FIELD MEMO

TO:

Warren Gordon, P.E.

Resident Engineer, Pelham Bay Landfill

FROM:

Daniel Creighton

Geomembrane Supervisor

DATE:

March 19, 1996

SUBJECT:

Addendum: Geomembrane Damage to the Top of Landfill (3/14/96)

Due to the thunderstorm and winds last night, much more geomembrane liner was blown away and damaged beyond repair. The following is a summary of the additional panels that were damaged and must be replaced.

Panels Totally Blown Away:

S-4, 733, 734, 735, 736, 737, S-3, S-5, S-6, S-7, S-11, S-12, S-13, S-14, S-15, S-16, S-17, S-39, S-40, S-41, S-9. S-42, S-43, S-44, S-45, S-46, S-47, S-48, S-49, S-50, S-51, S-52, S-53, S-54, S-55, S-92, S-93, S-93A, S-94, S-95, S-96, S-97, S-98, S-99, S-100, S-112, S-113, and S-114.

Sub-Total SF = 122,657

New Total of Panels Blown Away = 324,563 SF New Total of Panels Damaged Beyond Repair = 65,516 SF New Approximate Total of Questionable Panels = 42,428 SF

Amended Grand Total of Damaged and Questionable Panels = 432,507 SF

A few other panels on top of landfill are now questionable and tests along the borders of damaged panels will have to be done more frequently to insure the integrity of the material. Again, tests should include all appropriate methods as per the Contract Documents to insure that the material still meets the specifications listed on page 02778-5, Part 2, Section 2.2.A.

xc: Ramaglia/Durig Ciancia (WCCI) NYS DEC Rant (BRECO)

BRECO MECHANICAL GROUP, INC. 201 SAW MILL RIVER ROAD YONKERS, NEW YORK 10701

TEL. (914) 963-3600 * FAX (914) 963-3989

June 17, 1996

Mr. Roy Durig, P.E.
Chief - Landfill Remediation
New York City Department of
Environmental Protection
96-05 Horace Harding Expressway
5th Floor - Lefrak Plaza
Corona, New York 11368

Re: Pelham Bay Landfill Closure Contract No. 876-HP Letter No. 78

Dear Mr. Durig,

The attached letter from GSE Lining Technology Inc. dated June 14, 1996 was forwarded directly to you by GSE. GSE's letter essentially states that GSE has again completed the installation of the geomembrane liner. Per the provisions of Paragraph 3.3K of Specification 02778, GEOMEMBRANE ACCEPTANCE, the geomembrane installation has been accepted by the DEP. Per paragraph 3.3K, ownership and responsibility for the geomembrane now belongs to NYCDEP, (and not to Breco, as erroneously stated in GSE's 6/14/96 letter).

Consistent with this, GSE states that any damage that occurs to the geomembrane from and after June 14, 1996 will be repaired by GSE at and for the account of the NYCDEP.

We will be completing the final tabulation of costs for the repair and will submit them to you shortly.

Very Truly Yours,

BRECO MECHANICAL GROUP, INC.

Mark SanAngelo Project Manager

Enc.

cc: P. Zoltanesky, Jr

P. Smith/ J. Jarahari

W. Gordon

A. Ciancia

S. Mokbel Durig.617



19103 Gundle Road Houston, Texas 77073 800-435-2008 713-443-8564 Fac: 713-475-6010

June 14, 1996

Mark San Angelo Breco Mechanical Group, Inc. 201 Saw Mill River Road Yonkers, New York 10701

RE:

Pelham Bay Landfill, Cover and Protection of Work GSE Lining Technology, Inc. Project Number XA4790

Dear Mr. San Angelo:

On June 14, 1996, GSE Lining Technology, Inc. completed its installation subcontract requirements on the above referenced project, including the repairs to the damaged liner. As of this date, the Scope of Work required of GSE has final acceptance by DEP's third party inspector (four (4) final acceptance sheets attacked) and you as the onsite representative of Breco Mechanical Group, Inc. With these acceptances, except for the submittal of as-built panel drawings; final submittals of conformance testing; and final billing, GSE has completed the installation of the geomembrane and the responsibility for protection of the geomembrane now belongs to Breco.

Please be advised that the exposed liner is now at risk to the elements. Acts of God and the onsite construction activities of Breco Mechanical Group, Inc. and its other subcontractors, invitees, and other third parties. Any damage that occurs to the geomembrane from and after June 14, 1996 will be repaired by GSE at and for the account of Breco Mechanical Group, Inc. GSE, in the very near future, will be submitting the remaining contract items for approval by the onsite Resident Engineer and the onsite representative of Breco Mechanical Group, Inc.

Sincercly,

Ronald Zunker, Jr. Project Manager -

Installation Services

RZ/cr

CC:

Warren Gordon, NYCDEP

Master File



PROJECT: PELLAM BOY LANDA'LL LOCATION: BROWN NEW YORK DATE 5-24-56 P.F. * XAYTO

Final PRE-START SITE INSPECTION

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CONDLE REPRESENTATIVE

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PROJECT: Pel han Day 1. F LOCATION: BROWN NEW YORK DATE 5/28/86 P.F. # XA 4790

Final PRESTART SITE INSPECTION

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LOCATION: BROWN NOW YOUR
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PRESTART SITE INSPECTION

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GLINDLE REPRESENTATIVE.

Gundle

PROJECT: Pelham Bay
LOCATION: Branx 714

DATE 6/11/16 P.F. XA4790

Final PRESTART SITE INSPECTION

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Gundle Representative

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Gundle Lining Construction Corp

CERTIFICATE OF **ACCEPTANCE** JOBNO: XA 4790
JOBNAME PELLAM Bay Landfill
CLIENT: BEECO MECHANCAL GRE BILL TO: SAME

Toll Free (800) 485-2006 Teles: 364657 GUNDLE HOU

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New York City Department of Environmental Protection
Division of Landfill Remediation
Pelham Bay Landfill
Contract 876-HP
Geomembrane Capping and Gas Collection System

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New York City Department of Environmental Protection
Division of Landfill Remediation
Petham Bay Landfill
Contract 876-HP

Geomembrane Capping and Gas Collection System

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New York City Department of Environmental Protection
Division of Landfill Remediation Pelham Bay Landfill
Contract 876-HP
Geomembrane Capping and Gas Collection System

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SAMPLES ALONG PERIMETER OF DAMAGED LINER

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Contract 876-HP

Geomembrane Capping and Gas Collection System

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All weld test field reports must be phoned in or faxed in daily to the attention of Patti Spencer. Phone 1 (800) 435-2008 Fax (713) 875-6010

ATTN: Nan. lep, x747	FIELD REPORT -	- WELL ,ESTS	

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All weld test field reports must be faxed in or phoned in daily. PHONE (800) 435-2008; FAX (713) 875-6010 CALL ED ZIMMEL (x821) OR YOUR PROJECT MANAGER UPON NOTIFICATION OF A FAILURE!!!

FIELD REPORT - WE__ TESTS DATE FAXED OR CALLED IN: DATE WELDED: JOB SPECIFICATION REQUIREMENTS: MATERIAL PEEL IN: PEEL OUT: MIL PEELOUT: the state of the MATERIAL MIL PEELIN: FUS/ PEELIN PEELOUT SHEAR PASS/ MACHINE SETTINGS SAMPLE # EXT PPI SPEED PRESSURE MAT/MIL SEAM # OR SEAM TEST TECH I.D. # MACHINE # PPI FAIL VOLTS. 10

All weld test field reports must be phoned in or faxed in daily to the attention of Patti Spencer. Phone 1 (800) 435-2008 Fax (713) 875-6010

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All weld test field reports must be phoned in or faxed in daily to the attention of Patti Spencer. Phone 1 (800) 435-2008 Fax (713) 875-6010

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☐ Resubmitcopies for approval	☐ Approved as submitted	☐ For approval	
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RE:), P.E.	10 WARREN GORDON	
ATTENTION 50 50 50 50 50 50 50 50 50 50 50 50 50		(914) 963-3850 (914) 963-3600	
LETTER OF TRANSMITTAL		BRECO MECHANICAL GROUP, INC. 201 Saw Mill River Road YONKERS, NEW YORK 10701	BRI

If enclosures are not as noted, kindly notify us at once.

GSE I ining Technology, Inc.

Pelham Bay L....dfill GSE MR No. 1413-01 GSE Job No. XA4790

				Tensile Stre	ıgth @ Yield	_		Tensile Stren	ıgtlı @ Break	_	ation @ Break		Tear Resistance ASTM D 1004	
				Smooth Spe Textured Sp	sc = 130 ppi	Smooth Sp	e length xc = 13 % pec = 13 %		ec = 243 ppi pec = 243 ppi	2.0" gage length Smooth Spec = 500% Textured Spec = 150%		Smooth Spec = 40 lb. Textured Spec = 40 lb.		
		Date	(S)mooth/	MD	CD	MD	CD	MD	CD	MD	CD	MD	CD	
Sample#	Pass/Fail		(T)extured	[ppi]	[ppi]	[%]	[%]	[ppi]	[ppl]	%	[%]	[lb.]	[lb.]	
ı	Pass	5/8/96	\$	143	165	19	19	256	295	729	809	54	52	
2	Pass	5/8/96	S	168	166	18	15	305	287	777	793			
3	Pass	5/8/96	S	153	148	20	16	277	255	794	793	49	54	
4	Pass	5/8/96	<u>s</u>	171	164	17	16	291	280	743	769			
5	Pass	5/8/96	<u>s</u>	146	160	18	17	249	303	704	853			
6	Pass	5/8/96	S	168	166	21	18	258	262	675	759	52	61_	
7	Pass	5/8/96	s	163	160	19	. 17	264	244	685	720	49	55	
8	Pass	5/8/96	s	162	161	. 21	16	314	309	806	853			
9	Pass	5/8/96	s	153	148	18	16 .	317	287	83.5	816			
10	Pass	5/8/96	T	155	169	20	16	276	300	772	830			
11	Pass	5/8/96	S	151	151	18	17	311	284	837	828			
12	Pass	5/8/96	s	157	168	18	18	298_	298	791	817			
13	Pass	5/8/96	S	169	162	20	16	289	264	756_	760			
14	Pass	5/8/96	<u>s</u>	166	166	18	18	298	254	764	709			
15	Pass	5/8/96	S	162	163	19	15	294	270 .	782	792	52	58	
16	Pass	5/8/96	S	154	176	18	18	270	302	738	804			
1.7	Pass	5/8/96	S	160	171	20	16	315	282	887	812			
18	Pass	5/8/96	s	155	171	17	18	285	314	798	863			
19	Pass	5/8/96	S	158	178	18	17	303	324	827	897	52	56	

Report By: Melody Adams Nathan Ivy

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GSE I ing Technology, Inc.

Pelham Bay Landfill GSE MR No. 1413-01 GSE Job No. XA4790

				Tensile Stren	gth @ Yield	Tensile Elong	ASTM D 638,	Tensile Stren Type IV, 2 iµm	gth @ Break	Tensile Elonga	•	Tear Re	
		Date	(S)mooth/	Smooth Spe Textured Sp MD		1.3" gag Sinooth Sp Textured S MD	pec = 13 % pec = 13 % CD	Textured Sp MD	ec = 243 ppi ec = 243 ppi CD	2.0" gag Smooth Sp Textured Sp MD	ec = 500% oec = 150% CD	Smooth Sp Textured Sp MD	pec = 40 lb. CD
Sample #	Pass/Fail	Received	(T)extured	[ppi]	[ppi]	[%]	[%]	[ppi]	(ppi)	[%]	[%]	[lk.]	[lb.]
20	Pass	5/8/96	<u>s</u>	152	157	19	16	276	293	768	857		
21	Pass	5/8/96	s	149	178	20	17	278	288	809	794		
22	Pass	5/8/96	S	158	176	17	17	304	337	821	903		
23	Pass	5/8/96	<u>s</u> .	175	169	19	17_	312	289	767	809	53	56
24	Pass	5/8/96	8_	155	168	17	17	255	320	689	856	·	
25	Pass	5/8/96	S	156	158	20	16	275	284	728	804		
26	Pass	5/8/96	S	155	165	20	17	285	342	766	914	53	58
27	Pass	5/8/96	s	169	178	17	17	255	296	744	818		
28	Pass	5/8/96	<u>s_</u>	163	177	17	17	253	268	705	760		
29	Pass	5/8/96	S	195	172	15	16	293	313	753	824		
30	Pass	5/8/96	Š	178	155	16	17	290	292	794	798	53	53
31	Pass	5/8/96	<u>s</u>	181	161	17	17	267	271	746	765		
32	Pass	5/8/96	S	180	167	14	16	281	310	768	805		
33	Pass	5/8/96	Т	180	182	16	17	193	209	541	604_	49	
34	Pass	5/8/96	Т	178	182	17	16	155	154	416	461	55	52
35	Pass	5/8/96	Т	168	172	16	16	180	181	504	519		
36	Pass	5/8/96	τ	166	172	17	17	185	177	516	-511	52	47
37	Pass	5/8/96	Т	164	164	16	16	120	112	393	318		
38	Pass	5/8/96	т	182	175	16	17	182	207	489	553		
<u> </u>			<u>-</u>										

Report By: Melody Adams

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GSE Lining Technology, Inc.

Pelham Bayndfill GSE MR No. 1413-01 GSE Job No. XA4790

			Tensile Strength @ Yield Smooth Spec = 130 ppi Textured Spec = 13(ppi			Tensile Elougation @ Yield Tensile Strength @ Break ASTM D 638, Type IV, 2 ipm 1.3" gage length Smooth Spec = 13 % Smooth Spec = 243 ppl				2.0" gag	ation @ Break ge length	Tear Resistance ASTM D 1004 Smooth Spec = 40 lb.		
				•	•••	•	pec = 13 %		ec = 243 ppi		pec = 150%	Textured S		
		Date	(S)mooth/	MD	CD	MD	CD	MD	CD	MD	CD	MD	CD	
Sample #	Pass/Fail	Received	(T)extured	ppi	[ppl]	[%]	[%]	[ppi]	[ppi]	[%]	[%]	[lb.]	[lb.]	
39	Pass	5/8/96	T	160	164	17	17	102	157	416	501	55	51	
40	Pass	5/8/96	T	170	179	17	16	194	113	576	440			
41	Pass	5/8/96	Т	174	178	16	15	132	142	220	449	<u> </u>		
42	Pass	5/8/96	<u>T</u>	164	£ 75	17	16	202	128_	560.	418			
43	Pass	5/8/96	т	172	165	17	16	193	124	564	529			
44	Pass	5/8/96	T	169	179	17	14	164_	178	475	<u>544</u>			
45	Pass	5/8/96	Т	171	175	17	16	175	130	483	269	54	49	
46	Pass	5/8/96	<u>T</u>	173	170	18	. 16	166	171	516	480			
47	Pass	5/8/96	S	191	161	15	16	296	282	779_	786			
48	Pass	5/8/96	s	155_	161	16_	15	240	265	703	7 90			
49	Pass	5/8/96	S	170	185	16	14	280	292	734	770	54	52	
50	Pass	5/8/96	S	175	187	16	14	290	303	765	810			
51	Pass	5/8/96	s	167	173	16	. 14	285	289	774	803			
52	Pass	5/8/96	S	173	168	17	15	272	277	730	798			
53	Pass	5/8/96	S	156	160	17	17	242	257	705	761			

Report By: Melody Adams Nathan Ivy

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Pelham Bay Lundfill GSE MR No. 1413-01 GSE Job No. XA4790

					02200	7110, 2121	****									
				•			·	(S)mooth/		Puncture FTMS 101/Method 2065 Smooth Spec = 60 lb. Textured Spec = 60 lb.	ASTM 1 br. @ :	al Stability D 1204 100 degC +/- 3%	Specific Gravity ASTM D 792/D 1505 Spec = >0.93	OIT ASTM D 3895 1 atm @ 200 degC GSE Spec = 100 mln.	Low Temp. Brittleness ASTM D 746 Spec = -40°F	Average Thickness ASTM D 1593 Spec = 60 +/-10%
Sample#	Pass/Fail	Date Received	(S)mooth/ (T)extured	Resistance [lb.]	MD [% change]	TĐ [% change]		[minutes]	[0]	[mil]						
1	Pass	5/8/96	S	92	-0.17	-0.15	0.95	150	<-40	59						
2	Pass	5/8/96	S							62						
3	Pass	5/8/96	<u>s_</u>	92	0.1	80.0	0.95	150	<-40	58						
4	Pass	5/8/96	S							61						
5	Pass	5/8/96	S					·		59						
6	Pass	5/8/96	<u>s_</u>	104	0.15	0.25	0.95	150	<-40	61						
7	Pass	5/8/96	S	102	-0.07	-0.15	0.95	150	<-40	61						
8	Pass	5/8/96	8							60						
9	Pass	5/8/96	S							60						
10	Pass	5/8/96	T			 				60						
11_	Pass	5/8/96	S							59						
12	Pass	5/8/96	S	· · · · · · · · · · · · · · · · · · ·						59						
13	Pass	5/8/96	S							61						
14	Pass	5/8/96	S							62						
15	Pass	5/8/96	S	101	-0.08	. 0.07	0.95	150	<-40	60						
- 16	Pass	5/8/96	S							62						
17	Pass	5/8/96	S							60						
18	Pass	5/8/96	S							61						
19	Pass	5/8/96	S	89	-0.15	-0.37	0.95	150	<:40	61						

Report By: Melody Adams Nathan Ivy

GSE Jining Technology, Inc.

Pelham Bayndfill GSE MR No. 1413-01 GSE Job No. XA4790

					(S)mooth/	Puncture FTMS 101/Method 2065 Smooth Spec = 60 lb. Textured Spec = 60 lb.	ASTM	al Stability D 1204 100 degC +/- 3%	Specific Gravity ASTM D 792/D 1505 Spec = >0.93	OIT ASTM D 3895 1 atm @ 200 degC GSE Spec = 100 min.	Low Temp. Brittleness ASTM D 746 Spec = -40°F	Average Thickness ASTM D 1593 Spec = 60 +/-10%
Sainple#	Pass/Fail	Date Received	(S)mooth/ (T)extured	Resistance [lb.]	MD [% change]	TD [% change]		[minutes]	[°]	[nii]		
20	Pass	5/8/96	s							60		
21	Pass	5/8/96	S							60		
22	Pass	5/8/96	s							61		
23	Pass	5/8/96	S	97	-0.23	0.1	0.95	150	<-40	62		
24	Pass	5/8/96	<u>s</u>				<u> </u>			60		
25	Pass	5/8/96	8							60		
. 26	Pass	5/8/96	<u>s</u>	106	0.17	-0.35	0.95	150	<-40	62		
27	Pass	5/8/96								62		
28	Pass	5/8/96	S	·						60		
29	Pass	5/8/96	8							63		
30	Pass	5/8/96	<u>s</u>	102	0.42	0.12	0.95	Pending	Pending	61		
31	Pass	5/8/96	S							61		
32	Pass	5/8/96	\$			 				62		
33	Pass	5/8/96	T	111	0.25	0.02	0.95	112	Pending	63		
34	Pass	5/8/96	T	101	0.12	0.1	0.95			63		
35	Pass	5/8/96	T				· .			62		
36	Pass	5/8/96	<u>T</u>	96	0.12	0.05	0.95	174	Pending	61		
37	Pass	5/8/96	Т							64		
38	Pass	5/8/96	T							65		

Report By: Molody Adams Nathan Ivy

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GSE Ling Technology, Inc.

Pelham Bay Lanafill GSE MR No. 1413-01 GSE Job No. XA4790

				Puncture FTMS 101/Method 2065 Smooth Spec = 60 lb. Textured Spec = 60 lb.	ASTM	al Stability D 1204 100 degC	Specific Gravity ASTM D 792/D 1505 Spec = >0.93	OIT ASTM D 3895 1 atm @ 200 degC GSE Spec = 100 min.	Low Temp. Brittleness ASTM D 746 Spec = 40°F	Average Thickness ASTM D 1593 Spec = 60 +/-10%
Sample #	Pass/Fail	Date Received	(S)mooth/ (T)extured	Resistance	MD [% change]	TD [% change]		[minutes]	[6]	[mil]
39	Pass	5/8/96	T	97	0.02	0.2	0.95	Pending	Pending	63
40	Pass	5/8/96	тт							62
41	Pass	5/8/96	T							61
42	Pass	5/8/96	T							63
43	Pass	5/8/96	Т							64
44	Pass	5/8/96	<u>T</u>							62
45	Pass	5/8/96	_T	101	-0.13	0.2	0.95	Pending	Pending	63
46	Pass	5/8/96	T							63
47	Pass	5/8/96								59
48	Pass	5/8/96	S							56
49	Pass	5/8/96	<u>s</u>	95	-0.18	0.33	0.95	Pending	Pending	66
50	Pass	5/8/96	S							60
51	Pass	5/8/96	s							58
52	Pass	5/8/96	<u>s</u>							60
53	Pass	5/8/96	S							60



Quality Control Certificate

RAILCAR : ACFXS3288
MATERIAL : HDT 060 MIL
BATCH # : 050595
ROLL # : 03032371

MANF. DATE : 05/05/1995

PROJECT NAME : PELHAM BAY CLOSURE

MR NUMBER : 1413-01 PROJECT #: XA4790

LOCATION : MOUSTON IX 054

ESCR (hrs)	Dimensional Stability (%)	Tear Resistance (lb)	Puncture Resistance (1b)	Break Elongation (%)	Break Strength (ppi)	Tensile Properties: Yield Strength (ppi)	Density (g/cc)	Carbon Black Dispersion	Carbon Black (%)	Minimum Thickness (mil)	TEST PARAMETER
1/RAILCAR	EVERY ROLL	EVERY ROLL	EVERY ROLL	EVERY ROLL	EVERY ROLL	EVERY ROLL	STH ROLL	STH ROLL	STH ROLL	EVERY ROLL	FREQUENCY
1500 min	-2.00 to 2.00	\$	80	120	3	130	0.940 min	A-1/A-2/B-1	2.0 to 3.0	54.0 min	TYPICAL SPECIFICATIONS
Pending	-0.28	61	122	589	192	154	0.947	A-1	2.5	57.0	TEST
D 1693 NSF MOD.	0 1204 (1 hr, 100c)	b 1004	FIMS 101, Meth. 2065	r pe	0 638 Type IV		D 1505 (Meth.A)	D 3015	0 1603	D 751 NSF Mod.	ASTM METHOD

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Quality Control Certificate

. HEL	ROLL #	BATCH # : 012295	RAILCAR
HANF, DATE PROJECT NAME NR NUMBER LOCATION	ROLL # : 04019914	: HDT 060 MIL : 012295	: TR9316-2
		PROJECT NAME : PELNAM BAY CLOSURE NR NUMBER : 1413-01 PROJECT # : XA4790	MANF. DATE : 01/22/1995

ESCR (hrs)	Dimensional Stability (%)	Tear Resistance (lb)	Puncture Resistance (lb)	Break Elongation (%)	Yield Elongation (%)	Break Strongth (ppi)	Tensile Properties: Yield Strength (ppi)	Density (g/cc)	Carbon Black Dispersion	Carbon Black (%)	Minimum Thickness (mil)	TEST PARAMETER
1/RAILCAR	EVERY ROLL	EVERY ROLL	EVERY ROLL	EVERY ROLL	EVERY ROLL	EVERY ROLL	EVERY ROLL	STH ROLL	STH ROLL	STH ROLL	EVERY ROLL	TEST ING FREQUENCY
1500 ສາຄ	-2.00 to 2.00	\$	80	120	10	75	130	0.940 min	A-1/A-2/B-1	2.0 to 3.0	54.0 min	TYPICAL SPECIFICATIONS
Pending	0.05	\$\$	120	490	17	155	172	0.946	A-1	2.1	56.0	TEST RESULTS
D 1693 NSF MOD.	D 1204 (1 hr, 100c)	p 1004	FTMS 101, Meth. 2065		2 ipm	D 638 Type IV		D 1505 (Meth.A)	0 3015	D 1603	D 751 MSF Mod.	WETHOO HETHOO



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Quality Control Certificate

ROLL #	BATCH #	MATERIAL	RAILCAR
ROLL # : 03034514	BATCH # : 082195	MATERIAL : HOT 060 MIL	RAILCAR : PSPX1109
LOCATION	MR NUMBER	PROJECT NAME	MANF. DATE
: HOUSTON TX 054	MR NUMBER : 1413-01 PROJECT # : XA4790	PROJECT NAME : PELHAH BAY CLOSURE	: 08/21/1995

ESCR (hrs)	Dimensional Stability (%)	Tear Resistance (lb)	Puncture Resistance (1b)	Break Elongation (%)	Break Strength (ppi)	Tensile Properties: Yield Strength (ppi)	Density (g/cc)	Cerbon Black Dispersion	Carbon Black (%)	Minimum Thickness (mil)	TEST PARAMETER
1/RAILCAR	EVERY ROLL	EVERY ROLL	EVERY ROLL	EVERY ROLL	EVERY ROLL	EVERY ROLL	STH ROLL	STH ROLL	SIH ROLL	EVERY ROLL	TEST ING FREQUENCY
1500 min	-2.00 to 2.00	45	80	120	K &	130	0.940 min	A-1/A-2/B-1	2.0 to 3.0	54.0 min	TYPICAL SPECIFICATIONS
Pending	0.02	57	112	408	157	157	0.947	A-1	2.3	56.0	RESULTS
D 1693 NSF MOD.	D 1204 (1 hr, 1000)	D 1004	FTKS 101, Meth. 2065		D 638 Type IV		D 1505 (Meth.A)	D 3015	D 1603	D 751 NSF Mod.	ASTM METHOD



Geocomposite Production Minimum Property Values Quality Control Certificates C-1

Appendix C-1 GEOCOMPOSITE PRODUCTION MINIMUM PROPERTY VALUES QUALITY CONTROL CERTIFICATES

The Tensar Corporation supplied the geocomposite (Tensar product code DC4205) for the Pelham Bay Landfill Closure. Geocomposite for this project was delivered to the project site from April 1995 through May 1996. Each shipment of geocomposite material was accompanied by quality control certification from the manufacturer. Each certificate provide information on the thickness, tensile strength, melt index, density, %CB and Peel and/or Bond Strength. The range of values for each parameter were as follows:

Thickness (mm)	5.20 - 5.98
Tensile Strength (lb/ft)	588.6 – 904.8
Melt Index (gm/10min)	0.318 - 0.669
Density (gm/cc)	0.948 - 0.978
% CB	2.16 - 2.92

Peel Strength Addendum (gm/in)

Top 1104 - 5148 Bottom 1052 - 4791

Bond Strength (g/in) 1129 - 4640

In addition to the QC certification for the particular lot of material shipped, Material Property Data Sheets were provided. Copies of representative QC documentation that accompanied each shipment are included in this appendix.



The Tensar Corporation

1210 Citizens Parkway Morrow, Georgia 30260 (404) 968-3255

MAY 04, 1995

AGAM CONSTRUCTORS, INC. CONSTRUCTION MANAGERS RECEIVED

MAY 0 5 1995

ARMANDO M. BYRNE S.

AGAM CONSTRUCTORS INC 4E DOWNING PLACE POUGHKEEPSIE, NY 12603

REFERENCE:

TENSAR ORDER NUMBER:

400895

PURCHASE ORDER NUMBER:

135-03/94-144

BILL OF LADING NUMBER:

53705

SOLD TO: AGAM CONSTRUCTORS INC

4E DOWNING PLACE

SHIP TO: AGAM FIELD OFFICE

PELHAM BAY LANDFILL

3599 BRUCKNER BLVD.

POUGHKEEPSIE, NY 12603

BRONX, NY 10464

This is to certify that TENSAR DC420501 geocomposite as manufactured by the TENSAR Corporation, meets the characteristics and properties per the attached specification sheet.

Sincerely,

Ron Whum olick

Manager of Continuous Improvement

and Quality Control

Notary Public, Clayton County, Georgia My Commission Expires May 10, 1998



The Tensar Corporation

1210 Citizens Parkway Morrow, Georgia 30260 (404) 968-3255

AGAM CONSTRUCTORS INC

PELHAM BAY LANDFILL

DC 4205 018 PEEL STRENGTH ADDENDUM

(qm/in)

	(911/////	
LOT NO.	TOP _	BOTTOM
5-0240-07A	2782	2486
5-0241-05A	3091	2514
5-0241-17B	2439	2348
5-0241-37B	2963	1911
5-0241-42A	2421	3599
5-0241-47A	3463	2259
5-0241-51A	3424	1895
5-0241-57A	2111	3372
5-0241-61A	2241	3436
5-0241-26A	4168	4696
5-0241-14A	2499	2196
5-0241-09B	2143	2163

DRAINAGE COMPOSITE DC4205

The drainage composite shall consist of a geotextile bonded to each side of a drainage net. The drainage composite shall have a low compressibility in order to maintain high flow capacity over a wide range of confining pressures. The bonding process shall not introduce adhesives or other foreign products. The strength of the bond between the drainage net and the geotextile shall be greater than the friction developed between the geotextile and a soil. The drainage composite shall maintain a high flow under long term loading conditions and shall be resistant to all forms of biological or chemical degradation normally encountered in a soil environment. The drainage composite shall be made from the drainage net and geotextile products whose property requirements are listed below.

PROPERTY TEST METHOD NOTES UNITS VA Flow Capacity ASTM 4716 1 • Gradient of 1 • Transmissivity @ 500 psf x10 ⁻³ ft ² /sec	<u>21</u>
Gradient of 1	
3.2.	
Transitionity & ooo per	J 661
···	9.55) 16
Transmission, & release her	
3.2.	7.24)
	8.6
- · -	3.86)
Mechanical Properties 3,4,5	
• Compression 1,2	
@ 20,000 psf %	50
 Peak Tensile Strength-MD ASTM D5035 6 lbs/ft 	575
Drainage Net	
 Aperture Size I.D. Calipered 7 inches 	0.3
 Thickness O.D. Calipered 8,9 inches 	0.20
Polyethylene Polymer	
-Specific Gravity ASTM D792 g/cm ³	0.940
-Carbon Black Stabilization ASTM D4218 %	2.5
Geotextile 10	
Grab Tensile Strength ASTM D4632 lbs 13	0/110
AOS ASTM D4751 US Std.Sv.Sz.	70
 Weight ASTM D1910 oz/sy 4.0,4.5,6.0,4 	3.0.10
Composite	• .
Laminate Bond Strength ASTM F904 11 g/in	400
Dimensions - Finished Product	
-Thickness O.D. Calipered in	0.24
-Roll Length ft	225
-Roll Width (Drainage Net) ft	14
Roll Weight	890
Notes	550

- 1. Test values are for the core net only.
- Compression Tests are performed on a 2-inch square sample loaded at a 1mm/minute constant rate of strain.
- 3. Test values are for drainage net prior to bonding process.
- 4. All test values are nominal, unless otherwise indicated.
- 5. MD Machine (roll) Direction.
- 6. Minimum value.
- 7. Inside dimensions in each principal direction are measured by calipers.
- 8. Outside dimensions in each principal direction are measured by calipers.
- 9. Thickness is measured by placing the specimen flat on a comparator base and lowering a round 1/2 inch diameter flat end contact surface squarely over a junction.
- 10. Geotextile splices within each roll of finished goods shall be considered acceptable product. The splicing methods shall include, but are not limited to, stitching or heat bonding. The finished splice shall maintain the continuity of the filtration function of the geotextile. These methods will be considered viable and acceptable unless otherwise specified.
- 11. Minimum value of a random 5 sample (MD) average between the polyethylene geonet and the needle punched geotextile.

APPENDIX D LOAMY SOIL TESTING

D-1 During Construction Loamy Soil Testing

D-1 During Construction Loamy Soil Testing

During Construction Loamy Soil Testing - Field Compaction Tests

Pelham Bay Landfill Closure and Final Remediation

Test No.	Location	Elev.	Water Content %	Percent Compactiion	Comment	Maximum Density (#/cu.ft.)	Optimum Moisture (%)
	Structu	rai Backtill (August 10, 19	95)		tald the first	Aria de la compansión de
			40.4		\ .		
	storm water on 200' slope, trench 3	80'	12.1	95.7	l A	124.8	10.3
	storm water on 200' slope, trench 3	40'	11.1	96.5	Α	124.8	10.3
6	storm water on 200' slope, trench 3	20'	9.0	95.4	Α .	124.8	10.3
v. 500 200	. Loamy So			4005)			
Maria di	Loamy So	II. Roadway	s (August 31,. 	1995) 			
7	lower road B at A-5.5	30	6.5	100.2	Α	122.8	10.0
	lower road B at A-8	32	5.3	100.2	Â	122.8	10.0
1 -	lower road B at A-11	35	7.3	95.1	Â	122.8	10.0
1	lower road B at A-13	38	6.0	98.0	Â	122.8	10.0
	lower road B at A-15	40	4.3	100.2	Â	122.8	10.0
	lower road B at A-17	42	6.4	99.7		122.8	
	lower road B at A-19	44	7.8	99.7	A	1	10.0
10	llower road B at A-19	**	/.0	99.3	^	122.8	10.0
e e van	Loamy on R	nad B. 1st I	ift (August 3:	1005)		F. L. War Shirt	Barrie Harris
00.000 no. 00			int fundance				Sald all all and
7	lower road B at A-5.5 = sta 35+00	30	6.5	100.2	A	122.8	10.0
	lower road B at A-8 = sta 33+00	32	5.3	100.0	Ä	122.8	10.0
	lower road B at A-8, anchor trench	32	7.5	95.9	A	122.8	10.0
1	lower road B at A-11 31+00	35	7.3	95.1	Â	122.8	10.0
	lower road B at A-11, anchor trench	35	7.0	98.8	Ä	122.8	10.0
	lower road B at A-13 39+00	38	6.0	98.0	Â	122.8	10.0
	lower road B at A-13, anchor trench	38	6.7	96.9	Ä	122.8	10.0
	lower road B at A-15 27+00	40	4.3	100.2	Â	122.8	10.0
	lower road B at A-15, anchor trench	40	7.5	98.7	Ä	122.8	10.0
ı ı	lower road B at A-17 25+00	42	6.4	99.7	Â	122.8	10.0
	lower road B at A-17, anchor trench	42	4.8	98.7	Â	122.8	10.0
	lower road B at A-19 23+00	44	7.8	99.3	Â	122.8	10.0
'	South Toda B at A-10 20.00	77	7.0	99.5	^	122.0	10.0
	Loamy o	n Roads (Se	entember 8 1	995)			
Transfer of the Land of the La		200			Sala ni Linita atrono		1.014.5
1 1	Road A, survey line A-10 / STA 35+00	12	4.4	99.5	Α	122.8	10.0
1 - 1	anchor trench adj. to test #1	12	7.5	95.4	A	122.8	10.0
3	Road A, survey line A-12 / STA 33+00	12	4.8	100.0	A	122.8	10.0
	anchor trench adj. to test #3	12	9.2	89.7	В	122.8	10.0
	Road A, survey line A-14 / STA 31+00	12	4.8	100.0	Ā	122.8	10.0
	anchor trench adj. to test #5	12	8.2	94.2	В	122.8	10.0
	Road A, survey line A-16 / STA 29+00	12	4.5	100.0	A	122.8	10.0
	nchor trench adj. to test #7	12	7.0	83.4	В	122.8	10.0
	Road A, survey line A-18 / STA 27+00	12	4.5	100.0	Ā	122.8	10.0
	Road A, survey line A-20 / STA 25+00	14	6.0	100.0	A	122.8	10.0
	Road A, survey line A-24 / STA 23+00	12	5.1	100.0	Â	122.8	10.0
I I	Road A, survey line A-26 / STA 21+00	12	6.9	100.0	Â	122.8	10.0
1 I	Road A, survey line A-29 / STA 19+00	12	7.4	100.0	Â	122.8	
.		12	7.5	100.0	^	122.0	10.0

During Construction Loamy Soil Testing - Field Compaction Tests

Pelham Bay Landfill Closure and Final Remediation

Test No.	Location	Flan	Water	Percent		l –	
		F1~		1 Clock		Density	Moisture
		Elev.	Content %	Compactiion	Comment	(#/cu.ft.)	(%)
	Loamy on Roa	ds (Septemi	oer 8, 1995) (continued)			Andreas Company
	Road A, survey line A-31 / STA 17+00	12	5.3	100.0	Α	122.8	10.0
15	lower Road B, survey line A-25 / STA 21+00	46	4.8	100.0	Α	122.8	10.0
	anchor trench adj. to test #5	46	9.2	99.2	Α	122.8	10.0
	lower Road B, survey line A-27 / STA 19+00	44	9.1	96.4	Α	122.8	10.0
	anchor trench adj. to test #17	44	5.5	99.6	Α	122.8	10.0
	lower Road B, survey line A-30 / STA 17+00	42	6.3	100.0	Α	122.8	10.0
	upper Road B, survey line B-0.5 / STA 93+00	78	6.1	100.0	Α	122.8	10.0
	upper Road B, survey line B-3 / STA 91+00	78	5.6	100.0	Α	122.8	10.0
	anchor trench adj. to test #21	78	9.4	93.3	Α	122.8	10.0
	upper Road B, survey line B-5 / STA 89+00	72	6.9	100.0	Α	122.8	10.0
	anchor trench adj. to test #23	72	9.2	87.1	Α	122.8	10.0
	upper Road B, survey line B-7 / STA 87+00	73	6.0	98.5	Α	122.8	10.0
	anchor trench adj. to test #25	73	5.7	100.0	Α	122.8	10.0
	upper Road B, survey line B-9 / STA 85+00	76	6.5	100.0	Α	122.8	10.0
	anchor trench adj. to test #27	76	7.1	96.1	Α	122.8	10.0
	upper Road B, survey line B-11 / STA 83+00	79	7.1	100.0	Α	122.8	10.0
	anchor trench adj. to test #29	79	7.2	95.1	Α	122.8	10.0
	upper Road B, survey line B-13 / STA 81+00	82	6.4	100.0	Α	122.8	10.0
	anchor trench adj. to test #31	82	7.2	95.7	Α	122.8	10.0
	upper Road B, survey line A-26 / STA 78+00	86	4.3	100.0	Α	122.8	10.0
	anchor trench adj. to test #33	86	6.1	100.0	Α	122.8	10.0
	upper Road B, survey line A-27 / STA 77+00	88	4.9	100.0	Α	122.8	10.0
	anchor trench adj. to test #35	88	6.1	100.0	Α	122.8	10.0
	upper Road B, survey line A-30 / STA 75+00	88	5.9	99.3	Α	122.8	10.0
	anchor trench adj. to test #37	88	6.5	97.1	Α	122.8	10.0
	Road C, survey line B-2 / STA 15+00	122	6.6	98.8	Α	122.8	10.0
	Road C, survey line B-6 / STA 17+00	118	6.4	100.0	Α	122.8	10.0
	Road C, survey line B-9 / STA 19+00	119	4.7	100.0	Α	122.8	10.0
	Road C, survey line B-11 / STA 21+00	122	5.9	100.0	Α	122.8	10.0
	Road C, survey line A-29 / STA 23+00	124	4.3	100.0	Α	122.8	10.0
	Road C, survey line A-31 / STA 25+00	121	4.3	100.0	Α	122.8	10.0
	Road C, survey line A-33 / STA 27+00	117	3.7	100.0	Α	122.8	10.0
	Road C, survey line A-35 / STA 29+00	112	3.6	99.8	Α	122.8	10.0
47	Road C, survey line A-37 / STA 31+00	110	3.1	100.0	Α	122.8	10.0
	3" Minus: And	hor Trench	(September 1	5, 1995)			
14	anchor trench lower road 1st lift A-1	21.5	6.4	100.0	Α	122.8	10.0
, i = 1, i = 12	Para dial mana a funda in . Person	200 d 'C		1005)	200	Island State	
arabili y s	3" Minus: F	koadway (Se	eptember 15,	1995)		int who	
13	lower road B 1st lift above line A-1	21.5	5.9	96.2	Α	122.8	10.0
	line 4 lower road B 1st lift above liner	20.5	6.5	100.0	A	122.8	10.0
16 I	line 4 lower road B 1st lift above anchor trench	20.5	4.6	93.8	В	122.8	10.0
	line 1 lower road B 1st lift above liner	19.5	6.2	99.7	Ā	122.8	10.0
	line E-5 lower road 1st lift above liner	15.5	7.0	97.7	A	122.8	10.0
							. 5.0

During Construction Loamy Soil Testing - Field Compaction Tests

Pelham Bay Landfill Closure and Final Remediation

Test			Water	Percent	0	Maximum Density	Optimum Moisture				
No.	Location	Elev.	Content %	Compactiion	Comment	(#/cu.ft.)	(%)				
3" Minus: Roadway (September 15, 1995) (continued)											
	line E-3 lower road 1st lift line E-0.5 lower road 1st lift	16.5 24.5	8.7 7.4	98.0 100.1	Α .	122.8 122.8	10.0 10.0				
-	mile E die letter rede Tet int		'	100.1	,,	122.0	10.0				
100 M 400 M	Slope Drain	- Loamy (S	eptember 21	1995)							
_											
1	80' north MHSP 10	70	8.2	95.1	A	121.9	12.1				
8	MHSP 11	63	6.8	97.8	Α	121.9	12.1				
Loamy; Slope Drain Pond C (September 29, 1995)											
- CONTRACTO	A Marian (1996) Standard Marian (1996) Control of the Control of t		TOWN	and the second s							
	1st lift above down slope drain between					ļ					
13	SP10-SP11	82.0'	11.3	95.0	Α	121.9	10.0				
	2nd lift above down slope drain between	0.4.01		20.5		440.5					
14	SP10-SP11	84.0'	4.7	99.2	Α	112.3	9.6				
1342	Loamy: Ro	L Dadways (Se	eotember 29	1995)			e A Control				
200				200 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Land Land Control						
5	upper road B, station A62 / STA 107+00	70.0'	2.8	96.4	Α	112.3	9.6				
6	upper road B, station A61 / STA 105+00	72.0'	4.5	95.6	Α	112.3	9.6				
7	upper road B, station A59.5	73.0'	3.5	100.2	Α	112.3	9.6				
8	upper road B, station F8.5 / STA 104+00	74.0'	5.7	98.4	Α	112.3	9.6				
9	upper road B, station F7/ STA 103+00	74.0'	3.2	97.7	Α	112.3	9.6				
1	Road C, station F7 / STA 6+00	97.0'	7.6	98.6	Α	116.2	8.7				
11	Road C, station F8 / STA 4+00	95.0'	9.9	99.1	Α	116.2	8.7				
4,160,000,000	Loamy: Slope	Design Done	I C (Ontoboe	(2:400E)	S#1 #		Washing Zing San Jan				
western .	Evally, Stope	Diani Fond		Z, 199 5) 	aluba of medical	ATTEMPT TO	N AMOUND A				
6	30' ne of MH SP#11	66	7.0	95.6	Α	112.3	9.6				
	160' ne of MH SP#11	48	6.8	96.2	A	112.3	9.6				
8	10' sw of B.O. #4	10	7.1	91.2	В	112.3	9.6				
8A	Retest of #8	10	6.2	97.1	С	112.3	9.6				
o Talmina hali	Company of the Compan		120 Tr. 1 2 302//2		27 year 82 72 0 370. Oa	-73	12-00-10-10-1				
1.102	Loamy I	Road A (Nov	ember 28, 19	95) 🔄 📆 🙀	MINDA SE	Stell man and a first					
12	Loamy Road A line A-69	12	10.6	93.9	Α	122.8	10.0				
13	Loamy Road A line A-68	12	12.3	100.0	A	122.8	10.0				
14	Loamy Road A line A-67	12	13.4	94.8	Ä	122.8	10.0				
15	Loamy Road A line A-65	12	17.2	91.8	Â	122.8	10.0				
16	Loamy Road A line A-64	12	15.4	91.9	A	122.8	10.0				
- MALAL	Loamy	on Roads (I	March 28, 199	96)			774445				
1 1	Road A station 15+00	subgrade	11.2	96.3	Α	125.0	9.0				
2	Road A station 13+00	subgrade	9.8	99.3	A	125.0	9.0				
	Road A station 11+00	subgrade	9.9	98.2	Α	125.0	9.0				
4	Road A station 9+00	subgrade	10.1	96.4	A	125.0	9.0				

Prepared by: B. Magliaro/S. Albrecht Checked by: S. Albrecht 6/22/99

During Construction Loamy Soil Testing - Field Compaction Tests

Pelham Bay Landfill Closure and Final Remediation

						Maximum	Optimum
Test			Water	Percent		Density	Moisture
No.	Location	Elev.	Content %	Compactiion	Comment	(#/cu.ft.)	(%)
	Loamy on Ro	ads (March	28, 1996) (00	ntinued) 🛴 🏢	。 建	1. 1	AA
5	Road A station 7+00	subgrade	6.8	99.8	Α	125.0	9.0
6	Road A station 5+00	subgrade	5.0	97.2	Α	125.0	9.0
7	Road A station 3+00	subgrade	8.9	97.5	Α	125.0	9.0
8	Road A station 1+00	subgrade	8.6	95.9	Α	125.0	9.0
9	Road B station 1+00; 1st lift	subgrade	7.8	99.5	Α	125.0	9.0
10	Road B station 3+00; 1st lift	subgrade	8.7	98.2	Α	125.0	9.0
11	Road B station 5+00; 1st lift	subgrade	8.1	97.3	Α	125.0	9.0
12	Road B station 7+00; 1st lift	subgrade	6.3	96.9	Α	125.0	9.0
13	Road B station 9+00; 1st lift	subgrade	8.1	97.5	Α	125.0	9.0
14	Road B station 11+00; 1st lift	subgrade	4.8	96.8	Α	125.0	9.0
15	Road B station 13+00; 1st lift	subgrade	9.6	95.3	Α	125.0	9.0
16	Road B station 15+00; 1st lift	subgrade	8.1	96.9	Α	125.0	9.0
an finish only		la l	40000		Carlotta (Sara)	- Spiritus val all and a second	
15.00	Loar I	ny Roads (i 	//ay 10, 1996) 		the later and when		
1	Road B station 107+00	1	7.3	105.1	Α	see Procto	or Reports
2	Road B station 105+00	1	9.7	100.2	Α	dated 5	5/14/96
3	Road B station 101+00	4	10.5	101.1	Α		" "
4	Road B station 99+00	3	10.1	103.6	Α	" "	
5	Road B station 97+00	4	13.1	97.9	В	" "	* *
6	Road B station 95+00	3	12.3	102.6	Α		
7	Road B station 73+00	4	12.5	94.3	В	" "	" "
8	Road B station 71+00	3	12.0	98.2	Α	" "	" "
9	Road B station 69+00	4	11.9	94.1	В	" "	" "
10	Road B station 67+00	3	12.6	97.7	В	" "	* *
11	Road B station 65+00	1	8.8	102.8	Α	" "	" "
12	Road B station 63+00	1	7.8	104.6	Α		* *
13	Road B station 61+00	1	7.6	104.8	Α		" "
14	Road B station 59+00	1	7.1	103.2	Α	" "	" "
15	Road B station 57+00	1	7.6	100.7	Α		" "
16	Road B station 55+00	1	6.7	101.4	Α	" "	" "
17	Road B station 61+00*	1	6.3	100.4	Α	" "	
18	Road B station 59+00*	1	7.7	103.2	A	" "	** **
19	Road B station 57+00*	1	8.1	101.4	Α	* "	" "
20	Road B station 55+00*	1	7.2	104.1	Α	" "	" "
	*should be Lift 3 from 95+00 to 101+00					" "	" "
ı	Road B station 53+00	1	6.7	99.6	Α	" "	" "
	Road B station 51+00	1	9.5	94.7	В	" "	" "
	Road B station 37+00	1	6.6	96.8	A	" "	" "
	Road B station 1+00	4	6.8	102.9	Α	" "	" "
	Road B station 11+00 (?1+00)	3	7.0	105.2	A	" "	" "
26	Road B station 3+00	4	10.6	99.7	Α	" "	" "
27	Road B station 3+00	3	9.9	103.3	Α	" "	* *
28	Road B station 5+00	4	10.3	98.2	Α	" "	n n
	Road B station 5+00	3	8.1	105.8	Α	" "	* "
30	Road B station 7+00	4	10.0	93.2	В	" "	" "

During Construction Loamy Soil Testing - Field Compaction Tests

Pelham Bay Landfill Closure and Final Remediation

Test No.	Location	Elev.	Water Content %	Percent Compactiion	Comment	Maximum Density (#/cu.ft.)	Optimum Moisture (%)
	Loamy on R	oads (May	10, 1996) (cor	ntinued)			
31	Road B station 7+00	3	8.5	106.2	Α.	" "	и н
32	Road B station 9+00	4	9.4	104.7	Α	" "	" "
33	Road B station 11+00	4	8.9	100.8	Α	" "	* "
34	Road B station 11+00	3	8.0	107.1	Α	" "	* *
35	Road B station 13+00	4	14.0	94.8	В	" "	* *
36	Road B station 13+00	3	15.3	99.4	Α	" "	" "
37	Road B station 15+00	4	11.8	96.8	В	" "	* *
38	Road B station 15+00	3	12.2	99.8	Α	" "	* "
39	Road B station 17+00	4	12.8	93.2	В	" "	" "
40	Road B station 17+00	3	13.2	101.3	Α	" "	" "
41	Road B station 19+00	4	14.7	96.1	Α		
42	Road B station 19+00	3	12.7	105.7	Α	* *	* *
43	Road B station 21+00	4	13.9	99.1	Α	H H	* *
44	Road B station 21+00	3	14.2	102.9	Α		
	en was recommended to be a series	May 29,	1996		Con. Wi		destar?
	station 1+00	lift 3	6.3	107.6	A	117.0	10.3
	station 1+00	lift 4	6.3	92.3	В	117.0	10.3
3	station 7+00	lift 3	5.3	110.3	A	117.0	10.3
4	station 9+00	lift 3	4.8	107.7	A	117.0	10.3
5	station 13+00	lift 3	7.7	101.6	/ A	117.8	11.4
6	station 15+00	lift 3	6.3	104.2	A	117.8	11.4
7	station 17+00	lift 3	6.1	106.6	Α	117.8	11.4
8	station 19+00	lift 3	5.4	104.8	A	117.8	11.4
9	station 23+00	lift 3	6.4	115.0	Α	110.8	10.4
10	station 23+00	lift 4	8.2	106.5	Α	110.8	10.4
11	station 25+00	lift 3	6.5	115.3	Α	110.8	10.4
	station 25+00	lift 4	6.3	108.1	Α	110.8	10.4
	station 27+00	lift 3	9.2	104.7	Α	110.8	10.4
	station 27+00	lift 4	9.9	98.4	A	110.8	10.4
	station 29+00	lift 3	7.8	111.5	Α	110.8	10.4
	station 29+00	lift 4	8.2	108.3	Α	110.8	10.4
	station 31+00	lift 3	5.8	94.6	! *	124.1	11.3
	station 31+00	lift 4	5.8	96.8	.	124.1	11.3
	station 33+00	lift 3	8.1	95.*		124.1	11.3
	station 33+00	lift 4	8.6	9*.*	*	124.1	11.3
	station 35+00	lift 3	7.4	*	*	124.1	11.3
	station 35+00	lift 4	7.7	*		124.1	11.3
,	station 37+00	lift 3	5.8	*	· ·	124.1	11.3
	station 37+00	lift 4	7.?	*	٠ ا	124.1	11.3
	station 39+00	lift 3	7.5	96.1	В	124.1	11.3
	station 39+00	lift 4	7.1	98.6	A	124.1	11.3
27	station 41+00	lift 3	7.6	100.2	A	124.0	8.5
28	station 41+00	lift 4	7.5	94.4	В	124.0	8.5
29	station 43+00	lift 2	5.1	95.4	В	124.0	8.5

During Construction Loamy Soil Testing - Field Compaction Tests

Pelham Bay Landfill Closure and Final Remediation

Test No.	Location	Elev.	Water Content %	Percent Compactiion	Comment	Maximum Density (#/cu.ft.)	Optimum Moisture (%)
7.43	Maria de la companya	ay 29, 1996	(continued)	ta a sa	ena Lindson	قىدىن ئ	Liker only &
20	etation 42 : 00	lift 3	5 2	98.0	Λ .	124.0	8.5
	station 43+00	lift 2	5.3 4.7	103.5	A A	124.0	8.5
31 32	station 45+00 station 46+00	lift 3	5.0	99.4	A	124.0	8.5
33	station 47+00	lift 2	5.2	104.7	Â	124.0	8.5
34	station 47+00	lift 3	4.5	109.5	A	124.0	8.5
35	station 49+00	lift 2	6.6	95.6	В	124.0	8.5
36	station 49+00	lift 3	8.3	99.4	A	119.2	9.6
37	station 51+00	lift 3	7.7	100.2	Ä	119.2	9.6
38	station 53+00	lift 2	6.9	107.7	A	119.2	9.6
39	station 53+00	lift 3	7.7	103.5	A	119.2	9.6
40	station 55+00	lift 2	7.7	103.6	A	119.2	9.6
41	station 55+00	lift 3	8.8	97.1	В	119.2	9.6
42	station 57+00	lift 2	5.5	102.2	Ā	119.2	9.6
43	station 57+00	lift 3	5.5	98.7	Α	119.2	9.6
44	station 59+00	lift 2	5.3	108.7	Α	119.2	9.6
45	station 59+00	lift 3	5.5	103.6	Α	119.2	9.6
46	station 61+00	lift 2	4.3	108.2	Α	120.2	12.8
47	station 61+00	lift 3	5.6	106.8	Α	120.2	12.8
48	station 63+00	lift 3	5.4	108.6	Α	120.2	12.8
49	station 63+00	lift 3	5.7	105.5	Α	120.2	12.8
50	station 65+00	lift 2	5.8	111.6	Α	120.2	12.8
51	station 65+00	lift 3	6.3	107.3	Α	120.2	12.8
52	station 67+00	lift 2	5.7	105.2	Α	120.2	12.8
53	station 67+00	lift 3	6.3	102.0	Α	120.2	12.8
54	station 69+00	lift 2	6.1	99.6	Α	120.2	12.8
55	station 69+00	lift 3	6.2	100.0	Α	120.2	12.8
56	station 71+00	lift 3	6.4	103.2	Α	119.7	12.5
57	station 71+00	lift 4	7.6	100.5	Α	119.7	12.5
58	station 73+00	lift 3	6.9	108.8	Α	119.7	12.5
59	station 73+00	lift 4	8.1	106.0	Α	119.7	12.5
60	station 75+00	lift 3	6.9	102.8	Α	119.7	12.5
61	station 75+00	lift 4	6.8	93.5	В	119.7	12.5
62	station 77+00	lift 3	5.5	102.4	Α	119.7	12.5
63	station 77+00	lift 4	6.7	98.9	Α	119.7	12.5
64	station 79+00	lift 3	7.1	100.9	Α	119.7	12.5
65	station 79+00	lift 4	7.3	93.3	В	119.7	12.5
	station 91+00	lift 3	8.6	103.0	A	119.7	12.5
	station 91+00	lift 4	11.0	96.3	В	119.7	12.5
l	station 81+00	lift 3	7.7	94.7	В	123.8	10.7
69	station 81+00	lift 4	8.3	93.9	В	123.8	10.7

COMMENTS:

- A. Test results comply with specifications
- B. Recompaction required
- C. Test is after recompaction

Prepared by: B. Magliaro/S. Albrecht Checked by: S. Albrecht 6/22/99

^{*} Values to be provided by NYCDEP

APPENDIX E TOPSOIL TESTING

- E-1 Topsoil Testing pH, TOC, Grain Size Analysis
- E-2 Topsoil Testing Nutrient Analysis
- E-3 Topsoil Analysis pH Adjustment

E-1 Topsoil Testing – pH, TOC, Grain Size Analysis

1.

Lab ID	TCLI							
LAB#	FVG-001							
Report#	MC-44	MC-43	MC-42	MC-41	MC-40	MC-39	MC-38	MC-37
Sample ID	061801	061701	061501	061201	061101	061001	060901	060801
Sample Date	06/18/98	06/17/98	06/15/98	06/12/98	06/11/98	06/10/98	06/09/98	06/08/98
pН	6.8	7.2	6.7	6.8	6.3	6.5	7.2	6.9
TOC*	6.0%	7.7%	7.7%	7.9%	7.0%	8.4%	5.7%	6.4%

Graiı	n Size	Anal	vsis

| | | | | | | | | | | |

	Percent							
Seive Size	Passing (%)							
1"				100.0		100.0	100.0	_
3/4"		100.0	100.0	98.4	100.0	98.5	99.0	100.0
1/2"	100.0	98.8	99.5	97.9	98.7	93.5	96.9	98.7
3/8"	99.2	96.4	99.5	97.2	96.6	90.8	94.3	96.9
1/4"	96.7	92.6	97.7	95.1	93.5	87.3	90.8	93.9
#4	94.1	89.6	95.8	93.1	91.0	84.6	88.5	91.7
#8	85.8	81.4	90.6	88.2	84.3	79.8	83.3	84.7
#1 0	83.6	80.2	88.7	86.4	82.2	78.1	81.9	83.2
#16	77.7	72.4	81.9	81.7	75.5	72.6	78.4	75.5
#2 0	73.8	68.0	76.6	78.1	70.7	69.5	72.9	71.3
#3 0	68.5	62.6	69.6	73.0	64.0	64.3	67.0	62.9
#3 5	66.1	61.4	67.7	71.7	63.0	63.0	66.1	62.6
#40	61.9	57.8	62.8	67.8	58.9	58.5	61.1	59.2
#50	56.6	51.4	55.1	61.4	52.0	51.6	55.6	52.1
#6 0	51.6	47.3	49.4	58.6	47.0	46.8	50.8	47.1
#8 0	43.3	40.0	44.0	49.0	39.6	39.9	43.3	39.3
#100	38.3	35.5	35.7	44.0	34.9	35.5	38.8	34.7
#200	21.0	21.5	19.8	27.4	20.6	22.2	22.9	21.6
#270	14.4	15.1	12.8	19.7	14.3	16.6	12.1	16.3

Lab ID	TCLI							
LAB#	FVG-001							
Report#	MC-36	MC-35	MC-34	MC-33	MC-32	MC-30	MC-31	MC-29
Sample ID	060501	060401	060301	060201	060101	052901	0529PB	052801
Sample Date	06/05/98	06/04/98	06/03/98	06/02/98	06/01/98	05/29/98	05/29/98	05/28/98
рH	6.9	7.0	7.4	6.8	6.8	7.1	7.0	6.6
TOC*	6.7%	6.9%	7.2%	4.8%	7.1%	7.3%	10.6%	6.6%
Grain Size Analys	i							
	Percent							
Seive Size	Passing (%)							
1"			-			100.0	100.0	
3/4"	100.0	100.0	100.0	100.0	100.0	99.8	98.4	100.0
1/2"	99.4	95.7	96.8	98.9	98.6	98.2	93.6	98.7
3/8"	97.0	92.5	96.0	98.2	98.0		90.8	96.6
1/4"	92.7	89.4	92.9	96.3	95.1	92.0	87.7	93.4
#4	89.7	86.9	90.8	94.6	92.1	90.8	86.1	91.8
#8	82.6	71.3	85.1	88.8	85.7	84.7	82.2	86.2
#1 0	80.9	80.1	83.9	87.3	84.4	83.6	81.1	85.4
#1 6	75.2		78.7	81.0	79.7	79.7	76.8	80.2
#2 0	71.1	71.0		77.8				76.5
#3 0	64.8		68.9	70.7	70.7			
#3 5	63.8	63.2	63.4	70.5	69.9	71.1	65.9	
#40	51.9		56.0	67.1	66.0	65.6		
#5 0	47.7	51.1	53.2	59.8				54.8
#6 0	44.1	48.1	51.6			I	I	I I
#80	40.2	39.0	43.2	45.9				I
#100	33.8		37.6		40.1	I		
#200	20.0		22.3	23.9		30.7		
#270	14.8	17.0	17.2	17.2	17.3	23.8	17.2	19.9

Prepared By: K. Petruzzelli Checked By: S. Albrecht 6/18/98

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Lab ID	TCLI							
LAB#	FVG-001							
Report#	MC-28	MC-27	MC-24	MC-25	MC-26	MC-23	MC-22	MC-20
Sample ID	052701	052201	052001	052002	052003	0501801	0501401	0501201
Sample Date	05/27/98	05/22/98	05/20/98	05/20/98	05/20/98	05/18/98	05/14/98	05/12/98
pH	6.	8 7.2	6.8	6.5	6.9	6.9	6.9	6.4
TOC*	7.29	6.2%	5.7%	3.6%	6.7%	5.6%	4.9%	5.2%

Grair	Size	Analy	VS
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(11 1 1 11)

1	Percent							
Seive Size	Passing (%)							
1"	100.0	100.0	_		100.0			
3/4"	99.6	97.0	100.0		97.6	100.0	100.0	100.0
1/2"	97.4	95.7	99.0	100.0	95.7	99.4	99.2	97.7
3/8"	96.3	93.4	99.0	99.8	94.9	97.6	98.6	97.1
1/4"	93.5	91.0	97.4	99.0	93.2	94.6	96.8	95.4
#4	91.5	88.7	96.2	98.2	92.1	93.1	95.5	94.1
#8	85.6	84.1	92.1	94.9	87.9	88.6	92.4	90.4
#10	83.6	82.8	90.4	93.5	86.4	87.2	91.3	89.2
#16	76.6	78.2	84.9	88.8	81.8	82.0	87.9	85.5
#20	72.2	74.8	80.5	85.4	78.4	77.8	85.2	82.7
#3 0	68.5	69.6	74.5	80.4	73.6	71.9	80.1	78.5
#3 5	66.9	68.3	72.5	78.6	72.1	70.0	79.2	76.9
#40	62.5	64.3	67.7	74.5	68.1	66.7	75.6	73.4
#5 0	57.4	57.9	59.9	67.6	61.7	58.9	69.9	67.7
#60	53.5	53.5	54.2	62.3	57.0	54.0	65.6	63.6
#80	43.5	46.1	45.1	53.3	48.8	46.1	58.4	56.4
#10 0	38.9	41.7	39.6	47.6	43.7	41.3	53.3	51.7
#200	32.0	26.8	31.3	28.3	26.7	26.4	35.4	34.2
#270	24.0	20.0	19.8	20.6	19.2	17.6	26.5	26.7

Lab ID	TCLI							
LAB#	FVG-001							
Report#	MC-21	MC-19	MC-18	MC-17	MC-16	MC-15	MC-14	MC-13
Sample ID	0501202	050701	050501	050101	042801	042401	042101	041701
Sample Date	05/12/98	05/07/98	05/05/98	05/01/98	04/28/98	04/24/98	04/21/98	04/17/98
рН	6.5	6.6	6.9	7.0	6.4	6.2	6.7	6.2
Tod*	4.6%	5.3%	4.5%	6.4%	6.6%	5.0%	6.2%	4.9%

Grain	Size	Ana	hvei
Grair	ı əize .	Ana	VSI

Grant	ant Size Analysi									
		Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	
Seive	Size	Passing (%)	Passing (%)	Passing (%)	Passing (%)					
1"						100.0				
3/4"		100.0	100.0	100.0	100.0	98.3	100.0	100.0		
1/2"		99.5	98.0	99.2	97.4	95.3	98.9	97.5	100.0	
3/8"		98.9	96.9	98.2	96.2	94.4	96.3	96.6	99.5	
1/4"		96.3	94.9	95.1	94.2	92.9	94.0	94.8	96.0	
#4	J	94.6	93.2	93.8	92.7	91.4	92.3	92.9	93.7	
#8		90.1	89.2	89.1	88.4	86.7	87.9	88.6	88.7	
#10		89.0	88.0	88.0	87.0	85.0	86.5	87.3	87.0	
#16		85.3	84.1	83.5	82.9	79.4	82.8	83.3	80.5	
#2 0		82.3	80.1	79.9	79.8	74.7	79.4	80.2	76.1	
#3 0		77.7	75.9	74.8	75.8	68.0	75.6	75.7	70.4	
#35		76.8	74.5	73.9	73.7	66.2	72.6	73.9	68.4	
#4 0		71.8	70.1	70.1	70.0	60.0	69.2	70.1	64.0	
#5 0		65.2	64.0	83.8	63.9	53.2	63.0	63.8	57.3	
#6 0		60.4	59.3	59.3	59.5	47.9	58.5	59.3	52.6	
#8 0		52.7	51.7	51.8	52.0	39.8	51.1	51.5	45.1	
#10 0		47.9	46.8	46.9	47.2	34.9	46.5	46.7	40.5	
#2 0 0		31.3	29.7	29.5	30.2	20.5	30.6	30.2	25.5	
#270		23.5	22.7	21.9	22.2	<u>1</u> 3.1	23.2	23.0	19.5	

Lab ID	TCLI	TCLI	TCLI	TCLI	ITL	TCLI	TCLI	TCLI
LAB#	FVG-001	FVG-001	FVG-001	FVG-001			FVG-001	FVG-001
Report#	MC-12	MC-10	MC-11	MC-09			MC-08	MC-07
Sample ID	041401	041001	041002	040801	040601	040301	033101	033102
Sample Date	04/14/98	04/10/98	04/10/98	04/08/98	04/06/98	04/03/98	03/31/98	03/31/98
pН	6.2	6.5	6.4	6.0	7.4	7.0 / 7.7	6.7	6.4
TOC*	6.1%	5.6%	3.7%	5.7%	3.8%	2.3% / 2.6%	3.8%	3.9%
Grain Size Analys	i		_			_		
	Percent							
Seive Size	Passing (%)							

	Percent							
Seive Size	Passing (%)							
1"	100.0	100.0	100.0	100.0			100.0	100.0
3/4"	100.0	100.0	97.7	100.0			100.0	99.8
1/2"	100.0	98.7	96.4	97.9	100.0	100.0	98.7	99.2
3/8"	99.9	96.7	95.6	94.4	97.9	99.1	96.6	96.9
1/4"	97.8	93.4	93.9	91.1			93.5	93.8
#4	96.6	90.0	91.8	88.6	95.7	95.7	91.3	92.0
#8	89.5	82.2	86.7	83.1			85.6	86.2
#10	88.4	80.2	85.0	80.3	90.0	89.9	84.0	84.2
#16	82.8	75.1	79.4	71.9	85.5	86.2	78.7	78.8
#20	77.2	71.6	75.2	65.2			74.7	74.3
#3 0	70.0	65.8	69.4	56.9		,	68.4	67.8
#3 5	69.3	64.6	87.5	54.3			67.6	66.2
#4 0	65.7	60.3	63.2	49.8	70.0	73.0	64.3	62.9
#5 0	58.7	53.3	58.2	43.0	63.5	66.9	57.8	56.2
#60	53.9	48.2	51.1	38.5			52.3	50.8
#8 0	46.1	40.0	42.7	31.4			44.7	42.5
#100	41.3	35.1	37.7	27.3	46.0	49.8	39.3	37.3
#200	26.6	20.6	23.0	15.5	33.8	35.5	22.8	21.4
#270	20.3	14.3	17.0	10.3			17.1	14.4

Prepared By: K. Petruzzelli Checked By: S. Albrecht 6/18/98

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	FELIAM BAT EARDITEE GEOSORE AND THAT REMEDIATION											
Lab ID	TCLI	TCLI	TCLI	TCLI	TCLI	TCLI	ITL	ITL				
LAB#	FVG-001	FVG-001	FVG-001	FVG-001	FVG-001	FVG-001						
Report#	MC-08	MC-01	MC-02	MC-03	MC-04	MC-05						
Sample ID	033103	032501	032502	032503	032504	032505	030401	030201				
Sample Date	03/31/98	03/25/98	03/25/98	03/25/98	03/25/98	03/25/98	03/04/98	03/02/98				
рН	6.5	6.8	6.1	7.2	7.3	6.5	6.7	7.3				
TOC*	3.8%	7.5% / 1.9% ⁽¹⁾	6.3%	8.5%	9.8%	6.6%	7.2%	4.3%				
Grain Size Analys	si											
	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent				
Seive Size	Passing (%)	Passing (%)	Passing (%)	Passing (%)	Passing (%)	Passing (%)	Passing (%)	Passing (%)				
1"	100.0	100.0	100.0	100.0	100.0	100.0						
3/4"	100.0	100.0	100.0	100.0	100.0	100.0						
1/2"	99.5	98.7	99.5	98.9	98.1	100.0	100.0	100.0				
2/01	1 000		20.0	l 000	07.5	4000	07.0	1 00.2				

Seive Size	Passing (%)							
1"	100.0	100.0	100.0	100.0	100.0	100.0		
3/4"	100.0	100.0	100.0	100.0	100.0	100.0		
1/2"	99.5	98.7	99.5	98.9	98.1	100.0	100.0	100.0
3/8"	98.6	98.2	98.9	98.0	97.5	100.0	97.6	99.3
1/4"	95.9	96.1	97.7	96.0	95.0	99.5		
#4	95.1	95.0	96.3	94.0	93.5	98.4	93.4	93.1
#8	90.2	94.4	91.2	88.8	88.8	94.1		
#10	88.8	90.7	89.8	87.4	87.2	92.6	88.1	86.8
#16	83.6	87.8	84.1	83.0	83.1	87.8	83.9	83.2
#20	80.4	85.7	80.2	76.0	80.0	84.6		
#3 0	75.8	82.5	75.3	70.5	76.2	79.7		
# 3 5	74.4	80.1	71.8	68.6	73.7	78.1		
#40	71.3	78.2	68.4	66.7	70.6	75.1	68.1	70.8
#5 0	65.8	73.0	61.5	62.7	64.4	66.9	60.8	65.1
#6 0	61.0	68.8	56.9	59.5	60.0	64.4		
#8 0	53.7	61.2	49.1	51.5	52.3	51.5		
#10 0	48.6	55.8	44.7	46.6	47.3	46.7	43.6	49.6
#200	30.3	36.0	29.7	29.4	30.8	34.5	23.8	26.9
#270	23.0	28.5	23.4	23.3	23.8	28.7		

Lab ID	ITL	ITL	ITL	ITL	ITL	ITL	ITL	ITL
LAB#								
Report#								
Sample ID	022301		021901	021902	021701			021101
Sample Date	02/23/98		02/19/98	02/19/98	02/17/98			02/11/98
pН	7.1	7.3					I	7.4
TOC*	4.9%	6.4%	6.3%	3.3% ⁽²⁾	9.3%	8.9%	13.1%	10.2%
Grain Size Analys		_		_				
} _	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent
Seive Size	Passing (%)	Passing (%)	Passing (%)	Passing (%)	Passing (%)	Passing (%)	Passing (%)	Passing (%)
1"					100.0			
3/4"	100.0	100.0	100.0		97.4	100.0	100.0	100.0
1/2"			99.2	100.0	97.4	98.8	100.0	98.4
3/8"	95.2	99.7	97.0	99.3	96.2	97.4	96.9	97.2
1/4"								
#4	90.5	95.5	89.0	96.3	92.3	93.0	91.6	92.5
#8								
#10	69.0	79.3	76.0	88.5	85.0	85.7	83.9	85.1
#16	63.4	64.1	72.7	84.2	79.9	81.1	79.5	74.2
#20			_					
#30								
#35								
#40	38.8	39.2	61.5	69.5	63.0	65.7	65.6	45.8
#50	30.2	30.7	56.2	62.5	55.8	57.9	59.3	37.9
#60		-		_				
#80								
#100	18.4	18.9	42.8	48.1	38.7	41.6	43.5	23.8
#200	12.9	I	25.8			29.3	29.3	13.7
#270								

Prepared By: K. Petruzzelli Checked By: S. Albrecht 6/18/98

4 1 1 L

Lab	D	ITL						
LAB#	‡							
Repo	ort#							
Sam	ple ID	021001	020901	020601	020602	020603	#1	#2
Sam	ple Date	02/10/98	02/09/98	02/06/98	02/06/98	02/06/98	02/16/98	02/16/98
pН		7.4	7.3	6.7	7.4	7.5		_
TOO	*	10.5%	6.2%	5.5%	13.5%	7.9%		

Grair	Size	Ana	lysi
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	Percent						
Seive Size	Passing (%)						
1"				_		100.0	100.0
3/4"		98.9		100.0	100.0	98.1	99.1
1/2"	100.0	97.9	100.0	98.0	96.1	96.4	95.1
3/8"	98.1	95.4	98.3	95.5	95.1	95.3	92.5
1/4"							
#4	93.4	89.9	94.2	91.2	90.7	92.0	87.9
#8							
#10	83.2	81.6	87.9	85.0	84.4	86.3	81.9
#16	70.8	69.9	83.2	81.0	79.9	82.0	77.9
#20			,				
#30							
#35							
#40	35.9	30.8	65.7	65.5	63.5	64.6	
#50	31.2	24.6	58.1	58.6	56.3	56.6	56.5
#60							
#80							
#10 0	18.1	13.8	40.9	42.9	40.5	38.5	41.0
#200	10.7	9.5	29.6	31.9	30.0	26.3	29.1
#270				_			

Notes:

^{*} TOC = Total Organic Carbon

⁽¹⁾ Original result 7.5%, 1.9% on re-test

⁽²⁾ This is an increase in weight of soil, therefore Total Organic Content by this method (ASTM D-2974), is not possible.

E-2 Topsoil Testing – Nutrient Analysis

TOPSOIL ANALYSIS - pH ADJUSTMENT PELHAM BAY LANDFILL CLOSURE AND FINAL REMEDIATION

			SAMPLE DATE		ATE		SAMPLI	E DATE
			8/25/97	9/2/97	9/15/97		10/2	?/97
		DATE OF FIRST				DATE OF SECOND	- DU	CO3
AREA#	ACREAGE	SULFUR APPLICATION		pН		SULFUR APPLICATION	рН	003
1	1.6	7/29	7.5		7.8		7.5	6.22
2	1.8	7/28	7.8	8.2	8.1		7.8	2.93
3	2.5	7/28	7.8	8.4			7.5	5.44
4	3.0	7/28	7.9	7.9	9.4		7.8	3.38
5	3.0	7/28-7/29	8.6	8.1	9.8		7.9	4.17
6	2.3	7/28-7/30	7.8	8.3			8.0	
7	2.8	7/28-7/29	8.0	8.0	7.4		8.4	5.49
8	2.8	7/29-8/01	8.0	7.9	8.4		7.9	
9	2.8	7/30-8/01	8.5	8.7	7.9		7.8	
10	2.8	7/30	8.1	8.6	7.5		7.9	
11	3.2	7/30	8.5	7.5	7.5		7.4	3.17
12	3.0	7/31	9.1	7.1			7.3	
13	5.3	7/31	7.8	7.7	7.6		7.6	
14	3.7	8/4,8/7	8.0	7.6	7.6		7.3	
15	4.0	8/4,8/7	8.5	8.7	7.8		7.4	
16	3.0	8/4,8/7	7.8	7.8	7.7		7.3	7.22
17	3.1	8/5,8/7	8.0	8.2			7.6	
18	3.9	8/5,8/7	7.9	8.0			7.5	
19	3.7	8/5,8/7	7.8	7.8	8.5		7.6	3.54
20	3.0	8/5,8/6	8.1	8.7/7.9	8.7		7.5	
21	4.1	8/5,8/6	7.7	7.7	7.8		7.4	
22	3.2	8/6	8.0	8.5	8.1		7.2	5.56
23	3.2	8/6	8.0	9.8	8.3		8.0	7.58
24	3.0	8/1, 8/6	7.9	8.0	9.7	}	7.7	
25	3.0	8/1, 8/6	7.9	8.5	8.3		7.7	8.87
26	4.8	8/1, 8/7	8.1	8.6	8.1		7.7	5.39
27	2.0	8/1, 8/4	7.8	7.8	8.2		7.6	7.75

E-3 Topsoil Analysis – pH Adjustment

Top Soil Nutrient Analysis Pelham Bay Landfill Closure and Final Remediation

s	Lab ID Lab# ample ID	NJAES 5576 PBTS19/8/97	NJAES 5577 PBTS1	NJAES 5579 PBTS2	NJAES 5580 PBTS39/8/97	NJAES 5578 PBTS29/8/97	NJAES 5581 PBTS3	NJAES 5716 1A1	NJAES 5717 1A2
	mple Date	9/5/97	9/5/97	9/5/97	9/5/97	9/5/97	9/5/97	9/5/97	9/15/97
Soil Test	inplo Dato	0,0,0,	0,0,0,	0,0,0,	0,0,0,	0,0,0	5,5,5	5,5,5,	0 0. 0 .
So	il Texture	sandy loam	sandy loam	sandy loam	sandy loam	sandy loam	sandy loam	sandy loam	sandy loam
5	oil pH ¹	7.5	7.6	8.2	7.3	7.9	6.8	7.8	7.8
Essential N	utrients (lbs/acre) ²								
Ph	osphorus	125	133	91 ³	125	83 ³	46 ³	86 ³	94 ³
	otassium	407	460	326	516	201 ³	147 ³	194 ³	199³
Ma	agnesium	547	511	621	446	520	220 ³	516	540
(Calcium	4093	4180	10620	5083	4019	1433 ³	3513	3758
Kjeld	ahl Nitrogen	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Trace N	utrients (ppm)⁴								
	Copper	4.9	5.2	4	3.3	3.1	1.4	2.7	2.8
Ma	anganese	49.7	48	39	73.2	61.9	108.2 ⁵	48.2	56.8
	Zinc	18.7	20.1	24.4	17.1	13.5	4.1	12.7	14.8
Α	luminum	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
	1 ro n	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

Comments:

Note:

NJAES = New Jersey Agricultural Experiment Station

CNL = Cornell Nutrient Analysis Laboratories

ITL = Independent Testing Labs

N/A = Not analyzed

? = Data not legible

¹pH 6.8 - 6.9 very slightly acidic, 7.0 neutral, 7.1 - 7.3 - very slightly alkaline; 7.4 - 8.2 moderately alkaline.

² Unless noted, values are considered very high; well above desirable range for plant growth.

³ Values are considered within the desirable range for plant growth.

⁴ Unless noted, values are considered adequate for plant growth.

⁵ Values are considered high; above range for plant growth.

⁶ Acceptability for plant growth not indicated.

Top Soil Nutrient Analysis
Pelham Bay Landfill Closure and Final Remediation

	Lab ID Lab# \$ample ID	NJAES 5718 2A1	NJAES 5719 2A2	NJAES 6485 100907	CNAL 4264-47 (H) 280410	ITL A3341-1 B7/S-5.20-22	ITL A3341-2 B7/S-4.15-17	NJAES 539 20604	NJAES 540 20605
	Sample Date	9/15/97	9/15/97	10/9/97	10/9/97	12/16/97	12/16/97	2/6/98	2/6/98
Soil Test		0, 10.0.	0, 10, 0,						
5	oil Texture	sandy loam	sandy loam	sandy loam	N/A	N/A	N/A	sandy loam	sandy loam
	Soil pH 1	7.8	7.8	8.1	7.0	N/A	N/A	7.8	7.7
Essential	Nutrients (lbs/acre) ²								
F	hosphorus	88 ³	82 ³	102	43 ³	90.7 (ppm) ⁶	83.2 (ppm) ⁶	137	218
	Potassium	187 ³	174 ³	163 ³	140 ³	241 (ppm) ⁶	223 (ppm) ⁶	845	1014
ı	Magnesium	503	481	623	840	N/A	N/A	722	909
	Calcium	3553	3374	4928	6600	N/A	N/A	9483	11735
Kje	ldahl Nitrogen	N/A	N/A	N/A	N/A	369 (ppm) ⁶	395 (ppm) ⁶	n	N/A
Trace	Nutrients (ppm)⁴								
-	Copper	2.7	2.5	3.5	N/A	N/A	N/A	11.4	23.5 ⁵
ľ	Manganese	53.9	47.5	50.8	32.0	N/A	N/A	38.4	47.5
	Zinc	11.8	11.3	18.8	?	N/A	N/A	44.4	56.2 ⁵
	Aluminum	N/A	N/A	N/A	36.0	N/A	N/A	N/A	N/A
	Iron	N/A	N/A	N/A	8.0	N/A	N/A	N/A	N/A

Comments:

Note:

NJAES = New Jersey Agricultural Experiment Station

CNL = Cornell Nutrient Analysis Laboratories

ITL = Independent Testing Labs

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¹ pH 6.8 - 6.9 very slightly acidic, 7.1 - 7.3 very slightly alkaline; 7.4 - 8.2 moderately alkaline.

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⁶ Acceptability for plant growth not indicated.

Top Soil Nutrient Analysis Pelham Bay Landfill Closure and Final Remediation

Lab ID Lab# Sample ID Sample Date	NJAES 541 20606 2/6/98	NJAES 774 21711 2/17/98	NJAES 775 21712 2/17/98	NJAES 776 21713 2/17/98
Soil Test				
Soil Texture	sandy loam	sandy loam	sandy loam	sandy loam
Soil pH ¹	7.6	7.7	7.8	7.9
Essential Nutrients (lbs/acre) ²				
Phosphorus	221	209	252	175
Potassium	1099	966	1186	987
Magnesium	981	781	934	732
Calcium	10230	7422	7286	6038
Kjeldahl Nitrogen	N/A	N/A	N/A	N/A
Trace Nutrients (ppm)4				
Copper	21.7 ⁵	4.1	5.5	3.7
Manganese	45.0	45.4	40.3	32.4
Zinc	49.3	32.3	45.1	29.6
Aluminum	N/A	N/A	N/A	N/A
Iron	N/A	N/A	N/A	N/A

Comments:

Note:

NJAES = New Jersey Agricultural Experiment Station

CNL = Cornell Nutrient Analysis Laboratories

ITL = Independent Testing Labs

N/A = Not analyzed

¹ pH 6.8 - 6.9 very slightly acidic, 7.1 - 7.3 very slightly alkaline; 7.4 - 8.2 moderately alkaline.

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⁶ Acceptability for plant growth not indicated.

APPENDIX F PHOTOS

- Photo No. 1 Construction of Concrete Slurry Wall Cap
- Photo No. 2 View of Pond B and Landfill Geomembrane Layer
- Photo No. 3 Installation of Smooth HDPE Geomembrane at Top of Landfill
- Photo No. 4 Seaming of Textured and smooth HDPE Membrane at Top of Landfill
- Photo No. 5 Detail of LFG Vent Boot
- Photo No. 6 Installation of 24" Diameter Pipe Downchute
- Photo No. 7 Geocomposite Layer
- Photo No. 8 LFG Collection Pipe Installation over Geocomposite Layer (with Geogrid Reinforcement)
- Photo No. 9 Installation of 30" Diameter HDPE Pipe Connection between Ponds B and C
- Photo No. 10- Roadway Construction
- Photo No. 11- Installation of Barrier Protection Material over Geocomposite Layer
- Photo No. 12- Covering LFG Collection Line with Barrier Protection Material
- Photo No. 13- Installation of LFG Flare Station
- Photo No. 14- Construction of Swale E
- Photo No. 15- Access Roadway and Drainage Swale
- Photo No. 16- Construction of Topsoil Layer

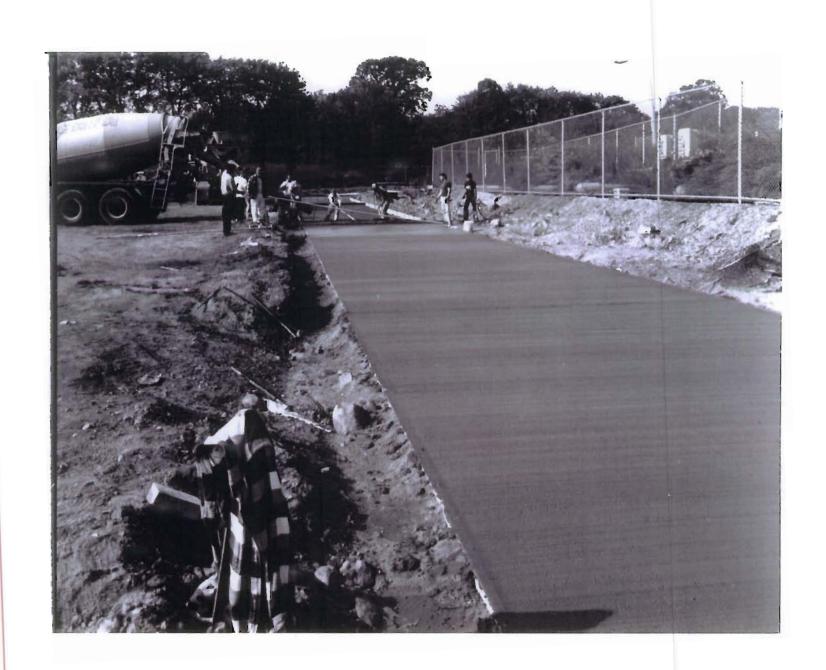


Photo No.1. Construction of Concrete Slurry Wall Cap. (October 14, 1994)



Photo No. 2. View of Pond B and Landfill Geomembrane Layer. (August 18, 1995)



Photo No. 3. Installation of Smooth HDPE Geomembrane at Top of Landfill (November 1, 1995)



Photo No. 4. Seaming of Textured and Smooth HDPE Geomembrane at Top of Landfill (September 27, 1995)



Photo No. 5. Detail of LFG Vent Boot. (May 11, 1995)



Photo No. 6. Installation of 24" Diameter Pipe Downchute. (June 7, 1995)



Photo No. 7. Geocomposite Layer. (June 26, 1995)



Photo No. 8. LFG Collection Pipe Installation over Geocomposite Layer (with Geogrid Reinforcement). (August 1, 1995)



Photo No. 9. Installation of 30" Diameter HDPE Pipe Connection between Ponds B and C. (June 7, 1995)



Photo No. 10. Roadway Construction. (June 7, 1995)



Photo No. 11. Installation of Barrier Protection Material over Geocomposite Layer.
(September 27, 1995)



Photo No. 12. Covering LFG Collection Line with Barrier Protection Material.

(July 12, 1995)



Photo No. 13. Installation of LFG Flare Station. (February 15, 1996)



Photo No. 14. Construction of Swale E. (August 21, 1996)



Photo No. 15. Access Roadway and Drainage Swale. (May 20, 1998)



Photo No. 16. Construction of Topsoil Layer. (May 20, 1998)

APPENDIX G FIGURES

G-7

G-8

G-9

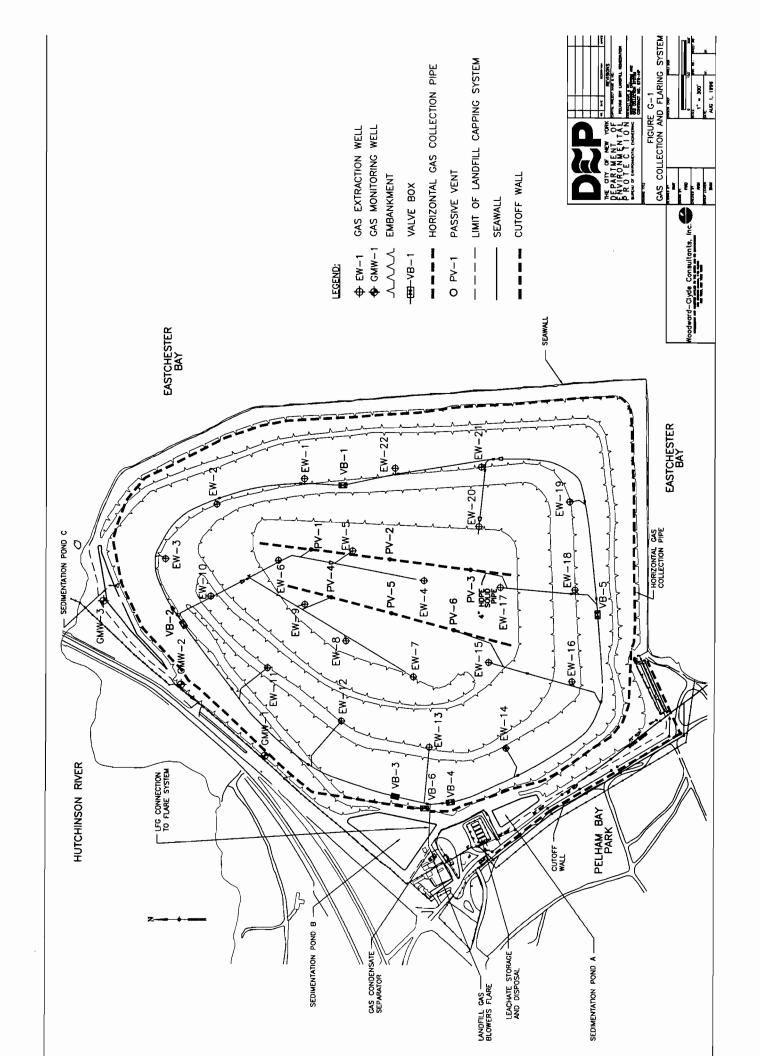
e)

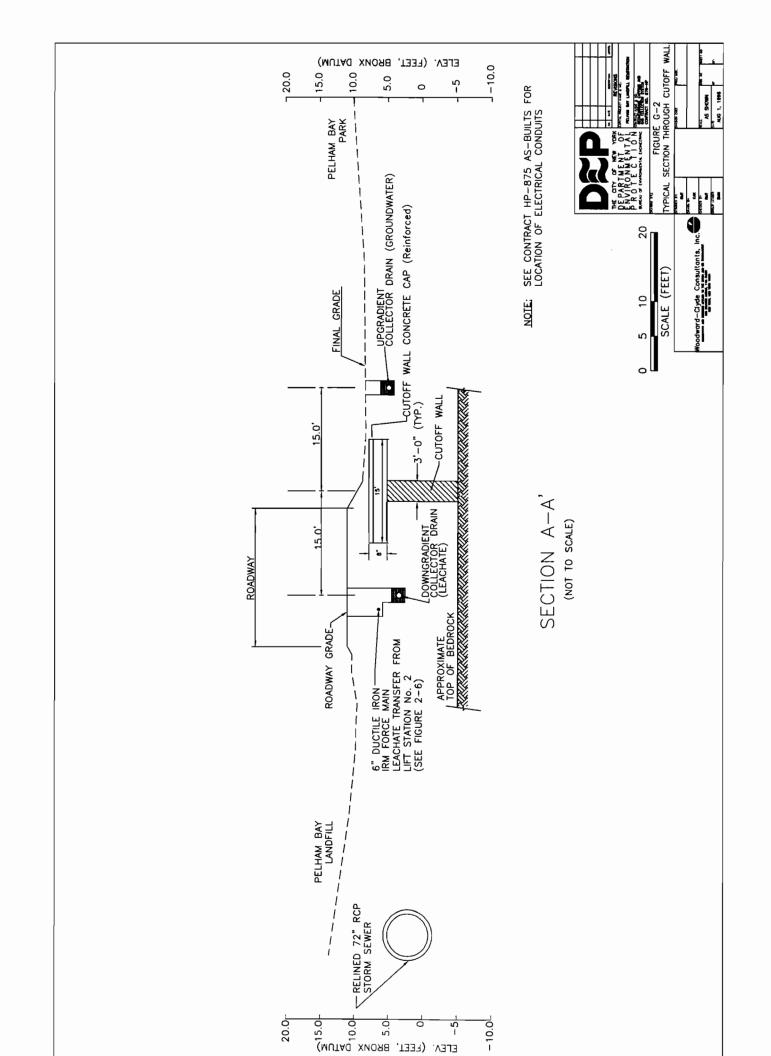
G-1	Gas Collection and Flaring System
G-2	Typical Section Through Cutoff Wall
G-3	Leachate Collection System Schematic Diagram
G-4	Stormwater Management System
G-5	Typical Landfill Cover Section
G-6	Groundwater Management System

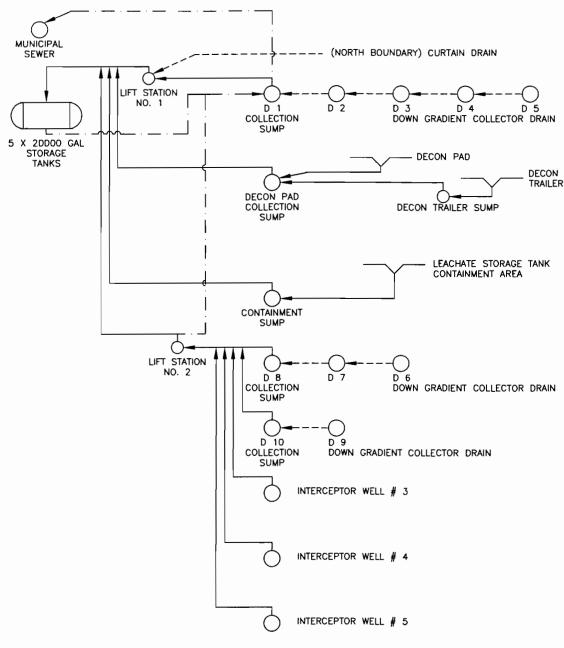
HDPE Geomembrane Panel Layout

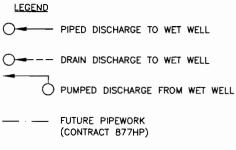
Landscape Plan

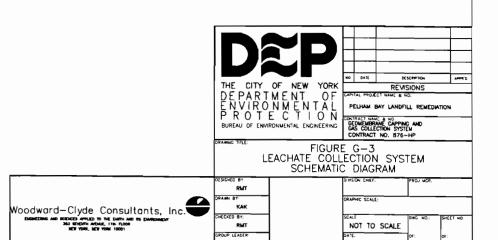
Access Roads Plan

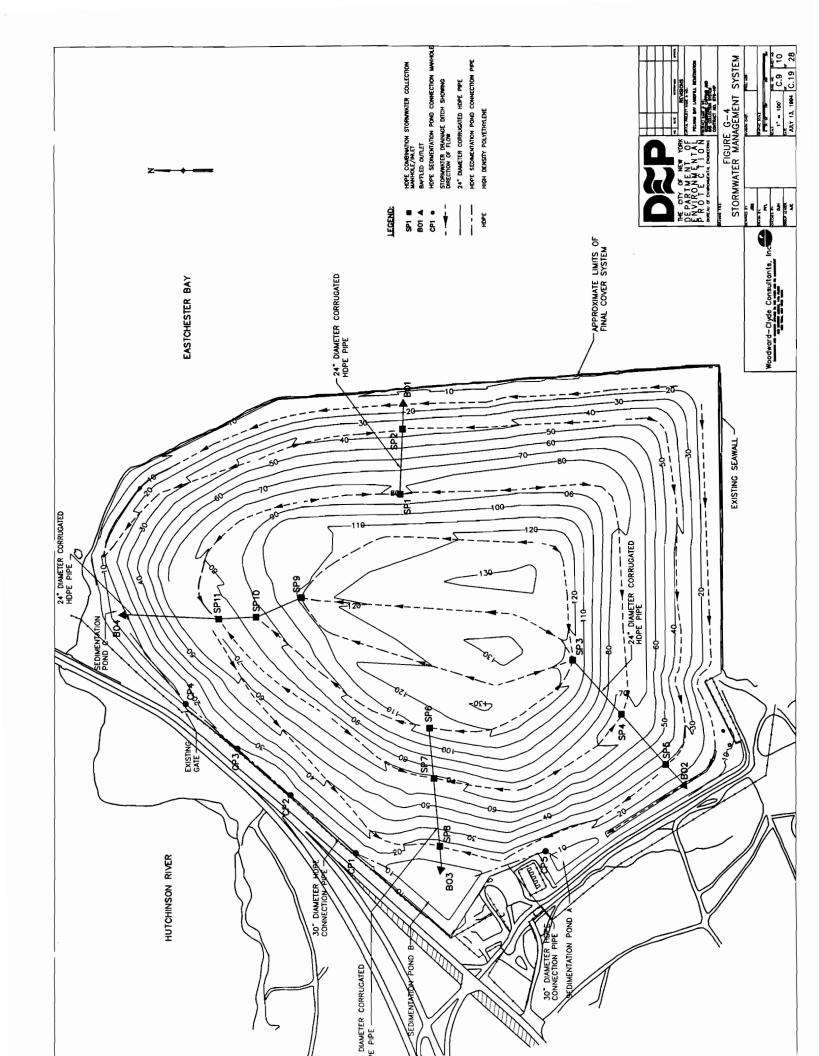


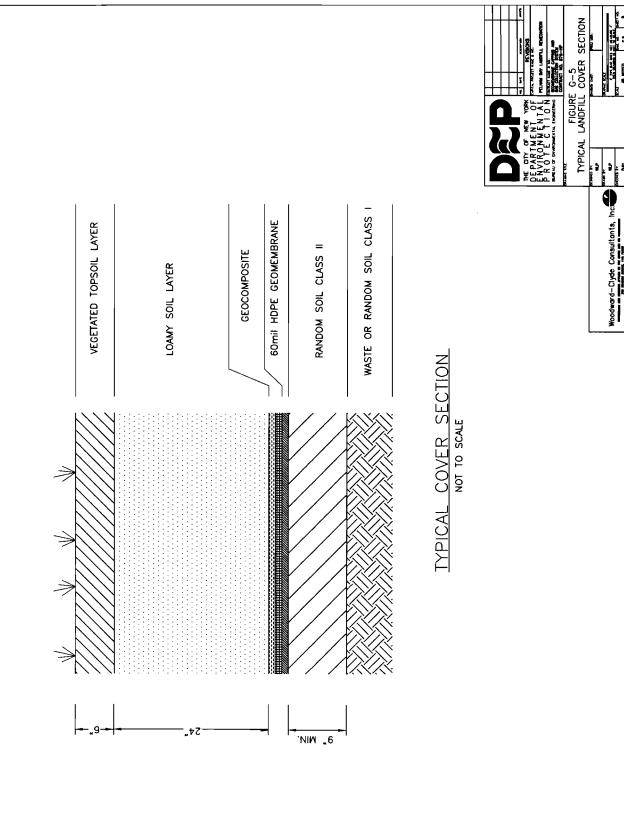


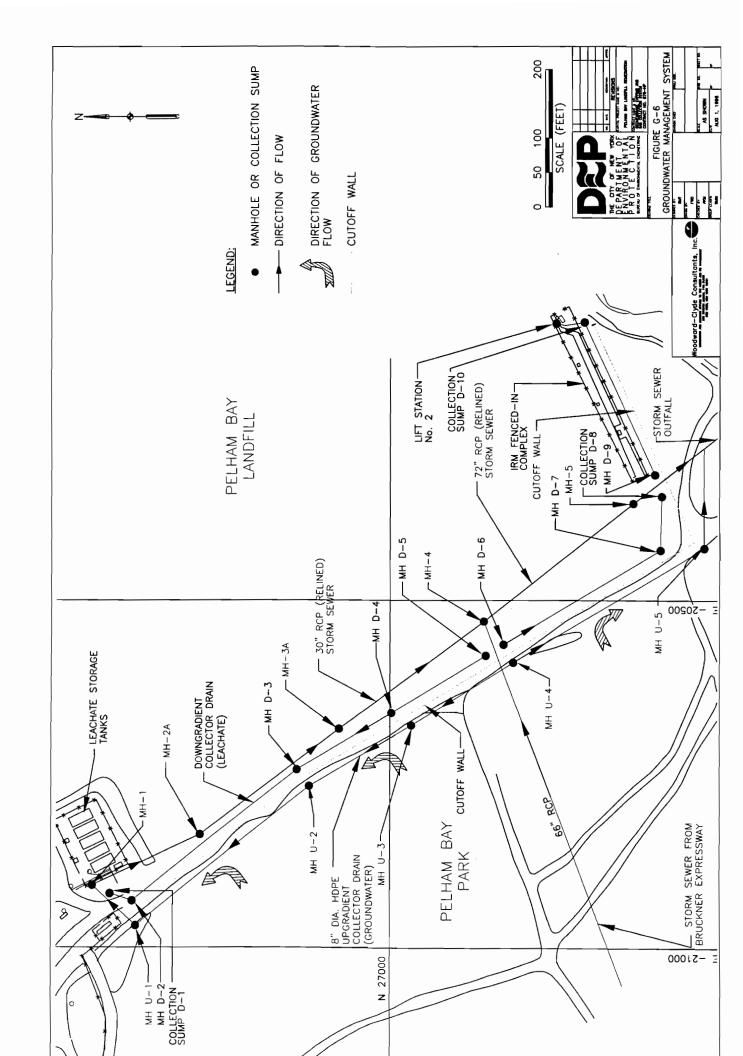


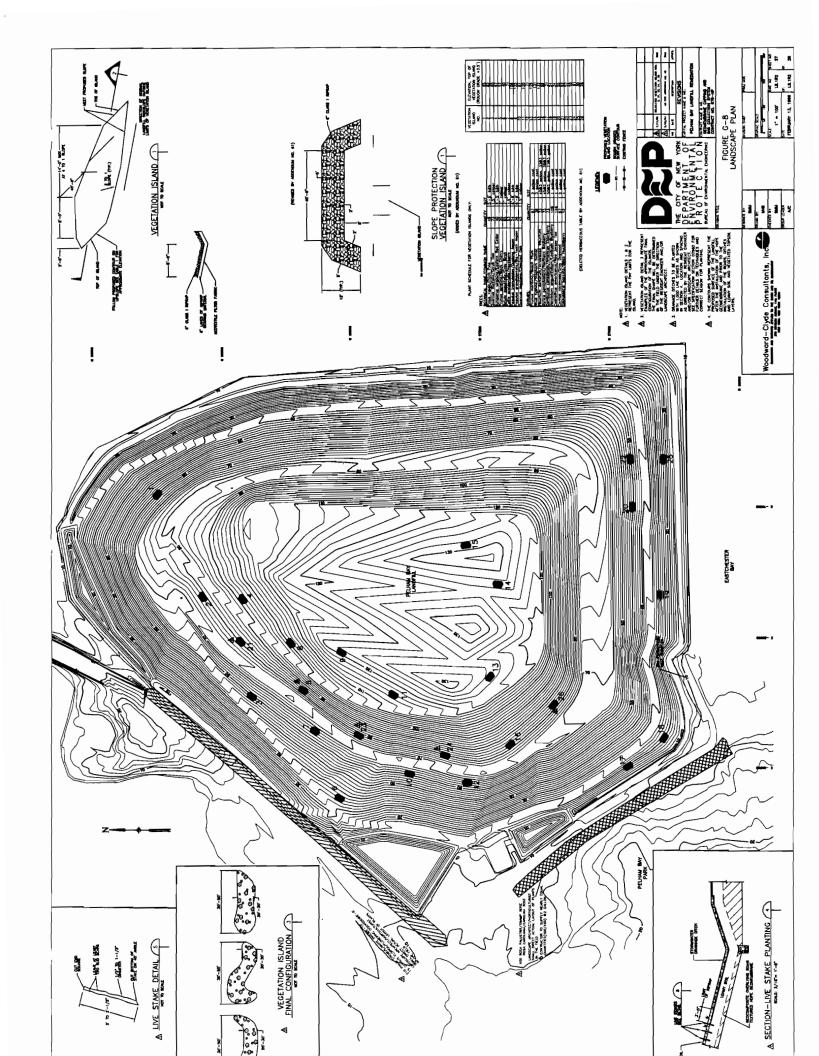


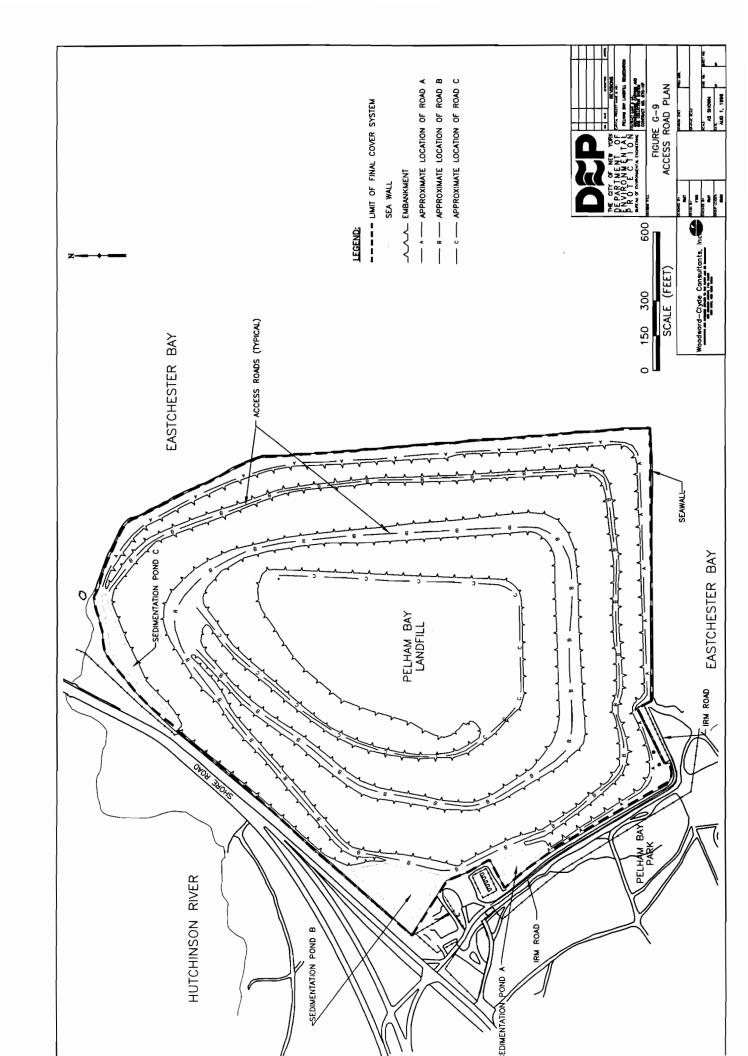












Damage to the Liner

The Problem

High winds started on Friday, February 26, 1996, forcing a halt to all construction activities on the landfill. At the time we were in the process of installing geo-composite material and Barrier Protection Layer (BPL) on the geomembrane previously installed on the top of the landfill.

Since the wind exceeded 40mph at the base of the landfill no one was allowed to travel to the top where the wind was usually 10-15MPH higher and the potential for injury greater.

The high wind condition continued for the weekend and subsided by Monday March 1st On Monday afternoon the crew ventured back on the landfill to investigate the extent of the damage the weekend storm has caused to the liner. At the top of the landfill it was revealed that approximately 13:5 acres of lining on the top was damaged.

Of the damaged areas approximately 10 acres were completely missing as it had blown off the top and was at the base or in the surrounding water or park. The nature of the damage to the liner that was left on the top was stretching in areas and shrinking in others.

Damage

Based on the condition of the damaged areas two theories emerged as the main cause of the damage: wind or fire.

The idea of a fire would seem to be remote at best, as conditions on the top of the landfill at that time would not be conducive to a fire. On the one hand, the conditions of high winds with little or no gas accumulation would make a fire unlikely. On the other hand, there could have been accumulation of landfill gas below the liner in the gas collection layer. This landfill gas could have been directed upward and accumulated below the liner on the landfill "plateau". However the shrinking and fusing of large portions of the line gave credence to the theory.

The second and more plausible theory is that of extensive wind damage. It is possible that the high winds at the top of the landfill reached over 70mph and caused excessive stretching of the liner. As the liner broke and flapped in the wind it stretched and then fused as it lost its elasticity.

Neither theory was extensively researched and the focus soon returned to repairing the damaged areas and the closure of the landfill.

Pelham Bay Landfill Closure and Final Certification Report-Addendum

The contractor made a claim to his insurance company and the insurance company of the liner installation subcontractors. A settlement was reached by all parties and the liner replacement started.

Replacing the Damaged Liner

Extensive testing on the liner that remained was conducted to set the limits of the damaged areas. Portions of the liner were removed and tested on site and samples were sent to the lab for conformation. All the liner that exhibited any result that did not meet the requirement of the contract was removed and new liner was installed.

Appendix B-6 and B-7 shows the QC testing results

New liner was installed in the spring and the liner was completed by the summer of 1996.

Section 6.5 Landscaping

In the fall of 1995 the contractor started to stock pile topsoil at the base of the landfill in anticipation of spreading the soil during the winter and start the final planting in the spring of 1996.

The contracts called for spreading 6"of topsoil over 2 feet of barrier protection layer and landscaping the soil with a design seed mix of prairie grass and other wild grasses. The seed mix was specially designed for the landfill and was purchased and stored at a seed depot.

Topsoil

The contractor investigated and submitted various sources that were going to be used proposed to provide the quantity and quality of topsoil to be used on the landfill. However due to the large volume and the quality required, the required material could not be obtained naturally and would have to be manufactured from soil and compost.

Soil delivery:

The contract required the topsoil testing @ 1 sample per source. As the possible sources increased and quality of the material decreased additional soil testing was required. A change order was issued to the contractor for additional testing at the source and at the site.

After soil testing at the various processing sites two subcontractors were eventually approved to deliver material to the site for use as topsoil. The two approved subcontractors delivered approximately 20,000 cubic yards of topsoil that was stockpiled at the base of the landfill. The material was tested at the source and at the landfill and the data in the resulting test report was in compliance with the contract and was submitted to the New York City DEP.

Soil Spreading and planting

Spreading of the topsoil started on the east side of the landfill in February of 1996. Starting on the lower level of the landfill 6" of topsoil was spread by bulldozers. After approximately 30 acres were covered with topsoil the area was hydro-seeded with the design seed mix and a rye grass seed mix.

Landscaping

The hydro-seeding operation consists of mixing the specified prairie seed with a rye grass and sheep fescue seeds, water and green coagulant indicator. The rye grass and fescue was used as a quick germinating grass that would provide shade for the prairie seed during the initial germination period. During April and May of 1996 the lower area of the landfill was hydro-seeded with the mix and the area covered with straw mulch for shade and moisture retention.

Initial Growth

In June and July of 1996 the specified prairie grass or the rye grass did not germinate as expected. It was initially believed that this was due to the hot summer days in June and July and the seeds would germinate as the heat subsides. The soil and the seeded areas were inspected by personnel from the New York City Parks Department, the landscaper and Cornell Cooperation extension to ascertain the reason why the grass was not germinating as anticipated. The results from the testing and inspection showed no adverse conditions that would prevent the specified seed mix from growing.

By September 1996 the grass did not show any improvement and additional testing and consultations with Cornell and Parks Department, revealed that the pH was above the acceptable limit for the specified prairie grass mix.

Investigation

The DEP and DEC commissioned Rutgers University as an outside source to investigate the problem with the lack of growth in the area previous landscaped. The focus of the investigation was on soil source, seed stock and planting technique.

Additional investigation was conducted by the NYC IG, NYS DEC and the court appointed Special Referee Office to see if any malfeasance was involved.

Soil: After additional testing on landfill, at the source and in the stockpile, it was determined that the soil was of low quality and had a high pH which would prevent the grass from growing.

The investigators reviewed the test results from the contractors approved lab and found inaccuracies with the data and poor QA/AC for the lab. The lab was dismissed and a new lab was contracted to do all further soil testing.

Soil Source: One of the approved sources for the topsoil to the site manufactured the topsoil from a blend of compost and dirt and stockpiled the material next to a recycling area. The investigation revealed that the recycled material along with other unspecified material was added to the topsoil blend as a bulking agent. These material consisting of wood, crushed concrete, glass and other crushed material.

Seed Stock: Testing of the seed that was purchased and stored for use on the landfill revealed germination rates below normal. The germination rates for the stock material were less than the specified rate. New seeds would therefore be required.

Planting Technique: The planting schedule and technique of the subcontractor were reviewed and found to be substandard and a new sub-contractor was hired to complete the project.

The investigation by the NYC DEP IG and the Federal Special Referee revealed that there was no malfeasance by City or State employees and the problem was contractual

Pelham Bay Landfill Closure and Final Certification Report-Addendum

between Brecco the contractor and their sub-contractors for the soil, seed and landscaping.

New Landscaping

The result of the investigation resulted in new techniques for planting and a new protocol for soil testing and delivery to the site.

The recommendation of the investigation was:

- (1) The existing soil at the site both topsoil and the soil for the barrier protection layer was to be treated with sulfur to reduce the pH
- (2) The entire landfill (including the areas previous topsoiled) was to be covered with 6 inches of new topsoil.
- (3) New seeds were to be used
- (4) A new and more experienced landscaper was to be hired.

With a new testing protocol featuring additional soil testing and more frequent site visits, new topsoil was manufactured and delivered to the site.

Sulfur was added to the existing soil and mixed to lower the pH of the existing soil. After mixing and testing the pH of the soil was lowered and the new topsoil was spread over the existing soil.

During the spring and fall of 1999 the landfill was landscaped using new soil, new seed and a new landscaper.

The new soil was hydroseeded and straw mulch was used to cover the seeds for protection from the sun and also as a moisture retention barrier.

Growth on the landfill was established by the summer of 2000 and deemed to be successful by the spring of 2001.