.20	0.93		0.93	0.9
1.25	0.95		0.95	0.9
1.30	0.97		0.97	0.9
1.35	0.99		0.99	0.9
1.40	1.00		1.00	0.9
1.45	1.01		1.01	1.0
1.50	1.04		1.04	1.0
1.00	1.04		1.04	1.0
1.65	1.05		1.05	1.0
1.70	1.07		1.07	1.0
1.75	1.08		1.08	1.0
1.80	1.09		1.09	1.0
1.85	1.08		1.08	1.0
1.90	1.10		1.10	1.09
1.95	1.11		1.11	1.10
2.00	1.10		1.10	1.10
	Pumping test duration         [min]         0.05         0.10         0.15         0.20         0.25         0.30         0.35         0.40         0.45         0.50         0.55         0.60         0.65         0.70         0.75         0.80         0.85         0.90         0.95         1.00         1.05         1.00         1.55         1.00         1.55         1.00         1.55         1.00         1.55         1.00         1.55         1.00         1.55         1.60         1.55         1.60         1.65         1.70         1.75         1.80         1.90         1.95         2.00	Pumping test duration         Water level           [min]         [ft]           0.05         -0.01           0.10         0.01           0.15         0.03           0.20         0.05           0.25         0.10           0.30         0.14           0.35         0.20           0.40         0.24           0.45         0.31           0.50         0.37           0.55         0.43           0.60         0.448           0.65         0.54           0.70         0.59           0.75         0.64           0.80         0.68           0.85         0.72           0.90         0.77           0.95         0.79           1.00         0.82           1.05         0.86           1.15         0.90           1.20         0.93           1.25         0.95           1.30         0.97           1.35         0.99           1.40         1.00           1.45         1.01           1.55         1.04           1.66         1.05	Pumping test duration         Water level         Draw           [min]         [ft]         [           0.05         -0.01	Pumping test duration         Water level         Drawdown           [min]         [ft]         [ft]           0.05         -0.01         -0.01           0.10         0.01         0.01           0.15         0.03         0.03           0.220         0.05         0.05           0.25         0.10         0.10           0.30         0.14         0.14           0.35         0.20         0.20           0.44         0.24         0.24           0.45         0.31         0.31           0.50         0.37         0.37           0.55         0.43         0.43           0.60         0.48         0.48           0.65         0.54         0.54           0.70         0.59         0.59           0.75         0.64         0.64           0.80         0.68         0.88           0.85         0.72         0.77           0.95         0.79         0.79           1.00         0.82         0.82           1.01         0.89         0.89           1.15         0.90         0.90           1.30         0.97

134.02



Transmissivity [ft²/min]: 1.07 x 10<sup>0</sup>

Hydraulic conductivity [ft/min]: 1.49 x 10<sup>-2</sup>

Dvirka and Bartilucci 330 Crossways Park Drive Woodbury N.Y. 11797 ph.(516)364-9890		Pumping test analysis		Date: 07.01.2000 Page 2		
		Distance-Time-Drawd after COOPER & JAC	lown-method COB	Project: FRANKI	Project: FRANKLIN CLEANERS	
		Unconfined aquifer		Evaluated by: W	Evaluated by: WM	
Pumping Test No. 3 PTMW-1			Test conducted	on: 11/11/99		
			PTMW-1			
Discharge 62.00 U.S.gal/min			Distance from th	ne pumping well 27.00 f	1	
Static wa	ater level: 0.00 ft below datum					
	Pumping test duration	Water level	Dra	awdown	Corrected drawdown	
	[min]	[ft]		[ft]	[ft]	
2	0.05	-0.01		-0.01	-0.0	
3	0.10	0.01		0.01	0.0	
4	0.15	0.03		0.03	0.0	
5	0.20	0.05		0.05	0.1	
6	0.25	0.10		0.10	0.	
7	0.30	0.14		0.14	0.	
8	0.35	0.20		0.20	0.:	
9	0.40	0.24		0.24	0.:	
10	0.45	0.31		0.31	0.3	
11	0.50	0.37		0.37	0.3	
12	0.55	0.43		0.43	0.4	
13	0.60	0.48		0.48	0	
14	0.65	0.54		0.54	0	
15	0.70	0.59		0.59	0.:	
10	0.75	0.64		0.64	0.0	
18	0.80	0.68		0.08	0.1	
19	0.05	0.72		0.72	0.	
20	0.95	0.77		0.79	0.	
21	1.00	0.79		0.82	0.	
22	1.05	0.86		0.86	0.1	
23	1.10	0.89		0.89	0.1	
24	1.15	0.90		0.90	0.9	
25	1.20	0.93		0.93	0.9	
26	1.25	0.95		0.95	0.9	
27	1.30	0.97		0.97	0.9	
28	1.35	0.99		0.99	0.9	
29	1.40	1.00		1.00	0.9	
30	1.45	1.01		1.01	1.(	
31	1.50	1.04		1.04	1.(	
32	1.55	1.04		1.04	1.(	
33	1.60	1.05		1.05	1.0	
34	1.65	1.06		1.06	1.(	
36	1.70	1.07		1.07	1.	
37	1.75	1.08		1.00	1.1	
38	1.85	1.09		1.08	1.(	
39	1.90	1.00		1.10	1.0	
40	1.95	1.11		1.11	1.1	
41	2.00	1.10		1.10	1.1	

the second s



Transmissivity [ft²/min]: 5.67 x 10<sup>-1</sup>

Hydraulic conductivity [ft/min]: 7.88 x 10<sup>-3</sup>

Dvirka and Bartilucci 330 Crossways Park Drive Woodbury N.Y. 11797 ph.(516)364-9890		Pumping test analysis		Date: 07.01.200	0 Page 2
		Time-Drawdown-meth COOPER & JACOB	od after	Project: FRANKLIN CLEANERS	
		Unconfined aquifer		Evaluated by: W	M
Pumping Test No. 3			Test conducted on: 11/11/99		
PTMW-2			PTMW-2		
Discharge	e 62.00 U.S.gal/min		Distance from th	ne pumping well 12.00 f	t
Static wat	er level: 0.00 ft below datum				
	Pumping test duration	Water level	Dra	awdown	Corrected
					drawdown
	[min]	[ft]		[ft]	[ft]
2	0.05	0.04		0.04	0.0
3	0.10	0.12		0.12	0.1
4	0.15	0.31		0.31	0.3
5	0.20	0.55		0.55	0.5
7	0.25	0.77		0.77	0.7
8	0.35	1 17		1 17	0.9
9	0.40	1.17		1.34	1.1
10	0.45	1.49		1.49	1.4
11	0.50	1.63		1.63	1.6
12	0.55	1.75		1.75	1.7
13	0.60	1.86		1.86	1.8
14	0.65	1.96		1.96	1.9
15	0.70	2.04		2.04	2.0
16	0.75	2.12		2.12	2.0
17	0.80	2.18		2.18	2.1
19	0.05	2.24		2.24	2.2
20	0.95	2.23		2.34	2.2
21	1.00	2.37		2.37	2.3
22	1.05	2.41		2.41	2.3
23	1.10	2.44		2.44	2.4
24	1.15	2.48		2.48	2.4
25	1.20	2.50		2.50	2.4
26	1.25	2.53		2.53	2.4
27	1.30	2.54		2.54	2.5
28	1.35	2.57		2.57	2.5
30	1.40	2.58		2.58	2.5
31	1.50	2.61		2.61	2.5
32	1.55	2.61		2.61	2.5
33	1.60	2.63		2.63	2.5
34	1.65	2.63		2.63	2.5
35	1.70	2.64		2.64	2.5
36	1.75	2.65		2.65	2.6
37	1.80	2.65		2.65	2.6
30	1.00	2.65		2.05	2.6
40	1.90	2.00		2.00	2.0
41	2.00	2.67		2.67	2.6



Transmissivity [ft²/min]: 5.88 x 10<sup>-1</sup>

Hydraulic conductivity [ft/min]: 8.18 x 10<sup>-3</sup>

Dvirka and Bartilucci 330 Crossways Park Drive Woodbury N.Y. 11797 ph.(516)364-9890		Pumping test analysis Distance-Time-Drawdown-method		Date: 07.01.200	D Page 2	
				Project: FRANKLIN CLEANERS		
		Unconfined aquifer	fined aquifer Evaluated by: WM		M	
Pumping	g Test No. 3		Test conducted of	on: 11/11/99		
PTMW-2			PTMW-2			
Dischar	ge 62.00 U.S.gal/min		Distance from the	e pumping well 12.00 f	t	
Static wa	ater level: 0.00 ft below datum					
	Pumping test duration	Water level	Dra	wdown	Corrected	
					drawdown	
	[min]	[ft]		[ft]	[ft]	
2	0.05	0.04		0.04	0.03	
3	0.10	0.12		0.12	0.11	
4	0.15	0.31		0.31	0.31	
5	0.20	0.55		0.55	0.54	
6	0.25	0.77		0.77	0.76	
/	0.30	0.98		0.98	0.97	
8	0.35	1.17		1.17	1.10	
10	0.40	1.34		1.34	1.32	
11	0.50	1.43		1.43	1.40	
12	0.55	1.75		1.75	1.72	
13	0.60	1.86		1.86	1.84	
14	0.65	1.96		1.96	1.93	
15	0.70	2.04		2.04	2.01	
16	0.75	2.12		2.12	2.08	
17	0.80	2.18	-	2.18	2.15	
18	0.85	2.24		2.24	2.20	
19	0.90	2.29		2.29	2.26	
20	0.95	2.34		2.34	2.30	
21	1.00	2.37		2.37	2.33	
22	1.05	2.41		2.41	2.37	
23	1.10	2.44		2.44	2.40	
25	1.10	2.40		2.50	2.45	
26	1.25	2.53		2.53	2.48	
27	1.30	2.54		2.54	2.50	
28	1.35	2.57		2.57	2.52	
29	1.40	2.58		2.58	2.54	
30	1.45	2.60		2.60	2.55	
31	1.50	2.61		2.61	2.56	
32	1.55	2.61		2.61	2.57	
33	1.60	2.63		2.63	2.58	
34	1.65	2.63		2.63	2.59	
35	1.70	2.64		2.64	2.59	
37	1.75	2.00		2.00	2.00	
38	1.85	2.05		2.65	2.60	
39	1.90	2.66		2.66	2.61	
40	1.95	2.67		2.67	2.62	
41	2.00	2.67		2.67	2.62	

...



Transmissivity [ft²/min]: 1.12 x 10<sup>0</sup>

Hydraulic conductivity [ft/min]: 1.56 x 10<sup>-2</sup>

Dvirka and Bartilucci 330 Crossways Park Drive Woodbury N.Y. 11797 ph.(516)364-9890		Pumping test analysis Time-Drawdown-method after COOPER & JACOB Unconfined aquifer		Date: 07.01.200	0 Page 2	
				Project: FRANK	Project: FRANKLIN CLEANERS	
				Evaluated by: V	Evaluated by: WM	
Pumping Test No. 3			Test conducted of	on: 11/11/99		
PTMW-3			PTMW-3			
Discharge 62.00 U.S.gal/min			Distance from the pumping well 50.00 ft			
Static wa	ater level: 0.00 ft below datum					
	Pumping test duration	Water level	Drawdown		Corrected	
					drawdown	
	[min]	[ft]		[ft]	[ft]	
2	0.05	0.00		0.00	0.00	
3	0.10	0.01		0.01	0.00	
4	0.15	0.01		0.01	0.01	
5	0.20	0.03		0.03	0.03	
7	0.25	0.05		0.05	0.05	
- /	0.30	0.09		0.09	0.09	
0	0.35	0.14		0.14	0.14	
10	0.40	0.10		0.18	0.18	
11	0.45	0.23		0.23	0.23	
12	0.50	0.20		0.20	0.20	
13	0.60	0.37		0.37	0.37	
14	0.65	0.43		0.43	0.43	
15	0.70	0.47		0.47	0.47	
16	0.75	0.52		0.52	0.52	
17	0.80	0.55		0.55	0.55	
18	0.85	0.60		0.60	0.60	
19	0.90	0.63		0.63	0.63	
20	0.95	0.67		0.67	0.67	
21	1.00	0.70		0.70	0.70	
22	1.05	0.73		0.73	0.73	
23	1.10	0.76		0.76	0.75	
24	1.15	0.79		0.79	0.78	
25	1.20	0.81		0.81	0.81	
26	1.25	0.83		0.83	0.83	
27	1.30	0.86		0.86	0.85	
28	1.35	0.87		0.87	0.87	
29	1.40	0.89		0.89	0.89	
31	1.40	0.91		0.91	0.91	
32	1.50	0.93		0.95	0.92	
33	1.60	0.95		0.96	0.95	
34	1.65	0.97		0.97	0.96	
35	1.70	0.98		0.98	0.98	
36	1.75	1.00		1.00	0.99	
37	1.80	1.00		1.00	1.00	
38	1.85	1.01		1.01	1.00	
39	1.90	1.02		1.02	1.02	
40	1.95	1.03		1.03	1.03	
41	2.00	1.04		1.04	1.03	

18,08



Transmissivity [ft²/min]: 1.11 x 10<sup>0</sup>

Hydraulic conductivity [ft/min]: 1.54 x 10<sup>-2</sup>

Dvirka	and Bartilucci	Pumping test analysis		Date: 07.01.200	0 Page 2
330 Crossways Park Drive Woodbury N.Y. 11797 ph.(516)364-9890		Distance-Time-Drawd	Distance-Time-Drawdown-method after COOPER & JACOB Unconfined aquifer		LIN CLEANERS
		Unconfined aquifer			Evaluated by: WM
Pumping Test No. 3			Test conducted	on: 11/11/99	
PTMW-3			PTMW-3		
Discharg	ge 62.00 U.S.gal/min		Distance from th	ne pumping well 50.00 f	ť
Static wa	ater level: 0.00 ft below datum				
	Pumping test duration	Water level	Dra	awdown	Corrected drawdown
	[min]	[ft]		[ft]	[ft]
2	0.05	0.00		0.00	0.00
3	0.10	0.01		0.01	0.00
4	0.15	0.01		0.01	0.01
5	0.20	0.03		0.03	0.03
6	0.25	0.05		0.05	0.05
8	0.30	0.09		0.09	0.09
9	0.40	0.14		0.14	0.14
10	0.45	0.23		0.23	0.23
11	0.50	0.28		0.28	0.28
12	0.55	0.33		0.33	0.33
13	0.60	0.37		0.37	0.37
14	0.65	0.43		0.43	0.43
15	0.70	0.47		0.47	0.47
16	0.75	0.52		0.52	0.52
1/	0.80	0.55		0.55	0.55
10	0.85	0.60		0.63	0.60
20	0.90	0.03		0.67	0.03
21	1.00	0.70		0.70	0.70
22	1.05	0.73		0.73	0.73
23	1.10	0.76		0.76	0.75
24	1.15	0.79		0.79	0.78
25	1.20	0.81		0.81	0.81
26	1.25	0.83		0.83	0.83
27	1.30	0.86		0.86	0.85
28	1.35	0.87		0.87	0.87
30	1.40	0.89		0.89	0.89
31	1.45	0.91		0.91	0.91
32	1.55	0.95		0.95	0.94
33	1.60	0.96		0.96	0.95
34	1.65	0.97		0.97	0.96
35	1.70	0.98		0.98	0.98
36	1.75	1.00		1.00	0.99
37	1.80	1.00		1.00	1.00
38	1.85	1.01		1.01	1.00
39	1.90	1.02		1.02	1.02
40	2.00	1.03		1.03	1.03
41	2.00	1.04		1.04	1.05

## Appendix E

## **APPENDIX E**

: 5

CORRESPONDENCE FROM NASSAU COUNTY DEPARTMENT OF PUBLIC WORKS CONCERNING CONNECTION TO STORM WATER DRAINAGE MANHOLE

I



330 Crossways Park Drive, Woodbury, New York, 11797-2015 516-364-9890 • 718-460-3634 • Fax: 516-364-9045 e-mail: db-eng@worldnet.att.net

February 28, 2000

Mr. John Waltz, P.E., Commissioner Nassau County Department of Public Works 1550 Franklin Avenue Mineola, NY 11501

Re: Franklin Cleaners Site Remedial Measure D&B No. 1640-2

Dear Commissioner Waltz:

Dvirka and Bartilucci Consulting Engineers (D&B) has been retained by the New York State Department of Environmental Conservation (NYSDEC) to design a groundwater extraction and treatment system to contain contamination from the above-referenced site. The treatment system will include air stripping for removal of volatile organic compounds (VOCs). We are requesting approval to discharge the treated effluent to the existing 18-inch diameter storm sewer located in Hempstead Avenue and to install piping below grade within the right-of-way and under Hempstead Avenue connecting to the storm sewer manhole located near the intersection of Woodland Drive.

Preliminary discussions with your staff have indicated that the existing storm drain may be surcharged during substantial storm events. In this case we will propose to include a float switch in the existing storm sewer which will shut down our well pumps before the storm drain is surcharged.

The proposed flow rate is 70 gpm, based on the current conceptual design. The influent water will be pumped from two extraction wells located along the Southern State Parkway to the treatment system. The treated water will then be discharged to the storm drain. The attached figure shows the general layout described above.

If you have any questions or require additional information, please do not hesitate to contact me at (516) 364-9890.

David S

Associate

DSG/kd cc: D. Camp (NYSDEC) T. Maher (D&B) W. Mann (D&B) • 1640/DSG00LTR-03.DOC(R03)



THOMAS 5. GULOTTA



JOHN M. WALTZ, P.E.

COUNTY OF NASSAU DEPARTMENT OF PUBLIC WORKS MINEOLA, NEW YORK 11501-4822

March 29, 2000

Dvirka & Bartilucci, Consulting Engineers 330 Crossways Park Drive Woodbury, NY 11797-2015

Attn: David S. Glass, P.E.

Re: Nassau County Drainage Connection Permit For Connection to County Drainage System Hempstead Avenue at Woodland Drive, Rockville Centre

Dear Mr. Glass:

We are in receipt of your February 28, 2000, requesting permission to connect into the County's existing manhole at the referenced location with a groundwater treatment system.

Although we have no objection to the proposed drainage connection, a permit must be obtained from this Department for the connection and excavations within the County right-of-way of Hempstead Avenue. Failure to obtain the permit is a violation of Nassau County Ordinance No. 105-1985.

For your convenience, we have enclosed a permit application that can be completed and returned to the attention of Mathew Morhart in our permit section at 1West Street, Room 309, Mineola, NY 11501. If the New York State Department of Environmental Conservation (NYSDEC) agrees to be the permittee, the application fee of \$100.00 and permit deposit monies are waived. However, a representative of the Village will be required to sign the application form. If NYSDEC requires their contractor to obtain the permit, all fees and charges will apply. If you have any questions, please feel free to contact Mathew Morhart at 571-4184.

Very truly yours,

John M. Waltz, P.

Commissioner

JMW:MP:ca Attachment

HIVCLERICALISECVANODEONDRAINPER, WPC
03/27/2000 12:07	5165714199	NCDPW	COMM OFFICE	PAGE 03
·	ROAI Nassau for wo	O OPENING PERMIT	APPLICATION of Public Works f County Roads	
Non-refundable ap	plication fee \$1(	0.00		
Please Print or Type this application. Check where applicable:		n.	Receipt No .:	
	Site Drawings (	5) are required to be atta	ached to this application	
New Worl	k R	econstruction	Grass Area	Drainage
Road Ope	ning	_ Sidewalk Opening	Curb Cut	Oth
Applicant:	(Owner or Ager	nt)	Tel No.:	
Address:	_	·		
School Dist .:	, Section	, Block	&Lot	
I request permission	to ope	en,(re) c	construct the (N_F_9	W Middle) aid
		(-)	(c	ricle one)
of				at a distance
(name of road)		(Com	munity)	
feet N-E-S-	W of			for the numoso o
(Circle one	e)	(nearest	Intersection)	ion the purpose (
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O. Highways & Gono		FUN UFFICIAL USE ON	NLY	
Your approval or dis	approval is requ	ired. When completed.	please return this referra	to the Contracts
Permits unit for proc	cessing. (Use rev	verse side for additional	l comments).	
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W-1634, 4/87, Rev. 11/90.				



