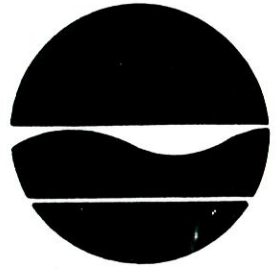
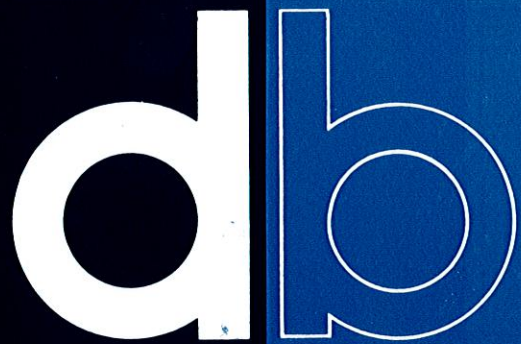


**- SUPPLEMENTAL INFORMATION -
NOT A PART OF CONTRACT VOLUME**



**REMEDIAL DESIGN
ENGINEERING REPORT**

Storonske Cooperage Site
Town of Schodack,
Rensselaer County, New York
(Site Registry No. 442021)



Dvirka and Bartilucci

Consulting Engineers

MARCH 1994

REMEDIAL DESIGN ENGINEERING REPORT

**STORONSKE COOPERAGE SITE
TOWN OF SCHODACK
RENSSELAER COUNTY, NEW YORK**

(SITE REGISTRY NO. 442021)

PREPARED FOR

**THE NEW YORK STATE DEPARTMENT
OF ENVIRONMENTAL CONSERVATION**

BY

**DVIRKA AND BARTILUCCI
CONSULTING ENGINEERS
SYOSSET, NEW YORK**

MARCH 1994

**STORONSKE COOPERAGE SITE
REMEDIAL DESIGN ENGINEERING REPORT**

TABLE OF CONTENTS

<u>Section</u>	<u>Title</u>	<u>Page</u>
1.0	INTRODUCTION	1-1
1.1	Site History	1-1
1.2	Previous Investigations	1-1
1.3	Record of Decision	1-7
2.0	REMEDIAL DESIGN ACTIVITIES PERFORMED TO DATE	2-1
2.1	Supplemental Surface and Subsurface Soil Sampling Program	2-1
2.2	Vapor Extraction/Air Sparging Pilot Test	2-4
3.0	PILOT TESTING EVALUATION	3-1
3.1	Design Organic Compounds	3-1
3.2	Impact of Other Organic Compounds	3-1
3.3	Required Volatile Organic Compound Removal Efficiency	3-4
3.4	Air Quality Impacts	3-4
3.5	Condensate Treatment	3-6
3.6	Testing Equipment	3-6
3.7	Test Conditions and Procedures	3-6
3.8	Test Results	3-7
	3.8.1 Vacuum Extraction Testing	3-7
	3.8.2 Air Sparging Testing	3-8
	3.8.3 Dual Vacuum Extraction Testing	3-8
4.0	PROPOSED SOIL VAPOR EXTRACTION AND TREATMENT SYSTEM	4-1
4.1	System Design Parameters	4-1
4.2	Extraction Wells	4-3
4.3	Monitoring Wells	4-3
4.4	Blowers	4-6
4.5	Piping	4-6
4.6	Vapor Treatment System	4-6
4.7	Control System	4-8
4.8	Auxiliary Power	4-9
4.9	Equipment Enclosure	4-9
4.10	Sampling Taps	4-9
4.11	Monitoring Frequency	4-10

TABLE OF CONTENTS (continued)

<u>Section</u>	<u>Title</u>	<u>Page</u>
5.0	SOIL EXCAVATION, STORAGE, REMOVAL, DISPOSAL, BACKFILL AND REGRADING	5-1
5.1	Definition of Limits of Excavation	5-1
5.2	Temporary On-Site Storage	5-3
5.3	Decontamination Facilities	5-4
5.4	Transportation and Disposal Requirements	5-4
5.5	Confirmatory Sampling	5-5
5.6	Backfill Requirements	5-5
5.7	Site Regrading	5-6
5.8	Placement of an Additional Six Inches of Clean Soil	5-6
5.9	Revegetation	5-8
6.0	ESTIMATION OF CONSTRUCTION COSTS	6-1

<u>Appendices</u>	<u>Title</u>
APPENDIX A	Pre-Design Investigation Analytical Data
APPENDIX B	Vapor Extraction/Air Sparging Pilot Test Report
APPENDIX C	Application for Permit to Construct a Process, Exhaust or Ventilation System
APPENDIX D	Analytical Data for Surface and Subsurface Soil Samples
APPENDIX E	Soil Boring Logs and Grain Size Distribution Curves for Soil Borings Constructed in Area of Former Lagoon

LIST OF FIGURES

<u>Number</u>	<u>Title</u>	<u>Page</u>
1-1	Site Location Map	1-2
1-2	Facility Location Map	1-3
2-1	Supplemental Surface and Subsurface Soil Sample Location Map	2-2
2-2	Areas Exceeding Site Surface and Subsurface Clean-up Goals	2-3
2-3	Pilot Testing Process Schematic	2-5
4-1	Soil Vapor Extraction and Treatment System Schematic	4-2
4-2	Soil Vapor Extraction and Treatment System Site Plan	4-4
4-3	Extraction Well Construction Diagram	4-5
4-4	Proposed Floor Plan	4-7
5-1	Limits of Excavation, Temporary Contaminated Soil Storage and Decontamination Facilities	5-2
5-2	Site Grading, Cover and Revegetation Plan	5-7

LIST OF TABLES

<u>Number</u>	<u>Title</u>	<u>Page</u>
1-1	Summary of Contamination Detected in On-site Soil Samples	1-5
1-2	Cleanup Goals Established for On-site Soils	1-9
3-1	Organic Compounds Cleanup Goals	3-2
3-2	Volatile Organic Compound Required Concentration Reductions	3-3
3-3	Volatile Organic Compound Estimated Initial Extracted Production Rates	3-5
6-1	Estimated Cost for Vapor Extraction	6-2
6-2	Estimated Cost for Excavation and Cover	6-3

1.0 INTRODUCTION

1.1 Site History

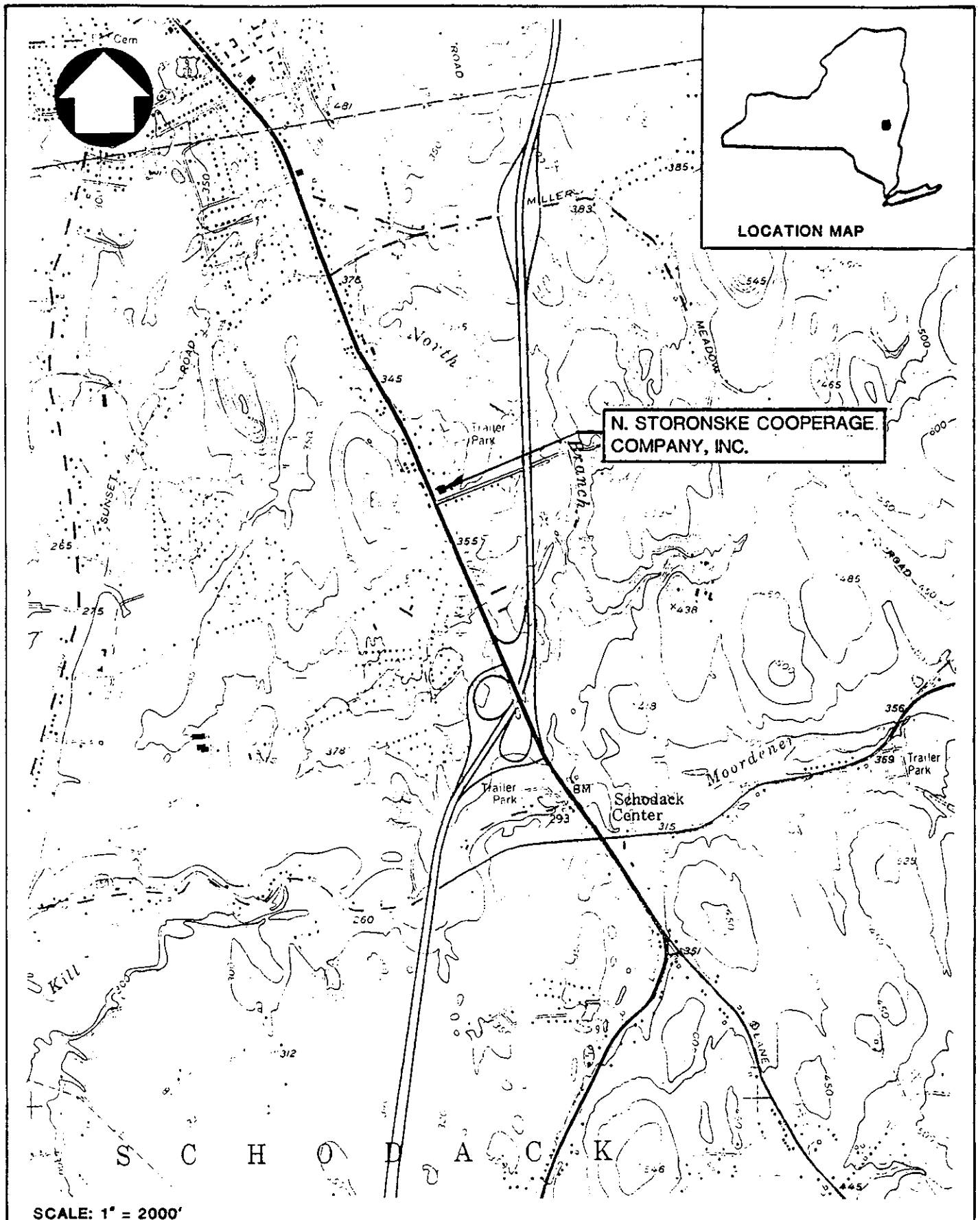
The Storonske Cooperage site, which is a New York State Superfund site, is a 5-acre parcel of land located in the Town of Schodack, Rensselaer County, New York. The site is located on the north side of Kraft Road, immediately east of the intersection of Kraft Road with U.S. Routes 9 and 20 (see Figure 1-1). The facility, until recently, was used for the cleaning and reconditioning of 55-gallon drums since it was purchased by N. Storonske Cooperage, Inc. in 1973. Prior to 1973, the property was utilized by the Albany-Nassau Bus Company as a bus garage and depot.

The earliest known concern regarding the Storonske Cooperage site as a possible source of contamination was reported by the Rensselaer County Department of Health in 1979, because of the large number of drums stored and processed on the site. It was also reported that soil samples collected on the site in 1980 showed elevated levels of benzene and xylene.

1.2 Previous Investigations

In March 1984, the New York State Department of Environmental Conservation (NYSDEC) conducted a facility inspection under the Resource Conservation and Recovery Act (RCRA) program. The sludge in the former wastewater lagoon at the site, which received rinse water from drum cleaning, was sampled and found to exceed the EP Toxicity limits for lead, which characterized the material as a hazardous waste. This resulted in N. Storonske Cooperage, Inc., entering into a Consent Order with the State of New York in March 1986, to remove the lagoon from operation and to conduct an investigation of the impacts of the lagoon (see Figure 1-2).

Since 1984, six investigations have been conducted at the site, four of which were commissioned by the site owner and two undertaken by NYSDEC. Provided below is a list of investigation reports prepared for the site, including both groundwater and soils:

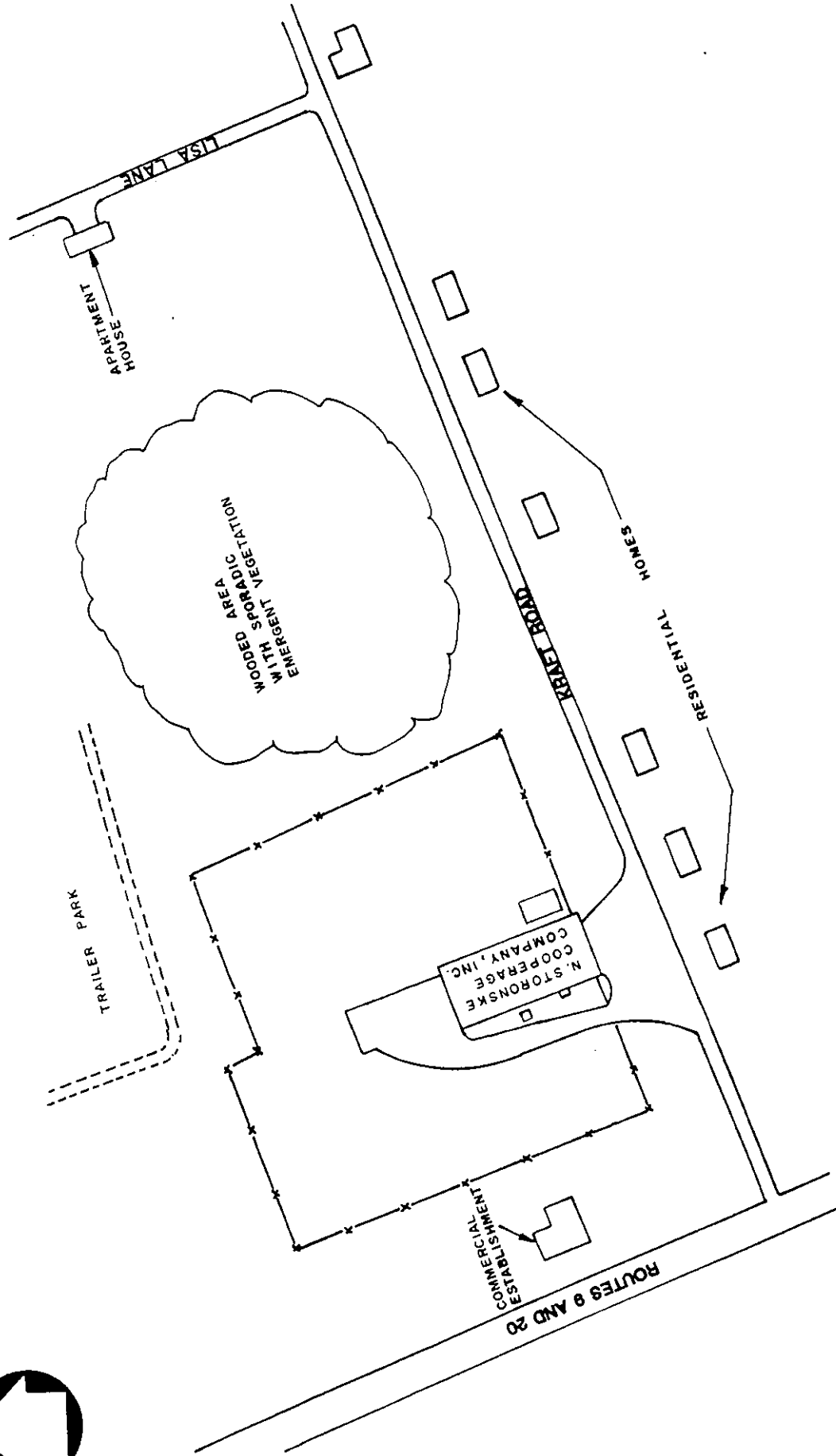


STORONSKE COOPERAGE SITE
FEASIBILITY STUDY



SITE LOCATION MAP

FIGURE 1-1



APPROXIMATE SCALE: 1" = 150'

STORONSKE COOPERAGE SITE
FEASIBILITY STUDY

- "Field Investigation and Monitoring Proposal," June 1986, by Fraser Associates.
- "Preliminary Hydrogeologic Assessment," October 1986, by Fraser Associates, Empire Soils Investigations, Inc. and Thomsen Associates.
- "Phase I Hydrogeologic Investigation," September 1987, by Malcolm Pirnie, Inc.
- "Phase II Hydrogeologic Investigation," December 1988, by Malcolm Pirnie, Inc.
- "Focused RI/FS Work Plan," April 1989 and "Focused Remedial Investigation and Feasibility Study Report," April 1990, by Malcolm Pirnie, Inc.
- "Phase I Remedial Investigation Report," November 1990, by Dvirka and Bartilucci Consulting Engineers.
- "Phase II Remedial Investigation Report," August 1992, by Dvirka and Bartilucci Consulting Engineers.

Based on the site investigations indicated above, groundwater samples collected from monitoring wells installed as part of the investigations indicated the presence of volatile organic compounds (VOCs). The latest round of groundwater sampling conducted in April 1992, indicated the following VOCs and highest concentrations in samples collected from the on-site groundwater monitoring wells: trichloroethene (19 ug/l), benzene (7 ug/l), chlorobenzene (8 ug/l), 1,1-dichloroethane (30 ug/l), tetrachloroethane (10 ug/l), 1,1,1-trichloroethane (15 ug/l) and xylene (63 ug/l). Levels of VOCs were also detected above New York State Drinking Water Standards at several residences along Kraft Road prompting the continued use of carbon filtration devices on private water supply systems.

Soil at the site was found to be contaminated with various volatile and semivolatile organic compounds, metals and polychlorinated biphenyls (PCBs) based upon the results reported in the Focused Remedial Investigation and Feasibility Study Report, dated April 1990, by Malcolm Pirnie, Inc. as indicated on Table 1-1. The most contaminated soils appeared to be confined to the area of the former lagoon and eastward to the site's eastern property boundary. Other contaminated areas included drum unloading and storage areas.

Table 1-1

**SUMMARY OF CONTAMINATION DETECTED IN
ON-SITE SOIL SAMPLES¹
STORONSKE COOPERAGE SITE**

	<u>Frequency of Detection</u>	<u>Range of Detected Values (ppb)</u>	<u>Average of Detected Values (ppb)</u>
<u>Volatile Organics</u>			
Tetrachloroethene	24/111	2-3,500	332
1,1,1-Trichloroethane	24/111	1-1,300	172
Total Xylenes	17/111	10-58,500	15,029
Ethylbenzene	16/111	2-20,000	5,474
Toluene	14/111	12-41,000	8,558
Chlorobenzene	10/111	2-3,900	1,230
Trichloroethene	10/111	2-2,600	321
1,1-Dichloroethane	7/111	1-3	1.9
Total 1,2-Dichloroethene	5/111	1-6	4.4
1,2-Dichloroethane	3/111	6-2,000	792
Styrene	2/111	8,900-19,000	13,950
Benzene	1/111	810	810
<u>Semivolatile Organics</u>			
Di-n-Butylphthalate	21/97	30-316,000	19,505
Naphthalene	19/97	41-9,100	1,151
2-Methylnaphthalene	17/97	41-3,900	965
Phenol	16/97	130-26,000	3,474
Hexachlorobenzene	13/97	160-1,900	655
Bis(2-ethylhexyl)phthalate	11/97	1,300-12,000	4,255
1,2,4-Trichlorobenzene	10/97	140-1,800	710
4-Methylphenol	9/97	100-1,900	1,050
Phenanthrene	7/97	42-800	326
Isophorone	6/97	93-1,400	392
2,4-Dimethylphenol	6/97	130-1,300	538
Di-n-octylphthalate	6/97	57-360	130
Butylbenzylphthalate	6/97	210-3,700	1,268
2-Methylphenol	4/97	390-790	610
Fluorene	3/97	73-380	224
Fluoranthene	3/97	310-830	587
Pyrene	3/97	220-560	453

Table 1-1 (continued)

**SUMMARY OF CONTAMINATION DETECTED IN
ON-SITE SOIL SAMPLES¹
STORONSKE COOPERAGE SITE**

	<u>Frequency of Detection</u>	<u>Range of Detected Values (ppb)</u>	<u>Average of Detected Values (ppb)</u>
Chrysene	3/97	150-420	300
Benzo(a)anthracene	2/97	310-370	340
1,2-Dichlorobenzene	1/97	440	440
Diethylphthalate	1/97	430	430
Anthracene	1/97	220	220
Benzo(a)fluoranthene	1/97	560	560
Benzo(a)pyrene	1/97	240	240
<u>PCB</u>			
Aroclor-1242 (as PCBs)	21/87	110-20,000	2,035
<u>Metals</u>			
Cadmium	100/103	ND-317,000	11,290
Chromium	82/82	11.1-943,000	40,950
Copper	103/103	8,700-15.1E4	33,870
Lead	103/103	3.1E3-508E4	113,130
Mercury	25/32	ND-1,810	398
Selenium	3/103	ND-7,500	3,600
Zinc	102/102	365E2-246E4	149,150

1 As reported in N. Storonske Cooperage Focused Remedial Investigation and Feasibility Study Report, April 1990, by Malcolm Pirnie, Inc.

The depth of contaminated soil was determined to vary with respect to on-site location and type of contaminant. In general, highest concentrations of total VOCs were detected in the former lagoon area at depths from 0.5 to 10 feet at 110 ppm. The VOCs extend generally eastward from the lagoon and were detected at depths extending to 10-16 feet at the eastern property boundary with total VOC concentrations greater than 2 ppm. The highest concentration of total VOCs at this eastern boundary location was 85.5 ppm at a depth of 4-10 feet. Significant contamination was typically not detected at depths greater than 10-16 feet. Note that the depth to groundwater in the former lagoon area (well MW-15) extending to the eastern site boundary (well MW-25) ranges from 16.5 feet to 13 feet, respectively.

Supplemental Surface and Subsurface Soil Sampling

As part of the Predesign Investigation, Dvirka and Bartilucci Consulting Engineers performed additional soil sample collection in April 1993, to further define areas of contamination at the site. These samples were collected for VOCs, PCBs and lead analysis. The analytical data from this predesign sampling is provided in Appendix A. The results further identified areas requiring remediation for PCBs and lead, however, VOCs were not detected in site surface soils.

1.3 Record of Decision

As a result of the on-site investigations and evaluation of remedial alternatives to address on-site soil contamination, a Record of Decision (ROD) was issued by NYSDEC in March 1992, which sets forth the selected remedial action plan for the Storonske Cooperage site Operable Unit 1 - On-site Soils. The remedial plan was developed in accordance with the Comprehensive Environmental Response, Compensation and Liability Act (CERCLA) of 1980, as amended by the Superfund Amendments and Reauthorization Act (SARA) of 1986, and the New York State Environmental Conservation Law (ECL). The ROD was based upon the Administrative Record for the Storonske Cooperage site and public input to the Proposed Remedial Action Plan (PRAP). The final screening of remedial alternatives as presented in the Focused RI/FS Report by Malcolm Pirnie, Inc., included a number of options, of which In Situ Vacuum Extraction and Off-site Disposal of Soils Contaminated with Heavy Metals, was selected by NYSDEC as

appropriate for the Storonske Cooperage site contaminants and site conditions for the on-site soils. Table 1-2 indicates the cleanup goals established for remediation activities for on-site soils.

The major components of the selected remedy include the following:

1. Predesign pilot testing to determine the number and locations of vacuum extraction wells.
2. Design and installation of a vacuum extraction system to remove and treat volatile organic contaminants from the soils. Methods for enhancing the removal of contaminants will be evaluated.
3. End-point sampling of subsurface soil to determine if treatment goals for soil vapor gas have been achieved.
4. Demobilization of the soil vapor gas extraction system.
5. Additional surface soil sampling to determine the areal extent of soil contaminated with volatile organic compounds, PCBs and lead. Areas of the site which exceed the cleanup goal for lead of 200 parts per million (ppm) will be identified to determine the limits of soil excavation.
6. Excavation and removal of contaminated soils from the site. Testing will be performed to ensure that the soil meets the applicable disposal facility requirements.
7. Soil/excavation end-point sampling to verify that the cleanup goals have been achieved.
8. Backfill of excavated areas with clean soil and the overall site covered with six inches of clean soil, regraded to promote proper drainage and revegetated to prevent erosion.
9. Long-term groundwater and water supply sampling to monitor the effectiveness of the remedial actions taken.

Table 1-2

**CLEANUP GOALS ESTABLISHED FOR ON-SITE SOILS
STORONSKE COOPERAGE SITE**

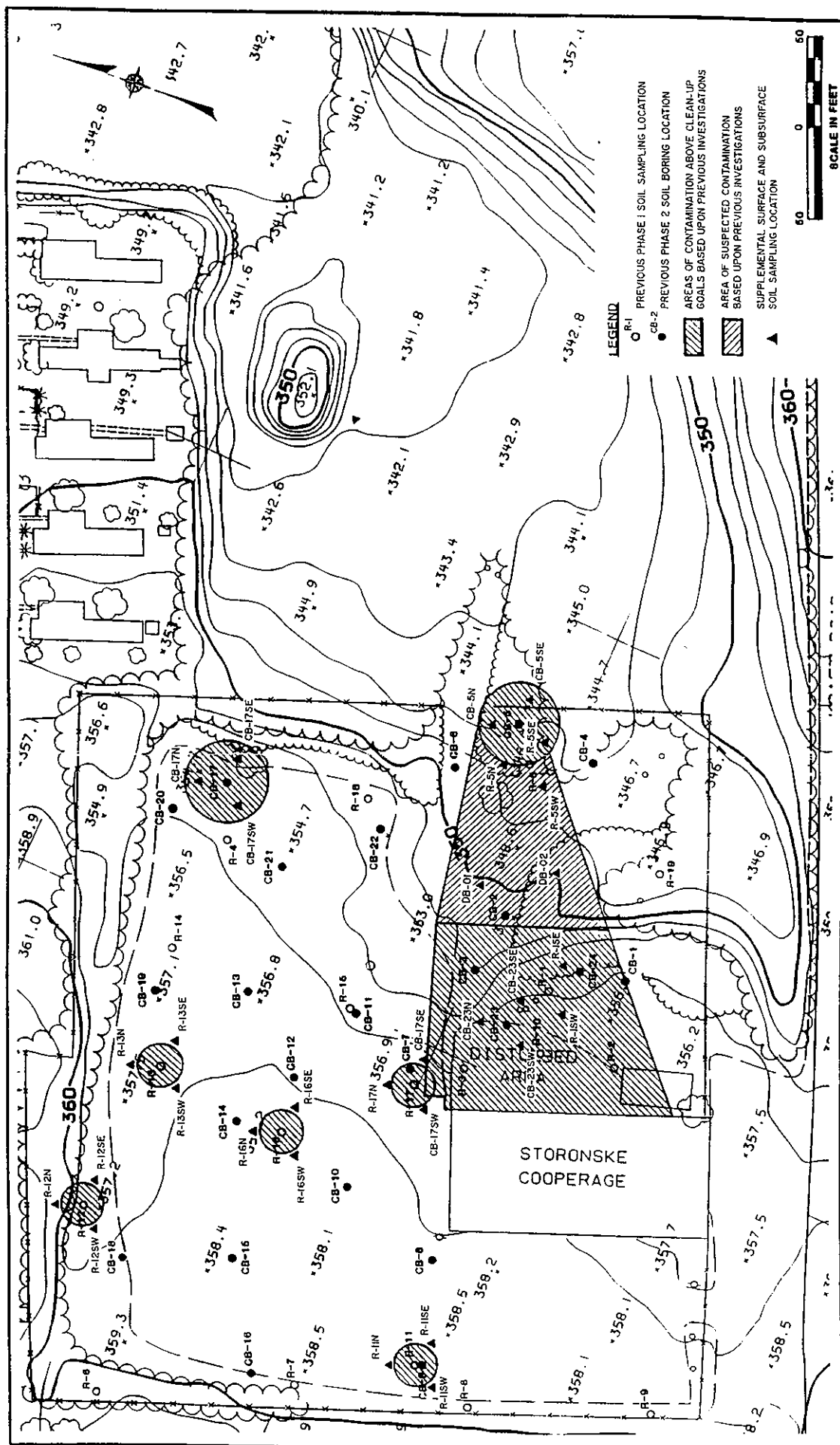
<u>Organic Compounds</u>	<u>Soil Cleanup Goal (ppm)</u>
Tetrachloroethene	1.5
1,1,1-Trichloroethane	1.0
Trichloroethene	1.0
1,2-Dichloroethane	0.1
Ethylbenzene	5.5
Chlorobenzene	1.5
Toluene	1.5
Total Xylenes	1.2
Phenols	0.33
PCB Aroclor-1242	1.0
 <u>Metals</u>	
Lead	200

2.0 REMEDIAL DESIGN ACTIVITIES PERFORMED TO DATE

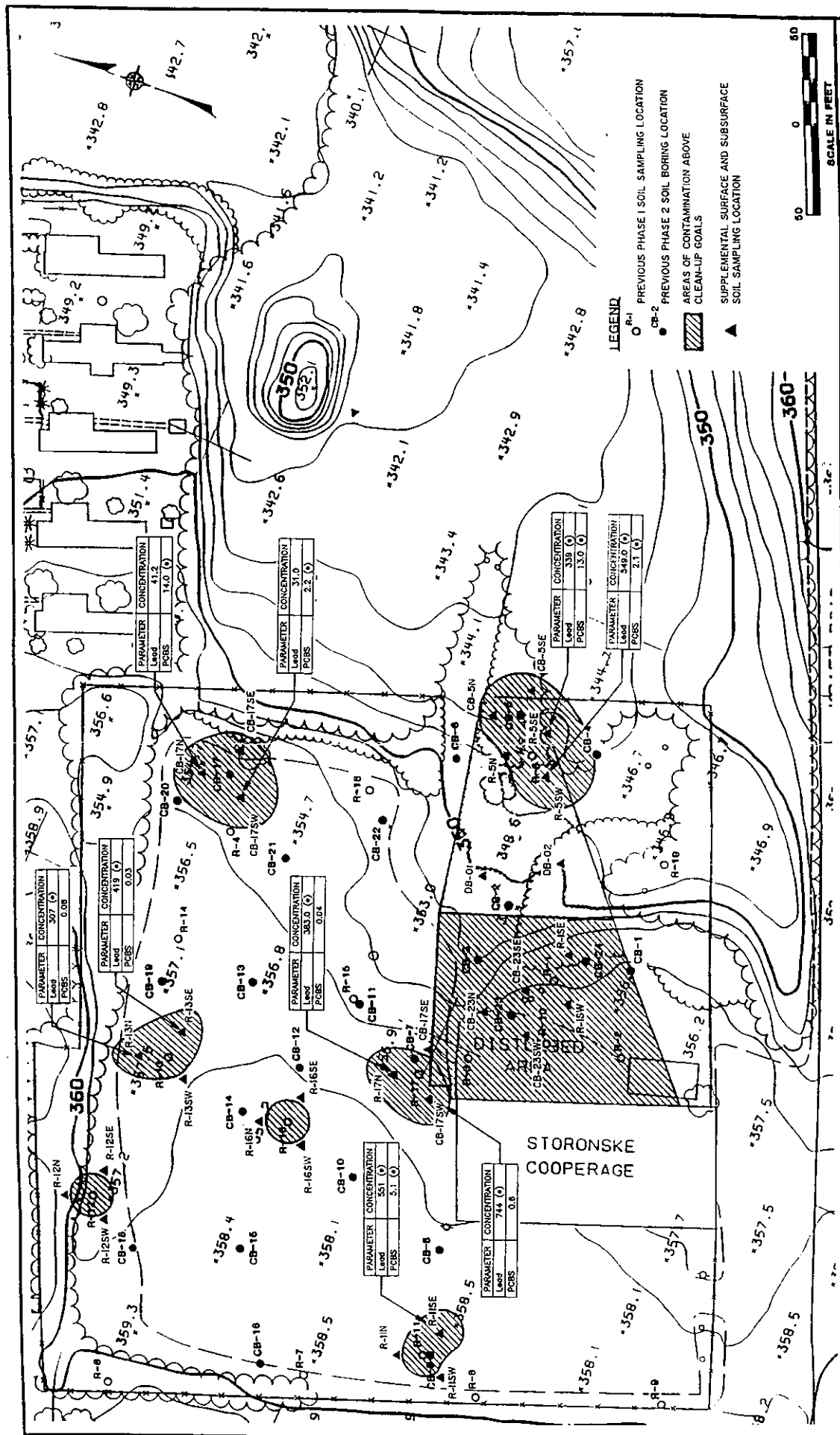
2.1 Supplemental Surface and Subsurface Soil Sampling Program

On April 19 and 20, 1993, Dvirka and Bartilucci Consulting Engineers conducted a supplemental/predesign surface and subsurface soil sampling program in areas at the site in which limits of the contamination had not been defined. The sampling consisted of the collection of 30 samples at locations identified in Figure 2-1. Seven of the 30 samples for PCB analysis were collected at a depth of 2 to 4 feet in the area of the former lagoon. All of the remaining samples were collected at or just below ground surface. All 30 of the sample locations were in areas which had been identified as exceeding or suspected of exceeding cleanup goals based upon previous investigations. The surficial samples were analyzed for Target Compound List (TCL) volatiles +10, TCL PCBs and lead. Surface samples were collected at a depth of 0 to 6 inches below vegetative cover or ground surface utilizing disposable sterile polystyrene scoops and sterile wooden tongue depressors. The seven subsurface samples collected at a depth of 2-4 feet in the former lagoon area were obtained utilizing stainless steel shovels and a hand auger, and analyzed for PCBs only. Detailed descriptions of the sampling procedures are provided in Section 6.7 of the Remedial Design Work Plan, dated January 1993.

A summary of elevated analytical results of this supplemental sampling program are indicated in Figure 2-2. The actual analytical data from this predesign sampling is provided in Appendix A. Areas of the site which exceed site specific cleanup goals based upon interpolation of previous and supplemental analytical results are shaded. As illustrated on Figure 2-2, areas which exceed the cleanup goals represent an area of approximately 2,600 sy. Excavation of these areas is planned to be conducted to an estimated depth from 0.5 to 6 feet based upon results of the remedial and supplemental investigations for protection of human health and the environment. The quantity of soils estimated to require excavation and off-site treatment/disposal is 3,300 cy.



SUPPLEMENTAL SURFACE AND SUBSURFACE SOIL SAMPLING LOCATION MAP



STORONSKE COOPERAGE SITE
TOWN OF SHODACK, NEW YORK

AREAS EXCEEDING SITE SURFACE AND SUBSURFACE CLEAN-UP GOALS

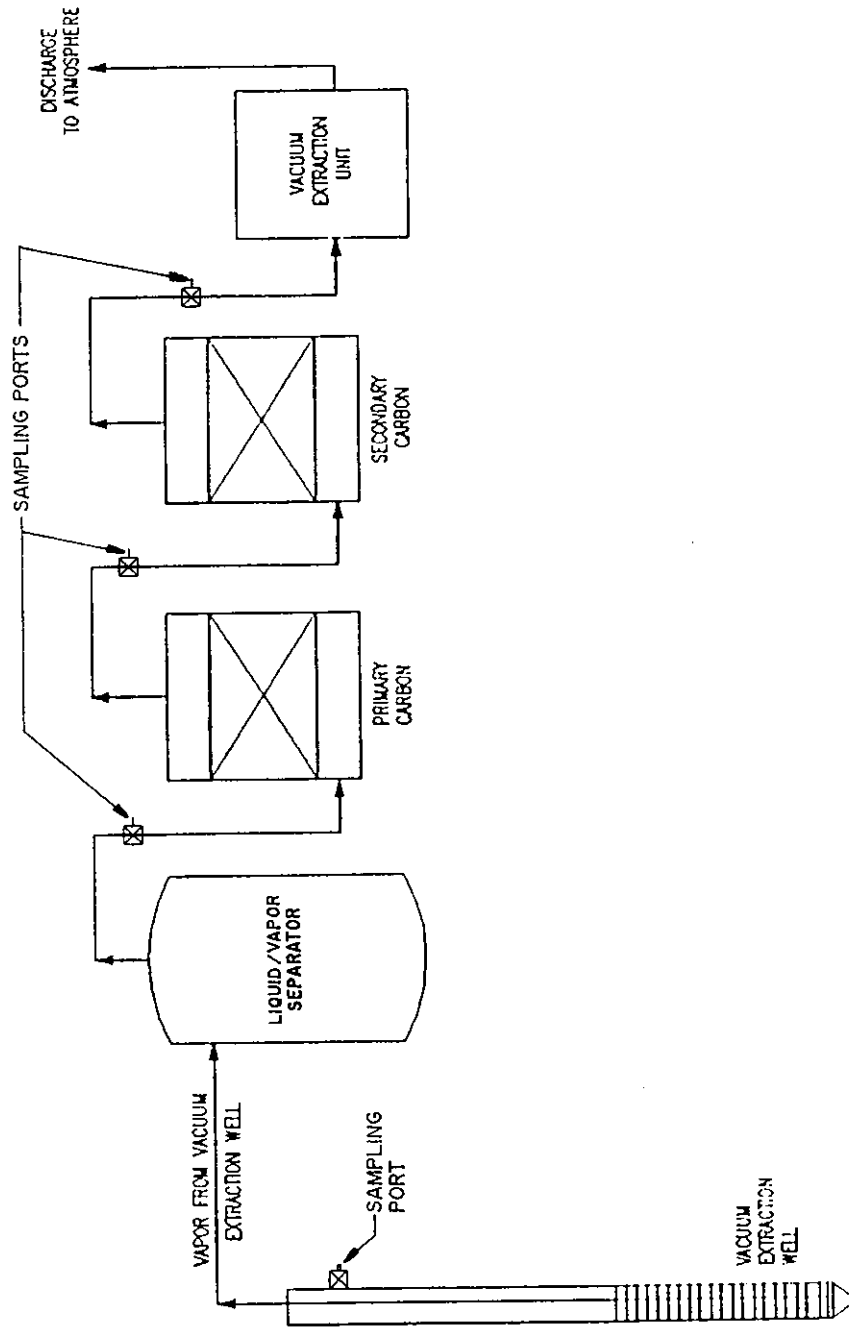
2.2 Vapor Extraction/Air Sparging Pilot Test

Based upon the Record of Decision (ROD), a predesign pilot test was to be conducted to determine the number and locations of vacuum extraction wells. Included in the ROD was the design and installation of the full scale vacuum extraction system with an additional evaluation of methods to enhance the removal of contaminants. The pilot testing conducted at the Storonske Cooperaage site included vapor extraction to remove contaminants from the unsaturated zone, air sparging which enhances contaminant removal from the aquifer by bubbling air into the saturated zone above bedrock and dual vapor extraction which extracts groundwater to expose additional unsaturated soil to the vapor extraction system. A pilot testing process schematic is illustrated in Figure 2-3.

On October 27, 1993, vapor extraction/air sparging pilot testing activities were initiated with the construction of one injection well, one extraction well and two monitoring wells. Pilot testing commenced on November 2, 1993, with vacuum radius of influence testing. Sparging cone-of-influence testing and dual vacuum extraction testing were conducted on subsequent days.

Based upon the information derived from the pilot test, the following conclusions were determined:

- Vacuum extraction (VE) is an effective method of remediating the unsaturated soils at the site, regardless of the method chosen to remediate the saturated zone.
- A minimum radius of influence of 12 feet was measured in monitoring wells/probes. The calculated radius of influence for vacuum extraction based upon measurements from the wells/probes and soil specific assumptions is from 15 to 17 feet, depending on the applied vacuum.
- Carbon adsorption is an effective method of vapor treatment for this site.
- Increased vacuums provided larger radii of influence, higher flows and higher extraction rates.
- The effectiveness of air sparging is limited due to the thin saturated thickness encountered in the source area.



STORONSKE COOPERAGE SITE
TOWN OF SCHODACK, NEW YORK

PILOT TESTING PROCESS SCHEMATIC

- Dual vacuum extraction (DVE) is an effective method of dewatering the source area, given the thin saturated thickness.
- The remedial system chosen for cleanup of the saturated zone should be flexible to handle changing water level conditions.
- Although the DVE integrated remediation system to cleanup the saturated and unsaturated soils at the site is a viable technology, based upon the depth of most prevalent VOC contamination at the site and the limited saturated thickness of the overburden aquifer in the area of the former lagoon, simple vapor extraction is recommended. This system would include 17 vacuum extraction wells in the source area and 3 vapor extraction wells in the eastern fence area. Carbon adsorption would be used for vapor treatment and for treatment of condensate from the water/vapor separator. The operating time of this system would be approximately 1.5 years.

A detailed description of the pilot test procedures and results is provided in Appendix B.

3.0 PILOT TESTING EVALUATION

3.1 Design Organic Compounds

There are ten organic compounds with recommended clean-up goals for on-site soils indicated in the Storonske Cooperage site Record of Decision. These organic compounds and their respective recommended cleanup goals are indicated in Table 3-1. Two of the organic compounds, phenols and PCBs, are not volatile and are not directly affected by induced vacuums in the soil as conducted during the vapor extraction pilot test. Phenols may, however, be affected by the increased oxygen levels in the soil which tend to increase biological degradation of this compound. All of the other organic compounds with cleanup goals were selected for vapor and groundwater analysis during the pilot test to determine testing effectiveness for removal of these compounds from the soil and groundwater.

Table 3-2 indicates the volatile organic compound clean-up goals for the site and the maximum concentration reduction required to achieve the goals based upon maximum soil concentrations. As indicated on the table, total xylenes require the most significant reduction in concentration (97.9%) to achieve cleanup goals at the site. Also significant are 1,2-dichloroethane (95.0%) and toluene (96.3%). Based upon detailed bench scale testing, approximately 9000 pore volumes may be required to achieve a 98% reduction in soil concentration for xylene.

3.2 Impact of Other Organic Compounds

Nonvolatile organic compounds at the site will, in general, not affect the operation of the soil vapor extraction system. Only volatile organic compounds will be removed from contaminated soil and require exhaust gas treatment. As previously indicated, semivolatile contamination (phenols) present in site soils may be indirectly affected by operation of the system. The oxygen levels in soils will be increased due to the drawing of atmospheric air into soil. This typically results in increased biological degradation of semivolatile organic compounds by aerobic bacteria. No impacts are likely to be observed with nonvolatile, highly chlorinated compounds, such as PCBs.

Table 3-1

**ORGANIC COMPOUND CLEANUP GOALS
STORONSKE COOPERAGE SITE**

<u>Compound</u>	<u>Soil Cleanup Goal (ppm)</u>
Tetrachloroethene	1.5
1,1,1-Trichloroethane	1.0
Trichloroethane	1.0
1,2-Dichloroethene	0.1
Ethylbenzene	5.5
Chlorobenzene	1.5
Toluene	1.5
Total Xylenes	1.2
Phenols	0.33
PCB Aroclor-1242	1.0

Table 3-2

**VOLATILE ORGANIC COMPOUND
REQUIRED CONCENTRATION REDUCTIONS
STORONSKE COOPERAGE SITE**

Compound	Average Soil Conc. (ppb)	Maximum Soil Conc. (ppb)	Cleanup Goal (ppb)	Maximum Reduction Required
Tetrachloroethene	332	3500	1500	57.1%
1,1,1-Trichloroethane	172	1300	1000	23.1%
Trichloroethene	321	2600	1000	61.5%
1,2-Dichloroethane	790	2000	100	95.0%
Xylenes	15,029	58,500	1200	97.9%
Ethylbenzene	5474	20,000	5500	72.5%
Toluene	8558	41,000	1500	96.3%
Chlorobenzene	1230	3900	1500	61.5%

3.3 Required Volatile Organic Compound Removal Efficiency

Based upon the maximum concentrations of VOCs in the soil, and site clean-up goals required, removal efficiencies were calculated as indicated in Table 3-2. Based upon these efficiencies it has been determined that total xylenes will be the limiting compound for achievement of clean-up goals at the site due to a required removal efficiency of 97.9%. In order to achieve this level of removal efficiency, bench scale testing in the laboratory of soil with similar properties has determined an estimated withdrawal of 9000 pore volumes of soil vapor will be required. Based upon site specific radius of influence testing (determined to be 17 feet) assumptions of soil porosity (35%) and flow rates achieved during pilot testing (60 standard cubic feet per minute [scfm]), it is estimated that a duration of approximately 1.5 years will be necessary to achieve the required removal efficiency.

3.4 Air Quality Impacts

Results of analysis performed both prior and subsequent to vapor treatment during pilot testing indicated that activated carbon was effective in removing contaminants from the vapor stream prior to exhaust discharge. Based upon estimated mass removal rates for full scale system operation, vapor treatment will be required. Initially, it is estimated that VOCs will be extracted at the rates indicated in Table 3-3. The total VOC production rate could be initially as high as 7.9 lbs/hr and therefore will require treatment. Mass removal rates have been utilized to estimate the quantity of activated carbon necessary for treatment based upon a system operation duration of 1.5 years. The estimated quantity of carbon based upon an assumed loading rate of 10% is approximately 18,000 lbs. An air monitoring program will be developed as part of the Monitoring and Maintenance Plan for the full scale system to ensure activated carbon treatment of the discharge is effective in eliminating potential air quality impacts from operation of the system. A copy of the application for a permit to construct a process, exhaust or ventilation system is provided as Appendix C.

Table 3-3

**VOLATILE ORGANIC COMPOUND
ESTIMATED INITIAL EXTRACTED PRODUCTION RATES
STORONSKE COOPERAGE SITE**

<u>Compound</u>	<u>Vapor Concentration* (mg/l)</u>	<u>Estimated Production Rate**(lbs/hr)</u>
Tetrachloroethene	0.4026	1.96
1,1,1 Trichloroethane	0.0014	0.01
Trichloroethene	0.1704	0.83
1,2 Dichloroethane	0.0135	0.06
Xylenes	0.2386	1.16
Ethylbenzene	0.2147	1.04
Toluene	0.5363	2.61
Chlorobenzene	0.0471	0.23

*Based upon Pilot Test concentrations at extracted rate of 22 scfm.

**Assumes vapor concentration remains constant at total system flow rate of 1,300 scfm.

Catalytic or thermal oxidation could also be utilized for vapor treatment. However, based upon pilot testing, the expected total mass of VOCs to be extracted is 1,800 lbs and it is not likely that thermal or catalytic methods of vapor treatment would be cost effective.

3.5 Condensate Treatment

Water collected in the vapor/water separator would require treatment prior to discharge on-site. The water could also be transported off-site for disposal. It is anticipated that on-site treatment utilizing two 55-gallon liquid phase carbon adsorption drums can be economically utilized for this purpose. The drums would likely be effective for treatment without carbon exchange for the 1.5-year duration of the project. Separated water requiring treatment is anticipated to amount to approximately 150 to 500 gallons per month.

3.6 Testing Equipment

Vapor samples collected at the extraction wellheads and the carbon vapor treatment system influent, midpoint and effluent sample taps were performed utilizing gas-tight syringes. The samples were taken directly to a transportable GC on-site and analyzed for VOCs with site specific clean-up goals and additional compounds. These compounds consisted of tetrachloroethene, trichloroethene, 1,1,1-trichloroethane, xylenes, ethylbenzene, toluene, chlorobenzene, 1,2-dichloroethane, styrene and benzene. Other equipment utilized during system testing included a portable organic vapor monitor, flow measurement devices, vacuum and pressure gages, a dissolved oxygen meter and a water level gauging probe.

Equipment utilized during the pilot test generally operated satisfactorily and generated the necessary data for system performance evaluation.

3.7 Test Conditions and Procedures

The groundwater level conditions under which the pilot test was conducted were inconsistent with groundwater elevation measurements obtained previously at the site. In general,

groundwater elevations were approximately 3 feet lower than had been experienced during several rounds of groundwater elevation measurements conducted at the site during the RI/FS.

The lower water table had the effect of exposing additional soil volume to the pilot vapor extraction system which would tend to significantly increase the system effectiveness in removing the total mass of VOCs from the unsaturated zone. This effect is the same as that achieved by extracting groundwater and lowering groundwater levels during dual vapor extraction. Since the saturated thickness at the location of pilot testing was approximately only 1.5 feet, this limited observable effects of air sparging and rendered this portion of the test inconclusive at the test location, as well as for the thicker saturated locations of the site further removed from the former lagoon area.

Due to the low groundwater condition identified at the site, dual vapor extraction pilot testing was conducted which exposed additional quantities of soil to vapor extraction by lowering the water table the remaining 1.5 feet to bedrock. Results of dual vapor extraction system testing indicated increased total mass VOC removal rates as a result of exposure of this additional volume of contaminated soil to vacuum induced by the vapor extraction system.

3.8 Test Results

3.8.1 Vacuum Extraction Testing

The one day vacuum extraction test demonstrated the effectiveness of using vacuum extraction to remediate the unsaturated zone. A total mass of 1.8 lbs of VOCs was extracted from a single well in less than 3 hours of operation. Subsurface vacuums were detected up to 12 feet from the extraction well. Regression analysis performed on the collected data indicated that the calculated radius of influence is 15 feet for a 3 inch mercury (Hg) applied vacuum and 17 feet for a 6.5 inch Hg applied vacuum.

3.8.2 Air Sparging Testing

Because the saturated overburden thickness was 1.5 feet, which is substantially less than previous observations at the site, only limited air sparging data was able to be obtained. A determination of the pressure required to overcome hydrostatic forces and provide the point at which increasing pressure only marginally provides increases in air flow due to increasing turbulence and air flow was made. For the aquifer conditions observed at the site, 3 pounds per square inch gauge (psig) or six times the pressure needed to overcome hydrostatic forces was determined to be the point of significantly diminishing returns. No discernable increases in VOC concentrations or VOC extraction rates as a result of increasing air injection pressure were identified. Since the saturated thickness affected by the injection well was less than 1 foot, the cone of influence from sparging was likely only 1 to 2 feet in radius.

No significant increases in overall VOC removal during sparging as compared to vacuum extraction alone were observed. This was likely because of the limited area impacted by the injection well due to the low water table and the highest VOC soil concentrations identified in the upper 6 feet of soil (above the saturated zone). Noticeable decreases in groundwater VOC concentrations were observed, however, indicating that air sparging was effectively removing VOCs from the saturated zone.

3.8.3 Dual Vacuum Extraction Testing

Based upon regression analysis of measured subsurface vacuum at three monitoring wells, the calculated radius of influence during dual vacuum extraction (DVE) testing was 29 feet. The possible reasons for the significant increase in area affected by DVE is that a thicker unsaturated zone and a deeper well screen provide a larger area of influence.

In general, vapor concentrations during the DVE testing were lower than during either the vapor extraction (VE) testing or the air sparging testing. This may have been due to decreasing VOC soil concentrations in the area as a result of the previous tests or the additional exposed soil has lower contaminant concentrations. Mass removal rates of VOCs during the dual vapor

extraction testing were similar to those encountered during the VE testing.due to the higher flow rate utilized during DVE testing. Increases in VOC concentrations were observed during the first several hours after each of the two DVE start-ups providing evidence that the dewatering action exposed new areas to vapor flow.

4.0 PROPOSED SOIL VAPOR EXTRACTION AND TREATMENT SYSTEM

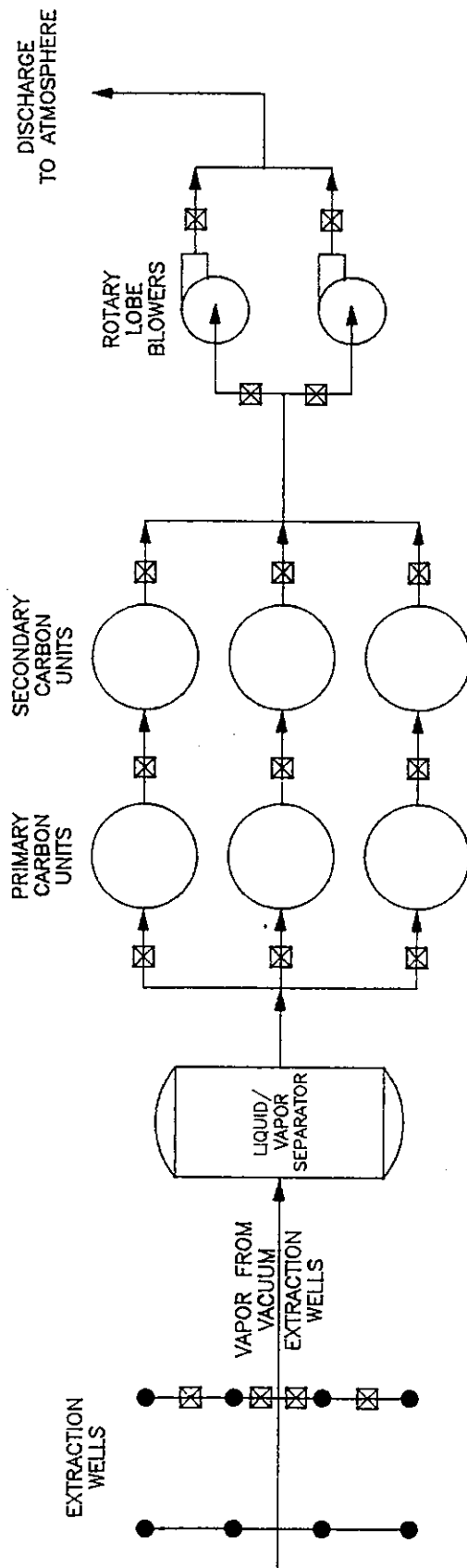
4.1 System Design Parameters

Vacuum extraction induces a negative pressure gradient within the soil matrix through wells specifically designed for this purpose. As the vacuum gradient propagates through the subsurface, liquid contaminants volatilize as the air and contaminant vapors migrate to the extraction well, where they are drawn to the surface for treatment. The process enhances the volatilization of VOCs in the soil matrix and desorbs contaminants from the soil matrix over time. A soil vapor extraction and treatment system schematic is illustrated in Figure 4-1.

The effectiveness of the vacuum extraction process at recovering VOCs is controlled by several factors including:

- Contaminant specific conditions, such as physical and chemical properties of the VOCs (vapor pressure, Henry's law constant and solubility);
- Subsurface soil characteristics (porosity, moisture content and permeability); and
- System operating parameters (well spacing and applied vacuum).

The equipment required for the implementation of a vacuum extraction system includes extraction wells, vacuum unit, liquid/vapor separation and subsequent treatment, vapor treatment unit, and system controls and instrumentation. The number of extraction wells required to attain cleanup goals is controlled by subsurface conditions. Generally, as the porosity and permeability of the subsurface soil decreases, the number of extraction wells required will increase. The vacuum unit design is based upon air flow rates and associated vacuum levels required to achieve the flow rates. Pilot testing conducted at the site established site specific conditions and estimates of required system design parameters necessary to achieve cleanup goals at the site as discussed below.



STORONSKE COOPERAGE SITE
TOWN OF SCHODACK, NEW YORK

SOIL VAPOR EXTRACTION AND TREATMENT SYSTEM
SCHEMATIC

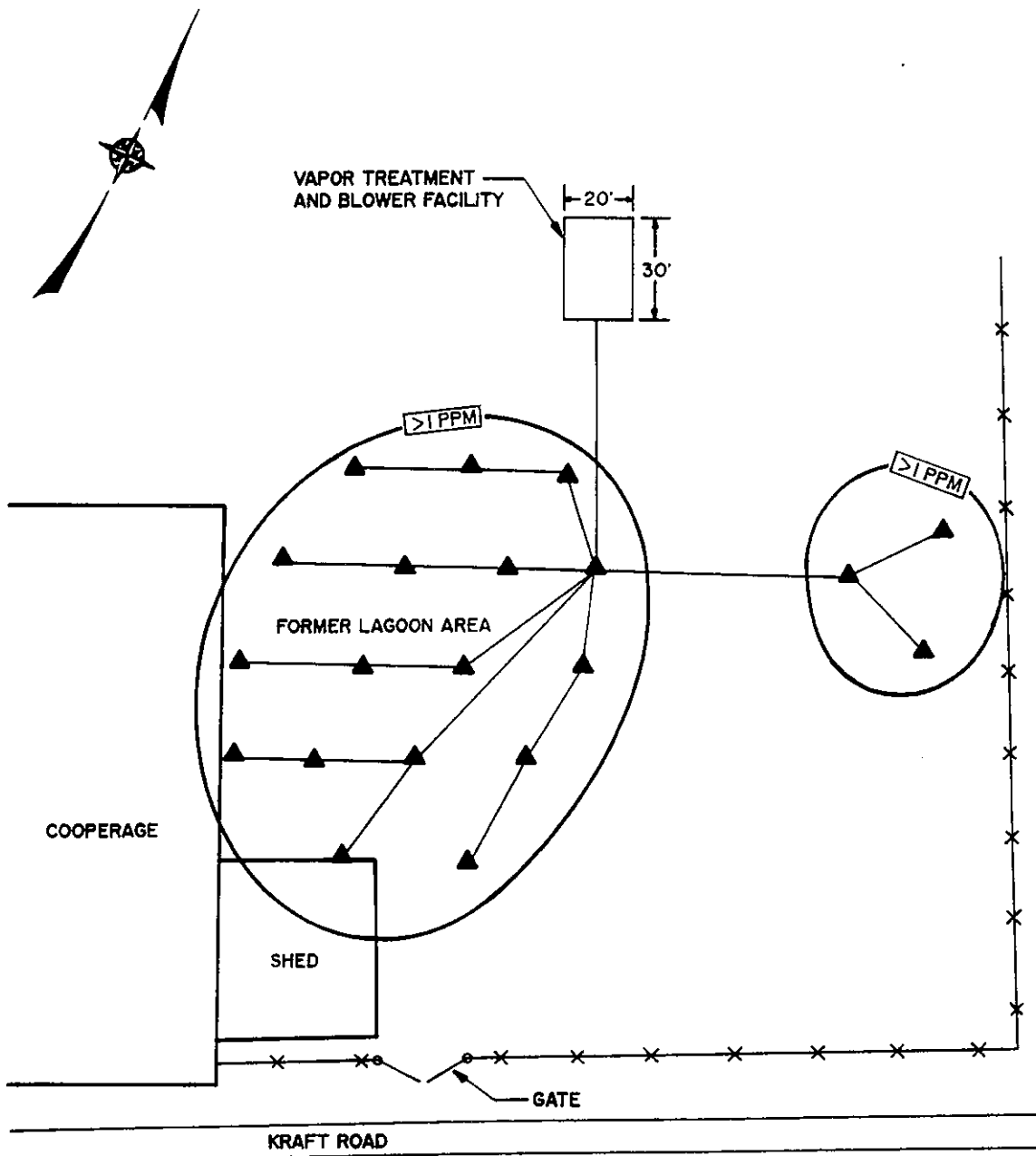
4.2 Extraction Wells

The determination of the number of extraction wells required is based upon the area of influence indicated by pilot testing measurements and the necessary duration to achieve cleanup goals. The duration is based upon the number of pore volumes of air drawn through the soil and increases in this volume are typically observed with closer well spacings. Based upon observations during the pilot testing, the radius of influence was calculated to be 17 feet. With assumptions of porosity (35%), an estimated 9,000 pore volumes necessary for required contaminant reductions, an unsaturated overburden thickness of 18 feet and a flow rate of 65 scfm measured during pilot testing, a duration to achieve cleanup goals at the site can be approximated at 1.5 years.

Based upon the areas of the site at which concentrations of total VOCs have been detected at greater than 1 ppm, approximately 20 vapor extraction wells would be required at the site. A soil vapor extraction and treatment system site plan is illustrated in Figure 4-2. Wells utilized for extraction can be constructed of 2-inch diameter PVC, since little difference in flow per foot of well screen was detected during pilot testing of 2-inch and 4-inch diameter extraction wells. The wells will be approximately 12 feet in depth to prevent drawing groundwater into the system and will have a screen length of 5 to 10 feet. Well screen lengths will be dependent upon permeability of soil during construction of the soil borings. An extraction well construction diagram is illustrated in Figure 4-3.

4.3 Monitoring Wells

Installation of monitoring wells to measure vacuum influences within the soil and determine vapor extraction system effectiveness on soil remediation will not be required. Monitoring can be performed by isolating extraction wells from the system and determining vacuums resulting from adjacent wells to monitor system influence effectiveness. In addition, it may be appropriate after performing half of the estimated system operation duration to perform soil borings within



LEGEND

- ▲ EXTRACTION WELL (TYPICAL)
- X— FENCE / PROPERTY BOUNDARY
- >1 PPM— VOC CONCENTRATION CONTOUR

0 50
SCALE IN FEET

STORONSKE COOPERAGE SITE
TOWN OF SCHODACK, NEW YORK

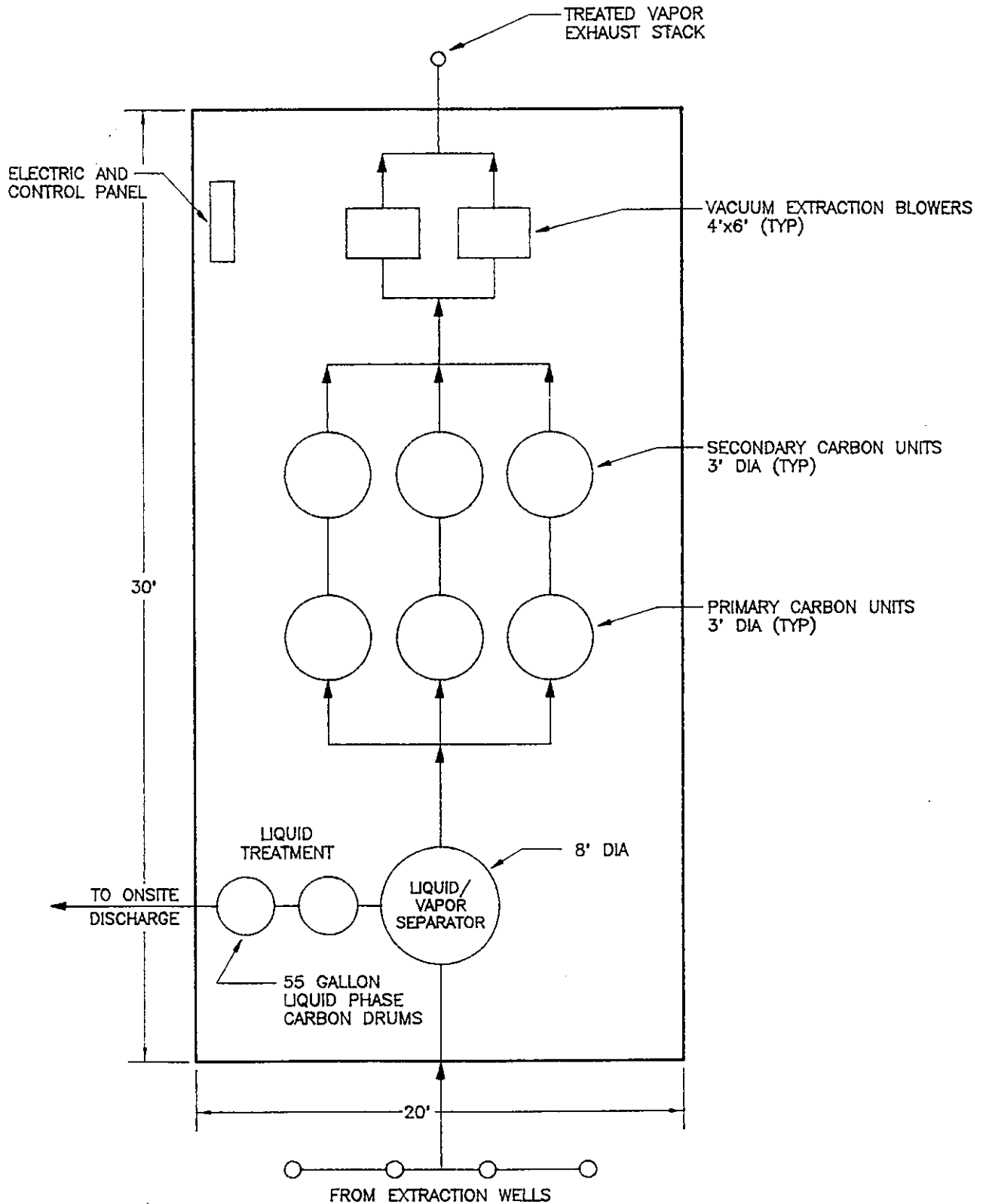
SOIL VAPOR EXTRACTION AND TREATMENT SYSTEM SITE PLAN



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Consulting Engineers

FIGURE 4 - 2

DIR: 1209 FILE: VAPORTB RDS-02/14/84



NOT TO SCALE

STORONSKE COOPERAGE SITE
TOWN OF SCHODACK, NEW YORK



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Consulting Engineers

PROPOSED VAPOR TREATMENT AND BLOWER FACILITY FLOOR PLAN

FIGURE 4-3

the extraction well network to determine progress in achieving cleanup goals at the site. If significant contamination is determined to be present after the system has been in operation for a while, installation of additional extraction wells resulting in a closer spacing may be appropriate. Testing locations and times may be based upon total VOC extraction rates from the individual wells.

4.4 Blowers

Based upon the pilot test, the size of the extraction system anticipated at the site consists of approximately 20 extraction wells and a total flow rate of 1300 scfm. A minimum well vacuum of 6.5 inches of mercury will be necessary to achieve the desired flow rates and an additional vacuum of 3.5 inches Hg are likely to be required to account for friction losses in system piping. The 1300 scfm at 10 inches Hg can be achieved by a 75-horsepower, positive displacement rotary lobe blower. To increase reliability and flexibility, use of two 40-hp blowers is recommended to meet vacuum/flow rate requirements. The proposed blower/vapor treatment facility plan is illustrated in Figure 4-4.

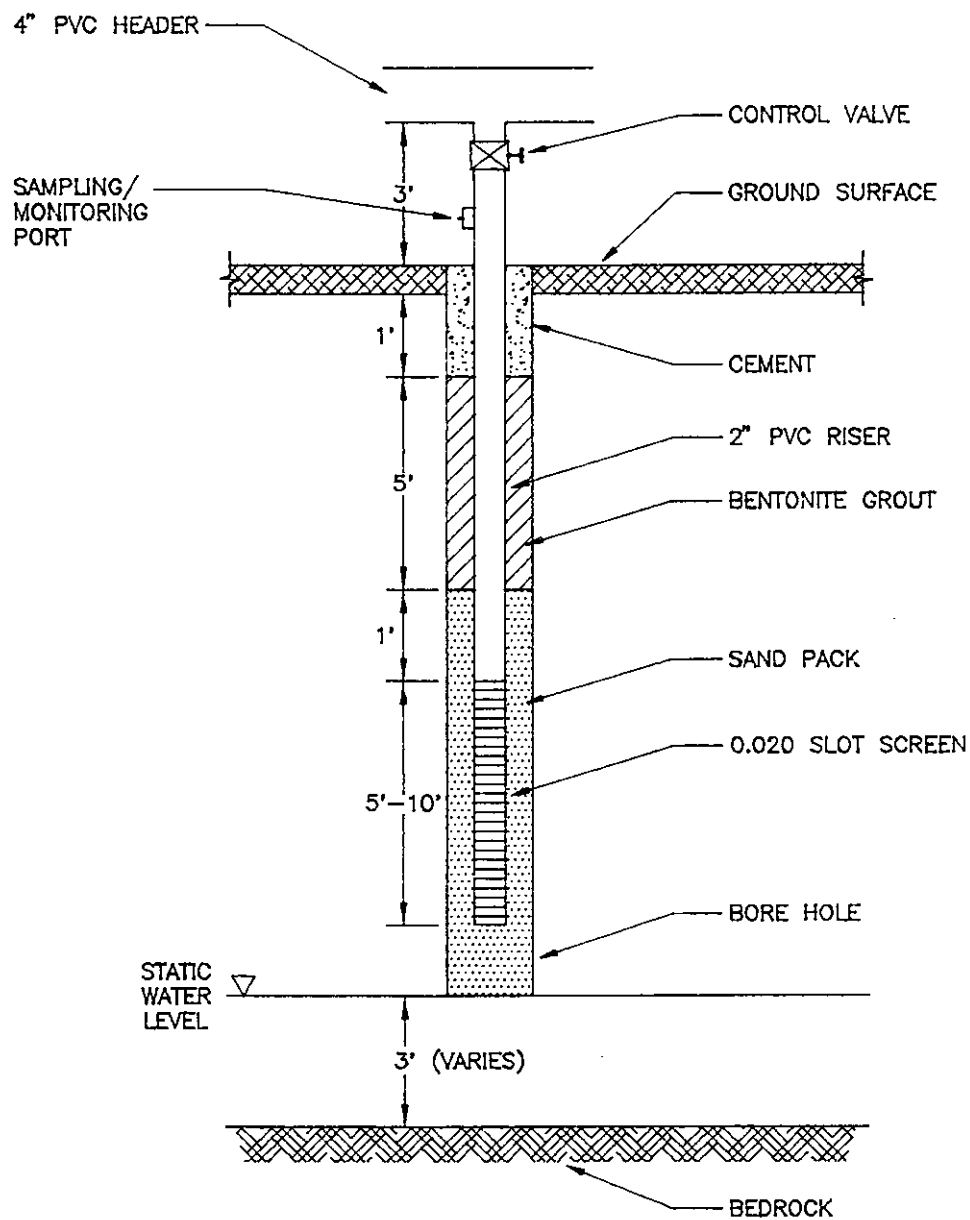
4.5 Piping

It is anticipated that schedule 40 PVC above ground piping can be utilized for all system piping. Size of piping will be 2-inch diameter at the well heads, increasing in size to 6-inch diameter at the main header entering the blowers through to ultimate discharge to atmosphere.

4.6 Vapor Treatment System

Based upon the results of the pilot test, a mass removal rate of 5 pounds per day per well is expected. Since the estimated total number of wells for vapor extraction is 20, a conservative initial estimate of the rate of total VOC extraction is 100 pounds per day. This is conservative due to the pilot test being conducted at the location of the former lagoon known to have the

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STORONSKE COOPERAGE SITE
TOWN OF SCHODACK, NEW YORK

EXTRACTION WELL CONSTRUCTION DIAGRAM



Dvirka and Bartilucci
Consulting Engineers

FIGURE 4-4

highest concentrations of total VOCs present. The actual average concentration over the duration of operation and for wells outside of the lagoon area is likely to be significantly less than this value. The average total VOC concentrations in soil as detected in prior investigations at the site was determined to be 50 mg/kg. Based upon an estimated total soil volume of 375,000 cubic feet from which soil samples with elevated VOC concentrations were collected, the total mass of VOCs in the soil is estimated to be approximately 1,800 lbs.

Carbon adsorption of VOCs was determined to be very effective during pilot testing. Based on an estimated initial system extraction rate of 100 lbs of VOCs per day and a carbon loading rate of 10%, carbon utilization rates may be as high as 1000 pounds per day during initial system operation. Based upon the estimated total mass of VOCs in the soil of 1,800 lbs, total carbon usage for vapor treatment during the duration of system operation is about 18,000 lbs. A conceptual design for the carbon adsorption system includes six 1000 lb vessels in three pairs. Each pair would operate in series and the three primary carbon vessels would require carbon replacement six times during the 1.5 year project duration.

4.7 Control System

System operation would be primarily controlled by manual methods. Valving arrangements would be designed to allow isolation and adjustment of individual extraction wells and isolation of equipment including blowers, water separator and carbon adsorption vessels. The system will be designed with fail safe operation in the event of power failure, so that no damage to equipment or discharge of untreated vapor would occur.

Sensors will be placed at appropriate locations to provide automatic shutdown of blowers should elevated operational temperatures or pressures be detected. Initially, monitoring of the system will be performed daily to determine actual carbon utilization rates and identify any potential operational problems. Approximately four weeks after start-up, an evaluation of system performance will be made to determine if weekly system inspections are adequate or if system modifications are required.

4.8 Auxiliary Power

As indicated in Section 4.7, the extraction system will be designed to allow fail safe operation. This is due to power outages being infrequent occurrences and they will have no long term effects on system operation other than to potentially increase the duration that the system will remain on-site equivalent to the period during which the system did not operate due to power loss. Since including auxiliary power activation at times of power failure would contribute significantly to the costs of the project while providing minimal operational benefits, including auxiliary power as part of the vapor extraction system will not be included in the contract documents.

4.9 Equipment Enclosure

Although equipment to be utilized at the site will be specified to be weather resistant, including electrical housings, placement of the blowers and water separator in an enclosure will provide additional noise abatement benefits as well as provide protection from temperature extremes which may contribute to premature failure of mechanical equipment. The enclosure will provide protection from precipitation, but it is not anticipated that it will be necessary to heat the structure due to heat generated in the blowers which will be transferred by way of the blower exhaust to the water separator and subsequently to the carbon adsorption vessels.

Should a prolonged shutdown occur due to power failure during subfreezing temperatures, thawing of the water separator may be required.

4.10 Sampling Taps

Sampling taps will be required on all extraction wells to determine the effectiveness of individual extraction locations. Measurements will include total VOCs, flow rate and static vacuums. Sampling taps will also be provided on the common header to the blower to determine total system VOC extraction concentrations, flow rates and static vacuums. There will be three sample taps provided on each pair of carbon adsorption vessels. One of these taps will be

provided prior to the primary vessel, one tap between the primary and secondary vessel and one tap will be located after the secondary vessel. These taps will be utilized to determine carbon removal efficiencies and time for contaminant break through, and carbon replacement.

4.11 Monitoring Frequency

Monitoring of all sampling taps should be performed daily during the first four weeks of system operation. This data will be useful in optimizing system effectiveness. Subsequent to the above start-up period, monitoring should be performed weekly to identify changes in system operating performance and determine adjustments that might be appropriate. Monitoring data will be evaluated to determine if adjustment is appropriate.

5.0 SOIL EXCAVATION, STORAGE, REMOVAL, BACKFILL AND REGRADING

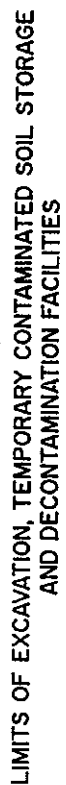
5.1 Definition of Limits of Excavation

Excavation limits have been identified based upon surface and subsurface samples from previous investigations which exceeded cleanup goals at the site, and the supplemental predesign soil sampling program which further defined the extent of contamination in known areas, as well as provided analytical data in areas of suspected contamination. Figure 5-1 indicates the aerial extent and depths of planned soil excavation based on previous and predesign investigations. In some locations, such as R-12 and R-16, the supplemental soil sampling program confirmed that the previously identified locations of contamination were confined to small areas less than 15 feet in radius from the original sampling location which exceeded the cleanup goal.

At location R-11, one sample (R-11SE) collected as part of the supplemental sampling program exceeded the cleanup goal for PCBs and lead, and the area to be excavated was extended in the south-east direction. End point sampling will be conducted after excavation of the contaminated soil to confirm that the soil cleanup goals have been attained as discussed in Section 5.5.

Locations R-5, R-13, R-17 and CB-17 had two of the three samples collected as part of the supplemental sampling program exceed the cleanup goals for PCBs, lead or both. The planned excavations in these areas were extended in the directions where the samples exceeding the cleanup criteria were detected.

The depths to which excavation will be performed in these identified areas is based upon the depth at which original and supplemental sampling results exceeded the cleanup criteria, the mobility of the contaminants of concern, site operations, and the need to protect human health and the environment.



Locations R-11, R-12, R-13, R-16 and R-7 were all surface soil samples which exceeded cleanup goals. Based upon operations at the site, the likely cause of the release of contaminants in these areas is attributable to leakage of drums stored on the site. As a result, excavation of soil to a depth of 6 inches, with 6 inches of backfill and an additional 6-inch soil cover and vegetation was determined to provide adequate protection of human health and the environment.

Soil contamination at locations CB-5 and CB-17 were identified at lower depths as a result of soil borings. Based upon the analytical results obtained in these areas, it was determined to excavate area CB-5 with additional area R-5 to a depth of 2 feet and area CB-17 to a depth of 3 feet.

The area of the former lagoon was identified as the primary source of contamination at the site. The area adjacent to the building and extending outward approximately 100 feet will be excavated to a depth of 4 feet. All excavated areas will be backfilled with an amount of clean fill equal to the contaminated material excavated as indicated in Section 5.5, and an additional 6 inches of soil or other permeable material (such as crushed stone) will be placed on top of the backfilled areas and remaining portions of the site.

5.2 Temporary On-Site Storage

Temporary on-site storage may be necessary to allow sampling of excavated soil to determine disposal requirements. Contaminated soil may need to be placed into roll-off containers or a lined area for staging. If staging is required, the temporary storage site will be located in an area that has been identified as not having elevated levels of contaminants in the soil and where it will not interfere with remediation of the site or disrupt of facility use to the greatest degree possible. The location of temporary on-site storage area is illustrated in Figure 5-1. If several samples indicated that no hazardous waste transportation or disposal restrictions are necessary, excavated material may be placed directly in vehicles for transportation to the disposal facility.

It should be noted that the preferred approach to securing approval from the disposal facility for acceptance of the contaminated soil will be to provide existing data and obtain additional samples for analysis prior to excavation if required by the disposal facility, so that temporary on-site storage of excavated soil will not be necessary.

5.3 Decontamination Facilities

On-site decontamination will be necessary to prevent spread of contaminants off-site or into additional on-site areas as a result of truck traffic or movement of excavation equipment from one location to another.

The decontamination pad will consist of a 60-mil high density polyethylene (HDPE) lined containment area which will be covered with 6 inches of sand and overlain by wood to support trucks and excavation equipment during decontamination. The pad will be sloped to a sump which will have a pump that will discharge wash water to drums or directly to carbon adsorption canisters for treatment prior to on-site discharge.

A steam cleaner along with scrub brushes and appropriate cleaning solutions will be utilized to ensure equipment is properly decontaminated prior to moving off-site or to other areas of the site. Visual inspection will be utilized to determine that decontamination has been undertaken properly.

5.4 Transportation and Disposal Requirements

Transportation of the contaminated soil will be regulated under New York State Department of Transportation (NYSDOT) regulations. These regulations limit the weight of vehicles/shipments and require precautions including information placards identifying the hazard classification of the material being transported. The ultimate disposal location has restrictions on waste entering the facility. These restrictions include contaminants such as PCBs that, when in concentrations greater than 50 ppm, are banned from direct landfilling and must undergo stabilization/fixation prior to landfilling or be incinerated. Due to the low concentrations and

types of contaminants present at the Storonske Cooperage site, it is unlikely that contaminated soil will require special handling and, depending upon characterization, may be classified as a nonhazardous waste with less significant transportation and disposal requirements.

5.5 Confirmatory Sampling

In all areas to be excavated, it will be necessary to perform end-point sampling to ensure that all contaminated soils associated with the location have been removed. Recommended parameters for analysis of end-point samples will be limited to PCBs and total lead based upon nonvolatile contaminants present in the on-site soil. It is recommended that field immuno assay techniques for PCBs with detection limits of 0.4 to 4 ppm, be performed at a minimum of three locations in the bottom of the excavation. If the field screening confirms that PCB contamination has been removed, it is recommended that samples be collected for laboratory analysis for lead and one sample from the highest concentration field screening location be analyzed for PCBs. These samples should be sent to a New York State Department of Health Environmental Laboratory Approval Program (ELAP) certified laboratory for analysis.

In locations where excavations will be performed to a depth greater than 6 inches, a minimum of four side wall field immuno assay PCB samples and will be obtained to ensure that the appropriate aerial extent of excavation has been performed. Should these samples confirm that appropriate excavation limits have been achieved, it is recommended that total lead samples be collected from the same locations as where the screening samples were collected and a PCB sample be collected from the side wall location with the highest field screen concentration. These samples should be sent to an ELAP certified laboratory to confirm the results of the field screening.

If the end-point and/or side wall samples indicate PCB levels greater than the cleanup criteria, additional soil excavation and end-point/side wall screening/confirmatory sample analysis will be conducted until the soil cleanup criteria is achieved. Should excavation to depths greater than 4 feet be required based upon results of confirmatory sampling, a concentration of 10 ppm

will be utilized as the screening criteria because the depth of clean fill will provide an effective barrier to PCB dermal exposure and therefore be adequately protective of human health.

5.6 Backfill Requirements

Excavations resulting from the removal of contaminated soil from the site will be backfilled with clean fill to the original grade. Fill will consist of clean material that has been tested for Target Compound List (TCL) +30 parameters to ensure that it is free of contaminants prior to placement at the site. The material will consist of a bank run sand or gravel which will not be of a low permeability such that precipitation infiltration would be inhibited.

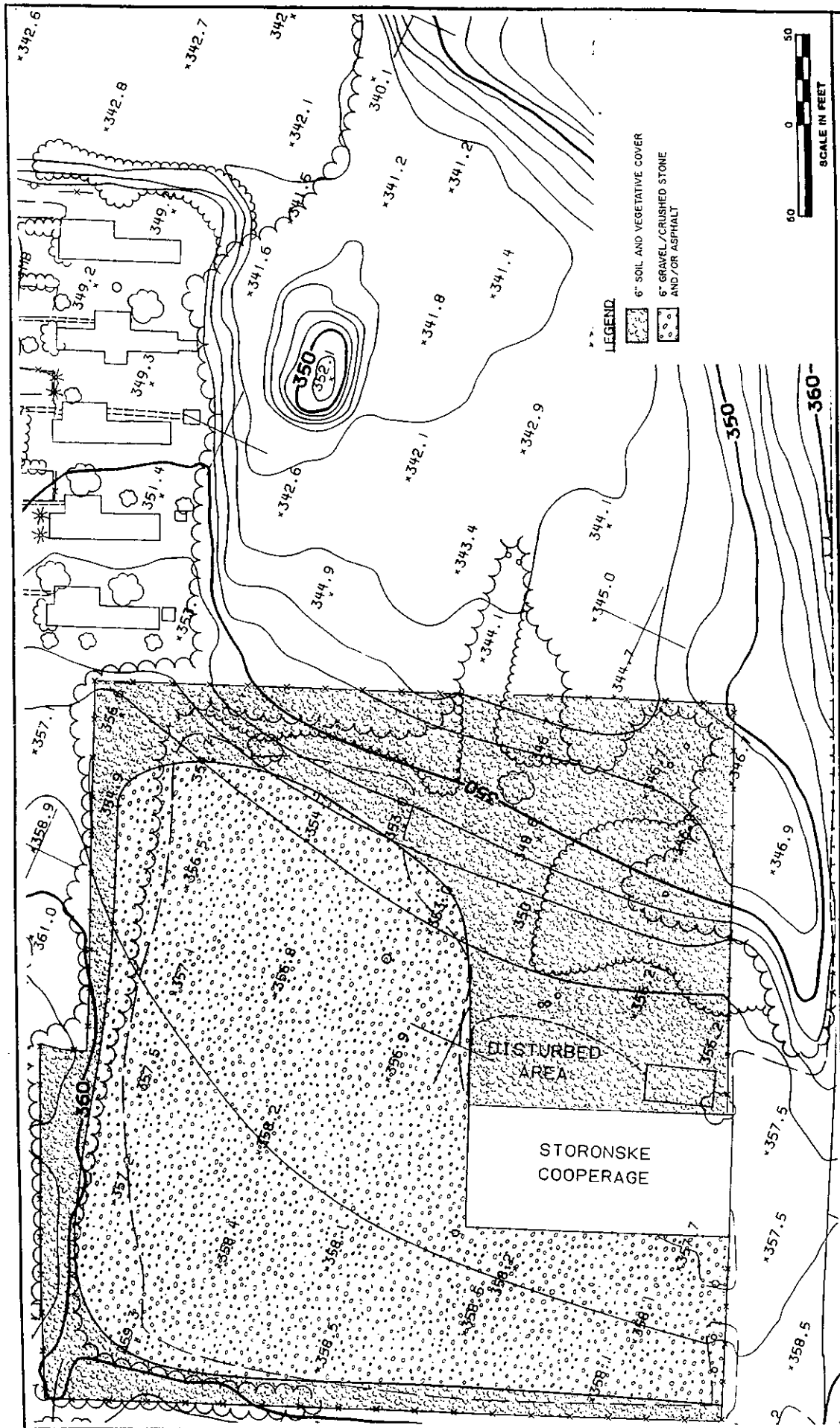
Once the backfill has been placed, minor regrading will be performed at the site in preparation for the final cover of 6 inches of soil or other suitable material (such as crushed stone) to be placed at the site as discussed in Sections 5.7 and 5.8.

5.7 Site Regrading

Site regrading will be necessary at the Storonske Cooperage site to provide suitable slopes for proper drainage and erosion control. A proposed site regrading and revegetation plan is illustrated in Figure 5-2. Although much of the area of the site is relatively flat, the most significantly contaminated area of the former lagoon has several short and steep slopes which may cause erosion of the final cover if not modified. Regrading may also be appropriate to minimize storm water from discharging off-site.

5.8 Placement of an Additional Six Inches of Clean Soil

The entire site, exclusive of the facility building, will be covered with 6 inches of clean soil or other suitable material. This cover will prevent contact with any potentially contaminated surface soil which has not been removed as part of excavation planned at the site. In areas of the site which are currently utilized to route vehicle traffic, and for parking and other vehicle



STORONSKE COOPERAAGE SITE
TOWN OF SHODACK, NEW YORK

SITE GRADING COVER AND REVEGETATION PLAN

traffic and equipment storage, placement of 6 inches of crushed stone, gravel or asphalt may be performed to prevent vehicle traffic from eroding these areas. All soil or other suitable material will be tested for TCL +30 parameters to ensure no contamination is present prior to transportation to the site. Portions of the site which are currently vegetated will have soil placed which is suitable for the establishment of a vegetative cover. These areas are illustrated in Figure 5-2.

5.9 Revegetation

Areas of the site which will not be utilized for vehicle traffic will be seeded with a grass mixture to allow the establishment of grass cover. Maintenance of the cover will be necessary to ensure that grass is established at the site and growth kept low to allow inspection and identification of burrowing animals, as well as prevention of growth which may cause a compromising of the protective cover. A quick growth/annual seed mixture to prevent erosion and a perennial seed will be utilized to establish the vegetation cover.

6.0 ESTIMATION OF CONSTRUCTION COSTS

Table 6-1 provides capital and O&M costs for the planned 1.5-year operation of both the vapor extraction and dual vapor extraction systems based on the data generated as a result of the pilot test. As indicated on the table, dual vapor extraction is significantly more costly (\$751,000) than standard vapor extraction (\$487,000). Since dual vapor extraction exposes only limited additional soil to the vacuum extraction process, the additional exposed soil has been identified to be less contaminated than the soil above, and the process would create treatment and disposal problems for the extracted groundwater, the DVE system is not recommended.

Table 6-2 provides estimated costs for soil excavation/disposal, backfill, regrading and revegetation. As indicated on the table, this portion of site remediation is expected to cost approximately \$421,000. Therefore, the total estimated cost for remediation of the Storonske Cooperage site, including vapor extraction is \$908,000.

Table 6-1

**ESTIMATED COST FOR VAPOR EXTRACTION
STORONSKE COOPERAGE SITE**

	<u>VE System</u>		<u>DVE System</u>	
CAPITAL COST				
Well Installation	20 wells, 15 ft deep	\$30,000	53 wells, 20 ft deep	\$86,000
Vacuum Extraction Blower	75 HP	\$35,000	100 HP	\$45,000
Carbon, vapor phase	18,600 lbs	\$56,000	18,600 lbs	\$56,000
Carbon, liquid phase			2,000 lbs	\$6,000
Utility Installation		\$28,000		\$30,000
Shed and Foundation Construction		\$35,000		\$35,000
Piping and System Installation		<u>\$33,000</u>		<u>\$52,000</u>
TOTAL CAPITAL COST		\$217,000		\$310,000
OPERATING COST				
Labor, per month		\$6,000		\$11,000
Materials and Expenses	\$500		\$1,000	
Analytical and Laboratory		\$4,500		\$7,000
Utilities		<u>\$4,000</u>		<u>\$5,500</u>
OPERATING COST PER MONTH	<u>\$15,000</u>		<u>\$24,500</u>	
TOTAL OPERATING COST	18 months	\$270,000	18 months	\$441,000
TOTAL COST		\$487,000		\$751,000

Table 6-2

**ESTIMATED COST FOR EXCAVATION AND COVER
STORONSKE COOPERAGE SITE**

<u>Item</u>	<u>Quantity</u>	<u>Units</u>	<u>Unit Cost</u>	<u>Total Cost</u>
<u>Excavation and Disposal</u>				
Excavate contaminated material	2,400	cy	\$14	\$33,600
Additional soil cuttings contained in drums	50	cy	\$20	\$1,000
Transport to Seneca Meadows Landfill disposal facility in Waterloo, NY (soil)	2,450	cy	\$25	\$61,250
Disposal at off-site facility (nonhazardous soil)	2,400	cy	\$50	\$120,000
<u>Backfill, Cover Material and Installation</u>				
Purchase/haul/place backfill material (bank run)	2,400	cy	\$12	\$28,800
Purchase/haul/place 6 inches topsoil	2,500	cy	\$18	\$45,000
Seed, fertilizer and mulch	15,000	sy	\$1	\$15,000
<u>Other Costs</u>				
Safety program	---	lump sum	\$8,000	\$8,000
Dust control	---	lump sum	\$5,000	\$5,000
Runoff control	---	lump sum	\$5,000	\$5,000
Equipment decontamination	---	lump sum	\$4,000	\$4,000
Mobilization/demobilization	---	lump sum	\$10,000	\$10,000
<u>Contingency Allowance (25%)</u>				<u>\$84,000</u>
TOTAL COST				\$421,000

APPENDIX A

PRE-DESIGN INVESTIGATION ANALYTICAL DATA

TABLE A-1
STORONSKE COOPERAGE SITE
PRE-DESIGN INVESTIGATION
SOIL SAMPLING

VOLATILE ORGANIC COMPOUND RESULTS

SAMPLE ID	01D&B	02D&B	CB-5N	CB-5SE	CB-17N	CB-17SE	CB-17SW	SITE
DATE OF COLLECTION	4/19/93	4/19/93	4/19/93	4/19/93	4/20/93	4/20/93	4/20/93	SPECIFIC
% MOISTURE	18	19	13	5	13	21	7	CLEAN-UP
DILUTION FACTOR	1	1	1	1	1	1	1	GOALS
COMPOUNDS	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)
Chloromethane	U	U	U	U	U	U	U	NA
Bromomethane	U	U	U	U	U	U	U	NA
Vinyl Chloride	U	U	U	U	U	U	U	NA
Chloroethane	U	U	U	U	U	U	U	NA
Methylene Chloride	6 BJ	5 BJ	3 BJ	16 BJ	3 BJ	14 BJ	3 BJ	NA
Acetone	9 BJ	11 BJ	3 BJ	29 BJ	4 BJ	19 BJ	4 BJ	NA
Carbon Disulfide	U	U	U	U	U	U	U	NA
1,1-Dichloroethene	U	U	U	U	U	U	U	NA
1,1-Dichloroethane	U	U	U	U	U	U	U	NA
1,2-Dichloroethene (total)	U	U	U	U	U	U	U	NA
Chloroform	U	U	U	U	U	U	U	NA
1,2-Dichloroethane	U	U	U	27	U	10 BJ	3 J	100
2-Butanone	U	U	U	U	2 J	U	U	NA
1,1,1-Trichloroethane	U	U	U	U	2 J	U	2 J	1000
Carbon Tetrachloride	U	U	U	U	U	U	U	NA
Vinyl Acetate	U	U	U	U	U	U	U	NA
Bromodichloromethane	U	U	U	U	U	U	U	NA
1,2-Dichloropropane	U	U	U	U	U	U	U	NA
cis-1,3-Dichloropropene	U	U	U	U	U	U	1	NA
Trichloroethene	U	U	U	U	U	U	U	NA
Dibromochloromethane	U	U	U	U	U	U	U	1000
1,1,2-Trichloroethane	U	U	U	U	U	U	U	NA
Benzene	U	U	U	U	U	U	U	NA
trans-1,3-Dichloropropene	U	U	U	U	U	U	U	NA
Bromoform	U	U	U	U	U	U	U	NA
4-Methyl-2-pentanone	U	U	U	U	U	U	U	NA
2-Hexanone	U	U	U	U	U	U	U	NA
Tetrachloroethene	U	U	U	U	U	U	7	NA
1,1,2,2-Tetrachloroethane	U	U	U	U	U	U	U	1500
Toluene	U	U	U	U	U	U	U	NA
Chlorobenzene	U	U	U	U	U	U	U	1500
Ethylbenzene	U	U	U	U	U	U	U	1500
Styrene	U	U	U	U	U	U	U	5500
Xylene (total)	U	U	U	U	U	U	U	NA

QUALIFIERS

B: Compound found in the blank as well as the sample
J: Compound found below the CRDL, value is estimated
U: Compound analyzed for but not detected

NOTES:

NA: Not Applicable

NOTE: No site specific clean-up goals for volatile organic compounds were exceeded.

TABLE A-2
STORONSKE COOPERAGE SITE
PRE-DESIGN INVESTIGATION
SOIL SAMPLING
VOLATILE ORGANIC COMPOUND RESULTS

SAMPLE ID	CB-23N	CB-23SE	CB-23SW	R-1SE	R-1SW	R-5N	R-5SE	SITE SPECIFIC CLEAN-UP GOALS (ug/kg)
DATE OF COLLECTION	4/19/93	4/19/93	4/19/93	4/19/93	4/19/93	4/19/93	4/19/93	
% MOISTURE	13	11	8	7	12	24	18	
DILUTION FACTOR	1	1	1	1	1	1	1	
COMPOUNDS	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	
Chloromethane	U	U	U	U	U	U	U	NA
Bromomethane	U	U	U	U	U	U	U	NA
Vinyl Chloride	U	U	U	U	U	U	U	NA
Chloroethane	U	U	U	U	U	U	U	NA
Methylene Chloride	6 BJ	5 BJ	4 BJ	2 BJ	2 BJ	3 BJ	4 BJ	NA
Acetone	7 BJ	7 BJ	5 BJ	5 BJ	U	15 B	8 BJ	NA
Carbon Disulfide	U	U	U	U	U	U	U	NA
1,1-Dichloroethene	U	U	U	U	U	U	U	NA
1,1-Dichloroethane	U	U	U	U	U	U	U	NA
1,2-Dichloroethene (total)	U	U	U	U	U	U	U	NA
Chloroform	U	U	U	U	U	U	U	NA
1,2-Dichloroethane	U	U	U	U	U	U	U	100
2-Butanone	U	U	U	U	U	U	U	NA
1,1,1-Trichloroethane	U	U	U	U	U	U	U	1000
Carbon Tetrachloride	U	U	U	U	U	U	U	NA
Vinyl Acetate	U	U	U	U	U	U	U	NA
Bromodichloromethane	U	U	U	U	U	U	U	NA
1,2-Dichloropropane	U	U	U	U	U	U	U	NA
cis-1,3-Dichloropropene	U	U	U	U	U	U	U	NA
Trichloroethene	U	U	U	U	U	U	U	1000
Dibromochloromethane	U	U	U	U	U	U	U	NA
1,1,2-Trichloroethane	U	U	U	U	U	U	U	NA
Benzene	U	U	U	U	U	U	U	NA
trans-1,3-Dichloropropene	U	U	U	U	U	U	U	NA
Bromoform	U	U	U	U	U	U	U	NA
4-Methyl-2-pentanone	U	U	U	U	U	U	U	NA
2-Hexanone	U	U	U	U	U	U	U	NA
Tetrachloroethene	U	U	U	U	U	U	U	NA
1,1,2,2-Tetrachloroethane	U	U	U	U	U	U	U	1500
Toluene	2 J	U	2 J	U	U	U	2 J	NA
Chlorobenzene	U	U	U	U	U	U	U	1500
Ethylbenzene	U	U	U	U	U	U	U	1500
Styrene	U	U	U	U	U	U	U	5500
Xylene (total)	11 J	U	U	U	U	6 J	5 J	NA

QUALIFIERS
B: Compound found in the blank as well as the sample
J: Compound found below the CRDL, value is estimated
U: Compound analyzed for but not detected

NOTES:
NA: Not Applicable

NOTE: No site specific clean-up goals for volatile organic compounds were exceeded.

TABLE A-3
STORONSKE COOPERAGE SITE
PRE-DESIGN INVESTIGATION
SOIL SAMPLING

VOLATILE ORGANIC COMPOUND RESULTS

SAMPLE ID	R-5SRE 4/19/93	R-5SW 4/19/93	R-5SWDL 4/19/93	R-11N 4/20/93	R-11SE 4/20/93	R-11SW 4/20/93	R-12N 4/20/93	SITE SPECIFIC CLEAN-UP GOALS (ug/kg)
% MOISTURE	18	24	24	2	9	6	13	
DILUTION FACTOR	1	1	5	1	1	1	1	
COMPOUNDS	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	
Chloromethane	U	U	U	U	U	U	U	NA
Bromomethane	U	U	U	U	U	U	U	NA
Vinyl Chloride	U	U	U	U	U	U	U	NA
Chloroethane	U	U	U	U	U	U	U	NA
Methylene Chloride	4 BJ	10 BJ	21 BJ	2 BJ	5 BJ	4 BJ	5 BJ	NA
Acetone	10 BJ	10 BJ	28 BJ	4 BJ	5 BJ	10 BJ		NA
Carbon Disulfide	U	U	U	U	U	U	U	NA
1,1-Dichloroethene	U	U	U	U	U	U	U	NA
1,1-Dichloroethane	U	U	U	U	U	U	U	NA
1,2-Dichloroethene (total)	U	U	U	U	U	U	U	NA
Chloroform	U	U	U	U	U	U	U	NA
1,2-Dichloroethane	U	U	U	U	U	U	U	100
2-Butanone	U	U	U	U	U	U	U	1000
1,1,1-Trichloroethane	U	U	U	U	U	U	U	NA
Carbon Tetrachloride	U	U	U	U	U	U	U	NA
Vinyl Acetate	U	U	U	U	U	U	U	NA
Bromodichloromethane	U	U	U	U	U	U	U	NA
1,2-Dichloropropane	U	U	U	U	U	U	U	NA
cis-1,3-Dichloropropene	U	U	U	U	U	U	U	NA
Trichloroethene	U	U	U	U	U	U	U	1000
Dibromochloromethane	U	U	U	U	U	U	U	NA
1,1,2-Trichloroethane	U	U	U	U	U	U	U	NA
Benzene	U	U	U	U	U	U	U	NA
trans-1,3-Dichloropropene	U	U	U	U	U	U	U	NA
Bromoform	U	U	U	U	U	U	U	NA
4-Methyl-2-pentanone	U	U	U	U	U	U	U	NA
2-Hexanone	U	U	U	U	U	U	U	NA
Tetrachloroethene	U	U	U	U	U	U	U	1500
1,1,2,2-Tetrachloroethane	U	U	U	U	U	U	U	NA
Toluene	U	2	U	U	U	U	U	1500
Chlorobenzene	U	U	U	U	U	U	U	1500
Ethylbenzene	U	U	U	U	U	U	U	5500
Styrene	U	U	U	U	U	U	U	NA
Xylene (total)	U	U	U	U	U	U	U	1200

QUALIFIERS

B: Compound found in the blank as well as the sample
J: Compound found below the CRDL, value is estimated
U: Compound analyzed for but not detected

NOTES

RE: Sample was reanalyzed
DL: Sample was analyzed at a secondary dilution
NA: Not Applicable

NOTE: No site specific clean-up goals for volatile organic compounds were exceeded.

TABLE A-4
STORONSKE COOPERAGE SITE
PRE-DESIGN INVESTIGATION
SOIL SAMPLING
VOLATILE ORGANIC COMPOUND RESULTS

SAMPLE ID	R-12SE	R-12SW	R-13N	R-13SE	R-13SW	R-16N	R-16SE	SITE
DATE OF COLLECTION	4/20/93	4/20/93	4/20/93	4/20/93	4/20/93	4/20/93	4/20/93	SPECIFIC
% MOISTURE	14	9	10	8	8	17	8	CLEAN-UP
DILUTION FACTOR	1	1	1	1	1	1	1	GOALS
COMPOUNDS	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)
Chloromethane	U	U	U	U	U	U	U	NA
Bromomethane	U	U	U	U	U	U	U	NA
Vinyl Chloride	U	U	U	U	U	U	U	NA
Chloroethane	U	U	U	U	U	U	U	NA
Methylene Chloride	2 BJ	2 BJ	2 BJ	1 BJ	U	2 BJ	2 BJ	NA
Acetone	7 BJ	3 BJ	4 BJ	3 BJ	U	5 BJ	4 BJ	NA
Carbon Disulfide	U	U	U	U	U	U	U	NA
1,1-Dichloroethene	U	U	U	2 J	U	U	U	NA
1,1-Dichloroethane	U	U	U	U	U	U	U	NA
1,2-Dichloroethene (total)	U	U	U	U	U	U	U	NA
Chloroform	U	U	U	U	U	U	U	NA
1,2-Dichloroethane	U	U	U	U	U	U	U	100
2-Butanone	U	U	U	U	U	U	U	NA
1,1,1-Trichloroethane	U	U	U	U	U	U	8 J	1000
Carbon Tetrachloride	U	U	U	U	U	U	U	NA
Vinyl Acetate	U	U	U	U	U	U	U	NA
Bromodichloromethane	U	U	U	U	U	U	U	NA
1,2-Dichloropropane	U	U	U	U	U	U	U	NA
cis-1,3-Dichloropropene	U	U	U	U	U	U	U	NA
Trichloroethene	U	U	U	2 J	U	U	50	NA
Dibromochloromethane	U	U	U	U	U	U	U	1000
1,1,2-Trichloroethane	U	U	U	U	U	U	U	NA
Benzene	U	U	U	2 J	U	U	U	NA
trans-1,3-Dichloropropene	U	U	U	U	U	U	U	NA
Bromoform	U	U	U	U	U	U	U	NA
4-Methyl-2-pentanone	U	U	U	U	U	U	U	NA
2-Hexanone	U	U	U	U	U	U	2 J	NA
Tetrachloroethene	U	U	U	U	U	U	2 J	1500
1,1,2,2-Tetrachloroethane	U	U	U	U	U	U	U	NA
Toluene	2 J	U	U	3 J	U	U	U	1500
Chlorobenzene	U	U	U	2 J	U	U	U	1500
Ethylbenzene	U	U	U	U	U	U	U	5500
Styrene	U	U	U	U	U	U	U	NA
Xylene (total)	U	U	U	U	U	U	U	1200

QUALIFIERS
B: Compound found in the blank as well as the sample
J: Compound found below the CRDL, value is estimated
U: Compound analyzed for but not detected

NOTES:
NA: Not Applicable

NOTE: No site specific clean-up goals for volatile organic compounds were exceeded.

TABLE A-5
STORNSKE COOPERAGE SITE
PRE-DESIGN INVESTIGATION
SOIL SAMPLING
VOLATILE ORGANIC COMPOUND RESULTS

SAMPLE ID	R-16SW	R-17N	R-17NRE	R-17SE	R-17SW	R-17SWDL	SITE
DATE OF COLLECTION	4/20/93	4/20/93	4/20/93	4/20/93	4/20/93	4/20/93	SPECIFIC
% MOISTURE	6	12	12	13	11	11	CLEAN-UP
DILUTION FACTOR	5	1	1	1	1	1.67	GOALS
COMPOUNDS	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)
Chloromethane	U	U	U	U	U	U	NA
Bromomethane	U	U	U	U	U	U	NA
Vinyl Chloride	U	U	U	U	U	U	NA
Chloroethane	U	U	U	U	U	U	NA
Methylene Chloride	15 BJ	5 BJ	4 BJ	3 BJ	6 BJ	6 BJD	NA
Acetone	50 BJ	4 BJ	5 BJ	3 BJ	7 BJ	5 BJD	NA
Carbon Disulfide	U	U	U	U	U	U	NA
1,1-Dichloroethene	U	U	U	U	U	U	NA
1,1-Dichloroethane	U	U	U	U	9 J	U	NA
1,2-Dichloroethene (total)	U	U	U	U	3 J	2 JD	NA
Chloroform	U	U	U	U	2 J	U	NA
1,2-Dichloroethane	U	U	U	U	2 J	U	100
2-Butanone	U	U	U	U	210	120	1000
1,1,1-Trichloroethane	U	U	U	U	U	U	NA
Carbon Tetrachloride	U	U	U	U	U	U	NA
Vinyl Acetate	U	U	U	U	U	U	NA
Bromodichloromethane	U	U	U	U	U	U	NA
1,2-Dichloropropane	U	U	U	U	U	U	NA
cis-1,3-Dichloropropene	U	U	U	U	2 J	U	1000
Trichloroethene	U	U	U	U	U	U	NA
Dibromochloromethane	U	U	U	U	U	U	NA
1,1,2-Trichloroethane	U	U	U	U	U	U	NA
Benzene	U	U	U	U	U	U	NA
trans-1,3-Dichloropropene	U	U	U	U	U	U	NA
Bromoform	U	U	U	U	U	U	NA
4-Methyl-2-pentanone	U	U	U	U	U	U	NA
2-Hexanone	U	U	U	U	6 J	8 JD	NA
Tetrachloroethene	920	9 J	6	U	U	U	1500
1,1,2,2-Tetrachloroethane	U	U	U	U	U	U	NA
Toluene	U	U	U	U	U	U	1500
Chlorobenzene	U	U	U	U	U	U	1500
Ethylbenzene	U	U	U	U	U	U	5500
Styrene	U	U	U	U	U	U	NA
Xylene (total)	U	U	U	U	U	U	1200

QUALIFIERS
B: Compound found in the blank as well as the sample
D: Concentration is from a diluted run
J: Compound found below the CRDL, value is estimated
U: Compound analyzed for but not detected

NOTES
RE: Sample was reanalyzed
DL: Sample was analyzed at a secondary dilution
NA: Not Applicable

NOTE: No site specific clean-up goals for volatile organic compounds were exceeded.

TABLE A-6
STORONSKE COOPERAGE SITE
PRE-DESIGN INVESTIGATION
SOIL SAMPLING
PCB RESULTS

SAMPLE ID	01D&B	02D&B	CB-5N	CB-5SE	CB-17N	CB-17SE	CB-17SW
DATE OF COLLECTION	4/19/93	4/19/93	4/19/93	4/19/93	4/20/93	4/20/93	4/20/93
% MOISTURE	18	19	13	5	13	21	7
DILUTION FACTOR	1	1	1	10	1	1	5
COMPOUNDS	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)
Aroclor-1016	U	U	U	U	U	U	U
Aroclor-1221	U	U	U	U	U	U	U
Aroclor-1232	U	U	U	U	U	U	U
Aroclor-1242	U	U	U	U	U	U	U
Aroclor-1248	U	U	U	U	38 P	80 P	620 P
Aroclor-1254	U	U	U	280 JP	5.5 JP	12 J	U
Aroclor-1260	U	U	U	U	U	U	U


QUALIFIERS

C: Compound identification confirmed by GC/MS

J: Compound found below the CRDL, value is estimated

P: Percent difference in concentrations is >25% between the 2 columns, lower value is reported

U: Compound analyzed for but not detected

 : Result exceeds clean-up goal

NOTE: Clean-up goal for individual Aroclors is 1000 ug/kg

TABLE A-7
STORONSKE COOPERAGE SITE
PRE-DESIGN INVESTIGATION
SOIL SAMPLING
PCB RESULTS

SAMPLE ID	CB-23N	CB-23SE	CB-23SW	R-1SE	R-1SW	R-5N	R-5SE
DATE OF COLLECTION	4/19/93	4/19/93	4/19/93	4/19/93	4/19/93	4/19/93	4/19/93
% MOISTURE	13	11	8	7	12	24	18
DILUTION FACTOR	1	10	1	1	1	1	10
COMPOUNDS	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)
Aroclor-1016	U	U	U	U	U	U	U
Aroclor-1221	U	U	U	U	U	U	U
Aroclor-1232	U	U	U	U	U	U	U
Aroclor-1242	U	U	U	U	U	U	U
Aroclor-1248	U	U	U	U	U	U	U
Aroclor-1254	U	U	U	U	U	U	U
Aroclor-1260	21 J	76 JP	U	32 J	U	6.9 J	U

QUALIFIERS

C: Compound identification confirmed by GC/MS

J: Compound found below the CRDL, value is estimated

P: Percent difference in concentrations is >25% between the 2 columns, lower value is reported

U: Compound analyzed for but not detected

8800 PG : Result exceeds clean-up goal

NOTE: Clean-up goal for individual Aroclors is 1000 ug/kg

TABLE A-8
STORONSKE COOPERAGE SITE
PRE-DESIGN INVESTIGATION
SOIL SAMPLING
PCB RESULTS

SAMPLE ID	R-5SEDL 4/19/93	R-5SW 4/19/93	R-5SWDL 4/19/93	R-11N 4/20/93	R-11SE 4/20/93	R-11SEDL 4/20/93	R-11SW 4/20/93	R-12N 4/20/93
DATE OF COLLECTION								
% MOISTURE	18	24	24	2	9	9	6	13
DILUTION FACTOR	100	2	20	5	10	100	2	1
COMPOUNDS	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)
Aroclor-1016								
Aroclor-1221	U	U	U	U	U	U	U	U
Aroclor-1232	U	U	U	U	U	U	U	U
Aroclor-1242	U	U	U	U	U	U	U	U
Aroclor-1248	13000 PC	2000 PC	2100 PC	780	4900 C	5100 C	210 P	U
Aroclor-1254	U	U	U	76 J	140	U	11 J	4.7 JP
Aroclor-1260								

QUALIFIERS

C: Compound identification confirmed by GC/MS

J: Compound found below the CRDL, value is estimated

P: Percent difference in concentrations is >25% between the 2 columns, lower value is reported

U: Compound analyzed for but not detected

NOTES

RE: Sample was reanalyzed

DL: Sample was analyzed at a secondary dilution

:Result exceeds clean-up goal

NOTE: Clean-up goal for individual Aroclors is 1000 ug/kg

TABLE A-9
STORNSKE COOPERAGE SITE
PRE-DESIGN INVESTIGATION
SOIL SAMPLING
PCB RESULTS

SAMPLE ID	R-12SE	R-12SW	R-13N	R-13SE	R-13SW	R-16N	R-16SE
DATE OF COLLECTION	4/20/93	4/20/93	4/20/93	4/20/93	4/20/93	4/20/93	4/20/93
% MOISTURE	14	9	10	8	8	17	8
DILUTION FACTOR	1	1	1	1	1	1	1
COMPOUNDS	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)
Aroclor-1016	U	U	U	U	U	U	U
Aroclor-1221	U	U	U	U	U	U	U
Aroclor-1232	U	U	U	U	U	U	U
Aroclor-1242	U	U	U	U	U	U	U
Aroclor-1248	49 P	U	80 P	33 J	U	200	U
Aroclor-1254	U	U	U	U	U	U	U
Aroclor-1260	25 J	U	36 JP	14 J	U	280	15 J

QUALIFIERS

C: Compound Identification confirmed by GC/MS

J: Compound found below the CRDL, value is estimated

P: Percent difference in concentrations is >25% between the 2 columns, lower value is reported

U: Compound analyzed for but not detected

 : Result exceeds clean-up goal

NOTE: Clean-up goal for individual Aroclors is 1000 ug/kg

TABLE A-10
STORONSKE COOPERAGE SITE
PRE-DESIGN INVESTIGATION
SOIL SAMPLING
PCB RESULTS

SAMPLE ID	R-16SW	R-17N	R-17NRE	R-17SE	R-17SW	R-17SWDL
DATE OF COLLECTION	4/20/93	4/20/93	4/20/93	4/20/93	4/20/93	4/20/93
% MOISTURE	6	12	12	13	11	11
DILUTION FACTOR	5	50	500	1	10	100
COMPOUNDS	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)	(ug/kg)
Aroclor-1016	U	U	U	U	U	U
Aroclor-1221	U	U	U	U	U	U
Aroclor-1232	U	U	U	U	U	U
Aroclor-1242	U	U	U	U	U	U
Aroclor-1248	14 J	11000 PC	14000 JPC	78	2200	2600 JP
Aroclor-1254	U	U	U	150 P	540 P	630 JP
Aroclor-1260	23 J	U	U			

QUALIFIERS

- C: Compound identification confirmed by GC/MS
J: Compound found below the CRDL, value is estimated
P: Percent difference in concentrations is >25% between the 2 columns, lower value is reported
U: Compound analyzed for but not detected

NOTES


- RE: Sample was reanalyzed
DL: Sample was analyzed at a secondary dilution
: Result exceeds clean-up goal

NOTE: Clean-up goal for individual Aroclors is 1000 ug/kg

TABLE A-11
STORONSKE COOPERAGE SITE
PRE-DESIGN INVESTIGATION
SOIL SAMPLING
LEAD RESULTS

SAMPLE ID	DATE OF COLLECTION	% SOLIDS	DILUTION FACTOR	LEAD (mg/kg)
01D&B	4/19/93	82.4	1	13.60
02D&B	4/19/93	78.2	1	27.90
CB-17N	4/20/93	88.5	1	41.20
CB-17SE	4/20/93	77.3	1	48.80
CB-17SW	4/20/93	91.2	1	31.00
CB-23N	4/19/93	86.2	1	30.20
CB-23SE	4/19/93	86.4	1	193.00
CB-23SW	4/19/93	92.9	1	25.50
CB-5N	4/19/93	85.7	1	31.70
CB-5SE	4/19/93	73	1	66.00
R-1SE	4/19/93	90.5	1	57.30
R-1SW	4/19/93	89	1	20.10
R-5N	4/19/93	78.1	1	25.40
R-5SE	4/19/93	86.9	1	339.00
R-5SW	4/19/93	74.8	1	549.00
R-11N	4/20/93	96.4	1	143.00
R-11SE	4/20/93	90.1	1	551.00
R-11SW	4/20/93	93.7	1	27.90
R-12N	4/20/93	85.8	1	28.30
R-12SE	4/20/93	91.4	1	25.20
R-12SW	4/20/93	89.8	1	82.10
R-13N	4/20/93	91	1	307.00
R-13SE	4/20/93	92.4	1	419.00
R-13SW	4/20/93	92.3	1	14.60
R-16N	4/20/93	90.4	1	67.30
R-16SE	4/20/93	91.3	1	15.90
R-16SW	4/20/93	91.9	1	37.10
R-17N	4/20/93	87.2	1	383.00
R-17SE	4/20/93	85.5	1	109.00
R-17SW	4/20/93	82.1	1	744.00

NOTE: Clean-up goal for Total Lead is 200 mg/kg.

 : Result exceeds clean-up goal

APPENDIX B

VAPOR EXTRACTION/AIR SPARGING PILOT TEST REPORT

FINAL

LIST OF FIGURES

FIGURE

- 1 Site Map
- 2 Well Locations
- 3 Spargevac[™] Diagram
- 4 Process Flow Diagram
- 5 Vacuum Extraction Influence Testing
- 6 Radius of Influence Regression @ 3" Hg
- 7 Radius of Influence Regression @ 6.5" Hg
- 8 VE Testing Flow vs. Vacuum
- 9 VE Test Extraction Rates
- 10 DVE Radius of Influence Regression
- 11 DVE Vacuum Development at Mon. Wells
- 12 DVE Development at TMW-2
- 13 DVE Test VOC Concentrations
- 14 Sparging Flow Versus Pressure
- 15 Soil Concentration Contours
- 16 Recommended Well Locations - VE System
- 17 Recommended Well Locations - DVE System

APPENDICES

APPENDIX A Boring Logs and Well Construction Detail

FINAL

EXECUTIVE SUMMARY

Terra Vac was contracted to perform a vacuum extraction/air sparging pilot test at the Storonske Cooperage, a former drum recycling facility in Schodack, New York. Field work began on October 27, 1993, with the installation of an injection well, an extraction well, and two monitoring wells. The pilot test equipment, consisting of an extraction blower, an injection blower, a water/vapor separator, and two carbon canisters, was mobilized to the site on October 29; and testing began on November 2.

The testing was planned to consist of one day of vacuum extraction testing and four days of air sparging testing. However, because of very low water levels in the test area limiting the effectiveness of air sparging, the air sparging testing was shortened to two days, and one day of Dual Vacuum Extraction testing was added.

The testing showed that vacuum extraction is a viable means of removing volatile organic compounds (VOCs) from the unsaturated soils. The air sparging testing indicated that the low water table prevented air sparging from being effective, though it was successful at lower groundwater concentrations in the area of the test. The Dual Vacuum Extraction testing showed that entrainment extraction is an effective method of dewatering the overburden and removing residual VOCs.

Based on the results of this testing, Terra Vac recommends the installation of a Dual Vacuum Extraction system at this site. The system would include 53 wells, one or two extraction blowers, and activated carbon for vapor treatment.

FINAL

1.0 INTRODUCTION

Storonske Cooperage is a former drum recycling facility undergoing environmental investigation by the New York State Department of Environmental Conservation (NYDEC). The nature and extent of soil contamination at the site has been characterized during previous investigations. The subsurface soils have been contaminated with volatile organic compounds (VOCs), semi-volatile organic compounds (SVOCs), metals, and PCBs. The pilot test addressed the feasibility of removing VOCs and some SVOCs from the soils and groundwater by using an air sparging/vacuum extraction system. Primary volatile contaminants of concern include xylenes, styrene, ethylbenzene, toluene, chlorobenzene, 1,1,1-trichloroethane (TCA), trichloroethene (TCE), and tetrachloroethene (PCE).

The primary objective of the SpargeVac™ pilot study was to determine the site-specific design parameters for the most-effective full scale system design and implementation. Specific objectives were to:

- * Determine the number and location of extraction wells and their expected radius of influence;
- * Determine the number and location of injection or inlet wells;
- * Determine the equipment requirements, including blower size and vapor treatment;
- * Determine the aquifer parameters and means of enhancing remediation effectiveness; and,
- * Determine the likely mass removal rates and estimated length of system operations.

The work conducted for this pilot test was the design, installation and operation of an air sparging/vapor extraction pilot-scale system at the former Storonske Cooperage facility in Schodack, New York. The pilot-scale system was installed near the former lagoon area, the suspected source area of the contamination.

All work was conducted in accordance with the Workplan, Health and Safety Plan (HASP), and the Quality Assurance Project Plan (QAPP) submitted previously by Terra Vac.

FINAL

2.0 BACKGROUND

2.1 SITE CHARACTERISTICS

The Storonske Cooperage site is a 5-acre parcel of land located in the Town of Schodack, Rensselaer County, New York. The site is located on the north side of Kraft Road, immediately east of the intersection of Kraft Road with U.S. Routes 9 and 20 (see Figure 1).

The facility was purchased by N. Storonske Cooperage, Inc. in 1973, and used for the cleaning and reconditioning of 55-gallon drums. The facility is no longer in use.

Soils at the site generally consist of approximately 20 feet of glacial till overlying bedrock. The glacial till has been described as mostly sandy silt, with gravels and some clay stringers. Grain size distribution tests performed by Malcom Pirnie indicate a preponderance of gravels and sands.

The depth to groundwater was reported to range from 16.5 feet in the former lagoon area to 13 feet at the eastern site boundary. Groundwater flow was reported to the east.

2.2 SITE CONTAMINATION

The Storonske Cooperage site was reported as a possible source of contamination as early as 1979, by the Rensselaer County Department of Health. In 1980 it was reported that soil samples collected at the site showed elevated levels of benzene and xylene.

In March 1984 the NYDEC conducted a facility inspection, and found the sludge in the former wastewater lagoon to exceed toxicity limits for lead. Since 1984, six additional studies were conducted prior to this pilot study.

Soils at the site were found to be contaminated with various volatile and semi-volatile organic compounds, metals, and PCBs as reported by Malcom Pirnie, Inc. in their *Focused Remedial Investigation and Feasibility Study Report* dated April 1990. The most contaminated soils appeared to be confined to the area of the former lagoon and eastward to the site's eastern boundary. Other contaminated areas included drum unloading and storage areas.

The depth of contaminated soil was determined to vary with respect to on-site location and type of contaminant. In general, highest concentrations of total VOCs were detected in the former lagoon area at depths from 0.5 to 10 feet. The VOCs extend generally eastward from the lagoon and were detected at depths extending to 10-16 feet at the eastern property boundary with total VOC concentrations greater than 2 ppm. The highest concentration of

FINAL

total VOCs at this eastern boundary location was 85.5 ppm at a depth of 4-10 feet. Significant contamination was not detected at depths greater than 10-16 feet.

The latest round of groundwater sampling prior to this pilot study were conducted in April of 1992. This sampling indicated the following VOCs and highest concentrations: TCE (19 mg/l), benzene (7 mg/l), chlorobenzene (8 mg/l), DCA (30 mg/l), PCE (10 mg/l), TCA (15 mg/l), and xylenes (63 mg/l).

3.0 PROCESS DESCRIPTION

3.1 VACUUM EXTRACTION

Vacuum extraction induces a negative pressure gradient within the soil matrix through a nearby extraction well. As the vacuum gradient propagates through the subsurface, liquid contaminants vaporize as air and contaminant vapors migrate to the extraction well, where they are drawn to the surface for treatment. The process enhances the volatilization of VOCs in the soil matrix, and desorbs contaminants from the soil matrix over time.

The effectiveness of the vacuum extraction process at recovering VOCs is controlled by several factors. Contaminant-specific conditions, such as the physical and chemical properties of the VOCs (vapor pressure, Henry's Law Constant and solubility), the subsurface characteristics (porosity, moisture content and permeability), in addition to such system operating parameters as well spacing and applied vacuum, make each site unique and the application of the process site-specific.

The equipment required for the implementation of a vacuum extraction system includes horizontal or vertical extraction wells, a vacuum unit, a liquid/vapor separator, a vapor treatment system and system controls and instrumentation. The number of extraction wells is controlled by subsurface conditions. As the porosity and permeability of the subsurface decreases, the number of extraction wells will generally increase. The vacuum unit design is dictated by the air flow rates and vacuum levels required. A variety of units are available for use, ranging from low vacuum, single stage centrifugal blowers to high vacuum rotary vane or positive displacement blowers. Vapor can be discharged to atmosphere or treated by either adsorption of extracted vapors onto activated carbon, catalytic oxidation or thermal incineration. Selection of a vapor treatment system will depend upon regulatory agency requirements and vapor phase VOC extraction rates.

3.2 SPARGEVAC™

SpargeVac™ is Terra Vac's trade name for its remedial technology using injection of air into the saturated zone to remove volatile compounds. SpargeVac™ (also referred to as air

FINAL

sparging or sparging) removes VOCs from saturated soils by introducing contaminant-free air into the saturated zone through specially designed injection wells. As the air leaves the well and moves outward and upward through the aquifer, it creates three zones, as shown in Figure 3.

The innermost zone, known as the pore-water displacement zone, extends radially from the well approximately 1/3 of the depth of the injection well below the water table. In the pore-water displacement zone, almost all of the water in the soil pore spaces has been displaced by air. The VOCs partition from the dissolved phase to the vapor phase, and are transported to the unsaturated zone and then to the vapor extraction system by the movement of air upwards. Some volatilization of residual VOCs also occurs. Significant mounding of the water table can be seen in this zone.

The next zone outward from the injection well is known as the micro-channel airflow zone. This zone extends from the end of the pore-water displacement zone radially outward to one to two times the depth of the sparging point beneath the water table. In this zone, the air travels along micro-fracture paths, displacing much less water than in the pore-water displacement zone. Again, the primary removal mechanism is the partitioning of the VOCs from the dissolved phase to the vapor phase, followed by mass transfer of the vapors upwards. Groundwater mounding in this zone is insignificant; however, this zone can be detected by measuring air flow through monitoring points.

The final zone is the dissolved oxygen zone, extending from the micro-channel air zone outward beyond three times the depth of the sparging point below the static water table. No air flow occurs in this zone; however, elevated levels of dissolved oxygen can be detected. The dissolved oxygen spreads from the micro-channel air flow through diffusion, due to the concentration gradient of dissolved oxygen produced by the sparging air flow. No significant mass transfer mechanisms exist in this zone; however, the increased dissolved oxygen levels may enhance the biodegradation of petroleum-based compounds.

The groundwater sparging process in the micro-channel airflow zone relies on the natural equilibrium which occurs between contaminants within the saturated zone and the contaminant-free air passed through it. The vapor/dissolved phase equilibrium concentrations are based on Henry's Law constants (H_c) for the contaminants of concern. Generally, contaminants with higher H_c values will partition to the vapor phase at a faster rate than those with lower values.

In addition, the equilibrium between the adsorbed and dissolved phase contaminants must be considered. This equilibrium is expressed by the octanol-water partition coefficient (K_{ow}). Typically, the lower the value, the higher the tendency of the contaminant to dissolve. For purposes of air sparging, contaminants with high K_{ow} values, which tend to adsorb within the

FINAL

soil matrix, will be remediated at a faster rate by sparging than by conventional pump and treat methods.

Most of the contaminants of concern (all except Arochlor 1242 and lead) at this site are readily recovered by the sparging process. The ability of the sparging process to treat contaminated groundwater and soils *in situ* reduces the costs and concerns regarding liquid-phase treatment and the disposal of treated groundwater.

3.3 DUAL VACUUM EXTRACTION

Dual Vacuum Extraction (DVE) is a synergistic combination of vacuum extraction and groundwater extraction, removing both vapors and water from the same well. Groundwater is extracted to lower the water table, thus exposing the contaminated saturated soil to vapor flow. Since vapor mass transport is considered 40 times as effective as water transport at removing contaminants from soil, exposing the saturated zone to air flow greatly speeds the remediation.

The vacuum applied to the soil via the extraction well not only extracts vapors, but also increases the well pumping capacity, drawdown, and capture zone. By increasing the well production, the remediation timeframe is again reduced.

Once the saturated soils are clean, the source of continuing contamination of the groundwater is removed, and the groundwater quickly cleans up.

In Terra Vac's Entrainment Extraction process, (a refinement of DVE), the water is extracted by entrainment in the vapor stream. A specially-designed entrainment tube is inserted down the well into the water. A vacuum is applied to the tube. The velocity of the air moving from the well into the entrainment tube causes water to be drawn up with the air. The vapor/water mixture is drawn into a separator tank, where the water is removed from the air stream. Both the vapors and water are then sent to separate appropriate treatment methods. A process flow diagram is provided as Figure 4.

4.0 FIELD ACTIVITIES

4.1 WELL INSTALLATION

Parratt-Wolfe Drillers, of Syracuse, New York, were contracted by Terra Vac to install one injection well, one extraction well, and two monitoring wells. Drilling was conducted on October 27 and 28, 1993. Under the supervision of a Terra Vac geologist, three borings were advanced in the vicinity of existing well MW-1S using an 8.5-inch outside diameter hollow stem auger. Well locations are shown on Figure 2.

FINAL

Soil samples were taken continuously from the first boring (TVE-1/TVI-1) using a 2-inch diameter driven split-spoon. Soil descriptions were logged using the split spoon samples. The samples were screened for the presence of VOCs using an organic vapor monitor (OVM). Groundwater was encountered deeper than expected, at approximately 18 feet below grade.

This first boring was advanced to 20 feet 3 inches, and completed as an injection/extraction well nest. The injection well was completed to a depth of 19 feet 6 inches, using 6" of 0.020 inch slot screen and 20 feet of 2" diameter PVC riser. The extraction well was completed to a depth of 11 feet six inches, using 5 feet of screen and 10 feet of 2" PVC riser. Both screens were seated in Morie #1 (10-20 mesh) sand, with six feet of hydrated bentonite chips between the screens, and one foot of hydrated bentonite chips above the upper screen. The upper three feet was sealed with a Portland Cement-bentonite mixture.

The other two borings (TVM-1 and TVM-2) were advanced to depths of 19 feet 3 inches and 19 feet 9 inches, respectively. At these depths augur refusal occurred, indicating bedrock. No soil samples were collected during drilling.

TVM-1 and TVM-2 were completed as monitoring wells, using 10 feet of 4-inch diameter, 0.020 slot PVC screen and 10 feet of 4-inch diameter PVC riser in each. Each screen was rested in Morie #1 (10-20 mesh) sand, and capped with one foot of hydrated bentonite chips. The wells were then finished with a black-iron riser cap set in a Portland Cement-bentonite mixture.

Not enough water was found in TVM-1 to allow development. Two gallons of water was bailed from TVM-2 for partial development.

Detailed lithological descriptions and well construction details can be found in Appendix A.

4.2 PILOT TESTING

4.2.1 Pilot System Installation

On October 29, 1993, a vacuum extraction/air sparging system was mobilized to the site. The system consisted of a 10 horsepower, positive-displacement air injection blower, a 10 horsepower, positive-displacement extraction blower, a 75-gallon vapor/water separator, and two 200 pound activated carbon canisters. A diesel generator was used for electrical power. A process flow diagram for the extraction system is provided in Figure 4.

In addition, a Terra Vac van equipped with a gas chromatograph (GC) and two flame ionization detectors (FID) was brought to the site.

FINAL

5.2.4 Vapor Treatment System Efficiency

No VOCs were detected in the outlet of the primary or secondary carbon throughout the test. Analytical results of vapor samples from the carbon treatment system are presented in Table 4.

5.3 AIR SPARGING TESTING**5.3.1 Injection Pressures and Flow Rates**

Injection pressures were varied from 2 pounds per square inch gauge (psig) to 6 psig. The resulting injection flow rates ranged from 38.8 SCFM to 59.4 SCFM. These are presented as Table 5. Higher pressures were not used due to the small saturated thickness of approximately one foot.

5.3.2 Cone-of-Influence Airflow Measurements

No airflow in the saturated zone was measured in any of the monitoring wells, at any depth, during the duration of the test, due to the small saturated thickness encountered at the time of the test.

5.3.3 Dissolved Oxygen Measurements

Dissolved oxygen measurements were taken from each of the monitoring wells seven times over the course of the air sparging testing. These readings ranged from 0 mg/L to 8 mg/L, and are provided as Table 6. The measurements taken on the afternoon of November 3, 1993, are suspect, as the meter was operating erratically during that time. The meter was subsequently recalibrated and groomed for measurements taken on November 4. Dissolved oxygen measurements taken on November 4 ranged from 1.1 mg/L, in MW-1S at the beginning of the day's testing, to 5.7 mg/L in TVM-1, also taken at the beginning of the testing. MW-1S showed a noticeable increase in dissolved oxygen during testing on the 4th; while TMW-1 and TMW-2 stayed relatively constant or increased slightly.

5.3.4 Water Table Mounding

During the air sparging test, water levels in the monitoring wells were routinely measured. This data is presented in Table 7. The water levels in the wells dropped by up to 1.5 feet during the morning of the 3rd; recovering to near their original levels by the end of the day. On the second day of sparging testing, the water levels in TVM-1 and TVM-2 fluctuated by less than 0.06 feet; while the level in MW-1S (furthest from the injection well) increased by 0.4 feet. (Note that the recorded depths to water are measured from the top of each

FINAL

individual well casing, and are intended to measure relative changes in each well only. The Terra Vac-installed wells were not surveyed for absolute elevations.)

5.3.5 Extracted Vapor Concentrations

Extracted vapor concentrations during the air sparging portion of the testing ranged from a total VOC concentration of 1.05 mg/L to a high of 11.04 mg/L. For most of the test, the total VOC concentration stayed between 1.4 mg/L and 1.6 mg/L. The primary compounds removed were toluene, PCE, ethylbenzene, and xylenes. Benzene was only detected in three of the 29 samples, these three being in conjunction with the extremely high total VOC peak noted during mid-day on November 3. Styrene, chlorobenzene, TCE, and 1,2-DCA were generally less than 0.1 mg/L each. The vapor analysis results are detailed on Table 8.

Extraction rates generally ranged from 0.08 to 0.1 pounds per hour during the extraction test. (Note, however, that extraction flow rates were significantly less than during the previous vapor extraction testing). A total of 2.72 pounds of VOCs were extracted during the two days of air sparging testing.

5.3.6 Groundwater Concentrations

Groundwater VOC concentrations measured before and during the air sparging test are presented in Table 1. VOC concentrations in wells TMW-1 and TMW-2 decreased by approximately 60% over the two days of testing. VOC concentrations in MW-1S showed an initial increase, followed by a decrease back to the original levels.

5.3.7 Vapor Treatment System Efficiency

No VOCs were detected in the outlet of the primary or secondary carbon throughout the test. Analytical results of vapor samples from the carbon treatment system are presented in Table 4.

5.4 DUAL VACUUM EXTRACTION TESTING

5.4.1 Extraction Flow Rates and Applied Vacuums

During the Dual Vacuum Extraction portion of the test, the vacuum applied to TVM-2 was initially set at 58.5 inches of water vacuum, then allowed to stabilize to 45.5 inches of water vacuum. The vacuum was again allowed to develop after the system re-start following the unintentional shut-down of the diesel generator. This data is presented in tabular format in Table 9. Flow was initially 66 SCFM, and developed to 74 SCFM as the area was dewatered. It took approximately one hour initially for steady-state conditions to develop;

FINAL

following the system restart, steady-state conditions were obtained in approximately one-half hour.

Overall, for similar applied vacuums, a greater flow rate was achieved during the DVE testing compared to the initial VE testing. For instance, during the initial VE testing, an applied vacuum of 78 inches of water achieved a flow rate of only 65 SCFM, while during the DVE test a vacuum of 45.5 inches of water obtained a flow rate of 74 SCFM.

5.4.2 Induced Vacuums in Monitoring Wells

The induced vacuum in each of the wells surrounding TVM-2 was monitored every thirty minutes during the DVE test. This data is also presented in Table 9. Induced vacuums ranged from 0.4 inches of water vacuum in MW-1S (18.5 feet from TVM-2) to 0.54 inches of water vacuum in TVE-1 (eight feet from TVM-2). Induced vacuums dropped off only slightly with increasing distance from the extraction well. In addition, induced vacuums increased during the initial development period, as the area was dewatered.

In general, the induced vacuums during the DVE test were higher than those noted during the initial vacuum influence testing, for similarly spaced wells. For instance, during the initial VE testing, with a vacuum of 65 inches of water applied to TVE-1, a vacuum of 0.24 inches of water was recorded at TVM-2. During the DVE testing, with a vacuum of only 45.5 inches of water applied to TVM-2, a vacuum of 0.54 was recorded at TVE-1.

5.4.3 Water Table Drawdown and Water Extraction Rate

Because of the entrainment process used to extract groundwater from the well, direct measurements of water flow were not possible. The water extraction rate was calculated by determining the total amount of water extracted by observation of water level in the water/vapor separator, and dividing by the run time.

At the end of the DVE test, the water/vapor separator was approximately 1/4 full. This equates to roughly 70 gallons of water. Since the DVE test ran for 5.5 hours, this gives a pumping rate of 12.7 gallons per hour, or 0.2 gallons per minute. At this pumping rate, the extraction well was kept de-watered.

Water table drawdowns measured in the surrounding monitoring wells are presented in Table 11. MW-1S and TMW-1 (located eighteen feet and ten feet from TMW-2, respectively) showed slight increases in water level. TVI-1, located eight feet from TMW-2, showed a decrease of approximately 0.12 feet.

FINAL

5.4.4 Extracted Vapor Concentrations

Vapor concentrations in the extracted vapor stream during the vacuum extraction testing ranged from 0.18 mg/L to 0.81 mg/L. The primary compounds detected were PCE (maximum concentration of 0.26 mg/L), toluene (maximum concentration of 0.17 mg/L), ethylbenzene (maximum concentration of 0.12 mg/L) and xylenes (maximum combined concentration of 0.15 mg/L). Benzene was only detected once, during the first sample of the day. A detailed tabulation of analytical results is presented in Table 10.

In general, VOC concentrations increased during the first few hours of operation, as the area was dewatered. Following the system shut-down, concentrations dropped off sharply, then again increased as the area was de-watered. Towards the end of the day, concentrations began slowly decreasing, as is typical for VE systems.

Overall, a total of 0.91 pounds of VOCs were removed during the five and one-half hour test, corresponding to an extraction rate of 3.97 pounds per day.

5.4.5 Vapor Treatment System Efficiency

No VOCs were detected in the outlet of the primary or secondary carbon throughout the test. Analytical results of vapor samples from the carbon treatment system are presented in Table 4.

6.0 EVALUATIONS

The VE testing demonstrated the effectiveness of using vapor extraction to remove VOCs from the unsaturated zone at the site. The air sparging testing showed that, although VOCs can be removed from the saturated zone using air sparging, the thin saturated thickness will limit the overall effectiveness of the technology due to the large number of air injection points needed. The DVE testing, although limited in scope, demonstrated the effectiveness of using the DVE process to dewater the saturated zone and extract VOCs.

6.1 VACUUM EXTRACTION TESTING

The one-day vacuum extraction test demonstrated the effectiveness of using vacuum extraction to remediate the unsaturated zone, by removing 1.8 pounds of VOCs from a single well in less than eight hours of operations. Subsurface vacuums were detected up to twelve feet from the extraction well.

FINAL

6.1.1 Radius of Influence

Figure 5 graphically displays the measured subsurface vacuums at the three monitoring wells for three different applied vacuums. A significant vacuum was measured at twelve feet from the extraction well, from the monitoring well furthest from the extraction well.

Theoretically, the subsurface vacuum should decrease logarithmically with increasing distance from the extraction well. Regression analysis was performed on this data, using the log of the vacuum. The results are presented in Figure 6, for a 3-inches of mercury ("Hg) applied vacuum, and in Figure 7 for a 6.5"Hg applied vacuum. Using 0.01 inches of water as the arbitrary cut-off point, the calculated radius of influence is 15 feet for a 3"Hg applied vacuum, and 17 feet for a 6.5" applied vacuum. This correlates with empirical data gathered at similar sites.

The measured induced vacuums are indicative of a low permeability soil type. This correlates with the clayey soils noted during the drilling of TVI-1/TVE-1. Previous investigations reported grain size analyses indicating that the soils were composed of silty sands. This classification is not supported by the findings during this pilot test.

6.1.2 Vacuum/Flow Relationship

Regression analysis performed on the flow obtained from each magnitude of induced vacuum indicates a linear relationship between vacuum and flow. This is presented graphically in Figure 8. Although the range of vacuums used during the pilot test provided a linear relationship with the resulting flow, it can be expected that at some point, turbulence will develop, resulting in proportionally less flow for increasing vacuum. However, for moderate levels of vacuum, an increase in vacuum will result in a corresponding increase in flow.

6.1.3 Vapor Extraction Rates

Figure 9 shows the VOC extraction rates as a function of run time. Also displayed are the applied vacuum levels as a function of run time. This graph shows how increasing the vacuum each time increased the extraction rates. Therefore, by applying a greater vacuum, and obtaining a greater flow rate, the remediation time can be reduced.

6.2 AIR SPARGING TESTING

The saturated overburden thickness was only 1.5 feet, which was smaller than expected. Because of this thin saturated thickness, only limited air sparging data was able to be obtained.

FINAL

6.2.1 Pressure/Flow Relationship

With one foot of water covering the injection screen, the calculated minimum injection pressure to overcome the hydrostatic forces is 1/2 psig. The sparging test was run with injection pressures ranging from 2 to 6 psig.

Figure 14 presents a graph of injection air flow versus injection pressure, with a best-fit curve added. At a certain pressure, further increases in pressure provide only marginal increases in air flow, due to increasing turbulence and friction losses. For the aquifer conditions found at the site, this point appears to be approximately 3 psig, or six times the pressure needed to overcome the hydrostatic pressure.

No discernable increases in VOC concentrations or VOC extraction rates as a result of increasing injection pressure were noted.

6.2.2 Cone-of-Influence

No measurable bubble flow was encountered in any monitoring well. The cone-of-influence for the aquifer conditions present at the site, with a saturated thickness of 1 foot, is therefore less than 4 feet. This correlates with published reports and prior experience, which suggest that the measurable airflow typically extends out one to two times the thickness of the saturated zone. For the 1-foot saturated zone encountered, this would equate to an expected measurable cone of influence of one to two feet in radius.

The dissolved oxygen measurements indicate that the sparging may have increased dissolved oxygen levels up to 12 feet from the sparging well. Increased dissolved oxygen levels can assist in the bioremediation of petroleum-based hydrocarbons. However, because of the high concentrations of chlorinated compounds, biodegradation of the petroleum compounds may not be occurring.

6.2.3 Effectiveness of Air Sparging

No significant increases in overall VOC removal during sparging as compared to vacuum extraction alone were noted. This is likely due to (a) the limited area impacted by the injection well due to the low water table; and (b) the fact that the highest soil concentrations were found in the upper 6 feet of soil. Because of these two factors, the additional VOC mass released by the sparging process was negligible compared to the mass being removed from the unsaturated zone.

However, noticeable decreases in groundwater VOC concentrations were seen (Table 1). This indicates that the air sparging system was effectively removing VOCs from the saturated zone. In addition, a very high VOC concentration spike was noted for 1-1/2 hours

FINAL

during mid-day on November 3, indicating that the injected air had found a 'pocket' of VOCs, volatilized them, and transported them to the extraction well. This demonstrates that these 'pockets' of VOCs can be cleaned up using air sparging.

The major limitation to the use of air sparging at this site is the small saturated thickness in the source area, necessitating a large number of injection points to provide adequate coverage.

6.3 DUAL VACUUM EXTRACTION TESTING

Because the DVE testing was not originally included in the pilot test plan, the scope of the testing was limited. However, the DVE testing did demonstrate that (a) Entrainment extraction can be used to dewater the saturated zone; (b) the expected water extraction rates are low; and (c) DVE can provide greater areas of influence than VE testing alone.

6.3.1 Radius of Influence

Figure 10 displays the measured subsurface vacuums at the three monitoring wells during the DVE testing. Regression analysis was performed on this data, using the log of the vacuum. The results are also presented in Figure 10. Using 0.01 inches of water as the arbitrary cut-off point, the calculated radius of influence is 29 feet. This is significantly larger than that measured during the initial VE testing.

Although this difference may be due to lithological differences in the soil surrounding TMW-2 versus TVE-1, because of the short distance between the two wells, and the fair amount of uniformity seen across the site, this is not likely. A more probable explanation is that in general, a thicker unsaturated zone and a deeper well screen will provide a larger radius of influence. In this case, the dewatering action of DVE increased the thickness of the unsaturated zone for TMW-2 as compared to TVE-1. In addition, TMW-2 was screened down to approximately 19 feet below grade, whereas TVE-1's screen extended down to only 11 feet below grade.

The effects of de-watering can be seen in Figure 11, showing the induced vacuum in the monitoring wells over time during the DVE test. In general, it took over one and one-half hours for steady-state vacuums to be achieved. This can be compared to the initial VE testing (Table 2), where steady-state vacuums were reached almost immediately, and further increases were slight.

6.3.2 Vacuum/Flow Relationship

Figure 12 displays the vacuum and flow during the DVE testing as a function of time. Again, steady-state conditions took over one and one-half hours to develop, as compared

FINAL

to the initial VE testing (Table 2), during which vacuums and flows stabilized almost immediately.

The flow rate per foot of screen for TVM-2 at 3.5" Hg (45" water) vacuum was 7.4 SCFM per foot. By interpolating from Figure 8, the flow rate per foot of screen for well TVE-1 at the same vacuum would be 7.2 SCFM. This shows that the flow characteristic of the soil near each well were similar, and that the longer screen provided additional flow capability.

6.3.3 Vapor Extraction Rates

In general, vapor concentrations during the DVE testing were lower than during either the VE testing or the air sparging testing. This may be due to varying VOC soil concentrations between TVE-1 and TVM-2. Mass removal rates during the DVE testing were similar to those encountered during the VE testing, due to the higher airflow rate.

Increases in VOC concentrations were noted during the first several hours after each of the two DVE start-ups (Figure 13). This also provides evidence of the dewatering action exposing new areas to vapor flow.

Based on the results of this one-day test, VOC extraction rates during DVE operations of 4 pounds per day per well can be expected.

6.3.4 Dewatering

A pumping rate of 0.2 gpm was able to keep the extraction well dewatered. A noticeable decrease in water level was recorded eight feet away, after only five hours of extraction. Based on this limited information, the saturated soils can be effectively dewatered using a network of properly spaced DVE wells.

As shown in section 6.3.2, the flow rate per foot of screen during the DVE testing was equal to or greater than the flow rate per foot of screen during the VE testing, for a similar vacuum. Since this calculation used the entire length of screen TVM-2, without an adjustment for the portion of the screen covered by water, this demonstrates that the DVE extraction process effectively kept the well screen clear of water.

7.0 RECOMMENDATIONS

Based on the results of the four days of pilot testing, a dual vacuum extraction system will be the most effective method of remediating all of the overburden. Although air sparging

FINAL

was able to remove VOCs from the saturated zone, the small saturated thickness makes the use of air sparging less effective than dual vacuum extraction.

Terra Vac's recommendations for a full scale system follow:

7.1 EXTRACTION WELLS

7.1.1 Vacuum Extraction Well Radius of Influence

When spacing vapor extraction wells, the measured vacuum influence is not the only factor to consider. Rather, this is only a maximum well spacing. The other factor to take into consideration is the desired remedial time frame. In general, with closer well spacings, more pore volumes of air are drawn through the soil per unit time, and remediation is faster.

The determination of required pore volumes can be calculated using the initial soil concentrations, desired final concentrations, and a detailed benchtop study. In absence of a bench-top study for a particular site, information from similar sites can be used.

Table 12 presents a summary of the initial VOC soil concentrations and the targeted clean-up goals, along with the required percent reduction for each compound. At similar sites where detailed bench testing was performed, approximately 9,000 pore volumes were required to achieve a 98% reduction. This correlates with other published data for removal of xylenes (the limiting compound per Table 12).

Using the radius of influence calculated during the VE testing of 17 feet (Section 6.1.1), an assumed porosity of 35%¹, and an unsaturated thickness of 18 feet, the pore volume is calculated as:

$$V_{pore} = \pi r^2 hn$$

where n is the soil porosity, h equals thickness of soil zone, and r is the radius of influence. For the parameters listed above, this becomes:

¹Theoretical porosities for uniform tight packed spheres ranges from 25.9% to 47.9%, depending on the packing pattern. Terra Vac's actual porosity measurements at various remedial sites shows that porosity values almost always fall between 30% and 45%. In addition, any retained soil moisture will occupy pore space, thereby lowering the effective porosity. Therefore, the assumed value of 35% provides a conservative estimate of the remedial timeframe.

FINAL

$$V_{pore} = \pi \times (17 \text{ ft})^2 \times 18 \text{ ft} \times 35 \%$$

$$V_{pore} = 5,720 \text{ ft}^3$$

Using the flow rate of 65 scfm measured during the VE testing, the time required to attain the remediation goals using the maximum well spacing is then:

$$T = \frac{N_{pore} V_{pore}}{Q}$$

$$T = \frac{9000 \text{ pores} \times 5,720 \text{ ft}^3}{65 \text{ ft}^3/\text{min} \times 525,600 \text{ min/year}}$$

$$T = 1.5 \text{ years}$$

This provides a recommended well spacing of 17 feet for the unsaturated zone. However, this does not take into account the need for some remediation of the saturated zone. This can be accomplished using dual vacuum extraction (below) or air sparging (see section 7.2).

7.1.2 Dual Vacuum Extraction Well Radius of Influence

For the spacing of DVE wells, both the vapor radius of influence and the water table drawdown need to be considered. However, detailed modeling of the aquifer parameters to ensure adequate drawdown is beyond the scope of this pilot test. The recommendations provided herein are based upon observations during the test and experience at similar sites. A more thorough examination of the hydrogeological properties is recommended.

Using the calculated DVE radius of influence of 29 feet (Section 6.3.1), an assumed porosity of 35%, and an overburden thickness of 20 feet, the pore volume is calculated as:

$$V_{pore} = \pi r^2 h n$$

where n is the soil porosity, h equals thickness of soil zone, and r is the radius of influence. For the parameters listed above, this becomes:

$$V_{pore} = \pi \times (29 \text{ ft})^2 \times 20 \text{ ft} \times 35 \%$$

$$V_{pore} = 18,494 \text{ ft}^3$$

FINAL

Using the measured flow rate of 74 scfm, the time required to attain the remediation goals using the maximum well spacing is then:

$$T = \frac{N_{pore} V_{pore}}{Q}$$

$$T = \frac{9000 \text{ pores} \times 18,494 \text{ ft}^3}{74 \text{ ft}^3/\text{min} \times 525,600 \text{ min/year}}$$

$$T = 4.3 \text{ years}$$

The well spacing required to reduce the remedial time frame to 1.5 years (to match the cleanup time frame presented for the unsaturated zone) can be calculated by rearranging the equations to solve for the maximum allowable pore volume:

$$V_{pore} = \frac{1.5 \text{ years} \times 74 \text{ ft}^3/\text{min} \times 525,600 \text{ min/year}}{9,000 \text{ pore volumes}}$$

$$V_{pore} = 6,482 \text{ ft}^3$$

then solving for r:

$$r = \sqrt{\frac{6,482 \text{ ft}^3}{20 \text{ ft} \times \pi \times 35\%}}$$

$$r = 17.2 \text{ feet}$$

This provides a well spacing of 34 feet. However, the necessary dewatering of the unsaturated zone must also be factored in..

At a spacing of 34 feet, it is unlikely that the saturated zone will be sufficiently dewatered based on the drawdowns seen during the DVE testing. From the limited data available, a spacing of no more than 20 feet is recommended for dewatering of the saturated zone. Terra Vac recommends conducting a more detailed aquifer analysis to verify this spacing. This modeling is beyond the scope of this pilot test.

Wells constructed for either DVE or vacuum extraction can be constructed of 2-inch diameter PVC, since little difference in flow per foot of screen was seen between the 2-inch well (TVE-1) and a four-inch well (TVM-2).

FINAL

7.1.3 Number and Location of Extraction Wells

According to the most recent soil sampling data (Figure 3-1 of *Request for Proposal for Soil Vapor Extraction Pilot Test*, D&B, July, 1993, reprinted herein as Figure 15), there are two major areas of the site requiring remediation of soils. The first is the suspected source area, an area 125 feet by 125 feet located near the former lagoon. The second area is 40 feet by 75 feet, located near the eastern fence line. These areas are located within the ">1 ppm VOC" contour lines.

The first area, with a total approximate area of 15,625 square feet, would require 17 wells at a spacing of 34 feet for a VE system to remediate the unsaturated zone. To dewater this area using DVE would require up to 50 wells using a 20-foot spacing.

The second area, with an area of approximately 3,000 square feet, would require approximately 3 wells at a 34 foot spacing to remediate the unsaturated zone. To dewater the overburden in this area would require at least 10 wells. However, DVE is not recommended in this area because (a) the saturated thickness is greater in this area (up to ten feet thick) than in the source area; and (b) VOCs in this area appear to be concentrated in the shallower soils. Due to the greater saturated thickness, air sparging is likely to be more effective in this part of the site; again, though, air sparging may not be warranted, as the VOCs appear to be concentrated in the upper soils.

Figure 16 shows the recommended well placement for the VE system. Figure 17 shows the recommended well placement for the DVE system.

7.2 NUMBER AND LOCATION OF INJECTION WELLS

As described above, air sparging is not recommended in the source area due to the small saturated thickness. Complete coverage with an air sparging network in this area would require between 1200 and 5000 injection points, using a spacing of 2 to 4 feet. These injection points would be 1/2" or 1" driven steel pipes with perforated sections near the bottom.

Sparging is an attractive option in the eastern area of the site, where the saturated thickness is greater. Given a saturated thickness of 10 feet, an injection point spacing of 20 feet would be reasonable. The number of sparging points to cover the eastern fence boundary area of 3000 square feet would then be 10 sparging points.

Sparging could also become an attractive option in the source area of the site, if the water table rises significantly, thereby extending the cone of influence for sparging, while requiring higher water extraction rates for DVE.

FINAL

7.3 EQUIPMENT REQUIREMENTS

7.3.1 Extraction Blower

For a vacuum extraction system consisting of 17 wells in the source area and 3 wells in the eastern fence area, a total flow rate of 1300 scfm can be expected. A minimum well vacuum of 6.5 inches of mercury is recommended; so to account for friction losses in the piping system, a minimum capability of 1300 SCFM at 10" Hg is recommended. This could be met with a 75-horsepower, positive-displacement rotary-lobe blower. It may be desirable to use two blowers to meet this requirement, for reliability and flexibility; in this case, two 40-hp blowers would also meet the requirement.

If a DVE system is installed, using 50 wells in the source area and 3 wells in the eastern fence area, a total flow rate of 3920 scfm can be expected. A minimum vacuum of 3.5 inches will be required at the well; therefore, allowing for friction losses, the blower must be capable of at least 6" Hg. For the DVE system, centrifugal blowers may be used in place of rotary lobe blowers. It is recommended that excess blower capacity be provided, to allow for increased water extraction rates should the water table rise.

7.3.2 Injection Blower

If an air sparging network is installed in the eastern fence zone, 10 wells are envisioned. The hydrostatic pressure required for 10 feet of water is 5 psig; per Figure 10, 8 psig would then provide the optimal injection air flow. (3 psig above the minimum pressure required). The expected air flow would be 45 scfm per point, or 450 scfm total. This can be provided by a rotary lobe blower, or by an oil-free compressor with a pressure regulating valve.

7.3.3 Vapor Treatment Requirements

Based on the results of the pilot test, a mass removal rate of 5 pounds per day per well is expected. For a VE system of 20 wells total (17 + 3), an initial total VOC extraction rate of 100 pounds per day can be expected. (This is a conservative estimate, since the pilot test was performed in the center of the source area). Given this, vapor treatment will be required by the NYDEC.

By summing the average values of soil VOC concentrations measured in prior investigations, an average total VOC concentration in the site soils of 50 milligrams per kilogram (mg/kg, or ppm) is derived. Using a total volume of 372,500 cubic feet (from the area and depth presented above), the total mass of VOCs in the soil is calculated at 1863 pounds of VOCs.

Carbon adsorption was proven to be effective during the pilot testing. Using a carbon loading rate of 10%, this means that carbon usage rates will start out as high as 1000 pounds

FINAL

of carbon per day for a VE-only system. With a total mass of VOCs of 1863 pounds, total carbon usage is estimated at 18,600 pounds over the life of the project. A conceptual design for the carbon adsorption system would include six 1000-pound vessels, in three pairs. The three primary carbon vessels would require change-out six times over the 1.5 year project life.

A DVE system would expend approximately the same amount of carbon over the life of the project, as the total mass extracted would remain the same. However, additional carbon vessels would be required to handle the higher flow rates required; but change-outs would be less frequent. To handle the expected flows, the system would require sixteen 1000-pound vessels in eight pairs.

Catalytic or thermal oxidation could also be used for vapor treatment. Thermal oxidation involves heating the air stream to approximately 1400°F, and oxidizing the organic compounds. Catalytic oxidation involves heating the air stream to approximately 750°F and passing the heated vapors over a catalyst bed, where the organic compounds are then oxidized. However, because of the low expected total mass of VOCs (only 1800 pounds), it is not likely that thermal oxidation or catalytic oxidation would be cost-effective due to the significant amounts of energy that are required to heat the air stream.

7.4 DVE WATER TREATMENT

With an anticipated 50 DVE wells, and an expected extraction rate of 0.2 gpm, a water treatment system of at least 10 gpm would be required. This would most easily be handled using a pair of carbon adsorption vessels, with discharge to a nearby drainage channel, storm drain, or sewage system. It is recommended that excess water treatment capacity be provided, to allow for increased groundwater extraction rates should the water table rise.

7.5 MEANS OF ENHANCING REMEDIATION EFFECTIVENESS

Two enhancement methods, DVE and air sparging, have been explored in depth in this study. Other possible methods of enhancing the remediation are air injection into the unsaturated zone, steam injection, and capping the surface.

Air injection into the unsaturated zone is often used in very tight, low permeability soils. Also, injected hot air can increase the volatility of semi-volatile compounds. However, at this site adequate subsurface flow was easily achieved, and most of the compounds of concern are easily removed by vacuum extraction. Two semi-volatile compounds, phenol and PCBs, are a concern at the site. Experience with phenol has shown that it can be removed at a slow rate with vacuum extraction; and that heating the soil does little to improve the extraction rate. PCB has not been found to be amenable to vapor extraction even with soil heating. In addition, these two compounds are primarily found in areas of

FINAL

the site also impacted with metals; and these areas are scheduled for excavation. Therefore, air injection into the unsaturated zone is not recommended.

Steam injection is another method of increasing the volatility of longer-chain hydrocarbons such as phenols. Again, because phenol is primarily found in areas of the site scheduled to be excavated due to metals contamination, and because experience has shown only minimal increases in extraction rates of phenol from soil heating, the cost of steam injection is not recommended.

A cap on the area undergoing vacuum extraction is often used to attempt to increase the radius of influence, especially where the unsaturated zone is very thin. The cap also serves to limit water infiltration into the area. However, an adequate radius of influence was developed without a cap; and water infiltration into the area of concern does not appear to be a significant problem. Therefore, installation of a cap for improving the VE process is not recommended.

7.6 BUDGET ESTIMATES FOR RECOMMENDED REMEDIAL SYSTEMS

A vacuum extraction system to treat the unsaturated zone only, consisting of 20 wells, a vacuum extraction blower, and a carbon adsorption vapor treatment system, is expected to have a capital cost of approximately \$148,000, and an operations and maintenance cost of \$270,000 over 1.5 years.

A dual vacuum extraction system to treat both the unsaturated zone and the saturated zone, consisting of 53 wells, a vacuum extraction blower, a carbon adsorption vapor treatment system, and a carbon adsorption water treatment system, is expected to have a capital cost of approximately \$250,000, and an operations and maintenance cost of \$441,000 over 1.5 years.

A breakdown of these estimates is provided in Table 13.

8.0 CONCLUSIONS

Based upon the information derived from the pilot test, the following conclusions are provided:

* Vacuum Extraction (VE) is an effective method of remediating the volatile compounds in the unsaturated soils at the site, regardless of the method chosen to remediate the saturated zone.

FINAL

- * A minimum radius of influence of 12 feet was measured. The calculated radius of influence for vacuum extraction is from 15 to 17 feet, depending on the applied vacuum.
- * Carbon adsorption is an effective method of vapor treatment for this site.
- * Increased vacuums provided larger radii of influence, higher flows, and higher extraction rates.
- * The effectiveness of air sparging was limited due to the thin saturated thickness encountered in the source area.
- * Dual Vacuum Extraction was an effective method of dewatering the source area, given the thin saturated thickness.
- * The remedial system chosen for cleanup of the saturated zone should be flexible to handle changing water level conditions.
- * Installation of an integrated remediation system to clean up the saturated and unsaturated soils at the site is recommended. This system would include 50 Dual Vacuum Extraction wells in the source area, and 3 vapor extraction wells in the eastern fence area. Carbon adsorption would be used for vapor treatment and for treatment of extracted groundwater. The operating time of this system would be approximately 1.5 years.

TABLE 1
GROUNDWATER VOC ANALYSES

WELL	DATE	TIME	1,2 DCA (mg/L)	BENZENE/ TCA (mg/L)	TCE (mg/L)	TOLUENE (mg/L)	PCE (mg/L)	CHLORO- BENZENE (mg/L)	ETHYL- BENZENE (mg/L)	P,M- XYLENES (mg/L)	STYRENE (mg/L)	O-XYLENE (mg/L)	TOTAL VOC (mg/L)
MW-1S	11/03/93	08:30	0.000	0.000	0.000	0.000	0.025	0.052	0.132	0.000	0.000	0.000	0.21
	11/03/93	16:50	0.000	0.000	0.080	0.000	0.000	0.161	0.177	0.000	0.021	0.000	0.44
	11/04/93	11:30	0.000	0.000	0.000	0.000	0.029	0.102	0.102	0.000	0.000	0.000	0.23
TMW-1	11/03/93	08:30	0.000	0.015	0.035	2.816	0.099	0.280	1.466	1.337	0.172	0.453	6.67
	11/03/93	17:03	0.000	0.009	0.000	1.085	0.000	0.138	0.747	0.628	0.061	0.234	2.90
	11/04/93	11:02	0.000	0.013	0.000	1.035	0.000	0.116	0.637	0.536	0.072	0.225	2.63
TMW-2	11/03/93	08:30	0.000	0.006	0.017	0.635	0.029	0.185	1.071	0.931	0.000	0.270	3.14
	11/03/93	16:53	0.000	0.000	0.000	0.448	0.000	0.073	0.670	0.590	0.000	0.171	1.95
	11/04/93	11:04	0.000	0.000	0.012	0.219	0.000	0.111	0.451	0.354	0.000	0.117	1.26

TABLE 2
VACUUM EXTRACTION VACUUMS AND FLOWS

DATE	TIME	TVE-1		TVM-1		TVM-2		MW-1S	
		DISTANCE							
		FROM TVE-1		4		8.17		11.75	
		(feet)							
		FLOW		VACUUM		VACUUM		VACUUM	
		SCFM		In. H2O		In. H2O		In. H2O	
11/02/93	08:30	22	39	1.00	0.10	0.08			
	09:00	24	39	1.10	0.12	0.10			
	09:30	24	39	1.25	0.12	0.10			
	10:00	25	39	1.25	0.14	0.12			
	10:30	25	39	1.25	0.14	0.12			
	11:00	42	65	2.25	0.20	0.20			
	11:30	42	65	2.25	0.24	0.22			
	12:00	44	65	2.40	0.22	0.22			
	12:30	44	65	2.40	0.24	0.22			
	13:00	62	91	3.40	0.32	0.32			
	13:30	64	90	3.50	0.34	0.31			
	14:00	64	90	3.50	0.34	0.31			
	14:30	65	85	3.60	0.37	0.34			
	15:00	65	78	3.60	0.35	0.34			
	15:30	65	78	3.60	0.35	0.32			
	16:00	65	78	3.60	0.34	0.33			
	16:30	65	75	3.70	0.37	0.35			

TABLE 3
VAPOR ANALYSES
VE TESTING
WELL TVE-1

DATE	TIME	RUN HOURS (TOTAL)	SCFM	WELL VACUUM (In. Hg)	1,2 DCA (mg/L)	BENZENE/TCA (mg/L)	TCE (mg/L)	TOLUENE (mg/L)	PCE (mg/L)	CHLORO-BENZENE (mg/L)	ETHYL-BENZENE (mg/L)	P-M-XYLENES (mg/L)	STYRENE (mg/L)	O-XYLENE (mg/L)	TOTAL VOCs (mg/L)	TOTAL POUNDS PER HOUR	CUMULATIVE LBS VOC'S RECOVERED
11/02/93	08:48	0:00	22.0	3.0	0.0135	0.0014	0.1704	0.5363	0.4026	0.0471	0.2147	0.1931	0.0084	0.0455	1.63	0.134	0.00
11/02/93	08:48	0:00	22.0	3.0	0.0099	0.0073	0.1323	0.4022	0.2444	0.0351	0.1525	0.1285	0.0065	0.0299	1.15	0.095	0.00
11/02/93	09:25	0:62	24.0	3.0	0.0167	0.0006	0.1008	0.6945	0.5666	0.0705	0.2755	0.2587	0.0119	0.0562	2.05	0.184	0.09
11/02/93	09:51	1:05	24.0	3.0	0.0186	0.0017	0.0879	0.5868	0.6663	0.0616	0.227	0.2216	0.0129	0.0492	1.93	0.174	0.16
11/02/93	10:28	1:67	25.0	3.0	0.0165	0.001	0.0853	0.7071	0.6845	0.0846	0.2979	0.3022	0.0224	0.07	2.27	0.212	0.28
11/02/93	10:54	2:10	25.0	3.0	0.0198	0.002	0.0755	0.6203	0.5247	0.0733	0.2549	0.2634	0.0171	0.0581	1.91	0.179	0.37
11/02/93	11:19	2:52	42.0	5.0	0.0144	0	0.0546	0.4375	0.4377	0.066	0.1973	0.2192	0.0156	0.05	1.49	0.234	0.45
11/02/93	11:45	2:95	42.0	5.0	0.0117	0	0.0463	0.3655	0.4031	0.0501	0.1613	0.1784	0.0131	0.0406	1.27	0.200	0.55
11/02/93	12:10	3:37	44.0	5.0	0.0107	0.0006	0.0441	0.405	0.3391	0.0537	0.178	0.1982	0.0163	0.0446	1.29	0.212	0.63
11/02/93	12:46	3:97	44.0	5.0	0.0156	0.001	0.0522	0.4104	0.4357	0.0614	0.2005	0.2341	0.0186	0.0546	1.48	0.244	0.77
11/02/93	12:46	3:97	44.0	5.0	0.0096	0.0006	0.0399	0.3716	0.3355	0.0528	0.1726	0.1958	0.0155	0.0447	1.24	0.204	0.77
11/02/93	13:11	4:38	62.0	7.0	0.0131	0	0.0411	0.3096	0.4044	0.0551	0.1506	0.1787	0.0146	0.0408	1.21	0.280	0.87
11/02/93	13:49	5:02	64.0	6.9	0.0079	0.0022	0.0526	0.3055	0.3654	0.0551	0.1648	0.2192	0.0051	0.0505	1.23	0.294	1.05
11/02/93	14:16	5:47	64.0	6.9	0.011	0	0.0396	0.3467	0.3199	0.0576	0.1863	0.2235	0.0201	0.0545	1.26	0.301	1.19
11/02/93	14:49	6:02	65.0	6.5	0.0144	0	0.0402	0.3257	0.2581	0.0544	0.1802	0.2204	0.0209	0.0541	1.17	0.284	1.35
11/02/93	15:16	6:47	65.0	6.0	0.0133	0	0.0394	0.2783	0.3072	0.0513	0.1452	0.1809	0.0156	0.0425	1.07	0.261	1.47
11/02/93	15:44	6:93	65.0	6.0	0.0122	0	0.0382	0.2947	0.422	0.059	0.1695	0.2328	0.008	0.053	1.29	0.313	1.60
11/02/93	16:19	7:52	65.0	6.0	0.0092	0	0.0334	0.2561	0.2044	0.0423	0.1363	0.1787	0.0071	0.0402	0.91	0.221	1.76

TABLE 4
VAPOR ANALYSIS
VAPOR TREATMENT SYSTEM

PRIMARY CARBON EFFLUENT

DATE	TIME	TOTAL VOCs (mg/L)
11/02/93	08:54	0.000
11/02/93	09:58	0.000
11/02/93	10:43	0.000
11/02/93	12:10	0.000
11/02/93	13:01	0.000
11/02/93	14:39	0.000
11/02/93	15:34	0.000
11/03/93	10:37	0.000
11/03/93	15:50	0.000
11/04/93	09:10	0.000
11/04/93	13:02	0.000
11/04/93	15:40	0.000
11/05/93	07:59	0.000
11/05/93	11:48	0.000
11/05/93	13:25	0.000

DISCHARGE STACK

DATE	TIME	TOTAL VOCs (mg/L)
11/02/93	09:41	0.000
11/02/93	10:17	0.000
11/02/93	11:35	0.000
11/02/93	13:40	0.000
11/02/93	15:06	0.000
11/03/93	15:50	0.000
11/04/93	08:20	0.000
11/05/93	08:14	0.000
11/05/93	15:50	0.000
11/05/93	15:50	0.000

TABLE 5
AIR SPARGING PRESSURES AND FLOWS

WELL TVI-1

SAMPLE DATE	SAMPLE TIME	FLOW D/P inches H2O	FLOW scfm	PRESSURE psig
11/03/93	10:30	(ns)	(ns)	2.0
	11:00	(ns)	(ns)	2.2
	11:30	0.90	42.4	5.0
	12:00	1.55	55.6	5.0
	12:30	1.40	52.8	5.0
	13:00	1.30	51.9	4.6
	13:30	1.30	52.2	4.5
	14:00	1.90	58.4	6.0
	14:30	1.55	55.6	5.0
	15:00	1.75	59.4	4.9
	15:30	1.60	57.6	4.6
	16:00	1.30	52.2	4.5
	16:30	1.45	55.1	4.5
11/04/93	08:45	0.90	48.3	2.0
	09:15	0.58	38.8	2.0
	09:45	0.80	45.6	2.0
	10:15	0.82	46.1	2.0
	10:45	0.64	40.8	2.0
	11:15	0.92	48.9	2.0
	11:45	0.88	47.8	2.0
	12:15	1.05	52.2	2.0
	12:45	1.35	54.4	4.0
	13:15	1.30	53.4	4.0
	13:45	1.50	57.4	4.0
	14:15	1.50	57.4	4.0
	14:45	1.55	58.3	4.0
	15:15	1.30	53.7	3.9
	15:45	1.25	52.6	3.9

TABLE 6
DISSOLVED OXYGEN MEASUREMENTS
AIR SPARGING TESTING

DATE	TIME	TMW-1			TMW-2		MW-1S
		DISSOLVED OXYGEN (mg/L)			DISSOLVED OXYGEN (mg/L)		DISSOLVED OXYGEN (mg/L)
11/03/93	08:30	1.0			0.0		8.0
11/03/93	11:10	1.6			3.4		6.8
11/03/93	14:30	0*			0*		0*
11/03/93	16:10	0*			0*		0*
11/04/93	07:15	5.7			2.2		1.1
11/04/93	11:40	2.9			1.9		2.5
11/04/93	16:30	4.4			2.5		4.3

* Readings questionable due to erratically operating meter

TABLE 7
WATER LEVELS
AIR SPARGING TEST

DATE	TIME	DEPTH TO WATER*			
		TVI-1	TMW-1	TMW-2	MW-1S
11/02/93	08:30	19.90			
11/02/93	16:30	19.70	19.60	20.60	18.60
11/03/93	07:00	19.60	19.45	20.50	18.70
11/03/93	11:00		19.95	20.54	20.40
11/03/93	14:00		19.55	20.41	20.27
11/03/93	16:00		19.43	20.45	20.24
11/04/93	07:10		19.22	20.49	19.75
11/04/93	11:55		19.28	20.54	20.17
11/04/93	15:20		19.21	20.50	20.15

* Measured From Top of Well Casing

TABLE 8
VAPOR ANALYSES
AIR SPARGING TESTING
WELL TVE-1

DATE	TIME	RUN HOURS (TOTAL)	WELL VACUUM (In. Hg)	1,2 DCA (mg/L)	BENZENE/TCA (mg/L)	TCE (mg/L)	TOLUENE (mg/L)	PCB (mg/L)	CHLORO-BENZENE (mg/L)	ETHYL-BENZENE (mg/L)	P.M. XYLENES (mg/L)	STYRENE ¹¹ (mg/L)	O-XYLENE ¹¹ (mg/L)	TOTAL VOCs (mg/L)	TOTAL POUNDS PER HOUR	CUMULATIVE LBS VOC'S RECOVERED
11/03/93	10:17	7.52	34.0	0.0162	0	0.0678	0.3928	0.4007	0.0649	0.1998	0.2434	0.0103	0.0536	1.45	0.184	1.76
11/03/93	10:17	7.52	34.0	0.0217	0	0.0796	0.468	0.5192	0.0853	0.2475	0.3012	0.0109	0.0691	1.80	0.229	1.76
11/03/93	10:47	8.02	48.6	0.0164	0	0.0619	0.4228	0.4659	0.0696	0.2083	0.2571	0.0108	0.0562	1.57	0.285	1.89
11/03/93	11:12	8.43	24.3	0.0267	0	0.0674	0.3717	0.4673	0.0635	0.1843	0.2123	0.0165	0.0493	1.46	0.133	1.98
11/03/93	11:12	8.43	24.3	0.0209	0	0.0664	0.4247	0.402	0.0751	0.2089	0.255	0.0094	0.0566	1.52	0.138	1.98
11/03/93	12:21	9.58	20.3	0.0204	0	0.0651	0.4237	0.5286	0.0703	0.2159	0.2643	0.0242	0.0638	1.68	0.127	2.13
11/03/93	12:48	10.03	15.4	0.0186	0	0.065	0.4002	0.4474	0.0727	0.2165	0.2633	0.0218	0.0623	1.57	0.090	2.18
11/03/93	13:22	10.60	15.4	0.0191	0.0555	0.3653	3.442	1.628	1.003	1.482	1.824	0.3383	0.653	10.91	0.628	2.38
11/03/93	13:53	11.12	19.6	0.0142	0.0531	0.3508	3.362	1.866	0.9912	1.474	1.8219	0.3449	0.6646	11.04	0.809	2.75
11/03/93	14:23	11.62	34.6	0	0.0408	0.0695	2.95	1.179	0.8643	1.239	1.4747	0.2773	0.5316	8.63	1.116	3.23
11/03/93	14:50	12.07	32.4	0.0158	0	0.053	0.3674	0.4044	0.0738	0.2069	0.2558	0.0215	0.0606	1.46	0.177	3.52
11/03/93	15:26	12.67	39.4	0.0112	0	0.0446	0.3506	0.5407	0.0674	0.1891	0.2351	0.0177	0.0536	1.51	0.223	3.64
11/03/93	15:26	12.67	39.4	0.0121	0	0.0459	0.3829	0.4426	0.0747	0.2197	0.2693	0.0284	0.0728	1.55	0.228	3.64
11/03/93	16:13	13.45	37.3	0.0109	0	0.0419	0.3428	0.4592	0.065	0.1933	0.2514	0.0235	0.0597	1.45	0.202	3.81
11/03/93	16:13	13.45	37.3	0.0111	0	0.0426	0.3499	0.3907	0.0615	0.1994	0.2627	0.0275	0.0622	1.41	0.196	3.81
11/04/93	08:20	13.45	11.6	0.0206	0	0.0621	0.2835	0.4996	0.0633	0.1541	0.1844	0.0273	0.0409	1.34	0.058	3.81
11/04/93	08:44	13.85	16.4	0.015	0	0.0568	0.3628	0.5343	0.0694	0.1968	0.2582	0.0116	0.0566	1.56	0.096	3.84
11/04/93	08:44	13.85	16.4	0.0115	0	0.0535	0.354	0.4255	0.0701	0.1891	0.221	0.0216	0.0542	1.40	0.086	3.84
11/04/93	09:47	14.90	16.4	0.0089	0	0.0397	0.2802	0.2716	0.0478	0.1537	0.1976	0.0079	0.0444	1.05	0.065	3.92
11/04/93	11:32	16.65	19.4	0.0118	0	0.0517	0.3834	0.5752	0.0782	0.2169	0.2736	0.0234	0.0651	1.68	0.122	4.09
11/04/93	12:07	17.23	15.6	0.0149	0	0.0515	0.3318	0.4191	0.0684	0.1867	0.229	0.0197	0.0553	1.38	0.080	4.14
11/04/93	12:07	17.23	15.6	0.0144	0	0.0504	0.3668	0.4514	0.0644	0.202	0.2604	0.0106	0.0599	1.48	0.086	4.14
11/04/93	13:02	18.15	14.7	0.0124	0	0.0515	0.3847	0.4814	0.07	0.2109	0.2538	0.0251	0.0628	1.55	0.085	4.22
11/04/93	13:42	18.82	16.4	0.0113	0	0.0493	0.3498	0.4469	0.0641	0.1998	0.2524	0.0215	0.0605	1.46	0.089	4.28
11/04/93	13:42	18.82	16.4	0.0115	0	0.0486	0.3737	0.4006	0.0673	0.2111	0.2774	0.0105	0.0639	1.46	0.090	4.28
11/04/93	14:21	19.47	14.7	0.0069	0	0.0491	0.3465	0.4467	0.0647	0.1958	0.2443	0.0215	0.0573	1.43	0.079	4.34
11/04/93	15:11	20.30	15.6	0.0107	0	0.0466	0.3498	0.5403	0.0708	0.1988	0.268	0.0126	0.0608	1.56	0.091	4.41
11/04/93	15:20	20.45	15.6	0.0118	0	0.0484	0.3597	0.4524	0.0648	0.2005	0.2576	0.011	0.0591	1.47	0.085	4.42
11/04/93	16:00	21.12	16.4	0.0075	0	0.1341	0.2811	0.4769	0.0598	0.1576	0.2196	0.0241	0.0545	1.42	0.087	4.48

TABLE 9
DVE TESTING VACUUMS AND FLOWS

DATE	TIME	TMW-2		TVE-1		TMW-1		MW-1S	
		DISTANCE							
		FROM TMW-2							
		(feet)							
		FLOW	VACUUM	VACUUM	VACUUM	VACUUM	VACUUM	VACUUM	VACUUM
	SCFM	In. H2O	In. H2O	In. H2O	In. H2O	In. H2O	In. H2O	In. H2O	
11/05/93	07:00	66	58.5		0.00		0.00		
	07:30	70	48.8		0.47		0.37		
	08:00	72	45.5		0.38		0.29		
	08:30	72	45.5		0.50		0.37		
	09:00	72	45.5		0.50		0.38		
	09:30	72	45.5		0.51		0.37		
	10:00	72	45.5		0.50		0.37		
	10:30	0	0		0		0		
	11:00	0	0		0		0		
	11:30	72	46.8		0.52		0.36		
	12:00	72	45.5	0.50	0.45		0.35		
	12:30	74	45.5	0.54	0.53		0.42		
	13:00	72	45.5	0.54	0.53		0.40		
	13:30	74	45.5	0.54	0.52		0.40		
	14:00	74	45.5	0.51	0.52		0.40		
	14:30	74	45.5	0.52	0.52		0.40		
	15:00	74	45.5	0.54	0.53		0.40		

TABLE 10
VAPOR ANALYSES
DVE TESTING
WELL TVM-2

DATE	TIME	RUN HOURS (TOTAL)	SCFM	WELL VACUUM (In. Hg)	1,2 DCA (mg/L)	BENZENE/ TCA (mg/L)	TCE (mg/L)	TOLUENE (mg/L)	PCE (mg/L)	CHLORO- BENZENE (mg/L)	ETHYL- BENZENE (mg/L)	P-M- XYLENES (mg/L)	STYRENE (mg/L)	O-XYLENE (mg/L)	TOTAL VOCs (mg/L)	TOTAL POUNDS PER HOUR	CUMULATIVE LBS VOC'S RECOVERED
11/05/93	07:44	21.12	66.0	4.5	0.0035	0.0004	0.0506	0.1202	0.1168	0.0221	0.0715	0.0716	0.0055	0.0154	0.48	0.118	4.48
11/05/93	08:06	21.48	72.0	3.5	0.006	0	0.0587	0.168	0.1843	0.0323	0.1155	0.1254	0.0041	0.0251	0.72	0.194	4.53
11/05/93	08:50	22.22	72.0	3.5	0.0066	0	0.0532	0.1487	0.1966	0.0273	0.0956	0.0973	0.0063	0.0205	0.65	0.176	4.67
11/05/93	08:52	22.25	72.0	3.5	0.0062	0	0.0489	0.1465	0.1572	0.027	0.0969	0.0962	0.007	0.021	0.61	0.163	4.68
11/05/93	09:25	22.80	72.0	3.5	0.0065	0	0.0491	0.1574	0.2486	0.0351	0.11	0.1153	0.0078	0.0258	0.76	0.203	4.78
11/05/93	09:30	22.88	72.0	3.5	0.0054	0	0.039	0.1244	0.1161	0.0223	0.0817	0.0801	0.0051	0.0167	0.49	0.132	4.79
11/05/93	11:50	23.72	72.0	3.5	0.0081	0	0.0082	0.0192	0.003	0.0113	0.0899	0.0057	0.0276	0.0038	0.18	0.048	4.87
11/05/93	12:18	24.18	74.0	3.5	0.0062	0	0.0419	0.1337	0.2042	0.0235	0.0832	0.0829	0.0053	0.0175	0.60	0.166	4.92
11/05/93	12:48	24.68	72.0	3.5	0.0074	0	0.0441	0.1577	0.1981	0.0315	0.1088	0.1122	0.0061	0.024	0.69	0.186	5.00
11/05/93	13:24	25.28	74.0	3.5	0.0075	0	0.045	0.1577	0.1977	0.0323	0.1089	0.1098	0.0065	0.0237	0.69	0.191	5.12
11/05/93	14:08	26.02	74.0	3.5	0.0089	0	0.0451	0.1711	0.2631	0.0357	0.1222	0.1247	0.0076	0.0271	0.81	0.223	5.27
11/05/93	14:20	26.22	74.0	3.5	0.0064	0	0.0366	0.1283	0.1336	0.026	0.0881	0.0842	0.0059	0.0188	0.53	0.146	5.30
11/05/93	15:00	26.88	74.0	3.5	0.005	0	0.0301	0.0948	0.1234	0.0211	0.0636	0.0611	0.0035	0.0131	0.42	0.115	5.39

TABLE 11
WATER LEVELS
DUAL VACUUM EXTRACTION TEST

DATE	TIME	DEPTH TO WATER (feet)*				DRAWDOWN (feet)			
		TVI-1	TMW-1	TMW-2	MW-1S	TVI-1	TMW-1	TMW-2	MW-1S
11/05/93	07:00	19.48	19.00	20.50	19.70	0.00	0.00	0.00	0.00
11/05/93	12:40	19.59	18.95	22.35	19.60	0.11	-0.05	1.85	-0.10
11/05/93	14:20	19.6	18.95	22.35	19.60	0.12	-0.05	1.85	-0.10

TABLE 12
SOIL CONCENTRATIONS AND CLEAN-UP GOALS

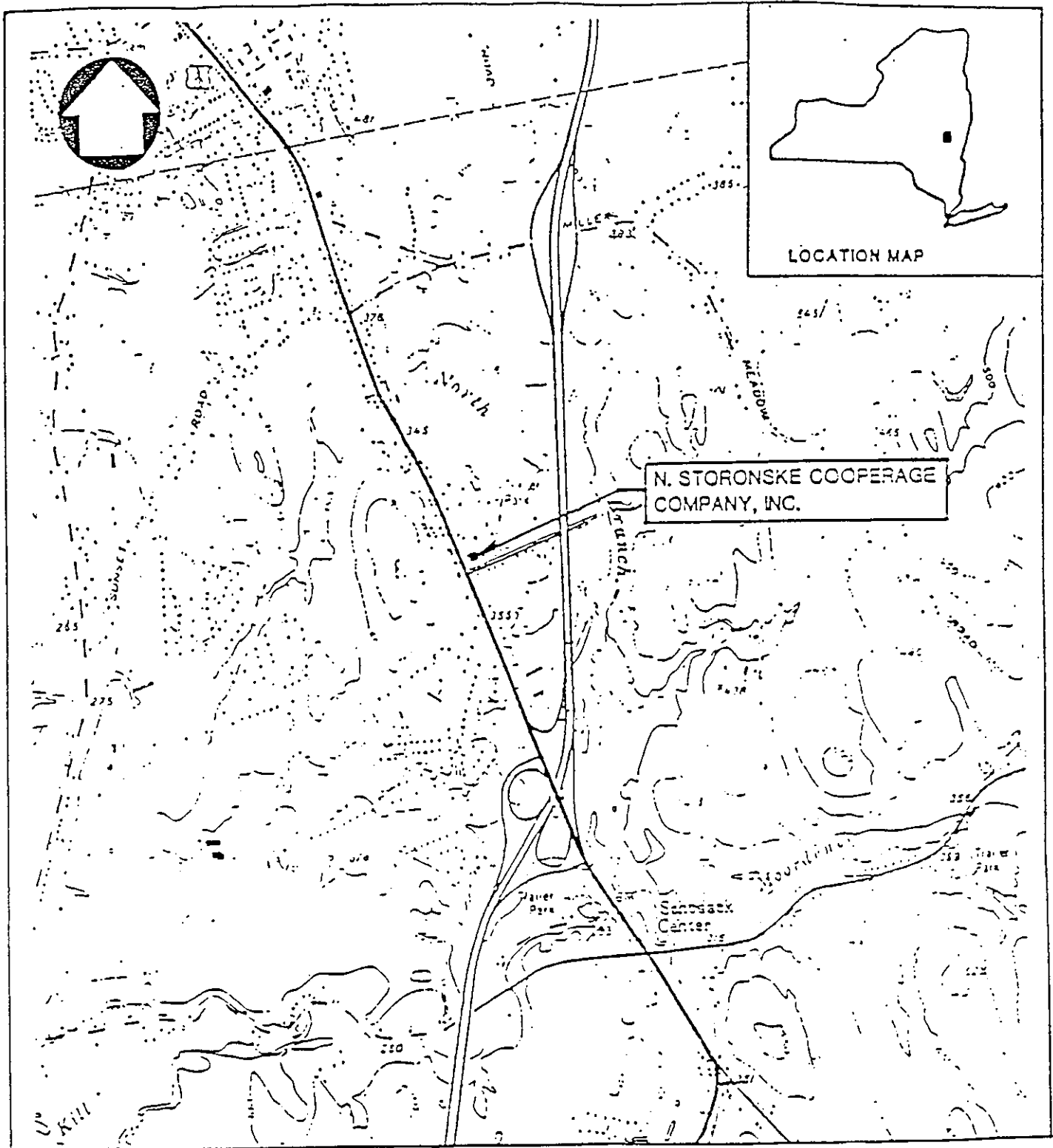
Compound	Abbrev.	Average Soil Conc. (ppb)	Maximum Soil Conc. (ppb)	Cleanup Goal (ppb)	Maximum Reduction Required
Tetrachloroethylene	PCE	332	3500	1500	57.1%
1,1-Trichloroethane	TCA	172	1300	1000	23.1%
Trichloroethylene	TCE	321	2600	1000	61.5%
1,2-Dichloroethane	1,2-DCA	790	2000	100	95.0%
Xylenes	X	15029	58500	1200	97.9%
Ethylbenzene	EB	5474	20000	5500	72.5%
Toluene	T	8558	41000	1500	96.3%
Chlorobenzene	CB	1230	3900	1500	61.5%

TABLE 13
BUDGETARY COST BREAKDOWN
STORONSKE COOPERAGE
SCHODACK, NEW YORK

	VE SYSTEM		DVE SYSTEM	
CAPITAL COSTS				
Well Installation	20 wells, 15 ft deep	\$30,000	53 wells, 20 ft deep	\$86,000
Vacuum Extraction Blower	75 hp	\$35,000	100 hp	\$45,000
Carbon, vapor phase	18,600 lbs	\$56,000	18,600 lbs	\$56,000
Carbon, liquid phase			2,000 lbs	\$6,000
Utility Installation		\$28,000		\$30,000
Piping & System Installation		\$33,000		\$52,000
TOTAL CAPITAL COSTS		\$182,000		\$275,000
OPERATING COSTS				
Labor, per month		\$6,000		\$11,000
Materials & Expenses		\$500		\$1,000
Analytical & Laboratory		\$4,500		\$7,000
Utilities		\$4,000		\$5,500
OPERATING COST PER MONTH		\$15,000		\$24,500
TOTAL OPERATING COST	18 months	\$270,000	18 months	\$441,000

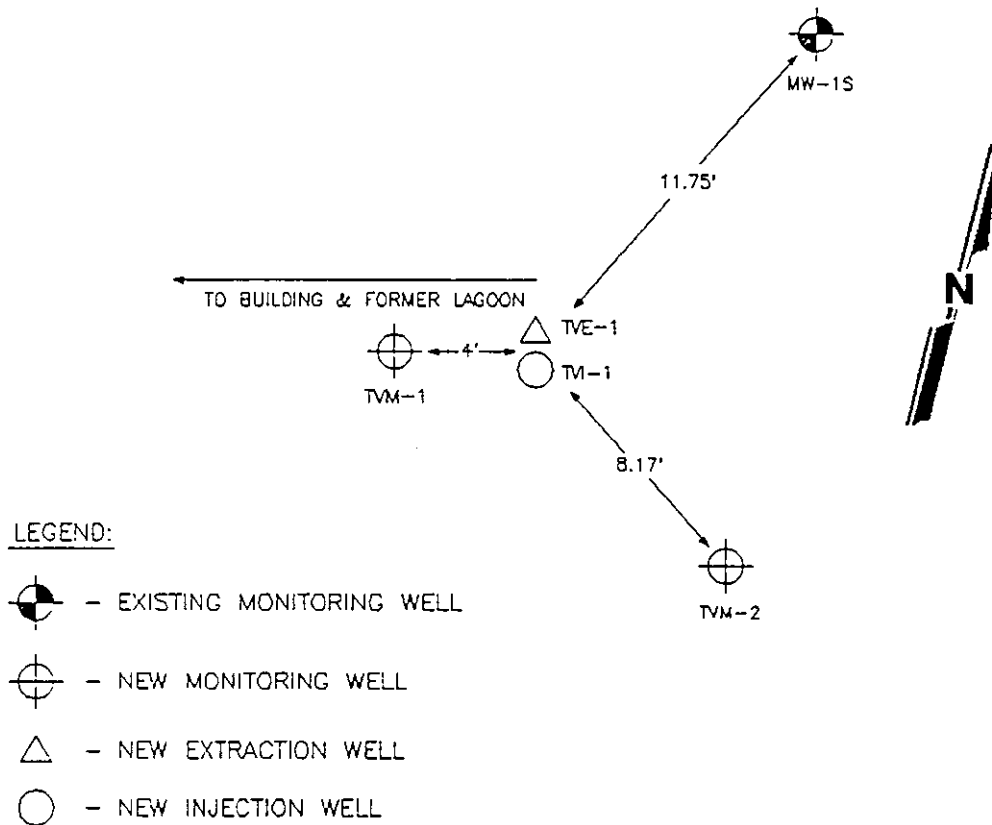
FIGURE 1

SITE MAP



*Taken from *Phase II Remedial Investigation Report*, August 1992, by Dvirka & Bartilucci

FIGURE 2
WELL LOCATIONS



STORONSKE COOPERAGE

WELL LOCATIONS

DRAWN: C CONNOLLY

DWG NO:

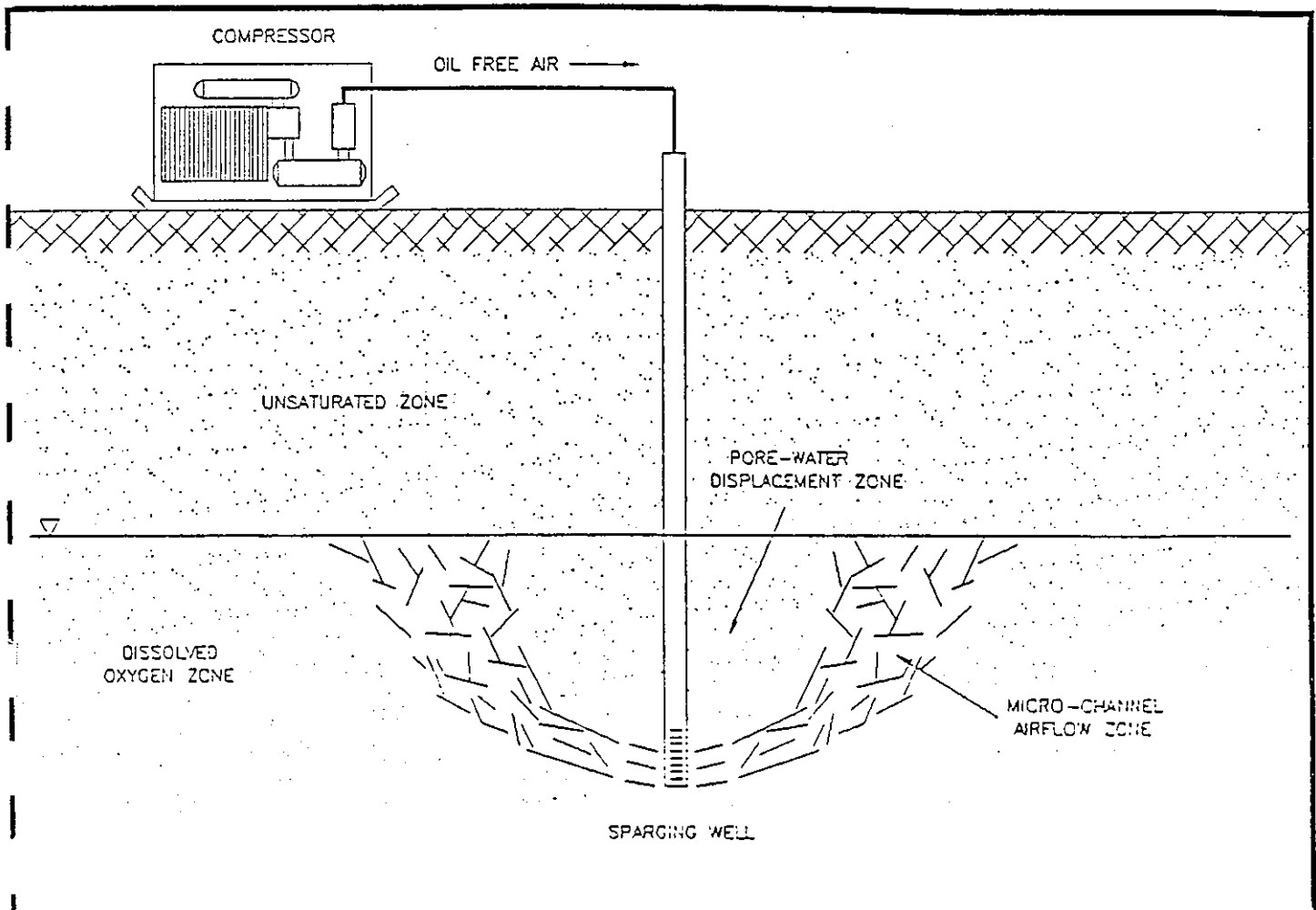
FIGURE:

SCALE: AS SHOWN

42-0075

2

FIGURE 3
SPARGEVAC™ DIAGRAM




	STORONSKE COOPERAGE	
	SPARGEVAC™ DIAGRAM	
	DRAWN: C. CONNELLY	DWG NO:
	SCALE: NOT TO SCALE	42-0075

FIGURE 4
PROCESS FLOW DIAGRAM

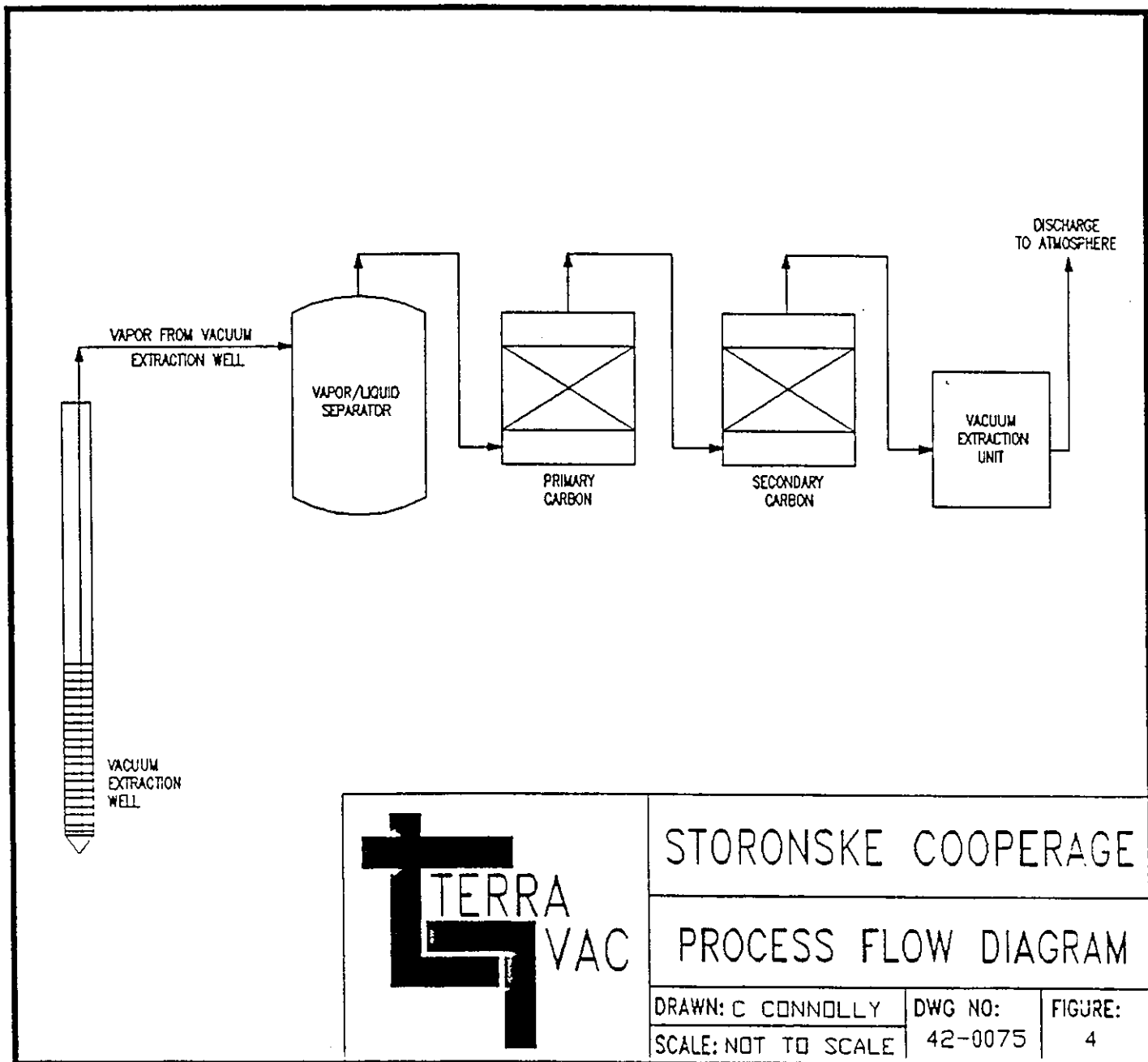


FIGURE 5
VACUUM EXTRACTION INFLUENCE TESTING

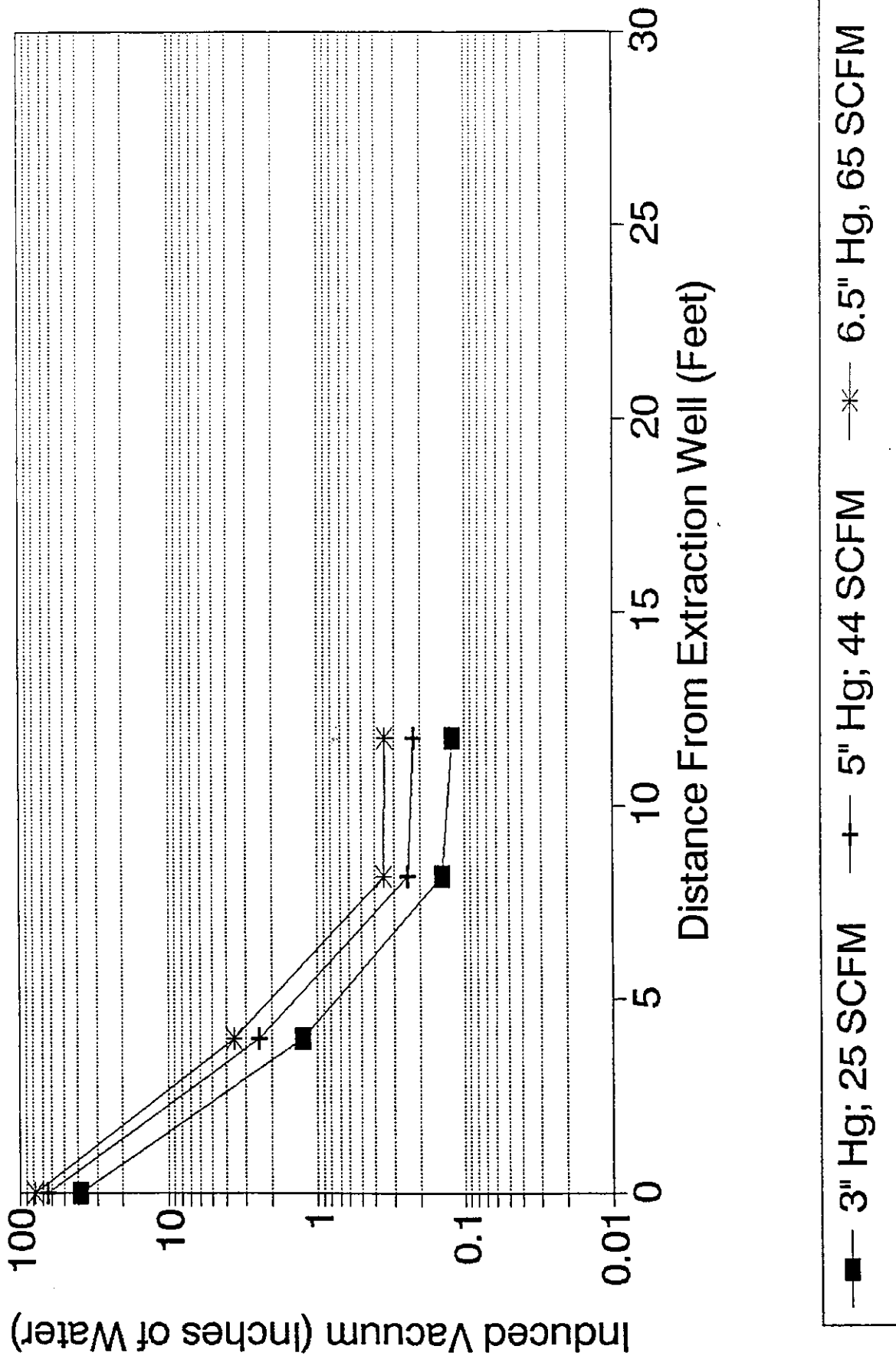


FIGURE 6

RADIUS OF INFLUENCE REGRESSION @ 3" Hg

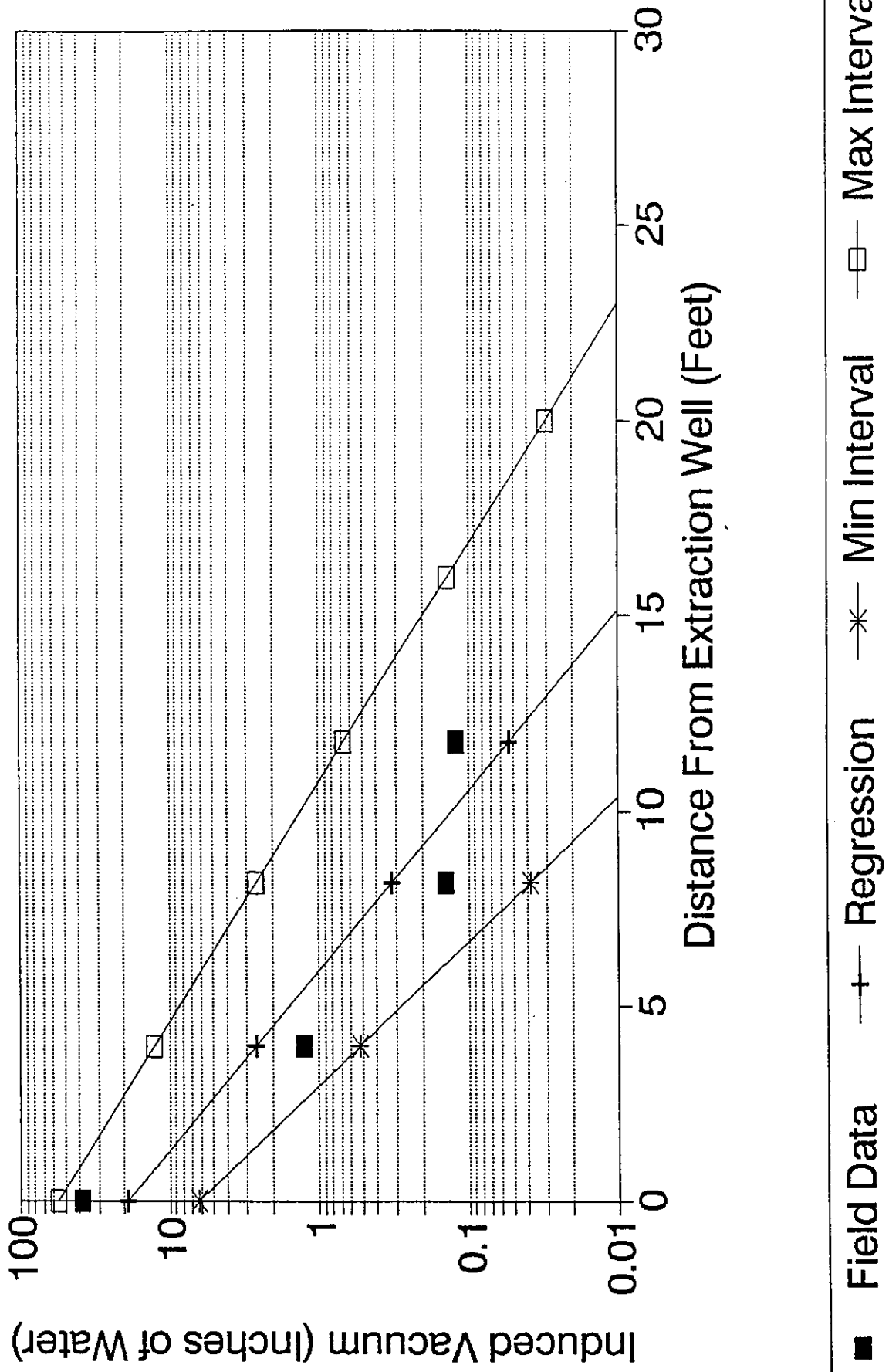
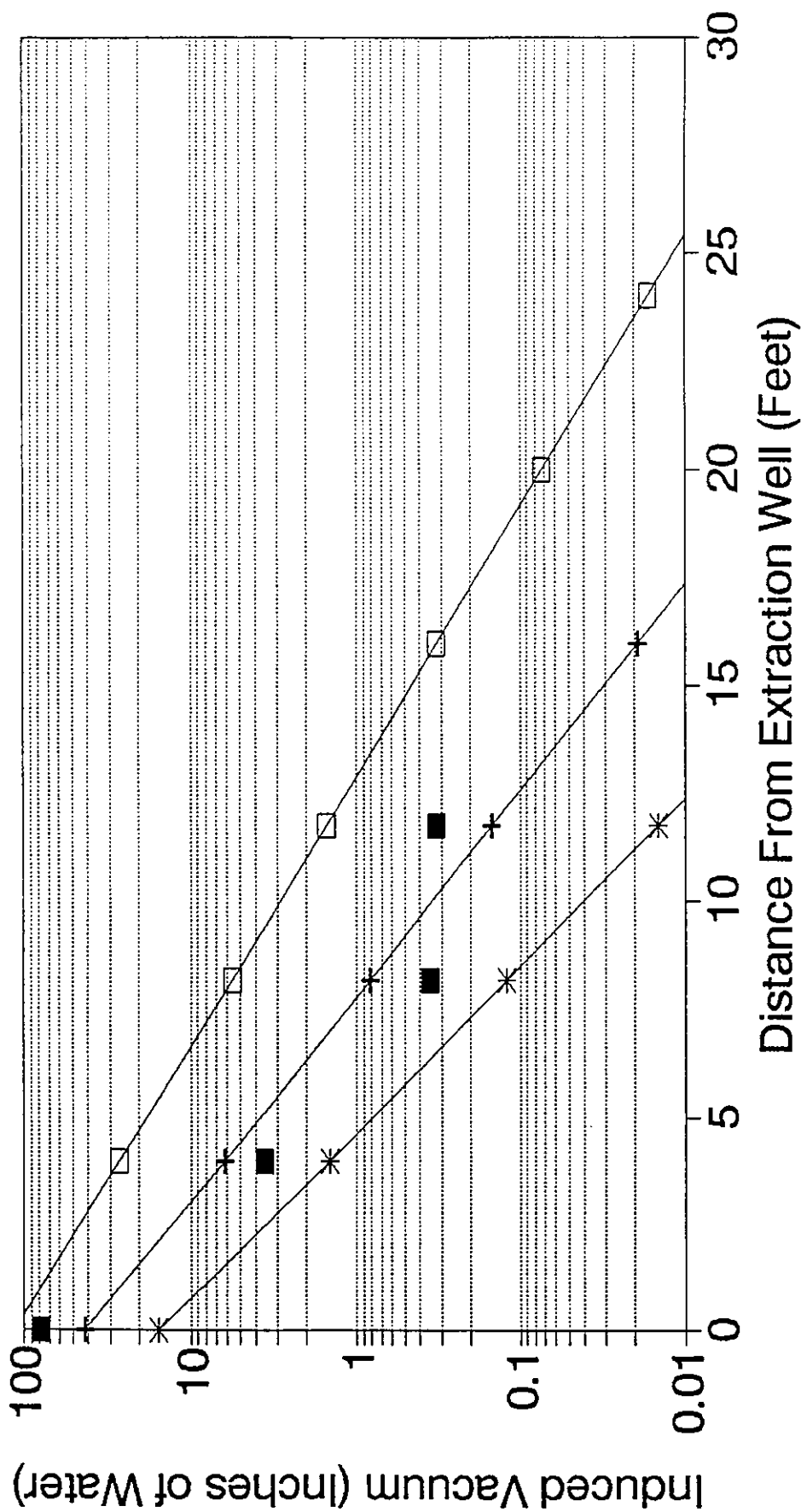


FIGURE 7

RADIUS OF INFLUENCE REGRESSION @6.5" Hg



■ Field Data + Regression * Min Interval □ Max Interval

FIGURE 8
VE TESTING FLOW vs. VACUUM

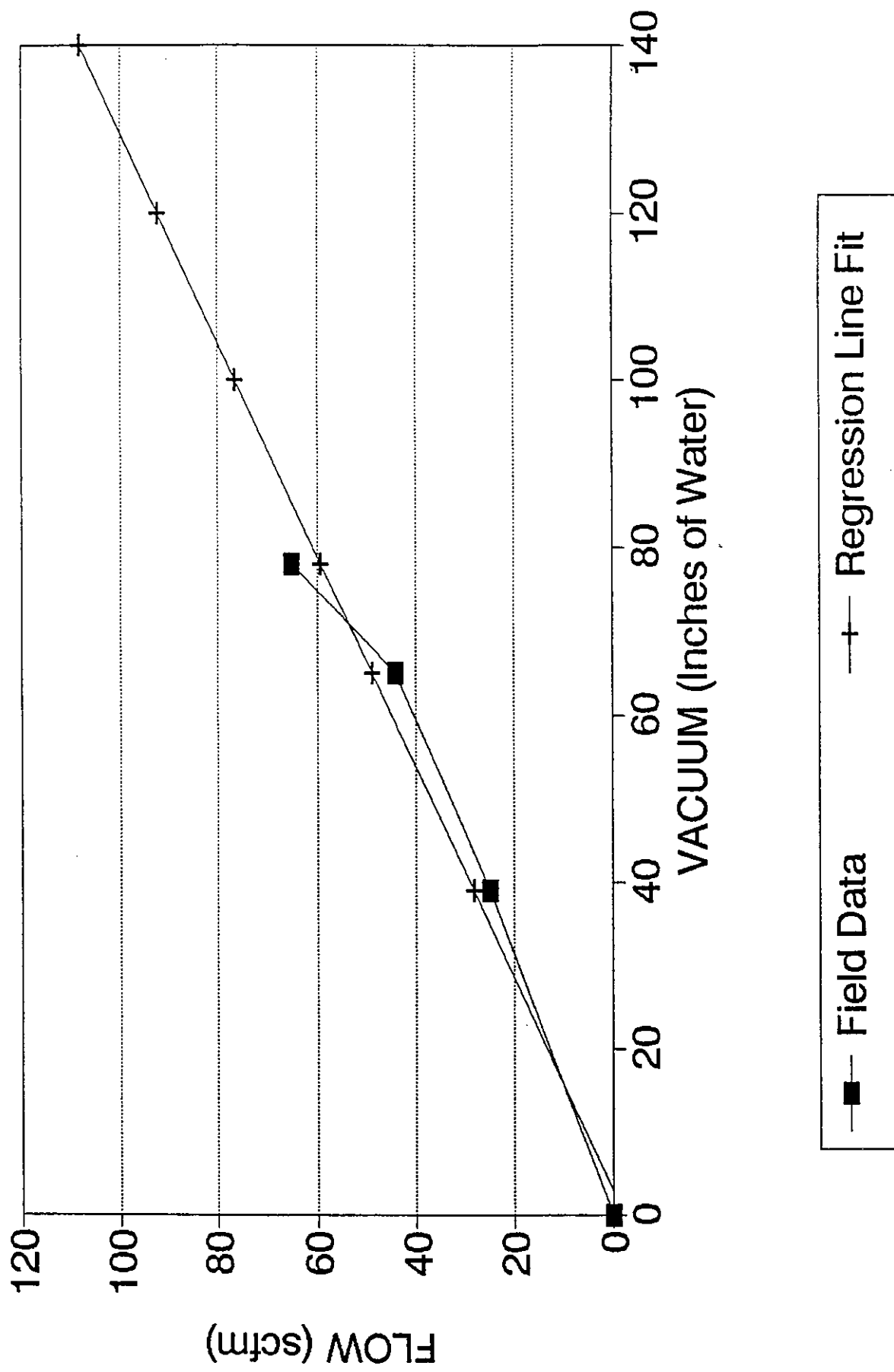
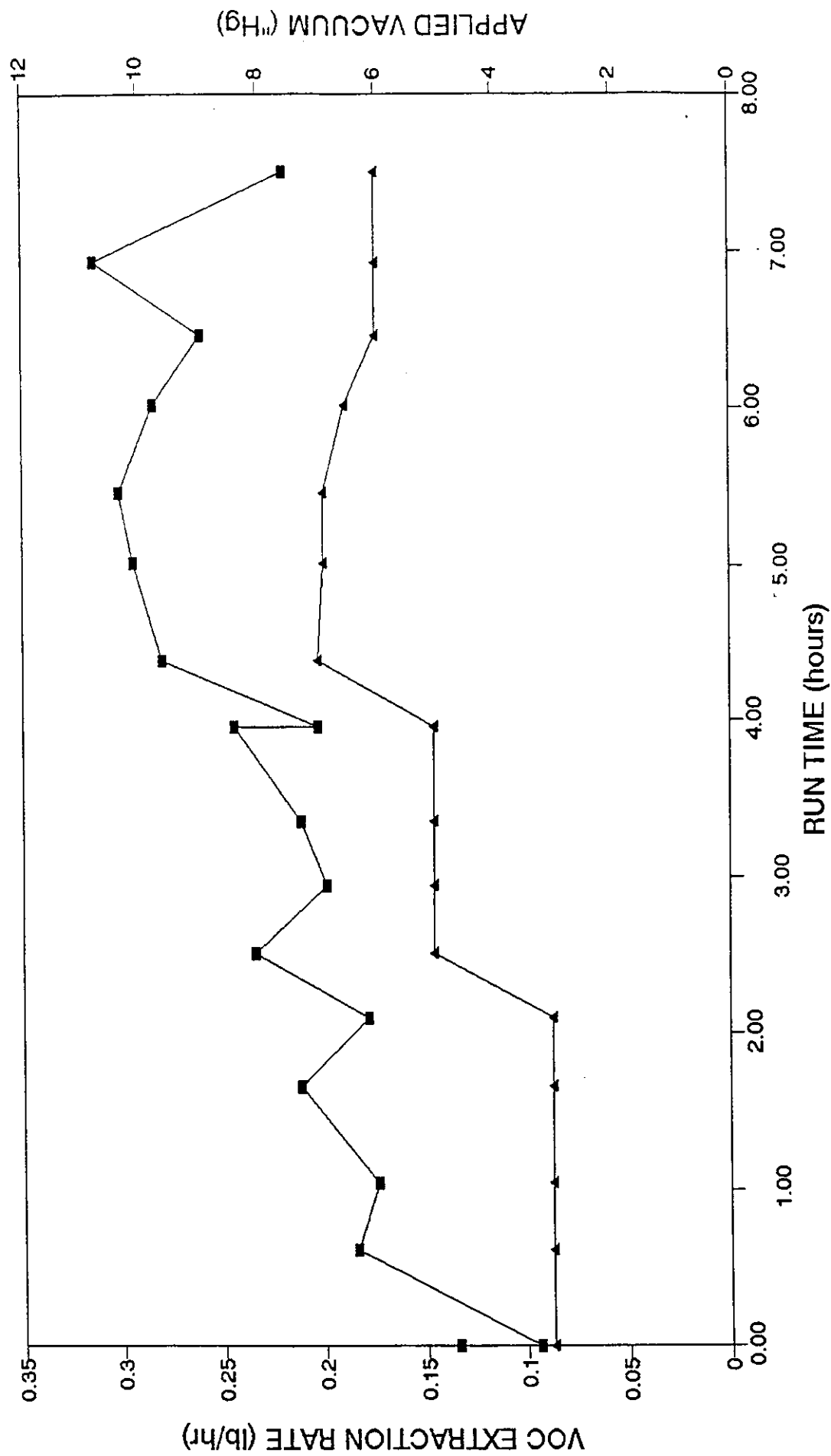


FIGURE 9

VE TEST EXTRACTION RATES



■ VOC Extraction Rate ▲ Applied Vacuum

FIGURE 14

SPARGING FLOW VERSUS PRESSURE

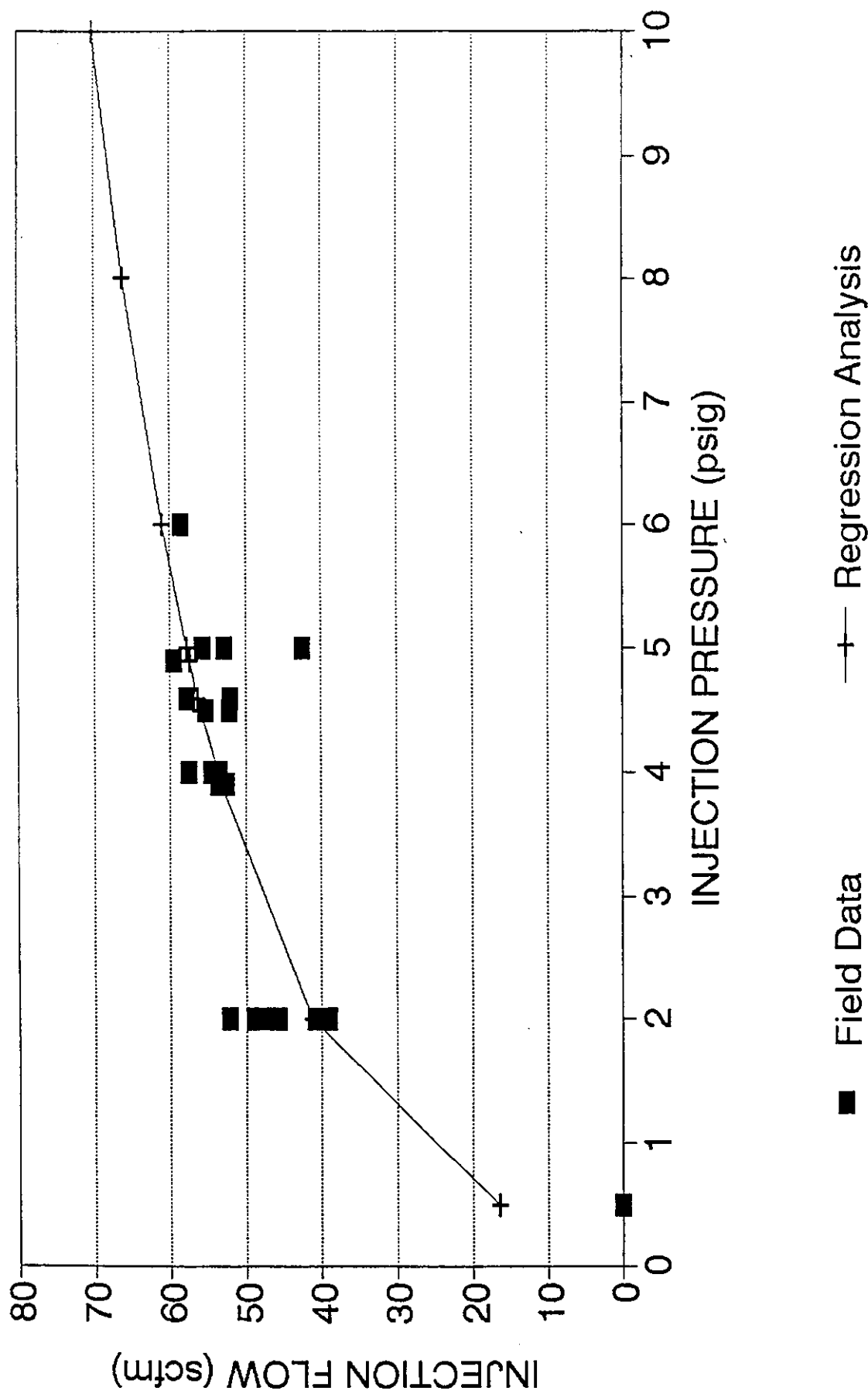
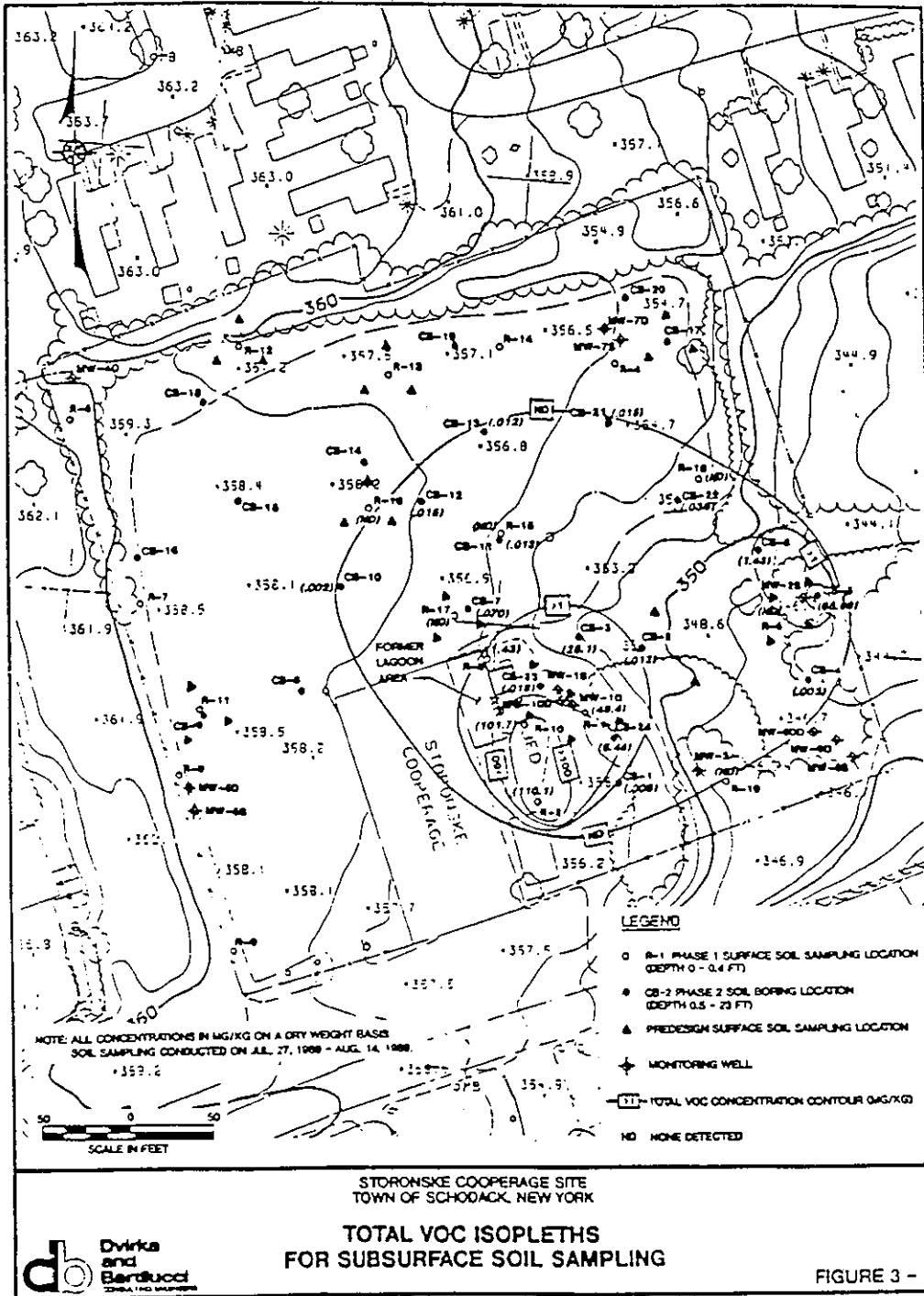
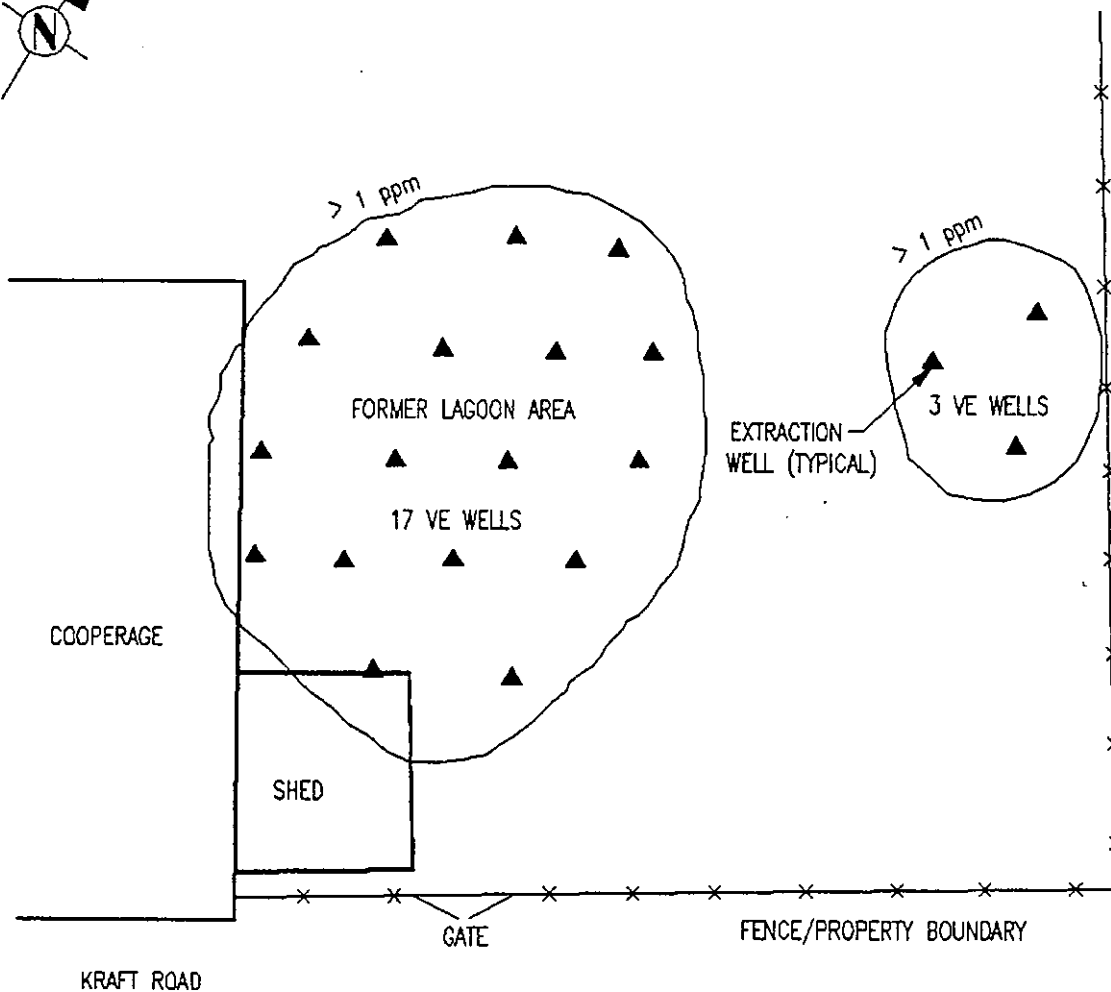


FIGURE 15
SOIL CONCENTRATION CONTOURS





STORONSKE COOPERAGE
SCHODACK, NY

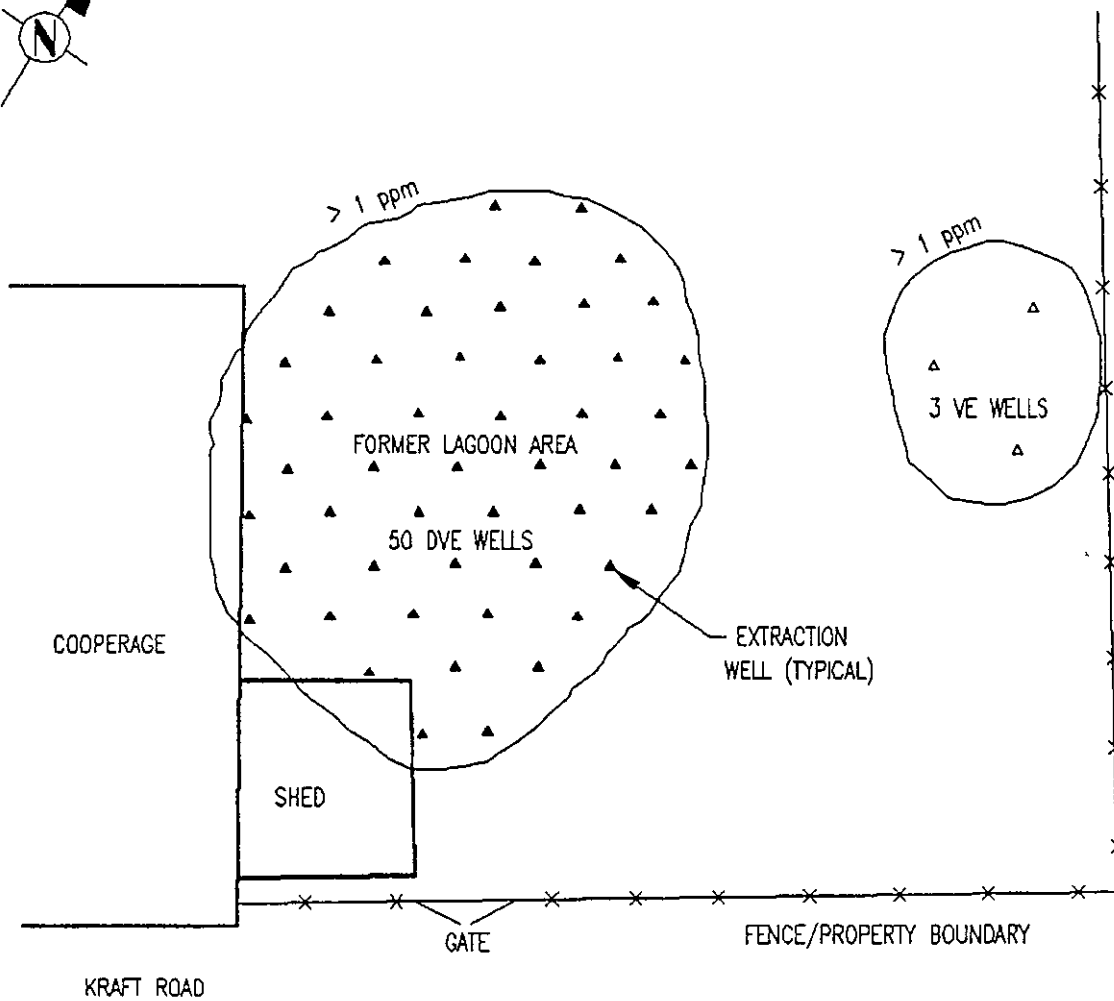
RECOMMENDED WELL LOCATIONS
VE SYSTEM

DRAWN: C CONNOLLY

DWG NO:
42-0075

FIGURE:
16

SCALE: AS SHOWN



STORONSKE COOPERAGE
SCHODACK, NY

RECOMMENDED WELL LOCATIONS
DVE SYSTEM

DRAWN: C CONNOLLY
SCALE: AS SHOWN

DWG NO:
42-0075

FIGURE:
17



BORING/WELL NUMBER:

TMW-2

DATE DRILLED:

10-28-93

Project: STORONSKE COOPERAGE Schodack, NY

Project Number:

42-0075

Drilling Contractor:

Parratt-Wolff, E. Syracuse, NY

Drilling Method:

6.25" I.D. Hollow Stem Augers

Log by:

J.W. Busanus

Driller:

Jim Hammond

SCREEN DIAM.: 4 inches

LENGTH: 10' 0"

MATERIAL: Sch. 40 PVC

RISER DIAM.: 4 inches

LENGTH: 10' 0"

MATERIAL: Sch. 40 PVC

FILTER MATL.: silica sand

FILTER SIZE: Morie #1(10-20 mesh)

SLOT SIZE: 0.020"

TOT. DEPTH: 19' 9"

WELL COMPLETION	DEPTH (ft.)	GRAPHIC LOG	USCS	S A M P L E	BLOWS PER 6"	REC. IN INCHES	GEOLOGIC DESCRIPTION (Color, Texture, Structure, etc.)	SOIL VAPOR (ppm) OVA Headspace in Bag	SOIL VAPOR (ppm) OVA in Breath. Zone	SOIL VAPOR (ppm) OVA at hole
	0		GC		N	N	Clay, silty & cobbly, brn-gry, moist, cobbles are well rnd			
	2		GC		S	S	Clay, silty, dk gry to gry-brn, w/ abund well rnd pebbles & cobbles throughout	N		
			GC		P	P		O		
			GC		L	L	Clay, A.A., cobbly, v moist	S		
			GC		I	I		O		
			GC		T	T		I		
	4		CL					L		
			CL		S	S	Clay, silty, dk gry, crumbly, v moist, w/ rare cobbles to pebbles, A.A., silty @ base	S	0.0	2.0
			CL		P	P		A		
			CL		O	O	Clay, A.A., dns., v. moist, sli silty, w/ rare to comm cobbles to pebbles, A.A.	M		
			CL		N	N	Clay, sli silty, brn-gry, w/ rare well rnd pebbles	P		
			CL		S	S		L		
	8		CL		T	T	Clay, silty, gry-brn, crumbly, v. moist, w/ comm well rnd cobbles, pebbles & crs. sand	S	0.0	40
			CL		A	A		C		
			CL		K	K		O		
			CL		E	E		L		
	10		GC		N	N	Cobbles, Crs. gravel & pebbles in silty clay matrix, dk gry to gry, crumbly, v. moist to wet	L	0.0	0.0
			GC					E		
			GC				Cobbles, Ss., well rnd, in silty clay matrix, A.A., dk gry-brn	C		
			GC				Crs. Sand, gravelly & pebbly, dk gry, w/ silty clay matrix, A.A., loose & crumbly	T	0.0	0.0
			GC					E		
	14		GC				Cobbles, well rnd, comp. A.A., w/ silty clay matrix, dk gry-brn, loose, wet, crsly sdy @ base	D	0.0	0.0
			GC							
	16		GP				Cobble, frag., gry-tan, silty Ss. comp.			
			GM				Pebbles, well rnd, dk gry, w/sdy & silty clay			
			GM				Cobble, gry-olive, silty Sh. comp., lam.			
	18		CL				Clay, silty, comm pebb. & sd., dk gry, wet			
			GP				Clay, silty to pebbly, gry-blue, dns, wet			
			GP				Cobble frags., Siltst. & Agillite, well rnd, w/ comm clay matrix, wet		0.0	0.0
	20									
	22						TOTAL DEPTH OF BORING TAPED AT 19' 9" BGL.			

Remarks: 6.25-inch I.D., 8.5-inch O.D. hollow-stem augers driven to a total depth of 19' 9" where refusal occurred. Soil vapor monitored with OVA throughout augering. Ova read 1000+ ppm inside augers at total depth. Taped total boring depth @ 19' 9". Inserted four-inch I.D., Schedule 40 PVC screw-on end cap (0'4"), 0.020" slot screen (10'0") and riser (10'0") into boring through augers. Added Morie #1 (10-20 mesh) sand to 8'3" below ground level (BGL). Added bentonite chips to 7'4" BGL (11") and wet @ 15:20. Pulled last augers from boring and grouted to 3.5 feet BGL with 1.5 sacks Portland #1-bentonite cement and one pound expansion agent additive per sack. Let stand overnight. Inserted 5.0 foot long, 6-inch I.D. black iron standpipe in boring. Grouted to surface with Portland #1 cement-bentonite mixture with one pound expansion agent per sack. Let stand 1.5 hours. Added round pad form and grouted to 5" above ground level with Sacrete mix. In A.M. on 10-29-93, bailed about 2.0 gallons of water from well to partially develop it.

Soil descriptions from boring for well TVE-1 & TVI-1.



BORING/WELL NUMBER:

TVE-1 & TVI-1

DATE DRILLED:

10-27-93

Project:

STORONSKE COOPERAGE Schodack, NY

Project Number:

42-0075

Drilling Contractor:

Parratt-Wolff, E. Syracuse, NY

Log by: J.W. Busanus

Drilling Method:

Split Spoons through 6.25" I.D. Hollow Stem Augers

Driller: Jim Hammond

SCREEN DIAM.: 2 inches

LENGTH: TVI-1 = 0'6"; TVE-1 = 5'0"

MATERIAL: Sch. 40 PVC

TOT. DEPTH(TVI-1): 19'6"

RISER DIAM.: 2 inches

LENGTH: TVI-1 = 20'0"; TVE-1 = 10'0"

MATERIAL: Sch. 40 PVC

TOT. DEPTH(TVE-1): 11'6"

FILTER MATL.: silica sand

FILTER SIZE: Morie #1(10-20 mesh)

SLOT SIZE: 0.020"

WELL COMPLETION	DEPTH (ft.)	GRAPHIC LOG	USCS	S A M P L E	BLOWS PER 6"	REC. IN INCHES	GEOLOGIC DESCRIPTION (Color, Texture, Structure, etc.)	SOIL VAPOR (ppm) OVA Headspace in Bag	SOIL VAPOR (ppm) OVA in Breath. Zone	SOIL VAPOR (ppm) OVA at hole
	0		GC				Clay, silty & cobbly, brn-gry, moist, cobbles are well rnd: 11"	140	0.0	0.0
			GC	*	5-8-8-6	19"	Clay, silty, dk gry to gry-brn, w/ abund well rnd pebbles to cobbles throughout: 8"			
	2		GC	*	4-3-3-4	11"	Clay, A.A., cobbly, v moist: 11"	1000+	0.0	0.0
	4		CL	*	1-2-1-2	21"	Clay, silty, dk gry, crumbly, v moist, w/ rare cobbles to pebbles, A.A., silty @ base: 21"	1000+	0.0	
	6		CL	*	2-2-3-8	16"	Clay, A.A., dns, v. moist, sli silty, w/ rare to comm cobbles to pebbles, A.A.: 9"	M=600 St=350	0.0	0.0
	8		CL	*	4-11-10-9	8"	Clay, silty, gry-brn, crumbly, v. moist, w/ comm well rnd cobbles, pebbles & crs. sand: 8"	400	0.0	
	10		GC	*	10-11-10-9	13"	Cobbles, Crs. gravel & pebbles in silty clay matrix, dk gry to gry, crumbly, v. moist to wet: 13"	160	0.0	0.0
	12		GC	*	7-10-11-14	9"	Cobbles, Ss., well rnd, in silty clay matrix, A.A., dk gry-brn: 7"	100	5.0	60
	14		GC	*	10-10-12-14	8"	Crs. Sand, gravelly & pebbly, dk gry, w/ silty clay matrix, A.A., loose & crumbly: 2"			
	16		GP	*	42-14-15-10	11"	Cobbles, well rnd, comp. A.A., w/ silty clay matrix, dk gry-brn, loose, wet, crsly sdy @ base: 8"	150	0.0	
	18		CL	*	5-8-27-15	13"	Cobble, frag., gry-tan, silty Ss. comp.: 3"	105	5.5	50
	20		GP	*	100/3"	6"	Pebbles, well rnd, dk gry, w/sdy & silty clay: 2"			
			CL	*			Cobble, gry-olive, silty Sh. comp., lam.: 4"			
			CL	*			Clay, silty, comm pebb. & sd., dk gry, wet: 2"			
			CL	*			Clay, silty to pebbly, gry-blue, dns, wet: 9"			
			CL	*			Cobble, frag., Siltst. comp., well lam., dns: 3"	250	0.0	0.0
			CL	*			Silt, gry to gry-blue, w/ abund Sd. & Pebbs., A.A., wet: 1"			
	22		GP	*			Cobble, Argillite, frag., in dk gry-blue clay matrix, wet: 6"	190	0.0	0.0
							NOTES: M=Maximum OVA rdg. St=Stabilized OVA rdg.			

Remarks: Continuous 2-inch I.D., 2-foot long split spoons driven ahead of 6.25-inch I.D., 8.5-inch O.D. hollow-stem augers to a total depth of 20'3". Soil sample for head space analysis in baggie collected from each split spoon. Taped total boring depth @ 19' 6". Inserted two-inch I.D., Schedule 40 PVC slip-on end cap (0'2"), 0.020" slot screen (0'6"), & riser (20'0") into boring through augers. Added Morie #1 (10-20 mesh) sand to 18'0" below ground level (BGL). Added bentonite chips to 12'0" BGL and wet @ 13:20. Added Morie #1 sand to 11'6" BGL. Inserted two-inch I.D., Schedule 40 end cap (0'2"), 0.020" slot screen (5'0"), & riser (10'0") into boring through augers. Added Morie #1 (10-20 mesh) sand to 5'6" BGL. Added bentonite chips to 4'6" BGL and wet @ 17:15. Let stand overnight. Pulled last auger from boring and grouted to 3.0' BGL with 1.5 sack Portland #1-bentonite cement and one pound expansion agent additive per sack. Let stand overnight. In A.M. of 10-29-93, bailed about 3 gallons of water to partially develop well. Grouted to 6 inches below ground surface with Portland #1 cement-bentonite mixture with one pound expansion agent per sack. No standpipe on this well cluster at present. No water found in TVE-1. TVI-1 screened interval is 19'4" to 18'10" BGL. TVE-1 screened interval is 11'4" to 6'4" BGL.

APPENDIX C

APPLICATION FOR PERMIT TO CONSTRUCT A PROCESS, EXHAUST OR VENTILATION SYSTEM

LOCATION: FACILITY: EMISSION POINT:

NEW YORK STATE
DEPARTMENT OF ENVIRONMENTAL CONSERVATION

COPIES
WHITE - ORIGINAL
GREEN - DIVISION OF AET
WHITE - REGIONAL OFFICE
WHITE - FIELD REP
YELLOW - APPLICANT



PROCESS, EXHAUST OR VENTILATION SYSTEM
APPLICATION FOR PERMIT TO CONSTRUCT OR CERTIFICATE TO OPERATE

1. NAME OF OWNER / FIRM: **NYSDEC, Division of Hazardous Waste Remediation**
2. NUMBER AND STREET ADDRESS: **50 Wolf Rd**
3. CITY - TOWN - VILLAGE: **Albany** 4. STATE: **NY** 5. ZIP: **12233**
6. NAME OF AUTHORIZED AGENT: **Dvirka and Bartilucci Consulting Engineers**
7. NUMBER AND STREET ADDRESS: **6800 Jericho Tpk**
8. CITY - TOWN - VILLAGE: **Syosset** 9. STATE: **NY** 10. ZIP: **11791**
11. TELEPHONE: **(516) 364 9892**
12. FACILITY NAME (IF DIFFERENT FROM OWNER / FIRM): **Storonske Cooperage Site**
13. FACILITY LOCATION NUMBER AND STREET ADDRESS: **Kraft Rd**
14. CITY - TOWN - VILLAGE: **E. Greenbush, Town of Schenectady** 15. ZIP: **12061**
16. BUILDING NAME OR NUMBER: **NA** 17. FLOOR NAME OR NUMBER: **NA**
18. OWNER CLASSIFICATION: ☒ STATE ☐ MUNICIPAL ☐ RESIDENTIAL ☐ COMMERCIAL ☐ UTILITY ☐ INDUSTRIAL ☐ FEDERAL ☐ EDUC. INST. ☐ OTHER
19. NAME OF OWNER'S REPRESENTATIVE: **Brian Heneveld, Proj. Mgr** 20. TELEPHONE: **(516) 364 9892**
21. SIGNATURE OF OWNER'S REPRESENTATIVE: **Brian Heneveld**
22. SIGNATURE OF AGENT: **Brian J. Heneveld** 23. TELEPHONE: **(516) 364 9892**
24. START-UP DATE: **8/94** 25. DRAWING NUMBERS OF PLANS SUBMITTED: **Figure 1**
26. CERTIFICATE TO OPERATE: ☒ NEW SOURCE ☐ EXISTING SOURCE ☐ MODIFICATION

27. SOURCE CODE: **001** 28. GROUND ELEVATION (FT.): **356** 29. HEIGHT ABOVE GROUND (FT.): **5** 30. DISTANCE FROM STRUCTURE (FT.): **20** 31. DISTANCE FROM PROPERTY LINE (FT.): **6** 32. DISTANCE FROM ADJACENT PROPERTY (FT.): **60** 33. DISTANCE FROM ROAD (FT.): **110** 34. DISTANCE FROM WATER BODY (FT.): **1300**
35. SOURCE CODE: **24** 36. DISTANCE FROM STRUCTURE (FT.): **365** 37. DISTANCE FROM PROPERTY LINE (FT.): **25** 38. DISTANCE FROM ADJACENT PROPERTY (FT.): **25** 39. DISTANCE FROM ROAD (FT.): **25** 40. DISTANCE FROM WATER BODY (FT.): **25**

41. DESCRIBE PROCESS OR UNIT: **SOIL VAPOR EXTRACTION SYSTEM**

42. EMISSION CONTROL EQUIPMENT: **01** 43. CONTROL TYPE: **20** 44. MANUFACTURER'S NAME AND MODEL NUMBER: **LIQUID/VAPOR SEPARATOR** 45. DISPOSAL METHOD: **9** 46. DATE INSTALLED MONTH / YEAR: **8 / 94** 47. USEFUL LIFE: **1.5**
48. EMISSION CONTROL EQUIPMENT: **02** 49. CONTROL TYPE: **17** 50. MANUFACTURER'S NAME AND MODEL NUMBER: **VAPOR PHASE ACTIVATED CARBON ADSORPTION** 51. DISPOSAL METHOD: **9** 52. DATE INSTALLED MONTH / YEAR: **8 / 94** 53. USEFUL LIFE: **1.5**

54. CALCULATIONS:
XYLENES* $0.2386 \text{ mg/lair} \left(\frac{1 \text{ g}}{1000 \text{ mg}} \right) \left(\frac{1 \text{ lb}}{454 \text{ g}} \right) \left(\frac{28.32 \text{ L}}{\text{ft}^3} \right) \left(\frac{1360 \text{ ft}^3}{\text{min}} \right) \left(\frac{60 \text{ min}}{1 \text{ hr}} \right) = 1.16 \text{ lb/hr Extracted}$
Treatment Efficiency = 99%
(Vapor Phase Activated Carbon in Series)
Actual Emissions = 1.16 lb/hr (1 - 0.99) = 0.012 lb/hr
Note: Activated Carbon will be regenerated offsite
NA = Not Applicable

CONTAMINANT	NAME	GAS NUMBER	INLET OF PRODUCTION	UNIT OF MEASUREMENT	EMISSIONS			CONTROL EFFICIENCY	HOURLY EMISSIONS (LBS/YR)		ANNUAL EMISSIONS (LBS/YR)	
					ACTUAL	UNIT	PERMISSIBLE		EXP.	ACTUAL	ACTUAL	PERMISSIBLE
Xylenes		01330-20-7			0.012	1	3	99	0.012	0.012	105	0
Toluene		00108-88-3			0.026	1	3	99	0.026	0.026	228	0
Ethylbenzene		00100-41-4			0.010	1	3	99	0.010	0.010	87.6	0
Chlorobenzene		00108-90-7			0.002	1	3	99	0.002	0.002	17.5	0
Tetrachloroethene		00127-18-4			0.020	1	3	99	0.020	0.020	175	0
Trichloroethene		00079-01-6			0.008	1	3	99	0.008	0.008	70.1	0

55. SOLID FUEL TONS/YR: **NA** 56. LIQUID FUEL TONS/YR: **NA** 57. TYPE: **NA** 58. THOUSANDS OF CUBIC FEET: **NA** 59. APPLICABLE RULE: **152** 60. APPLICABLE RULE: **154**

THE PROCESS, EXHAUST OR VENTILATION SYSTEM HAS BEEN CONSTRUCTED AND WILL BE OPERATED IN ACCORDANCE WITH STATE SPECIFICATIONS AND IN CONFORMANCE WITH ALL PROVISIONS OF ENVIRONMENTAL CONSERVATION LAW.

61. LOCATION CODE: **NA** 62. FACILITY ID NO: **NA** 63. DATE: **NA** 64. DATE APPL. RECEIVED: **NA** 65. DATE APPL. REVIEWED: **NA** 66. REVIEWED BY: **NA**

PERMIT TO CONSTRUCT
DATE ISSUED: **NA** EXPIRATION DATE: **NA** SIGNATURE: **NA**

CERTIFICATE TO OPERATE
DATE: **NA** EXPIRATION DATE: **NA** SIGNATURE: **NA**

APPENDIX D

ANALYTICAL DATA FOR SURFACE AND SUBSURFACE SOIL SAMPLES

ANALYTICAL RESULTS		All Solids Reported on a Dry Weight Basis										Page	
ANALYSIS	ANALYTICAL RESULTS	CB-230	CB-230	CB-4A	CB-23A	CB-4B	CB-20A	CB-20B	CB-20B	CB-20C	Blanket 01	CB-22A	
alcohol Piracic Sample Bubber		890001205	890001209	890001301	890001302	890001304	890001306	890001307	890001309	890001310	890001301	890001302	
laboratory Sample Bubber													
1st Solids		88	92	84	77	92	90	92	94	86		94	
	mg/kg												
2nd													
	mg/kg												
ORGANIC ELEMENTS													
	Detection Limit												
Carbon	P	10	88	88	88	88	88	88	88	88		88	
Hydrogen	P	2.5	88	88	88	88	88	88	88	88		88	
Isotopic	P	0.25	88	88	88	88	88	88	88	88		88	
Strontium	P	0.50	88	88	88	88	88	88	88	88		88	
Chlorine	P	0.25	88	88	88	88	88	88	88	88		88	
Barium	P/P	0.05/0.50	5.2 J	0.07 J	0.95 J		1.0 J	0.07 J	0.65 J	0.93 J		0.96 J	
Aluminum	P	2.5	88	88	88	88	88	88	88	88		88	
Bromine	P	0.50	26.0 J	21.1 J	26.6 J	22.0 J	25.3 J	23.6 J	19.9 J	25.0 J		30.2 J	
Sulfur	P	2.5	88	88	88	88	88	88	88	88		88	
Mercury	P	1.25	30.0 J	27.0 J	33.6 J	30.3 J	35.1 J	35.6 J	30.1 J	30.0 J		39.0 J	
Copper	P	2.5	88	88	88	88	88	88	88	88		88	
Lead	P/P	0.25/2.5	95.2	13.0	41.2	35.0	25.1	31.3	16.6	10.9		64.7	
Selenium	P	2.5	88	88	88	88	88	88	88	88		88	
Silver	P	0.75	88	88	88	88	88	88	88	88		88	
Chromium	CV	0.02	1.08 J	0.030	0.010	0.050	0.070	0.050	0.040	0.000		0.000	
Iron	P	2.0	88	88	88	88	88	88	88	88		88	
Calcium	P	25	88	88	88	88	88	88	88	88		88	
Fluorine	P	0.50											
Lithium	P	1.0	88	88	88	88	88	88	88	88		88	
Strontium	P	25	88	88	88	88	88	88	88	88		88	
Barium	P	0.25	88	88	88	88	88	88	88	88		88	
Vanadium	P	2.5	88	88	88	88	88	88	88	88		88	
...	P	0.50	102 J	81.2 J	90.5 J	91.3	106 J	86.5 J	89.6 J	91.5 J		106 J	
Yanide	DC	1.0	88	88	88	88	88	88	88	88		88	

Blanket was not detected.

(0) - The result is greater than or equal to the instrument detection limit, but less than the CLP required detection limit.

J - Quantitation is approximate due to limitations identified in the quality assurance review.

3 - This result is qualitatively suspect since this constituent was detected in a field and/or laboratory blank(s) at a similar level.

8 - Unreliable results - Analyte may or may not be present in this sample.

DL - Not detected, but the detection limit is probably higher than reported based upon a low bias identified during the quality assurance review.

NR - Analytes for that analyte not requested.

ANALYTICAL METHOD:

P - Inductively Coupled Plasma

F - Graphite Furnace Atomic Absorption

CV - Cold Vapor Atomic Absorption

8 - Hydride Generation

DC - Distillation/Colorimetric

[illegible]

VOLATILE ORGANIC ANALYSIS - ANALYTICAL RESULTS			ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS												Page 32	
	CB-130	CB-131C	CB-132	CB-133	CB-134	CB-135	CB-136	CB-137	CB-138	CB-139	CB-140	CB-141	CB-142	CB-143	CB-144	CB-145
Sample Number	890811806	890811807	890811808	890811809	890811810	890811811	890811812	890811813	890811814	890811815	890811816	890811817	890811818	890811819	890811820	890811821
Laboratory Sample Number																
Lot																
Notes																
VOLATILE COMPOUNDS																
	Quantitation Limit															
Chloro-1,3-bischloropropene	5.0															
Bromoforn	5.0															
1,2-Dichloroethane	10															
4-Ethyl-2-pentanone	10															
Tetrachloroethane	5.0	3.0 J	0.0	7.0			6.0 J	6.0 J	10	23	52					
Toluene	5.0															
Chlorobenzene	5.0															
Ethylbenzene	5.0															
Styrene	5.0															
Total Hydrocarbons	5.0															
Quantitation Limit Multiplier	1.2	1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.2	1.1	1.1	1.2	1.3	1.3	1.3	1.2
Date Received by Laboratory	8/10/09	8/10/09	8/10/09	8/10/09	8/10/09	8/10/09	8/10/09	8/10/09	8/10/09	8/10/09	8/10/09	8/10/09	8/11/09	8/11/09	8/11/09	8/11/09
Date of Analysis	8/23/09	8/23/09	8/26/09	8/26/09	8/26/09	8/26/09	8/26/09	8/26/09	8/26/09	8/26/09	8/26/09	8/25/09	8/25/09	8/25/09	8/25/09	8/25/09
Instrument Used for Analysis	7001A	7001A	7001A	7001A	7001A	7001A	7001A	7001A	7001A	7001A	7001A	7001A	7001A	7001A	7001A	7001A

NOTES:

- Compound was not detected
- Quantitation is approximate due to limitations identified during the quality control review (data validation).
- This result is qualitatively suspect since this compound was detected in a field and/or laboratory blank(s) at a similar level.
- Unreliable result - Analyte may or may not be present in this sample.
- This analyte was not detected, but the quantitation limit is probably higher due to a low bias identified during the quality assurance review.

EXTRACTIBLE ORGANIC ANALYSIS			ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS																								page 30																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																			
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Sample Number	Sample Number	Sample Number	Aqueous Quantitation Limit		Solid Quantitation Limit																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																									
			10	330	10	330	CB-128	CB-130	CB-132	CB-133	CB-134	CB-110	CB-278	CB-11C	CB-3A	CB-3B	CB-3C	CB-10A	CB-10B	CB-10C	CB-10D	CB-10E	CB-10F	CB-10G	CB-10H	CB-10I	CB-10J	CB-10K	CB-10L	CB-10M	CB-10N	CB-10O	CB-10P	CB-10Q	CB-10R	CB-10S	CB-10T	CB-10U	CB-10V	CB-10W	CB-10X	CB-10Y	CB-10Z	CB-10AA	CB-10AB	CB-10AC	CB-10AD	CB-10AE	CB-10AF	CB-10AG	CB-10AH	CB-10AI	CB-10AJ	CB-10AK	CB-10AL	CB-10AM	CB-10AN	CB-10AO	CB-10AP	CB-10AQ	CB-10AR	CB-10AS	CB-10AT	CB-10AU	CB-10AV	CB-10AW	CB-10AX	CB-10AY	CB-10AZ	CB-10BA	CB-10BB	CB-10BC	CB-10BD	CB-10BE	CB-10BF	CB-10BG	CB-10BH	CB-10BI	CB-10BJ	CB-10BK	CB-10BL	CB-10BM	CB-10BN	CB-10BO	CB-10BP	CB-10BQ	CB-10BR	CB-10BS	CB-10BT	CB-10BU	CB-10BV	CB-10BW	CB-10BX	CB-10BY	CB-10BZ	CB-10CA	CB-10CB	CB-10CC	CB-10CD	CB-10CE	CB-10CF	CB-10CG	CB-10CH	CB-10CI	CB-10CJ	CB-10CK	CB-10CL	CB-10CM	CB-10CN	CB-10CO	CB-10CP	CB-10CQ	CB-10CR	CB-10CS	CB-10CT	CB-10CU	CB-10CV	CB-10CW	CB-10CX	CB-10CY	CB-10CZ	CB-10DA	CB-10DB	CB-10DC	CB-10DD	CB-10DE	CB-10DF	CB-10DG	CB-10DH	CB-10DI	CB-10DJ	CB-10DK	CB-10DL	CB-10DM	CB-10DN	CB-10DO	CB-10DP	CB-10DQ	CB-10DR	CB-10DS	CB-10DT	CB-10DU	CB-10DV	CB-10DW	CB-10DX	CB-10DY	CB-10DZ	CB-10EA	CB-10EB	CB-10EC	CB-10ED	CB-10EE	CB-10EF	CB-10EG	CB-10EH	CB-10EI	CB-10EJ	CB-10EK	CB-10EL	CB-10EM	CB-10EN	CB-10EO	CB-10EP	CB-10EQ	CB-10ER	CB-10ES	CB-10ET	CB-10EU	CB-10EV	CB-10EW	CB-10EX	CB-10EY	CB-10EZ	CB-10FA	CB-10FB	CB-10FC	CB-10FD	CB-10FE	CB-10FF	CB-10FG	CB-10FH	CB-10FI	CB-10FJ	CB-10FK	CB-10FL	CB-10FM	CB-10FN	CB-10FO	CB-10FP	CB-10FQ	CB-10FR	CB-10FS	CB-10FT	CB-10FU	CB-10FV	CB-10FW	CB-10FX	CB-10FY	CB-10FZ	CB-10GA	CB-10GB	CB-10GC	CB-10GD	CB-10GE	CB-10GF	CB-10GG	CB-10GH	CB-10GI	CB-10GJ	CB-10GK	CB-10GL	CB-10GM	CB-10GN	CB-10GO	CB-10GP	CB-10GQ	CB-10GR	CB-10GS	CB-10GT	CB-10GU	CB-10GV	CB-10GW	CB-10GX	CB-10GY	CB-10GZ	CB-10HA	CB-10HB	CB-10HC	CB-10HD	CB-10HE	CB-10HF	CB-10HG	CB-10HH	CB-10HI	CB-10HJ	CB-10HK	CB-10HL	CB-10HM	CB-10HN	CB-10HO	CB-10HP	CB-10HQ	CB-10HR	CB-10HS	CB-10HT	CB-10HU	CB-10HV	CB-10HW	CB-10HX	CB-10HY	CB-10HZ	CB-10IA	CB-10IB	CB-10IC	CB-10ID	CB-10IE	CB-10IF	CB-10IG	CB-10IH	CB-10II	CB-10IJ	CB-10IK	CB-10IL	CB-10IM	CB-10IN	CB-10IO	CB-10IP	CB-10IQ	CB-10IR	CB-10IS	CB-10IT	CB-10IU	CB-10IV	CB-10IW	CB-10IX	CB-10IY	CB-10IZ	CB-10JA	CB-10JB	CB-10JC	CB-10JD	CB-10JE	CB-10JF	CB-10JG	CB-10JH	CB-10JI	CB-10JJ	CB-10JK	CB-10JL	CB-10JM	CB-10JN	CB-10JO	CB-10JP	CB-10JQ	CB-10JR	CB-10JS	CB-10JT	CB-10JU	CB-10JV	CB-10JW	CB-10JX	CB-10JY	CB-10JZ	CB-10KA	CB-10KB	CB-10KC	CB-10KD	CB-10KE	CB-10KF	CB-10KG	CB-10KH	CB-10KI	CB-10KJ	CB-10KK	CB-10KL	CB-10KM	CB-10KN	CB-10KO	CB-10KP	CB-10KQ	CB-10KR	CB-10KS	CB-10KT	CB-10KU	CB-10KV	CB-10KW	CB-10KX	CB-10KY	CB-10KZ	CB-10LA	CB-10LB	CB-10LC	CB-10LD	CB-10LE	CB-10LF	CB-10LG	CB-10LH	CB-10LI	CB-10LJ	CB-10LK	CB-10LL	CB-10LM	CB-10LN	CB-10LO	CB-10LP	CB-10LQ	CB-10LR	CB-10LS	CB-10LT	CB-10LU	CB-10LV	CB-10LW	CB-10LX	CB-10LY	CB-10LZ	CB-10MA	CB-10MB	CB-10MC	CB-10MD	CB-10ME	CB-10MF	CB-10MG	CB-10MH	CB-10MI	CB-10MJ	CB-10MK	CB-10ML	CB-10MM	CB-10MN	CB-10MO	CB-10MP	CB-10MQ	CB-10MR	CB-10MS	CB-10MT	CB-10MU	CB-10MV	CB-10MW	CB-10MX	CB-10MY	CB-10MZ	CB-10NA	CB-10NB	CB-10NC	CB-10ND	CB-10NE	CB-10NF	CB-10NG	CB-10NH	CB-10NI	CB-10NJ	CB-10NK	CB-10NL	CB-10NM	CB-10NO	CB-10NP	CB-10NQ	CB-10NR	CB-10NS	CB-10NT	CB-10NU	CB-10NV	CB-10NW	CB-10NX	CB-10NY	CB-10NZ	CB-10OA	CB-10OB	CB-10OC	CB-10OD	CB-10OE	CB-10OF	CB-10OG	CB-10OH	CB-10OI	CB-10OJ	CB-10OK	CB-10OL	CB-10OM	CB-10ON	CB-10OO	CB-10OP	CB-10OQ	CB-10OR	CB-10OS	CB-10OT	CB-10OU	CB-10OV	CB-10OW	CB-10OX	CB-10OY	CB-10OZ	CB-10PA	CB-10PB	CB-10PC	CB-10PD	CB-10PE	CB-10PF	CB-10PG	CB-10PH	CB-10PI	CB-10PJ	CB-10PK	CB-10PL	CB-10PM	CB-10PN	CB-10PO	CB-10PP	CB-10PQ	CB-10PR	CB-10PS	CB-10PT	CB-10PU	CB-10PV	CB-10PW	CB-10PX	CB-10PY	CB-10PZ	CB-10QA	CB-10QB	CB-10QC	CB-10QD	CB-10QE	CB-10QF	CB-10QG	CB-10QH	CB-10QI	CB-10QJ	CB-10QK	CB-10QL	CB-10QM	CB-10QN	CB-10QO	CB-10QP	CB-10QQ	CB-10QR	CB-10QS	CB-10QT	CB-10QU	CB-10QV	CB-10QW	CB-10QX	CB-10QY	CB-10QZ	CB-10RA	CB-10RB	CB-10RC	CB-10RD	CB-10RE	CB-10RF	CB-10RG	CB-10RH	CB-10RI	CB-10RJ	CB-10RK	CB-10RL	CB-10RM	CB-10RN	CB-10RO	CB-10RP	CB-10RQ	CB-10RR	CB-10RS	CB-10RT	CB-10RU	CB-10RV	CB-10RW	CB-10RX	CB-10RY	CB-10RZ	CB-10SA	CB-10SB	CB-10SC	CB-10SD	CB-10SE	CB-10SF	CB-10SG	CB-10SH	CB-10SI	CB-10SJ	CB-10SK	CB-10SL	CB-10SM	CB-10SN	CB-10SO	CB-10SP	CB-10SQ	CB-10SR	CB-10SS	CB-10ST	CB-10SU	CB-10SV	CB-10SW	CB-10SX	CB-10SY	CB-10SZ	CB-10TA	CB-10TB	CB-10TC	CB-10TD	CB-10TE	CB-10TF	CB-10TG	CB-10TH	CB-10TI	CB-10TJ	CB-10TK	CB-10TL	CB-10TM	CB-10TN	CB-10TO	CB-10TP	CB-10TQ	CB-10TR	CB-10TS	CB-10TT	CB-10TU	CB-10TV	CB-10TW	CB-10TX	CB-10TY	CB-10TZ	CB-10UA	CB-10UB	CB-10UC	CB-10UD	CB-10UE	CB-10UF	CB-10UG	CB-10UH	CB-10UI	CB-10UJ	CB-10UK	CB-10UL	CB-10UM	CB-10UN	CB-10UO	CB-10UP	CB-10UQ	CB-10UR	CB-10US	CB-10UT	CB-10UU	CB-10UV	CB-10UW	CB-10UX	CB-10UY	CB-10UZ	CB-10VA	CB-10VB	CB-10VC	CB-10VD	CB-10VE	CB-10VF	CB-10VG	CB-10VH	CB-10VI	CB-10VJ	CB-10VK	CB-10VL	CB-10VM	CB-10VN	CB-10VO	CB-10VP	CB-10VQ	CB-10VR	CB-10VS	CB-10VT	CB-10VU	CB-10VV	CB-10VW	CB-10VX	CB-10VY	CB-10VZ	CB-10WA	CB-10WB	CB-10WC	CB-10WD	CB-10WE	CB-10WF	CB-10WG	CB-10WH	CB-10WI	CB-10WJ	CB-10WK	CB-10WL	CB-10WM	CB-10WN	CB-10WO	CB-10WP	CB-10WQ	CB-10WR	CB-10WS	CB-10WT	CB-10WU	CB-10WV	CB-10WW	CB-10WX	CB-10WY	CB-10WZ	CB-10XA	CB-10XB	CB-10XC	CB-10XD	CB-10XE	CB-10XF	CB-10XG	CB-10XH	CB-10XI	CB-10XJ	CB-10XK	CB-10XL	CB-10XM	CB-10XN	CB-10XO	CB-10XP	CB-10XQ	CB-10XR	CB-10XS	CB-10XT	CB-10XU	CB-10XV	CB-10XW	CB-10XX	CB-10XY	CB-10XZ	CB-10YA	CB-10YB	CB-10YC	CB-10YD	CB-10YE	CB-10YF	CB-10YG	CB-10YH	CB-10YI	CB-10YJ	CB-10YK	CB-10YL	CB-10YM	CB-10YN	CB-10YO	CB-10YP	CB-10YQ	CB-10YR	CB-10YS	CB-10YT	CB-10YU	CB-10YV	CB-10YW	CB-10YX	CB-10YY	CB-10YZ	CB-10ZA	CB-10ZB	CB-10ZC	CB-10ZD	CB-10ZE	CB-10ZF	CB-10ZG	CB-10ZH	CB-10ZI	CB-10ZJ	CB-10ZK	CB-10ZL	CB-10ZM	CB-10ZN	CB-10ZO	CB-10ZP	CB-10ZQ	CB-10ZR	CB-10ZS	CB-10ZT	CB-10ZU	CB-10ZV	CB-10ZW	CB-10ZX	CB-10ZY	CB-10ZZ	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10	CB-10

IDENTIFIABLE ORGANIC ANALYSIS			ANALYTICAL RESULTS		ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS															Page 35	
			Quantitation Limit	Solid Limit	CB-130	CB-13C	CB-13D	CB-11A	CB-11B	CB-27B	CB-11C	CB-7A	CB-7B	CB-7C	CB-10A	CB-27A	CB-10B	CB-12A	CB-20A		
					890811A06	890811A07	890811A09	890811A10	890811A11	890811A12	890811A15	890811A16	890811A01	890811A02	890811A03	Duplicate CB-10A	Duplicate CB-12A				
					ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg		
SEMIVOLATILE COMPOUNDS																					
Bisphenol A			10	330	BA	BA	BA	UL	UL	BA	BA						BA				
Bisphenol B			10	330	BA	BA	BA	UL	UL		BA				300 J	73 J	BA				
Bisphenol C			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol D			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol E			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol F			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol G			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol H			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol I			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol J			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol K			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol L			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol M			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol N			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol O			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol P			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol Q			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol R			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol S			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol T			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol U			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol V			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol W			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol X			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol Y			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol Z			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AA			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AB			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AC			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AD			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AE			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AF			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AG			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AH			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AI			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AJ			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AK			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AL			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AM			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AN			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AO			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AP			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AQ			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AR			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AS			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AT			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AU			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AV			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AW			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AX			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AY			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol AZ			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BA			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BB			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BC			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BD			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BE			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BF			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BG			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BH			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BI			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BJ			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BK			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BL			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BM			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BN			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BO			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BP			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BQ			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BR			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BS			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BT			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BU			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BV			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BW			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BX			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BY			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol BZ			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CA			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CB			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CC			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CD			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CE			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CF			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CG			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CH			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CI			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CJ			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CK			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CL			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CM			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CN			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CO			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CP			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CQ			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CR			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CS			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CT			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CU			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CV			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CW			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CX			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CY			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol CZ			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol DA			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol DB			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol DC			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol DD			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol DE			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol DF			10	330	BA	BA	BA	UL	UL		BA						BA				
Bisphenol DG			10	330	BA	BA	BA	UL	UL		BA</										

IDENTIFIABLE ORGANIC ANALYSTS			ANALYTICAL RESULTS			ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS												Page 36	
Microscale Private Sample Number			CB-130			CB-130			CB-130			CB-130			CB-130				
Laboratory Sample Number			890811805			890811805			890811805			890811805			890811805				
As																			
Units			ug/kg			ug/kg			ug/kg			ug/kg			ug/kg				
SEMIVOLATILE COMPOUNDS			Quantitation			Quantitation			Quantitation			Quantitation			Quantitation				
Limit (ug/l) Limit (sol)			Limit (ug/l) Limit (sol)			Limit (ug/l) Limit (sol)			Limit (ug/l) Limit (sol)			Limit (ug/l) Limit (sol)			Limit (ug/l) Limit (sol)				
0.5			0.5			0.5			0.5			0.5			0.5				
Analog-1242			BA			BA			BA			BA			BA				
Quantitation Limit Multiplier			BA			BA			BA			BA			BA				
Date Sample Received			BA			BA			BA			BA			BA				
Date Sample Extracted			BA			BA			BA			BA			BA				
Date of Analysis			BA			BA			BA			BA			BA				

NOTES:

- Compound was not detected
- Quantitation is approximate due to limitations identified during the quality control review (data validation).
- This result is qualitatively suspect since this compound was detected in a field and/or laboratory blank(s) at a similar level.
- Unreliable result - Analyte may or may not be present in this sample.
- This analyte was not detected, but the quantitation limit is probably higher due to a low bias identified during the quality assurance review.

STRUCTURABLE ORGANIC ANALYSIS - ANALYTICAL RESULTS		ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS										-page 60-	
Sample Number	Sample Number	CD-120 #1	Blank #1	CD-200	CD-21A	CD-21B	CD-21C #5	Blank #5	Trig Blank #11	CD-3A			
090011207	090011208	090011207	090011208	090014202	090014203	090014204	090014205	090014207	090014209	090730302			
Sample Number	Sample Number												
Remarks												Analyzed Police	
Units		ug/kg	ug/l	ug/kg	ug/kg	ug/kg	ug/kg	ug/l	ug/l	ug/kg			
SEMIVOLATILE COMPOUNDS													
	Aqueous Limit	Solid Quantitation/ Limit											
Benzochlorocyclopentadiene	10	330	NA	R		NA	NA	UL	NA				
2,4,6-Trichlorophenol	10	330	NA	UL		NA	NA	UL	NA				
2,4,5-Trichlorophenol	50	1650	NA	UL		NA	NA	UL	NA				
2-Chloronaphthalene	10	330	NA	R		NA	NA	UL	NA				
2-Bicroniline	50	1650	NA	R		NA	NA	UL	NA				
Dibenzophthalate	10	330	NA	R		NA	NA	UL	NA				
Acenaphthylene	10	330	NA	R		NA	NA	UL	NA				
5-Tricroniline	50	1650	NA	R		NA	NA	R	NA				
Acenaphthene	10	330	NA	R		NA	NA	UL	NA				
2,4-Dinitrophenol	50	1650	NA	UL		NA	NA	UL	NA				
1-Nitrophenol	50	1650	NA	UL		NA	NA	UL	NA				
Dibenzofuran	10	330	NA	R		NA	NA	UL	NA				
2,4-Dinitrotoluene	10	330	NA	R		NA	NA	UL	NA				
2,6-Dinitrotoluene	10	330	NA	R		NA	NA	UL	NA				
Acetylphthalate	10	330	NA	R		NA	NA	UL	NA				
Chlorophenylphenylether	10	330	NA	R		NA	NA	UL	NA				
Isorene	10	330	NA	R		NA	NA	UL	NA				
Bicroniline	50	1650	NA	R		NA	NA	UL	NA				
6-Dinitro-2-nitrophenol	50	1650	NA	UL		NA	NA	UL	NA				
Dibenzodiphenylamine	10	330	NA	R		NA	NA	UL	NA				
Nonophenylphenylether	10	330	NA	R		NA	NA	UL	NA				
enachlorobenzene	10	330	NA	R		NA	NA	UL	NA				900/-
enachlorophenol	50	1650	NA	UL		NA	NA	UL	NA				
enanthrene	10	330	NA	R		NA	NA	UL	NA				

INSTRUMENT LOG/ANALYSIS			ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS										PAGE 62	
ANALYTICAL RESULTS			CB-120	Residue	CB-200	CB-21A	CB-21B	CB-21C	Residue	Trip Blank	CB-2A			
Alcain Pirnie Sample Number			44	44				PS	45	417				
Laboratory Sample Number			89081807	89081808	890814201	890814203	890814204	890814205	890814207	890814208	890726202			
Results														
Site			ug/kg	ug/l	ug/kg	ug/kg	ug/kg	ug/kg	ug/l	ug/l	ug/kg			
CBs														
recler-126C			BA	BA			BA	510	BA	BA	500			
Quantitation Limit Multiplier			BA	BA	1.125	1.06	BA		BA	BA				
ate Sample Received			BA	BA	8/14/89	8/14/89	BA	8/14/89	BA	BA	7/28/89			
ate sample extracted			BA	BA	8/16/89	8/16/89	BA	8/16/89	BA	BA	8/1/89			
ate of analysis			BA	BA	9/3/89	9/3/89	BA	9/3/89	BA	BA	9/1/89			

80785: Compound was not detected.

- J Quantitation is approximate due to limitations identified during the quality control review (data validation).
- K This result is qualitatively suspect since this compound was detected in a field and/or laboratory blank(s) at a similar level.
- N Reliable result - Analyte may or may not be present in this sample.
- OL This analyte was not detected, but the quantitation limit is probably higher due to a low bias identified during the quality assurance review.

[illegible]

3. Compound was not detected
4. Quantitation is approximate due to limitations identified during the
5. quality control review (data validation).
6. This result is qualitatively suspect since this compound was detected
7. in a field and/or laboratory blank(s) at a similar level.
8. Unreliable result - Analyte may or may not be present in this sample.
9. This analyte was not detected, but the quantitation limit is probably
10. higher due to a low bias identified during the quality assurance review.

INTERFERENCES ORGANIC ANALYSIS		ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS										ANALYTICAL RESULTS										page 5																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																															
		CO-5A 090727001	CO-5B 090727002	CO-5C 090727003	CO-5D 090727004	CO-5E 090727005	CO-5F 090727006	CO-5G 090727007	CO-5H 090727008	CO-5I 090727009	CO-5J 090727010	CO-5K 090727011	CO-5L 090727012	CO-5M 090727013	CO-5N 090727014	CO-5O 090727015	CO-5P 090727016	CO-5Q 090727017	CO-5R 090727018	CO-5S 090727019	CO-5T 090727020	CO-5U 090727021	CO-5V 090727022	CO-5W 090727023	CO-5X 090727024	CO-5Y 090727025	CO-5Z 090727026	CO-5AA 090727027	CO-5AB 090727028	CO-5AC 090727029	CO-5AD 090727030	CO-5AE 090727031	CO-5AF 090727032	CO-5AG 090727033	CO-5AH 090727034	CO-5AI 090727035	CO-5AJ 090727036	CO-5AK 090727037	CO-5AL 090727038	CO-5AM 090727039	CO-5AN 090727040	CO-5AO 090727041	CO-5AP 090727042	CO-5AQ 090727043	CO-5AR 090727044	CO-5AS 090727045	CO-5AT 090727046	CO-5AU 090727047	CO-5AV 090727048	CO-5AW 090727049	CO-5AX 090727050	CO-5AY 090727051	CO-5AZ 090727052	CO-5BA 090727053	CO-5BB 090727054	CO-5BC 090727055	CO-5BD 090727056	CO-5BE 090727057	CO-5BF 090727058	CO-5BG 090727059	CO-5BH 090727060	CO-5BI 090727061	CO-5BJ 090727062	CO-5BK 090727063	CO-5BL 090727064	CO-5BM 090727065	CO-5BN 090727066	CO-5BO 090727067	CO-5BP 090727068	CO-5BQ 090727069	CO-5BR 090727070	CO-5BS 090727071	CO-5BT 090727072	CO-5BU 090727073	CO-5BV 090727074	CO-5BW 090727075	CO-5BX 090727076	CO-5BY 090727077	CO-5BZ 090727078	CO-5CA 090727079	CO-5CB 090727080	CO-5CC 090727081	CO-5CD 090727082	CO-5CE 090727083	CO-5CF 090727084	CO-5CG 090727085	CO-5CH 090727086	CO-5CI 090727087	CO-5CJ 090727088	CO-5CK 090727089	CO-5CL 090727090	CO-5CM 090727091	CO-5CN 090727092	CO-5CO 090727093	CO-5CP 090727094	CO-5CQ 090727095	CO-5CR 090727096	CO-5CS 090727097	CO-5CT 090727098	CO-5CU 090727099	CO-5CV 090727100	CO-5CW 090727101	CO-5CX 090727102	CO-5CY 090727103	CO-5CZ 090727104	CO-5DA 090727105	CO-5DB 090727106	CO-5DC 090727107	CO-5DD 090727108	CO-5DE 090727109	CO-5DF 090727110	CO-5DG 090727111	CO-5DH 090727112	CO-5DI 090727113	CO-5DJ 090727114	CO-5DK 090727115	CO-5DL 090727116	CO-5DM 090727117	CO-5DN 090727118	CO-5DO 090727119	CO-5DP 090727120	CO-5DQ 090727121	CO-5DR 090727122	CO-5DS 090727123	CO-5DT 090727124	CO-5DU 090727125	CO-5DV 090727126	CO-5DW 090727127	CO-5DX 090727128	CO-5DY 090727129	CO-5DZ 090727130	CO-5EA 090727131	CO-5EB 090727132	CO-5EC 090727133	CO-5ED 090727134	CO-5EE 090727135	CO-5EF 090727136	CO-5EG 090727137	CO-5EH 090727138	CO-5EI 090727139	CO-5EJ 090727140	CO-5EK 090727141	CO-5EL 090727142	CO-5EM 090727143	CO-5EN 090727144	CO-5EO 090727145	CO-5EP 090727146	CO-5EQ 090727147	CO-5ER 090727148	CO-5ES 090727149	CO-5ET 090727150	CO-5EU 090727151	CO-5EV 090727152	CO-5EW 090727153	CO-5EX 090727154	CO-5EY 090727155	CO-5EZ 090727156	CO-5FA 090727157	CO-5FB 090727158	CO-5FC 090727159	CO-5FD 090727160	CO-5FE 090727161	CO-5FF 090727162	CO-5FG 090727163	CO-5FH 090727164	CO-5FI 090727165	CO-5FJ 090727166	CO-5FK 090727167	CO-5FL 090727168	CO-5FM 090727169	CO-5FN 090727170	CO-5FO 090727171	CO-5FP 090727172	CO-5FQ 090727173	CO-5FR 090727174	CO-5FS 090727175	CO-5FT 090727176	CO-5FU 090727177	CO-5FV 090727178	CO-5FW 090727179	CO-5FX 090727180	CO-5FY 090727181	CO-5FZ 090727182	CO-5GA 090727183	CO-5GB 090727184	CO-5GC 090727185	CO-5GD 090727186	CO-5GE 090727187	CO-5GF 090727188	CO-5GG 090727189	CO-5GH 090727190	CO-5GI 090727191	CO-5GJ 090727192	CO-5GK 090727193	CO-5GL 090727194	CO-5GM 090727195	CO-5GN 090727196	CO-5GO 090727197	CO-5GP 090727198	CO-5GQ 090727199	CO-5GR 090727200	CO-5GS 090727201	CO-5GT 090727202	CO-5GU 090727203	CO-5GV 090727204	CO-5GW 090727205	CO-5GX 090727206	CO-5GY 090727207	CO-5GZ 090727208	CO-5HA 090727209	CO-5HB 090727210	CO-5HC 090727211	CO-5HD 090727212	CO-5HE 090727213	CO-5HF 090727214	CO-5HG 090727215	CO-5HH 090727216	CO-5HI 090727217	CO-5HJ 090727218	CO-5HK 090727219	CO-5HL 090727220	CO-5HM 090727221	CO-5HN 090727222	CO-5HO 090727223	CO-5HP 090727224	CO-5HQ 090727225	CO-5HR 090727226	CO-5HS 090727227	CO-5HT 090727228	CO-5HU 090727229	CO-5HV 090727230	CO-5HW 090727231	CO-5HX 090727232	CO-5HY 090727233	CO-5HZ 090727234	CO-5IA 090727235	CO-5IB 090727236	CO-5IC 090727237	CO-5ID 090727238	CO-5IE 090727239	CO-5IF 090727240	CO-5IG 090727241	CO-5IH 090727242	CO-5II 090727243	CO-5IJ 090727244	CO-5IK 090727245	CO-5IL 090727246	CO-5IM 090727247	CO-5IN 090727248	CO-5IO 090727249	CO-5IP 090727250	CO-5IQ 090727251	CO-5IR 090727252	CO-5IS 090727253	CO-5IT 090727254	CO-5IU 090727255	CO-5IV 090727256	CO-5IW 090727257	CO-5IX 090727258	CO-5IY 090727259	CO-5IZ 090727260	CO-5JA 090727261	CO-5JB 090727262	CO-5JC 090727263	CO-5JD 090727264	CO-5JE 090727265	CO-5JF 090727266	CO-5JG 090727267	CO-5JH 090727268	CO-5JI 090727269	CO-5JJ 090727270	CO-5JK 090727271	CO-5JL 090727272	CO-5JM 090727273	CO-5JN 090727274	CO-5JO 090727275	CO-5JP 090727276	CO-5JQ 090727277	CO-5JR 090727278	CO-5JS 090727279	CO-5JT 090727280	CO-5JU 090727281	CO-5JV 090727282	CO-5JW 090727283	CO-5JX 090727284	CO-5JY 090727285	CO-5JZ 090727286	CO-5KA 090727287	CO-5KB 090727288	CO-5KC 090727289	CO-5KD 090727290	CO-5KE 090727291	CO-5KF 090727292	CO-5KG 090727293	CO-5KH 090727294	CO-5KI 090727295	CO-5KJ 090727296	CO-5KK 090727297	CO-5KL 090727298	CO-5KM 090727299	CO-5KN 090727300	CO-5KO 090727301	CO-5KP 090727302	CO-5KQ 090727303	CO-5KR 090727304	CO-5KS 090727305	CO-5KT 090727306	CO-5KU 090727307	CO-5KV 090727308	CO-5KW 090727309	CO-5KX 090727310	CO-5KY 090727311	CO-5KZ 090727312	CO-5LA 090727313	CO-5LB 090727314	CO-5LC 090727315	CO-5LD 090727316	CO-5LE 090727317	CO-5LF 090727318	CO-5LG 090727319	CO-5LH 090727320	CO-5LI 090727321	CO-5LJ 090727322	CO-5LK 090727323	CO-5LL 090727324	CO-5LM 090727325	CO-5LN 090727326	CO-5LO 090727327	CO-5LP 090727328	CO-5LQ 090727329	CO-5LR 090727330	CO-5LS 090727331	CO-5LT 090727332	CO-5LU 090727333	CO-5LV 090727334	CO-5LW 090727335	CO-5LX 090727336	CO-5LY 090727337	CO-5LZ 090727338	CO-5MA 090727339	CO-5MB 090727340	CO-5MC 090727341	CO-5MD 090727342	CO-5ME 090727343	CO-5MF 090727344	CO-5MG 090727345	CO-5MH 090727346	CO-5MI 090727347	CO-5MJ 090727348	CO-5MK 090727349	CO-5ML 090727350	CO-5MN 090727351	CO-5MO 090727352	CO-5MP 090727353	CO-5MQ 090727354	CO-5MR 090727355	CO-5MS 090727356	CO-5MT 090727357	CO-5MU 090727358	CO-5MV 090727359	CO-5MW 090727360	CO-5MX 090727361	CO-5MY 090727362	CO-5MZ 090727363	CO-5NA 090727364	CO-5NB 090727365	CO-5NC 090727366	CO-5ND 090727367	CO-5NE 090727368	CO-5NF 090727369	CO-5NG 090727370	CO-5NH 090727371	CO-5NI 090727372	CO-5NJ 090727373	CO-5NK 090727374	CO-5NL 090727375	CO-5NM 090727376	CO-5NO 090727377	CO-5NP 090727378	CO-5NQ 090727379	CO-5NR 090727380	CO-5NS 090727381	CO-5NT 090727382	CO-5NU 090727383	CO-5NV 090727384	CO-5NW 090727385	CO-5NX 090727386	CO-5NY 090727387	CO-5NZ 090727388	CO-5OA 090727389	CO-5OB 090727390	CO-5OC 090727391	CO-5OD 090727392	CO-5OE 090727393	CO-5OF 090727394	CO-5OG 090727395	CO-5OH 090727396	CO-5OI 090727397	CO-5OJ 090727398	CO-5OK 090727399	CO-5OL 090727400	CO-5OM 090727401	CO-5ON 090727402	CO-5OO 090727403	CO-5OP 090727404	CO-5OQ 090727405	CO-5OR 090727406	CO-5OS 090727407	CO-5OT 090727408	CO-5OU 090727409	CO-5OV 090727410	CO-5OW 090727411	CO-5OX 090727412	CO-5OY 090727413	CO-5OZ 090727414	CO-5PA 090727415	CO-5PB 090727416	CO-5PC 090727417	CO-5PD 090727418	CO-5PE 090727419	CO-5PF 090727420	CO-5PG 090727421	CO-5PH 090727422	CO-5PI 090727423	CO-5PJ 090727424	CO-5PK 090727425	CO-5PL 090727426	CO-5PM 090727427	CO-5PN 090727428	CO-5PO 090727429	CO-5PP 090727430	CO-5PQ 090727431	CO-5PR 090727432	CO-5PS 090727433	CO-5PT 090727434	CO-5PU 090727435	CO-5PV 090727436	CO-5PW 090727437	CO-5PX 090727438	CO-5PY 090727439	CO-5PZ 090727440	CO-5QA 090727441	CO-5QB 090727442	CO-5QC 090727443	CO-5QD 090727444	CO-5QE 090727445	CO-5QF 090727446	CO-5QG 090727447	CO-5QH 090727448	CO-5QI 090727449	CO-5QJ 090727450	CO-5QK 090727451	CO-5QL 090727452	CO-5QM 090727453	CO-5QN 090727454	CO-5QO 090727455	CO-5QP 090727456	CO-5QQ 090727457	CO-5QR 090727458	CO-5QS 090727459	CO-5QT 090727460	CO-5QU 090727461	CO-5QV 090727462	CO-5QW 090727463	CO-5QX 090727464	CO-5QY 090727465	CO-5QZ 090727466	CO-5RA 090727467	CO-5RB 090727468	CO-5RC 090727469	CO-5RD 090727470	CO-5RE 090727471	CO-5RF 090727472	CO-5RG 090727473	CO-5RH 090727474	CO-5RI 090727475	CO-5RJ 090727476	CO-5RK 090727477	CO-5RL 090727478	CO-5RM 090727479	CO-5RN 090727480	CO-5RO 090727481	CO-5RP 090727482	CO-5RQ 090727483	CO-5RR 090727484	CO-5RS 090727485	CO-5RT 090727486	CO-5RU 090727487	CO-5RV 090727488	CO-5RW 090727489	CO-5RX 090727490	CO-5RY 090727491	CO-5RZ 090727492	CO-5SA 090727493	CO-5SB 090727494	CO-5SC 090727495	CO-5SD 090727496	CO-5SE 090727497	CO-5SF 090727498	CO-5SG 090727499	CO-5SH 090727500	CO-5SI 090727501	CO-5SJ 090727502	CO-5SK 090727503	CO-5SL 090727504	CO-5SM 090727505	CO-5SN 090727506	CO-5SO 090727507	CO-5SP 090727508	CO-5SQ 090727509	CO-5SR 090727510	CO-5SS 090727511	CO-5ST 090727512	CO-5SU 090727513	CO-5SV 090727514	CO-5SW 090727515	CO-5SX 090727516	CO-5SY 090727517	CO-5SZ 090727518	CO-5TA 090727519	CO-5TB 090727520	CO-5TC 090727521	CO-5TD 090727522	CO-5TE 090727523	CO-5TF 090727524	CO-5TG 090727525	CO-5TH 090727526	CO-5TI 090727527	CO-5TJ 090727528	CO-5TK 090727529	CO-5TL 090727530	CO-5TM 090727531	CO-5TN 090727532	CO-5TO 090727533	CO-5TP 090727534	CO-5TQ 090727535	CO-5TR 090727536	CO-5TS 090727537	CO-5TT 090727538	CO-5TU 090727539	CO-5TV 090727540	CO-5TW 090727541	CO-5TX 090727542	CO-5TY 090727543	CO-5TZ 090727544	CO-5UA 090727545	CO-5UB 090727546	CO-5UC 090727547	CO-5UD 090727548	CO-5UE 090727549	CO-5UF 090727550	CO-5UG 090727551	CO-5UH 090727552	CO-5UI 090727553	CO-5UJ 090727554	CO-5UK 090727555	CO-5UL 090727556	CO-5UM 090727557	CO-5UN 090727558	CO-5UO 090727559	CO-5UP 090727560	CO-5UQ 090727561	CO-5UR 090727562	CO-5US 090727563	CO-5UT 090727564	CO-5UU 090727565	CO-5UV 090727566	CO-5UW 090727567	CO-5UX 090727568	CO-5UY 090727569	CO-5UZ 090727570	CO-5VA 090727571	CO-5VB 090727572	CO-5VC 090727573	CO-5VD 090727574	CO-5VE 090727575	CO-5VF 090727576	CO-5VG 090727577	CO-5VH 090727578	CO-5VI 090727579	CO-5VJ 090727580	CO-5VK 090727581	CO-5VL 090727582	CO-5VM 090727583	CO-5VN 090727584	CO-5VO 090727585	CO-5VP 090727586	CO-5VQ 090727587	CO-5VR 090727588	CO-5VS 090727589	CO-5VT 090727590	CO-5VU 090727591	CO-5VV 090727592	CO-5VW 090727593	CO-5VX 090727594	CO-5VY 090727595	CO-5VZ 090727596	CO-5WA 090727597	CO-5WB 090727598	CO-5WC 090727599	CO-5WD 090727600	CO-5WE 090727601	CO-5WF 090727602	CO-5WG 090727603	CO-5WH 090727604	CO-5WI 090727605	CO-5WJ 090727606	CO-5WK 090727607	CO-5WL 090727608	CO-5WM 090727609	CO-5WN 090727610	CO-5WO 090727611	CO-5WP 0907276

EXTRACTABLE ORGANIC ANALYSIS - ANALYTICAL RESULTS		ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS												page 6	
		CB-3A	CB-3B	CB-3C	CB-3D	CB-3E	CB-3F	CB-3G	CB-3H	CB-3I	CB-3J	CB-3K	CB-3L	CB-3M	CB-3N
Balsam Pine Sample Number		090727001	090727002	090727003	090727004	090727005	090727006	090727007	090727008	090727009	090727010	090727011	090727012	090727013	090727014
Laboratory Sample Number															
No															
Solids		mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg
SEMIVOLATILE COMPOUNDS															
Quantitation/Blank															
Limit															
Detector-1242		0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
Quantitation Limit Multiplier		1.125	1.125	1.125	1.125	1.125	1.125	1.125	1.125	1.125	1.125	1.125	1.125	1.125	1.125
Data Sample Received		7/27/09	7/27/09	7/27/09	7/27/09	7/27/09	7/27/09	7/27/09	7/27/09	7/27/09	7/27/09	7/27/09	7/27/09	7/27/09	7/27/09
Data Sample Extracted		8/1/09	8/1/09	8/1/09	8/1/09	8/1/09	8/1/09	8/1/09	8/1/09	8/1/09	8/1/09	8/1/09	8/1/09	8/1/09	8/1/09
Date of Analysis		9/1/09	9/1/09	9/1/09	9/1/09	9/1/09	9/1/09	9/1/09	9/1/09	9/1/09	9/1/09	9/1/09	9/1/09	9/1/09	9/1/09

NOTE: - Compound was not detected.
 1 Quantitation is approximate due to limitations identified during the quality control review (data validation).
 2 This result is qualitatively suspect since this compound was detected in a field and/or laboratory blank(s) at a similar level.
 3 Unreliable result - Analyte may or may not be present in this sample.
 4 This analyte was not detected, but the quantitation limit is probably higher due to a low bias identified during the quality assurance review.

ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS

ANALYTICAL RESULTS

INOLUBLE ORGANIC ANALYSIS

Sample Number	CB-2C 090001203	CB-2B 090001204	CB-23B 090001205	CB-23C 090001206	CB-23D 090001207	Trip Blank 090001210	CB-4A 090003001	CB-25A 090003002	CB-25B 090003003	CB-4C 090003005	CB-26A 090003006	CB-26B 090003007
Sample	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/l	mg/kg	mg/kg	mg/l	mg/kg	mg/kg	mg/kg
Quantification Limit												
Chloroethane	10											
Bromoethane	10											
Methyl Chloride	10											
Chloroethane	10											
Methylene Chloride	5.0	7.00	6.00	3.00	3.00	4.00	6.00	3.00	2.00	6.00	6.00	6.00
Acetone	10	1600	400	7.00	250	300	120	950	600	970	500	300
Carbon Disulfide	5.0											
1,1-Dichloroethane	5.0											
1,1-Dichloroethane	5.0											
1,1,2-Dichloroethane	5.0				6.0					2.00		
Chloroform	5.0	3.00	2.00	1.00	1.00	1.00	1.00		2.00	1.00	2.00	2.00
1,2-Dichloroethane	5.0											
2-Butanone	10	R	R							R		
1,1,1-Trichloroethane	5.0		3.00							2.00		
Carbon Tetrachloride	5.0											
Methyl Acetate	10											
Bromochloroethane	5.0											
1,1,2,2-Tetrachloroethane	5.0											
1,2-Dichloropropane	5.0											
trans-1,2-Dichloropropene	5.0											
Trichloroethene	5.0			4.00						5.00		
Dibromochloroethane	5.0											
1-Trichloroethane	5.0											
Benzene	5.0								BL			

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NOTES.

- Continued on previous page

quantitation is appropriate due to limitations identified during the quality control review (data validation).

3 this result is qualitatively suspect since this compound was detected in a field and/or laboratory blank(s) at a stellar level.

Unreliable result - Analyte may or may not be present in this sample. This analyte was not detected, but the quantitation limit is probably

EXTRACTABLE ORGANIC ANALYSIS			ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS												ANALYTICAL RESULTS			PAGE 10								
Labcode	Sample Number	Laboratory Sample Number	CB-2C		CB-10		CB-23A		CB-23B		CB-23C		CB-23D		Trip Blank		CB-6A		CB-6C		CB-20A		CB-20B		CB-20C	
			090001203		090001204		090001205		090001206		090001207		090001209		090001210		090001201		090001204		090001207		090001210			
Solids																	Duplicate									
Solids																	CB-6A									
EXTRACTABLE COMPOUNDS			aq/kg		aq/kg		aq/kg		aq/kg		aq/kg		aq/kg		aq/l		aq/kg		aq/kg		aq/l		aq/kg		aq/kg	
			Aqueous		Solid		Quantitation		Limit																	
methylcyclopentadiene			10		330										NA											
,4,6-Trichlorophenol			10		330										NA											
,4,5-Trichlorophenol			10		330										NA											
Chloronaphthalene			10		330										NA											
-Dibenzofuran			10		330										NA											
Isobutylphthalate			10		330										NA											
cyclopentadiene			10		330										NA											
-Dibenzofuran			10		330										NA											
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STRUCTURAL ORGANIC ANALYSIS			ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS												Page 10
ANALYTICAL RESULTS			CO-200	Blanco 01	CO-220	Wet Blank 01	CO-220	Wet Blank 01	CO-220	CO-100	Wet Blank 01	CO-100	Wet Blank 01	CO-100	CO-200
Sample Number			090031011	090031001	090031002	090031003	090031004	090031005	090031006	090031007	090031008	090031009	090031010	090031011	090031012
Laboratory Sample Number															
Date															
Notes															
PCBs															
Aqueous															
Solid															
Quantification Limit															
Limit															
Sample-2202			NA	1.0	1.06	NA	NA	NA	NA	1.06	1.125	NA	1.125	1.25	
Quantification Limit Multiplier															
Data Sample Received			NA	8/3/09	8/3/09	NA	NA	NA	NA	8/4/09	8/4/09	NA	8/8/09	8/9/09	
Data Sample Extracted			NA	8/6/09	8/10/09	NA	NA	NA	NA	8/10/09	8/10/09	NA	8/10/09	8/16/09	
Date of Analysis			NA	9/2/09	9/2/09	NA	NA	NA	NA	9/2/09	9/2/09	NA	9/3/09	9/3/09	

NOTES:

- 1. Compound was not detected
- 2. Quantification is approximate due to limitations identified during the quality control review (data validation).
- 3. This result is qualitatively suspect since this compound was detected in a field and/or laboratory blank(s) at a similar level.
- 4. Parallel results - Analyte may or may not be present in this sample.
- 5. This analyte was not detected, but the quantification limit is probably higher due to a low bias identified during the quality assurance review.

VOLATILE ORGANIC ANALYSIS - ANALYTICAL RESULTS										ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS												page 10																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																													
		CB-240	1741p Blank	CB-1A	CB-1B	CB-250	CB-1C	CB-1D	CB-1E	CB-1F	CB-1G	CB-1H	CB-1I	CB-1J	CB-1K	CB-1L	CB-1M	CB-1N	CB-1O	CB-1P	CB-1Q	CB-1R	CB-1S	CB-1T	CB-1U	CB-1V	CB-1W	CB-1X	CB-1Y	CB-1Z	CB-1AA	CB-1AB	CB-1AC	CB-1AD	CB-1AE	CB-1AF	CB-1AG	CB-1AH	CB-1AI	CB-1AJ	CB-1AK	CB-1AL	CB-1AM	CB-1AN	CB-1AO	CB-1AP	CB-1AQ	CB-1AR	CB-1AS	CB-1AT	CB-1AU	CB-1AV	CB-1AW	CB-1AX	CB-1AY	CB-1AZ	CB-1BA	CB-1BB	CB-1BC	CB-1BD	CB-1BE	CB-1BF	CB-1BG	CB-1BH	CB-1BI	CB-1BJ	CB-1BK	CB-1BL	CB-1BM	CB-1BN	CB-1BO	CB-1BP	CB-1BQ	CB-1BR	CB-1BS	CB-1BT	CB-1BU	CB-1BV	CB-1BW	CB-1BX	CB-1BY	CB-1BZ	CB-1CA	CB-1CB	CB-1CC	CB-1CD	CB-1CE	CB-1CF	CB-1CG	CB-1CH	CB-1CI	CB-1CJ	CB-1CK	CB-1CL	CB-1CM	CB-1CN	CB-1CO	CB-1CP	CB-1CQ	CB-1CR	CB-1CS	CB-1CT	CB-1CU	CB-1CV	CB-1CW	CB-1CX	CB-1CY	CB-1CZ	CB-1DA	CB-1DB	CB-1DC	CB-1DD	CB-1DE	CB-1DF	CB-1DG	CB-1DH	CB-1DI	CB-1DJ	CB-1DK	CB-1DL	CB-1DM	CB-1DN	CB-1DO	CB-1DP	CB-1DQ	CB-1DR	CB-1DS	CB-1DT	CB-1DU	CB-1DV	CB-1DW	CB-1DX	CB-1DY	CB-1DZ	CB-1EA	CB-1EB	CB-1EC	CB-1ED	CB-1EE	CB-1EF	CB-1EG	CB-1EH	CB-1EI	CB-1EJ	CB-1EK	CB-1EL	CB-1EM	CB-1EN	CB-1EO	CB-1EP	CB-1EQ	CB-1ER	CB-1ES	CB-1ET	CB-1EU	CB-1EV	CB-1EW	CB-1EX	CB-1EY	CB-1EZ	CB-1FA	CB-1FB	CB-1FC	CB-1FD	CB-1FE	CB-1FF	CB-1FG	CB-1FH	CB-1FI	CB-1FJ	CB-1FK	CB-1FL	CB-1FM	CB-1FN	CB-1FO	CB-1FP	CB-1FQ	CB-1FR	CB-1FS	CB-1FT	CB-1FU	CB-1FV	CB-1FW	CB-1FX	CB-1FY	CB-1FZ	CB-1GA	CB-1GB	CB-1GC	CB-1GD	CB-1GE	CB-1GF	CB-1GG	CB-1GH	CB-1GI	CB-1GJ	CB-1GK	CB-1GL	CB-1GM	CB-1GN	CB-1GO	CB-1GP	CB-1GQ	CB-1GR	CB-1GS	CB-1GT	CB-1GU	CB-1GV	CB-1GW	CB-1GX	CB-1GY	CB-1GZ	CB-1HA	CB-1HB	CB-1HC	CB-1HD	CB-1HE	CB-1HF	CB-1HG	CB-1HH	CB-1HI	CB-1HJ	CB-1HK	CB-1HL	CB-1HM	CB-1HN	CB-1HO	CB-1HP	CB-1HQ	CB-1HR	CB-1HS	CB-1HT	CB-1HU	CB-1HV	CB-1HW	CB-1HX	CB-1HY	CB-1HZ	CB-1IA	CB-1IB	CB-1IC	CB-1ID	CB-1IE	CB-1IF	CB-1IG	CB-1IH	CB-1II	CB-1IJ	CB-1IK	CB-1IL	CB-1IM	CB-1IN	CB-1IO	CB-1IP	CB-1IQ	CB-1IR	CB-1IS	CB-1IT	CB-1IU	CB-1IV	CB-1IW	CB-1IX	CB-1IY	CB-1IZ	CB-1JA	CB-1JB	CB-1JC	CB-1JD	CB-1JE	CB-1JF	CB-1JG	CB-1JH	CB-1JI	CB-1JJ	CB-1JK	CB-1JL	CB-1JM	CB-1JN	CB-1JO	CB-1JP	CB-1JQ	CB-1JR	CB-1JS	CB-1JT	CB-1JU	CB-1JV	CB-1JW	CB-1JX	CB-1JY	CB-1JZ	CB-1KA	CB-1KB	CB-1KC	CB-1KD	CB-1KE	CB-1KF	CB-1KG	CB-1KH	CB-1KI	CB-1KJ	CB-1KK	CB-1KL	CB-1KM	CB-1KN	CB-1KO	CB-1KP	CB-1KQ	CB-1KR	CB-1KS	CB-1KT	CB-1KU	CB-1KV	CB-1KW	CB-1KX	CB-1KY	CB-1KZ	CB-1LA	CB-1LB	CB-1LC	CB-1LD	CB-1LE	CB-1LF	CB-1LG	CB-1LH	CB-1LI	CB-1LJ	CB-1LK	CB-1LL	CB-1LM	CB-1LN	CB-1LO	CB-1LP	CB-1LQ	CB-1LR	CB-1LS	CB-1LT	CB-1LU	CB-1LV	CB-1LW	CB-1LX	CB-1LY	CB-1LZ	CB-1MA	CB-1MB	CB-1MC	CB-1MD	CB-1ME	CB-1MF	CB-1MG	CB-1MH	CB-1MI	CB-1MJ	CB-1MK	CB-1ML	CB-1MM	CB-1MN	CB-1MO	CB-1MP	CB-1MQ	CB-1MR	CB-1MS	CB-1MT	CB-1MU	CB-1MV	CB-1MW	CB-1MX	CB-1MY	CB-1MZ	CB-1NA	CB-1NB	CB-1NC	CB-1ND	CB-1NE	CB-1NF	CB-1NG	CB-1NH	CB-1NI	CB-1NJ	CB-1NK	CB-1NL	CB-1NM	CB-1NO	CB-1NP	CB-1NQ	CB-1NR	CB-1NS	CB-1NT	CB-1NU	CB-1NV	CB-1NW	CB-1NX	CB-1NY	CB-1NZ	CB-1OA	CB-1OB	CB-1OC	CB-1OD	CB-1OE	CB-1OF	CB-1OG	CB-1OH	CB-1OI	CB-1OJ	CB-1OK	CB-1OL	CB-1OM	CB-1ON	CB-1OO	CB-1OP	CB-1OQ	CB-1OR	CB-1OS	CB-1OT	CB-1OU	CB-1OV	CB-1OW	CB-1OX	CB-1OY	CB-1OZ	CB-1PA	CB-1PB	CB-1PC	CB-1PD	CB-1PE	CB-1PF	CB-1PG	CB-1PH	CB-1PI	CB-1PJ	CB-1PK	CB-1PL	CB-1PM	CB-1PN	CB-1PO	CB-1PP	CB-1PQ	CB-1PR	CB-1PS	CB-1PT	CB-1PU	CB-1PV	CB-1PW	CB-1PX	CB-1PY	CB-1PZ	CB-1QA	CB-1QB	CB-1QC	CB-1QD	CB-1QE	CB-1QF	CB-1QG	CB-1QH	CB-1QI	CB-1QJ	CB-1QK	CB-1QL	CB-1QM	CB-1QN	CB-1QO	CB-1QP	CB-1QQ	CB-1QR	CB-1QS	CB-1QT	CB-1QU	CB-1QV	CB-1QW	CB-1QX	CB-1QY	CB-1QZ	CB-1RA	CB-1RB	CB-1RC	CB-1RD	CB-1RE	CB-1RF	CB-1RG	CB-1RH	CB-1RI	CB-1RJ	CB-1RK	CB-1RL	CB-1RM	CB-1RN	CB-1RO	CB-1RP	CB-1RQ	CB-1RR	CB-1RS	CB-1RT	CB-1RU	CB-1RV	CB-1RW	CB-1RX	CB-1RY	CB-1RZ	CB-1SA	CB-1SB	CB-1SC	CB-1SD	CB-1SE	CB-1SF	CB-1SG	CB-1SH	CB-1SI	CB-1SJ	CB-1SK	CB-1SL	CB-1SM	CB-1SN	CB-1SO	CB-1SP	CB-1SQ	CB-1SR	CB-1SS	CB-1ST	CB-1SU	CB-1SV	CB-1SW	CB-1SX	CB-1SY	CB-1SZ	CB-1TA	CB-1TB	CB-1TC	CB-1TD	CB-1TE	CB-1TF	CB-1TG	CB-1TH	CB-1TI	CB-1TJ	CB-1TK	CB-1TL	CB-1TM	CB-1TN	CB-1TO	CB-1TP	CB-1TQ	CB-1TR	CB-1TS	CB-1TT	CB-1TU	CB-1TV	CB-1TW	CB-1TX	CB-1TY	CB-1TZ	CB-1UA	CB-1UB	CB-1UC	CB-1UD	CB-1UE	CB-1UF	CB-1UG	CB-1UH	CB-1UI	CB-1UJ	CB-1UK	CB-1UL	CB-1UM	CB-1UN	CB-1UO	CB-1UP	CB-1UQ	CB-1UR	CB-1US	CB-1UT	CB-1UU	CB-1UV	CB-1UW	CB-1UX	CB-1UY	CB-1UZ	CB-1VA	CB-1VB	CB-1VC	CB-1VD	CB-1VE	CB-1VF	CB-1VG	CB-1VH	CB-1VI	CB-1VJ	CB-1VK	CB-1VL	CB-1VM	CB-1VN	CB-1VO	CB-1VP	CB-1VQ	CB-1VR	CB-1VS	CB-1VT	CB-1VU	CB-1VV	CB-1VW	CB-1VX	CB-1VY	CB-1VZ	CB-1WA	CB-1WB	CB-1WC	CB-1WD	CB-1WE	CB-1WF	CB-1WG	CB-1WH	CB-1WI	CB-1WJ	CB-1WK	CB-1WL	CB-1WM	CB-1WN	CB-1WO	CB-1WP	CB-1WQ	CB-1WR	CB-1WS	CB-1WT	CB-1WU	CB-1WV	CB-1WW	CB-1WX	CB-1WY	CB-1WZ	CB-1XA	CB-1XB	CB-1XC	CB-1XD	CB-1XE	CB-1XF	CB-1XG	CB-1XH	CB-1XI	CB-1XJ	CB-1XK	CB-1XL	CB-1XM	CB-1XN	CB-1XO	CB-1XP	CB-1XQ	CB-1XR	CB-1XS	CB-1XT	CB-1XU	CB-1XV	CB-1XW	CB-1XX	CB-1XY	CB-1XZ	CB-1YA	CB-1YB	CB-1YC	CB-1YD	CB-1YE	CB-1YF	CB-1YG	CB-1YH	CB-1YI	CB-1YJ	CB-1YK	CB-1YL	CB-1YM	CB-1YN	CB-1YO	CB-1YP	CB-1YQ	CB-1YR	CB-1YS	CB-1YT	CB-1YU	CB-1YV	CB-1YW	CB-1YX	CB-1YY	CB-1YZ	CB-1ZA	CB-1ZB	CB-1ZC	CB-1ZD	CB-1ZE	CB-1ZF	CB-1ZG	CB-1ZH	CB-1ZI	CB-1ZJ	CB-1ZK	CB-1ZL	CB-1ZM	CB-1ZN	CB-1ZO	CB-1ZP	CB-1ZQ	CB-1ZR	CB-1ZS	CB-1ZT	CB-1ZU	CB-1ZV	CB-1ZW	CB-1ZX	CB-1ZY	CB-1ZZ	CB-1AAA	CB-1AAB	CB-1AAC	CB-1AAD	CB-1AAE	CB-1AAF	CB-1AAG	CB-1AAH	CB-1AAI	CB-1AAJ	CB-1AAK	CB-1AAL	CB-1AAM	CB-1AAN	CB-1AAO	CB-1AAP	CB-1AAQ	CB-1AAR	CB-1AAS	CB-1AAT	CB-1AAU	CB-1AAV	CB-1AAW	CB-1AAX	CB-1AAY	CB-1AAZ	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1AAB	CB-1A

VOLATILE ORGANIC ANALYSIS - ANALYTICAL RESULTS										ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS										Page 20	
Sample Number		CB-260	CB-260	Field Blank	CB-18	CB-18	CB-10	CB-250	CB-1C	CB-1B	CB-17B	CB-17B	Field Blank 21	Borate 12							
Laboratory Sample Number		890808706	890808707	890808712	890808701	890808702	890808703	890808704	890808705	890808706	890808707	890808708	890808709	890808711							
Results		Duplicate CB-260	ug/kg	ug/kg	ug/l	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/l	ug/l							
VOLATILE COMPOUNDS																					
Quantitation Limit																					
cis-1,3-Dichloropropene		5.0					UL	UL			UL										
Bromoforn		5.0					UL	UL			UL										
2-Dioxane		10					UL	UL			UL										
4-Ethyl-2-pentene		10					UL	UL			UL										
Tetrachloroethene		5.0					UL	UL			UL										
Toluene		5.0	12 J	550			UL	UL			UL										
Chlorobenzene		5.0	2.0 J	190			UL	UL			UL										
Ethylbenzene		5.0	8.0 J	810			UL	UL			UL										
Styrene		5.0					UL	UL			UL										
Total Styrene		5.0	19 J	1600 J			UL	UL			UL										
Quantitation Limit Multiplier		1.2	5.4	3.0	1.1	1.1	1.1	1.2	1.1	1.1	1.1	1.1	1.0	1.0							
Date Received by Laboratory		8/8/89	8/8/89	8/8/89	8/7/89	8/7/89	8/7/89	8/7/89	8/7/89	8/7/89	8/7/89	8/7/89	8/7/89	8/7/89							
Date of Analysis		8/22/89	8/15/89	8/15/89	8/16/89	8/22/89	8/22/89	8/22/89	8/11/89	8/31/89	8/22/89	8/21/89	8/15/89	8/15/89							
Instrument Used for Analysis		7001 A	7001 A	7001 A	7001 A	7001 A	7001 A	7001 A	7001 A	7001 A	7001 A	7001 A	7001 A	7001 A							

NOTES:

- Compound was not detected
- Quantitation is approximate due to limitations identified during the quality control review (data validation).
- This result is qualitatively suspect since this compound was detected in a field and/or laboratory blank(s) at a similar level.
- Unreliable result - Analyte may or may not be present in this sample.
- This analyte was not detected, but the quantitation limit is probably higher due to a low bias identified during the quality assurance review.

[illegible]

ESTRADIOL ANALYSIS			ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS										Page 24	
ANALYTICAL RESULTS			CB-240	CB-240	CB-240	CB-240	CB-240	CB-240	CB-240	CB-240	CB-240	CB-240	CB-240	CB-240
Laboratory Sample Number			09000002	09000002	09000002	09000002	09000002	09000002	09000002	09000002	09000002	09000002	09000002	09000002
Duplicate			CB-240	CB-240	CB-240	CB-240	CB-240	CB-240	CB-240	CB-240	CB-240	CB-240	CB-240	CB-240
mg/kg			mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg
Solid			mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg
Limit			mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg
0.5			mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg
Multiplier			mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg
1.19			1.19	1.19	1.19	1.19	1.19	1.19	1.19	1.19	1.19	1.19	1.19	1.19
0/9/09			0/9/09	0/9/09	0/9/09	0/9/09	0/9/09	0/9/09	0/9/09	0/9/09	0/9/09	0/9/09	0/9/09	0/9/09
0/10/09			0/10/09	0/10/09	0/10/09	0/10/09	0/10/09	0/10/09	0/10/09	0/10/09	0/10/09	0/10/09	0/10/09	0/10/09
0/3/09			0/3/09	0/3/09	0/3/09	0/3/09	0/3/09	0/3/09	0/3/09	0/3/09	0/3/09	0/3/09	0/3/09	0/3/09

NOTES:

1. Compound was not detected

2. Quantitation is appropriate due to limitations identified during the quality control review (data validation).

3. This result is qualitatively suspect since this compound was detected in a field and/or laboratory blank(s) at a similar level.

4. Unreliable result - Analyte may or may not be present in this sample.

5. This analyte was not detected, but the quantitation limit is probably higher due to a low bias identified during the quality assurance review.

VOLATILE ORGANIC ANALYSIS - ANALYTICAL RESULTS										ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS										- page 26 -			

[illegible]

INTERFERABLE ORGANIC ANALYTICAL RESULTS										ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS										Page 10	
Helicoin Plastic Sample Number		CD-15A	CD-15B	CD-15C	CD-9A	CD-9B	CD-8A	CD-8B	CD-8C	Field Blank #9	Blank #9	CD-10A	CD-10B	CD-10C	CD-10D	CD-10E					
Laboratory Sample Number		890809203	890809204	890809205	890809206	890809207	890809208	890809209	890809210	890809211	890809212	890811001	890811002	890811003	890811004	890811005					
Remarks													Duplicate								
													CD-10A								
Date		yy/mm	yy/mm	yy/mm	yy/mm	yy/mm	yy/mm	yy/mm	yy/mm	yy/mm	yy/mm	yy/mm	yy/mm	yy/mm	yy/mm	yy/mm					
VOLATILE COMPOUNDS		Quantitation	Quantitation	Quantitation	Quantitation	Quantitation	Quantitation	Quantitation	Quantitation	Quantitation	Quantitation	Quantitation	Quantitation	Quantitation	Quantitation	Quantitation					
Limit (ug./lit. sol.)		Limit	Limit	Limit	Limit	Limit	Limit	Limit	Limit	Limit	Limit	Limit	Limit	Limit	Limit	Limit					
Acceptor-1202		0.5	80																		
Quantitation Limit Multiplier		1.19	1.06	1.19	1.19	1.19	1.19	1.19	1.19	1.19	1.19	1.19	1.19	1.19	1.19	1.19					
Date Sample Received		8/9/89	8/9/89	8/9/89	8/9/89	8/9/89	8/9/89	8/9/89	8/9/89	8/9/89	8/9/89	8/10/89	8/10/89	8/10/89	8/10/89	8/10/89					
Date Sample Extracted		8/16/89	8/16/89	8/16/89	8/16/89	8/16/89	8/16/89	8/16/89	8/16/89	8/16/89	8/16/89	8/17/89	8/17/89	8/17/89	8/17/89	8/17/89					
Date of Analysis		9/3/89	9/3/89	9/3/89	9/3/89	9/3/89	9/3/89	9/3/89	9/3/89	9/3/89	9/3/89	9/3/89	9/3/89	9/3/89	9/3/89	9/3/89					

NOTES:

- Compound was not detected
- Quantitation is appropriate due to limitations identified during the quality control review (data validation).
- This result is qualitatively suspect since this compound was detected in a field and/or laboratory blank(s) at a similar level.
- Unreliable result - Analyte may or may not be present in this sample.
- This analyte was not detected, but the quantitation limit is probably higher due to a low bias identified during the quality assurance review.

Halocarbon Sample Number Laboratory Sample Number		CB-19A 890800AP01	CB-19C 890800AP03	CB-24A 890800AP04	CB-24C 890800AP10	CB-17A 890800AP08	CB-17C 890800AP10
Units		ng/kg	ng/kg	ng/kg	ng/kg	ng/kg	ng/kg
VOLATILE COMPOUNDS							
	Quantitation Limit						
Chloroethane	10						
Bromoethane	10						
Vinyl Chloride	10						
Chloroethane	10						
Methylene Chloride	5.0	2.0 B	3.0 B		800 B	8.0 B	7.0 B
Acetone	10				1400 B	11 B	
Carbon Disulfide	5.0						
1,1-Dichloroethene	5.0						
1,1-Dichloroethane	5.0						
1,2-Dichloroethane	5.0						
Chloroform	5.0						
1,2-Dichloroethane	5.0						
2-Butanone	10	B	B	B			
1,1,1-Trichloroethane	5.0						
Carbon Tetrachloride	5.0						
Vinyl Acetate	10						
Bromodichloroethane	5.0						
1,1,2,2-Tetrachloroethane	5.0						
1,2-Dichloropropane	5.0						
trans-1,2-Dichloropropene	5.0						
Trichloroethene	5.0				550 B		
Dibromochloroethane	5.0						
2-Trichloroethane	5.0						
Benzene	5.0						

Nalco Pirnie Sample Number		-page 2					
Laboratory Sample Number		CB-19A	CB-19C	CB-24A	CB-24C	CB-17A	CB-17C
		890808AP01	890808AP03	890808AP04	890808AP10	890808AP08	890808AP10
Units					Median Level		
Units		ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg
VOLATILE COMPOUNDS		Quantitation Limit					
cis-1,3-Dichloropropene	5.0						
Bromoform	5.0						
2-Hexanone	10						
4-Methyl-2-pentanone	10						
Tetrachloroethene	5.0			8.0			
Toluene	5.0				13,000		
Chlorobenzene	5.0				3900		
Ethylbenzene	5.0				20,000		
Styrene	5.0						
m,p-Xylenes	5.0				31,000		
Quantitation Limit Multiplier		1.1	1.1	1.1	150	1.1	1.2
Date Received by Laboratory		8/8/89	8/8/89	8/8/89	8/8/89	8/7/89	8/7/89
Date of Analysis		8/21/89	8/21/89	8/22/89	8/22/89	8/17/89	8/17/89
Instrument Used for Analysis		7001A	7001A	7001A	7001A	7001A	7001A

NOTES:

- Compound was not detected
- 2 Quantitation is approximate due to limitations identified during the quality control review (data validation).
- 3 This result is qualitatively suspect since this compound was detected in a field and/or laboratory blank(s) at a similar level.
- 4 Verifiable result - Analyte may or may not be present in this sample.
- 5 This analyte was not detected, but the quantitation limit is probably higher due to a low bias identified during the quality assurance review.

Laboratory Sample Number			CB-19A 890808AP01	CB-19C 890808AP03	CB-24A 890808AP04	CB-24C 890808AP10	CB-17A 890808P08	CB-17C 890808P10
Name								
Units			ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg
SEMI-VOLATILE COMPOUNDS	Aqueous	Solid						
	Quantitation Limit	Quantitation Limit						
Phenol	10	330				250 J	530	
Di-(2-Chloroethyl)ether	10	330						
2-Chlorophenol	10	330						
1,3-Dichlorobenzene	10	330						
1,4-Dichlorobenzene	10	330						
Benzyl Alcohol	10	330						
1,2-Dichlorobenzene	10	330						
2-Methylphenol	10	330						
2-chloroisopropyl ether	10	330						
4-Methylphenol	10	330				100 J		
3-Nitro-Di-n-propylamine	10	330					85	
Hexachloroethane	10	330						
Nitrobenzene	10	330						
Isophorone	10	330						
2-Nitrophenol	10	330						
2,4-Dimethylphenol	10	330						
Benzoic Acid	50	1650						
Di-(2-Chloroethoxy) methane	10	330						
2,4-Dichlorophenol	10	330						
1,2,4-Trichlorobenzene	10	330						
Naphthalene	10	330				1300		
6-Chloroaniline	10	330						
Hexachlorobutadiene	10	330						
6-Chloro-3-methylphenol	10	330						
2-Methyl-naphthalene	10	330				310 J		

VOLATILE ORGANIC ANALYSIS - ANALYTICAL RESULTS			ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS							Page 4
			CB-15A 090000001	CB-15C 090000003	CB-20A 090000004	CB-20C 090000010	CB-17A 090000008			
leola Petro Sample Number										
eratory Sample Number										
cho										
to										
VOLATILE COMPOUNDS		Aqueous Quantitation/								
		Limit								
		Solid Limit								
	acetylcyclopentadiene	10	330							
	4-Trichlorophenol	10	330							
	5-Trichlorophenol	50	1650							
	bromobenzene	10	330							
	transaniline	50	1650							
	ethylphthalate	10	330							
	naphthalene	10	330							
transaniline	50	1650								
styrene	10	330								
diisobutylene	50	1650								
styrene	50	1650								
acetylcyclopentadiene	10	330								
transaniline	50	1650								
transaniline	50	1650								
diisobutylene	50	1650								
transaniline	10	330								
transaniline	10	330								
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INTERPRETABLE ORGANIC ANALYSIS		ANALYTICAL RESULTS		ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS						page 5
Municipal Waste Sample Number		Municipal Waste Sample Number		CD-19A	CD-19C	CD-19A	CD-24C	CD-17A	CD-17C	
Laboratory Sample Number		Laboratory Sample Number		0500001701	0500001703	0500001704	0500001705	0500001706	0500001710	
Analysis		Analysis		ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	
Solid		Solid		ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	
Quantification		Quantification		ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	
Blank		Blank		ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	
SAMPLABLE COMPOUND		SAMPLABLE COMPOUND		ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	
Isotracene		Isotracene		10	330					
101-o-butylphthalate		101-o-butylphthalate		10	330	95 J				
Phloranthene		Phloranthene		10	330			310 J		
Pyrene		Pyrene		10	330			220 J		
Butylbenzylphthalate		Butylbenzylphthalate		10	330					
3,3'-Dichlorobenzidine		3,3'-Dichlorobenzidine		20	600	R	R	R	R	R
Benzo(a)anthracene		Benzo(a)anthracene		10	330					
1-methyl-2-ethylphthalate		1-methyl-2-ethylphthalate		10	330		07 B	120 B	1000 B	260 B
1-methyl-2-ethylphthalate		1-methyl-2-ethylphthalate		10	330				150	
Benzo(b)fluoranthene		Benzo(b)fluoranthene		10	330					
Benzo(k)fluoranthene		Benzo(k)fluoranthene		10	330					
Benzo(a)pyrene		Benzo(a)pyrene		10	330					
1-methyl-2,3-cd pyrene		1-methyl-2,3-cd pyrene		10	330					
Benzo(a)anthracene		Benzo(a)anthracene		10	330					
Benzo(g,h,i)perylene		Benzo(g,h,i)perylene		10	330					
Quantification Blank Multiplier		Quantification Blank Multiplier		1.12	1.06	1.03	1.21	1.20	1.21	
Date Received by Laboratory		Date Received by Laboratory		01/01/09	01/01/09	01/01/09	01/01/09	01/01/09	01/01/09	
Date Sample Extracted		Date Sample Extracted		01/01/09	01/01/09	01/01/09	01/01/09	01/01/09	01/01/09	
Date of Analysis		Date of Analysis		01/01/09	01/01/09	01/01/09	01/01/09	01/01/09	01/01/09	
Instrument Used for Analysis		Instrument Used for Analysis		70020	70020	70020	70020	70020	70020	

ICLP - PREPAREDLY IDENTIFIED COMPOUNDS		Estimated Concentrations				Page 6
		CB-19A	CB-19C	CB-24A	CB-24C	CB-11A CB-11C
		890808AP01	890808AP03	890808AP04	890808AP10	890808P00 890808P10
Phenanthrene						
BaP	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg
COMPOUNDS						
VOLATILE COMPONENTS						
Chlorocetylbenzene				900 J		
SEMITVOLATILE COMPONENTS						
Laboratory artifact (toluene bleed)					114,100 (1) B	
Laboratory artifact (aldol)	3000 B	3000 B	3000 B	1000 B	3000 B	2000 B
BaP		400 (2) J	2500 (5) J		9000 (5) J	
Polycyclic aromatic hydrocarbon					4000 (2) J	
1-chlorobenzene isomer					2000 J	
1-methylbenzene isomer				500 J		
1,2,3-trimethylbenzene				4000 (5) J		
1-methyl-2-ethylbenzene				500 J		
Saturated hydrocarbon				5200 (3) J		
Substituted phenol				3500 (3) J		
Carboxylic acid				700 J		
Enzyme derivative				5000 J		

ACTUALS ORGANIC ANALYSIS - ANALYTICAL RESULTS		ALL SOLIDS REPORTED ON A DRY WEIGHT BASIS						-page 1
old Parole Sample Number		CB-19A	CB-19C	CB-24A	CB-24C	CB-17A	CB-17C	
entry Sample Number		090000701	090000703	090000704	090000710	090000708	090000710	
cho								
g		ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	ug/kg	
VOLATILE COMPOUNDS								
	Aqueous	Solid						
	Quantitation(Quantitation)							
	Limit	Limit						
lor-1242	0.5	00				6500		
titration Limit Multiplier	1.125	1.06	1.125	1.10			1.10	
Sample Received	0/8/09	0/8/09	0/8/09	0/8/09	0/7/09	0/7/09	0/7/09	
Sample Extracted	0/10/09	0/10/09	0/10/09	0/10/09	0/16/09	0/16/09	0/16/09	
of Analysis	9/2/09	9/2/09	9/3/09	9/3/09	9/2/09	9/2/09	9/2/09	

NOTES:




- Compound was not detected.
- J Quantitation is approximate due to limitations identified during the quality control review (data validation).
- B This result is qualitatively suspect since this compound was detected in a field and/or laboratory blank(s) at a similar level.
- B Unreliable result - Analyte may or may not be present in this sample.
- 0L This analyte was not detected, but the quantitation limit is probably higher due to a low bias identified during the quality assurance review.

APPENDIX E

SOIL BORING LOGS AND GRAIN SIZE DISTRIBUTION CURVES FOR SOIL BORINGS CONSTRUCTED IN AREA OF FORMER LAGOON

PROJECT NAME : N.Storonske Cooperage
 DATE : 8/7/89
 CONTRACTOR : Empire Soils Invest.
 DRILL. METHOD: 4.25" I.D. H.S.A.
 BORING NUMBER: CB-1
 PROJECT NO. : 0852-13-1
 LOCATION : Schodack, N.Y.
 INSPECTOR : N.Thompson & A.Murtaugh
 SAMP. METHOD : Split spoon
 SURFACE ELEV.: 355.51
 DATUM : Ground level

=====

SAMPLE		SOIL DESCRIPTION		STR.	Field screening of split spoon with 11.7 Hnu
No.	N- Value	Depth (ft.)	Density, color, SOIL, admixtures moisture, other, CONTAMINATION		
1	3	1-3	Frm brn slt w/some m snd, tr f-m rnd gvl, tr rock frags, Fill, dry		0.0 PPME
2	3	5-7	Frm or-tan brn slt w/cl & snd becoming gry stained 6-7', Fill dry-moist		9.0 PPME
3	28	12-14	Frm brn slt, f-c snd, f-m ang gvl tr rock frags, Fill, dry		0.0 PPME
4	11	14-16	Lse-frm brn snd, slt, gvl, Fill, dry		0.0 PPME
5	20	16-18	16-17' Frm or brn slt & snd, dry 17-18' Lse c snd & gvl w/ltl slt, f snd, Outwash, dry		
6	22	18-20	Stf grn gry slt, ltl cl, ang gvl Till, moist		
Competent bedrock at 22.1' as determined by hollow stem augers.					


=====

PROJECT NAME : N.Storonske Cooperage
 DATE : 8/1/89
 CONTRACTOR : Empire Soils Invest.
 DRILL. METHOD: 4.25" I.D. H.S.A.

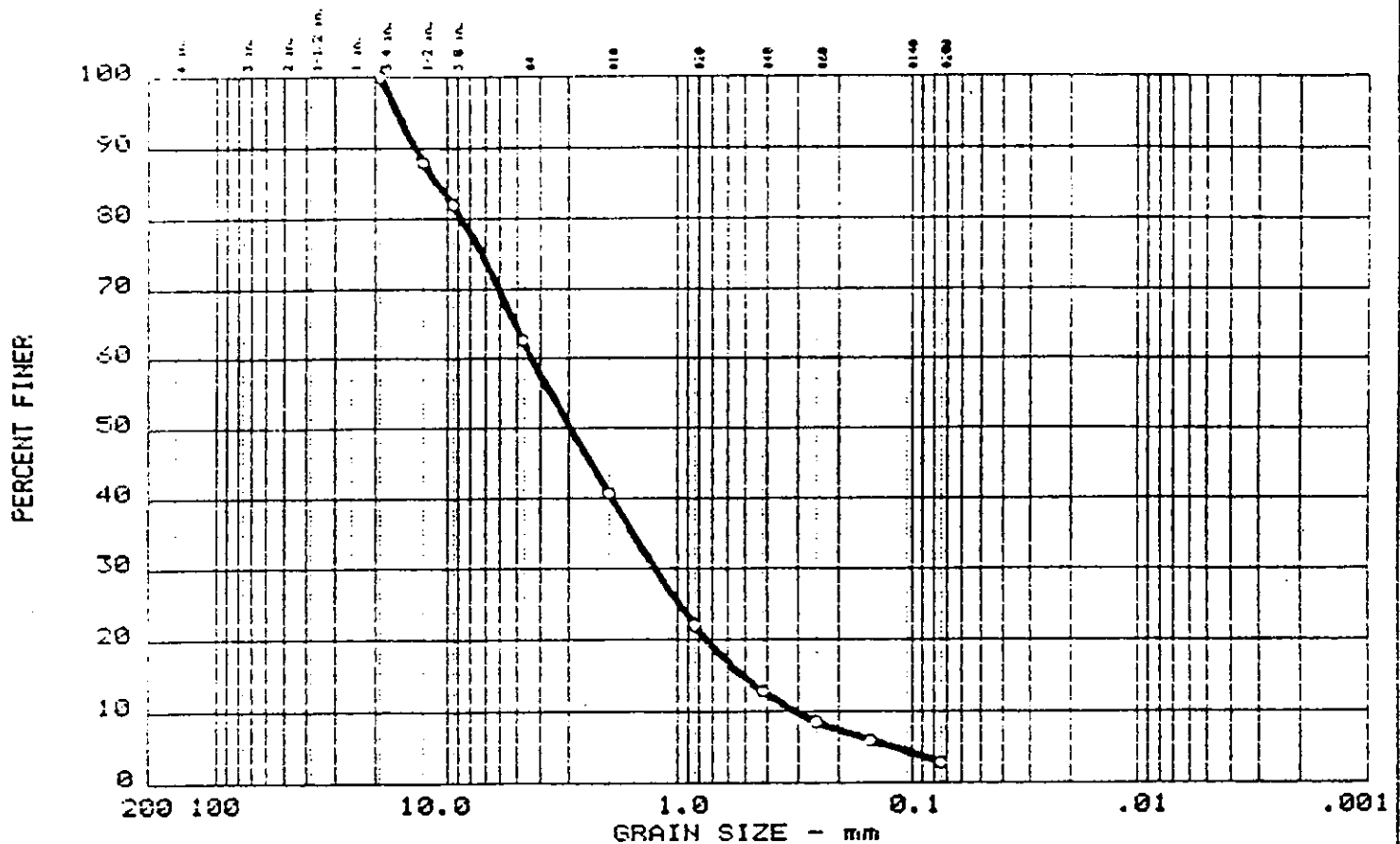
BORING NUMBER: CB-2
 PROJECT NO. : 0852-13-1
 LOCATION : Schodack, N.Y.
 INSPECTOR : N.Thompson & A.Murtaugh
 SAMP. METHOD : Split spoon

SURFACE ELEV.: 349.83

DATUM : Ground level

SAMPLE		SOIL DESCRIPTION		STR.	Field screening of split spoon with 10.2 Hnu
No.	N- Value	Depth (ft.)	Density, color, SOIL, admixtures moisture, other, CONTAMINATION		
1	3	1-3	Frm brn sndy topsoil w/f ang gvl rd brick,moist		.2 PPME
2	9	5-7	Same, w/c snd,f-m gvl,Fill		.2 PPME
3	19	12-14	Frm dk gry slt & snd matrix,ltl cl f-c rnd gvl,poorly srt,Outwash,moist		.6 PPME
4	75	17-19	Frm-stf dk grn slt,snd matrix w/ f-c gvl,dry-moist,Till		
			Competent bedrock at 18.9' as by split spoon.		

GRAIN SIZE DISTRIBUTION TEST REPORT



Test	%+3"	% GRAVEL	% SAND	% SILT	% CLAY
2	0.0	37.3	59.9	2.8	

LL	PI	D ₈₅	D ₆₀	D ₅₀	D ₃₀	D ₁₅	D ₁₀	C _c	C _u
		10.96	4.32	2.95	1.257	0.5123	0.3051	1.20	14.1

MATERIAL DESCRIPTION	USCS	AASHTO
o Brown SAND & GRAVEL, trace silt	SW	

Project No.: AT-89-363
 Project: STORONSKE COOPERAGE CO. INC. EAST GREENBUSH
 o Location: 2C (CB) - SAMPLE DEPTH= 12-14 ft

Date: 01-18-90

GRAIN SIZE DISTRIBUTION TEST REPORT
EMPIRE SOILS INVESTIGATIONS, INC.

Remarks:
 CLIENT: MALCOLM FIRNIE

LAB NO. 288.002




Fig. No.

PROJECT NAME : N.Storonske Cooperage
 DATE : 7/28-7/31/89
 CONTRACTOR : Empire Soils Invest.
 DRILL. METHOD: 4.25" I.D. H.S.A.

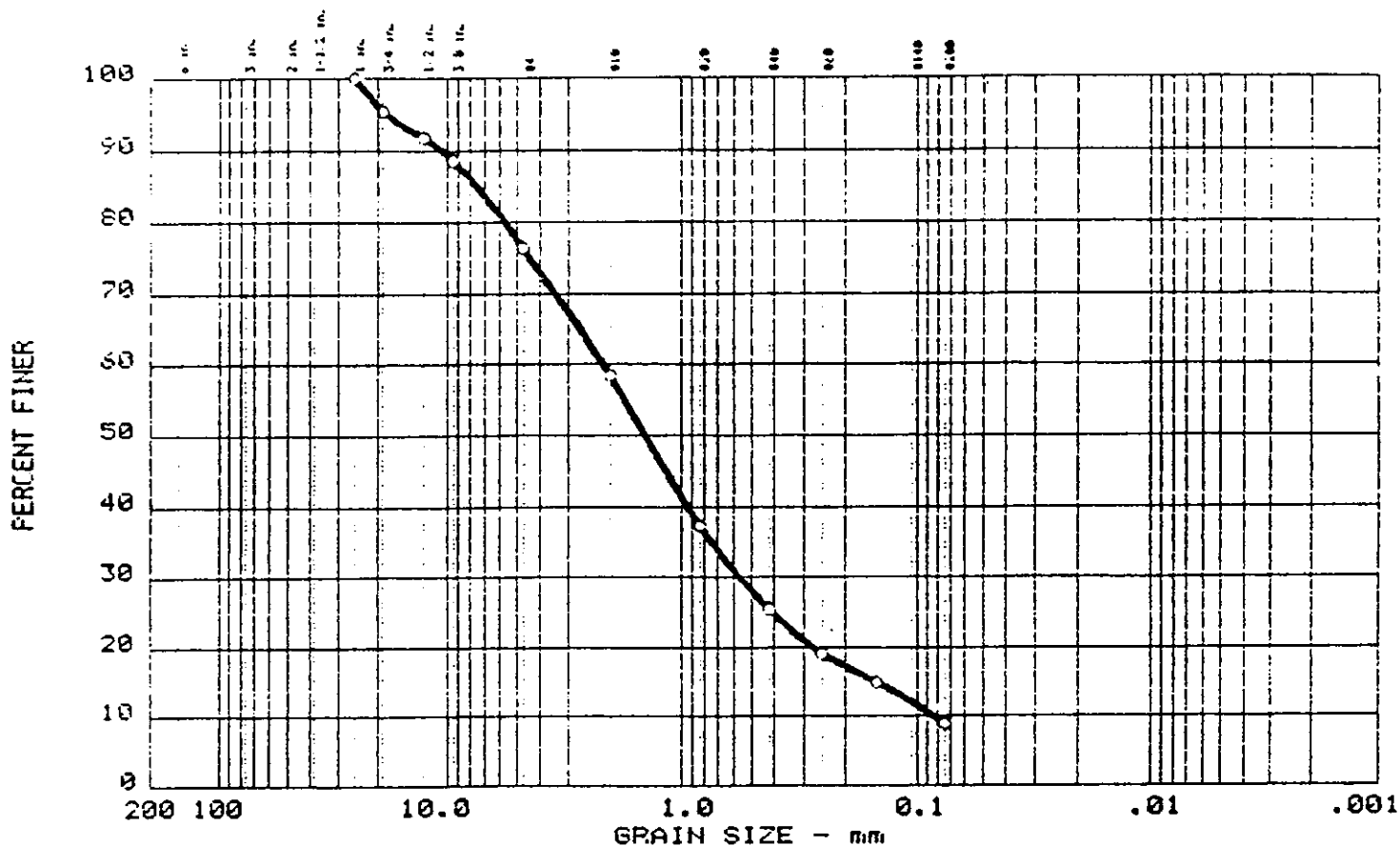
BORING NUMBER: CB-3
 PROJECT NO. : 0852-13-1
 LOCATION : Schodack, N.Y.
 INSPECTOR : N.Thompson & A.Murtaugh
 SAMP. METHOD : Split spoon

SURFACE ELEV.: 351.52

DATUM : Ground level

SAMPLE		SOIL DESCRIPTION		STR.	Field screening of split spoon with 11.7 Hnu
No.	N- Value	Depth (ft.)	Density, color, SOIL, admixtures moisture, other, CONTAMINATION		
1	2	1-3	Sft-frn, dk grn brn slt, ltl f.snd pbls, ltl cl, plastic, Fill, moist		1.4 PPME
2	4	3-5	Frm, brn-tan slt, snd, gvl, v. poorly srt, Fill, moist		100 PPME
3	33	5-7	Frm, brn slt, snd, abun pbls & gvl v. poorly srt, Fill, moist		
4	100	12- -12.3	Poor sample recovery, dns tan, slt snd, gvl		
5	10	13-15	Frm-stf, grn-gry, sandy slt w/ w rnd pbls & gvl, cl, sh frags, moist, Till		
6	100	17.7- 18.1	Hd gry slt-snd matrix w/gvl sh frags, Till		
Competent bedrock at 19.1' as determined by hollow stem augers					

GRAIN SIZE DISTRIBUTION TEST REPORT



Test	%+3"	% GRAVEL	% SAND	% SILT	% CLAY
3	0.0	23.7	67.4	8.9	

[illegible]

MATERIAL DESCRIPTION	USCS	AASHTO
o Brown SAND, some Gravel, trace silt	SW-SM	

Project No.: AT-89-363
Project: STORONSKE COOPERAGE CO. INC. EAST GREENBUSH
o Location: 3A & 3B (CA) - SAMPLE DEPTH = A-1-5ft
B-5-7ft

Date: 01-18-90

GRAIN SIZE DISTRIBUTION TEST REPORT
EMPIRE SOILS INVESTIGATIONS, INC.

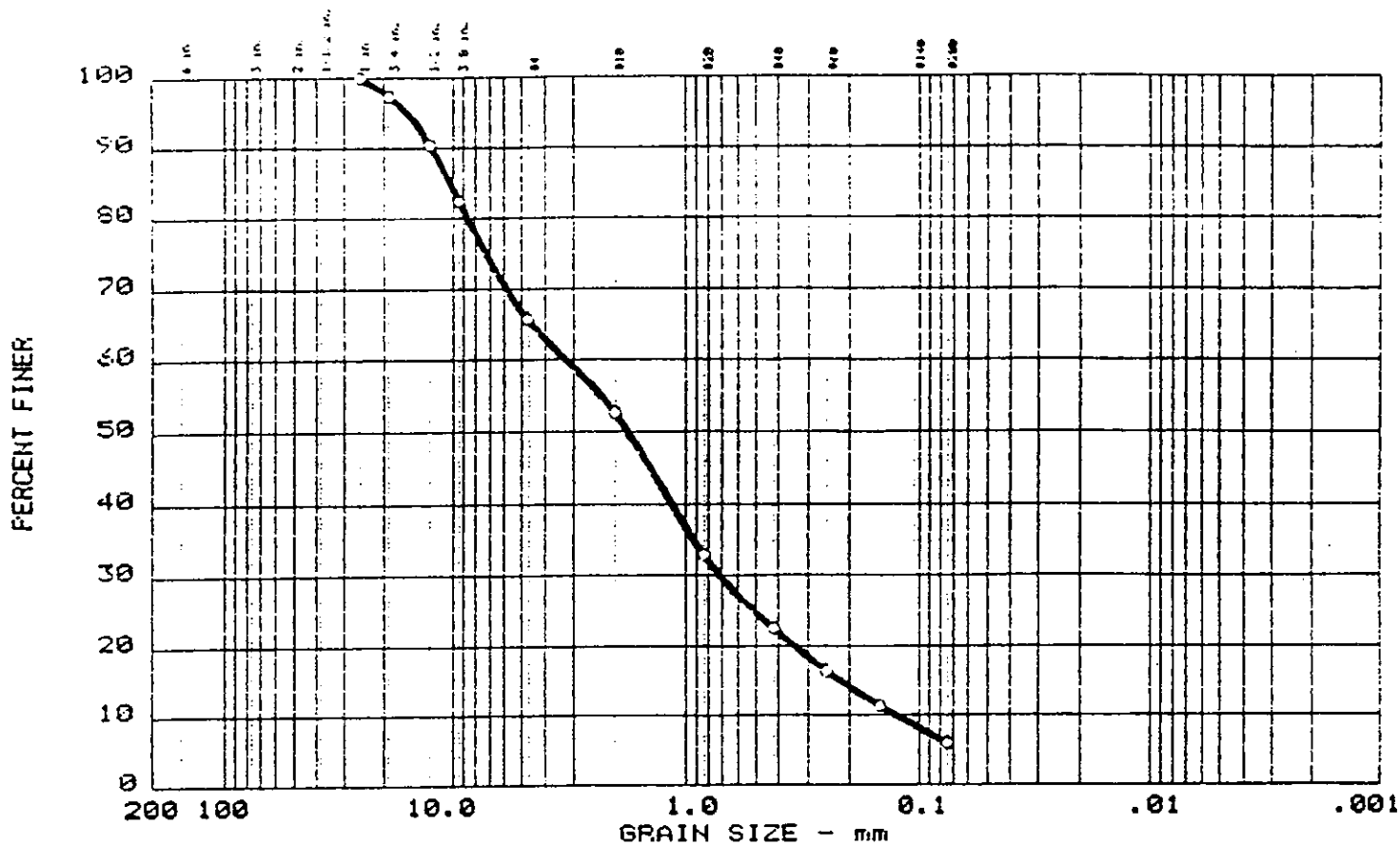
Remarks:

CLIENT: MALCOLM PIRNIE

LAB NO. 288.003

Fig. No.

GRAIN SIZE DISTRIBUTION TEST REPORT



Test	%+3"	% GRAVEL	% SAND	% SILT	% CLAY
1	0.0	34.3	59.7	6.1	

[illegible]

MATERIAL DESCRIPTION	USCS	AASHTO
o Brown SAND & GRAVEL, trace silt	SW-SM	

Project No.: AT-89-363
Project: STORONSKO COOPERAGE CO. INC. EAST GREENBUSH
o Location: 30 (CB) - SAMPLE DEPTH = 13-15 ft

Date: 01-18-90

GRAIN SIZE DISTRIBUTION TEST REPORT
EMPIRE SOILS INVESTIGATIONS, INC.

Remarks:

CLIENT: MALCOLM PIRNIE

LAB NO. 288.001

Fig. No.

PROJECT NAME : N.Storonske Cooperage	BORING NUMBER: CB-4
DATE : 7/31/89	PROJECT NO. : 0852-13-1
CONTRACTOR : Empire Soils Invest.	LOCATION : Schodack, N.Y.
DRILL. METHOD: 4.25" I.D. H.S.A.	INSPECTOR : N.Thompson & A.Murtaugh
	SAMP. METHOD : Split spoon
SURFACE ELEV.: 345.55	DATUM : Ground level


SAMPLE		SOIL DESCRIPTION		Field screening of split spoon with STR. 11.7 Hnu
No.	N- Value	Depth (ft.)	Density, color, SOIL, admixtures moisture, other, CONTAMINATION	
1	15	1-3	Frm lt brn slt w/f-c snd,gvl,dry	3.1 PPME
2	25	5-7	Frm brn-gr slt matrix w/snd & f-m ang gvl,sh frags,Outwash,dry	.2 PPME
3	65	11-13	Frm-stf slt,f-c snd,f-c rnd gvl Outwash,moist	.4 PPME
4	96	18- 18.6	No recovery	
Competent bedrock at 19' as determined by hollow stem augers				

PROJECT NAME : N.Storonske Cooperage		BORING NUMBER:CB-5
DATE : 7/27/89	PROJECT NO. : 0852-13-1	
CONTRACTOR : Empire Soils Investigati	LOCATION : Schodack, N.Y.	
DRILL. METHOD: 4.25" I.D. H.S.A.	INSPECTOR : N.Thompson & B.Nelson	
	SAMP. METHOD : Split spoon	
SURFACE ELEV.: 345.07	DATUM : Ground level	

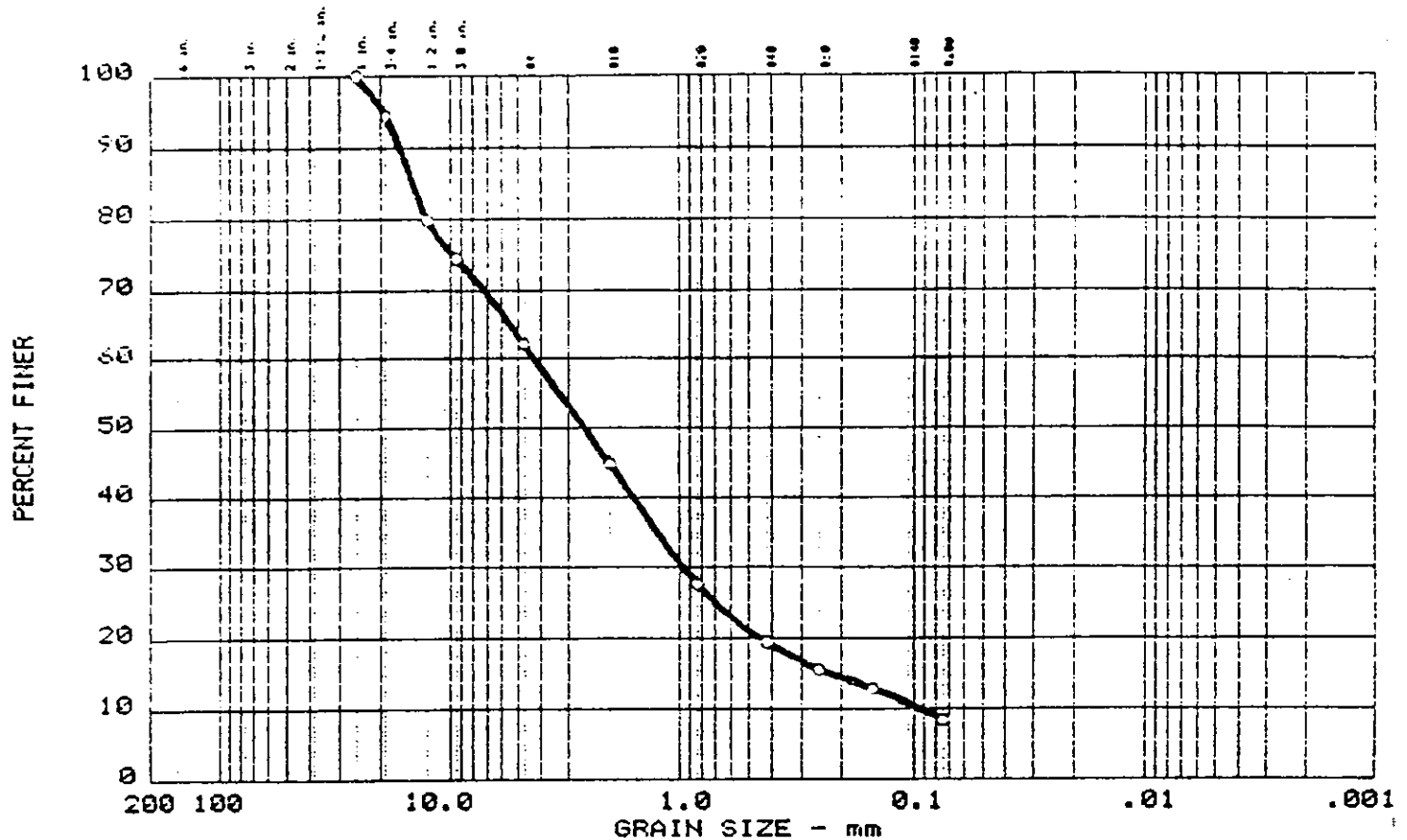
SAMPLE		SOIL DESCRIPTION		STR.	Well Construction
No.	N-Value	Depth (ft.)	Density, color, SOIL, admixtures moisture, other, CONTAMINATION		
1	3	1-3	Lse, brn-gr sdy top soil, tr f. ang gvl, moist		
2	17	3-5	Lse, gr sdy top soil w/ c. ang gvl tr sltst, dry-moist		
3	9	7-9	Lse gr c. sand, slt, f.- m. rnd gvl, tr sltst, tr rd, Outwash, moist		
4	27	10-12	Same as above, wet at 11.5'		
5	22	14-16	Frm, gr gvlly slt, w/fractured sltst & sm rnd m. gvl, sm rd brn c. sand, Outwash, wet		
6	78	19-20	Same as above w/ cl, Till		
7	45	21-22	Stf, gr sdy slt, moist		
			Weathered bedrock at 21.3'		

PROJECT NAME : N.Storonske Cooperage	BORING NUMBER: CB-6
DATE : 8/2/89	PROJECT NO. : 0852-13-1
CONTRACTOR : Empire Soils Invest.	LOCATION : Schodack, N.Y.
DRILL. METHOD: 4.25" I.D. H.S.A.	INSPECTOR : N.Thompson & A.Murtaugh
	SAMP. METHOD : Split spoon
SURFACE ELEV.: 348.17	DATUM : Ground level

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SAMPLE		SOIL DESCRIPTION		STR.	Field screening of split spoon with 10.2 Hnu
No.	N- Value	Depth (ft.)	Density, color, SOIL, admixtures moisture, other, CONTAMINATION		
1	3	1-3	Frm brn slt, snd, f rnd gvl, Fill, dry-moist		0.2 PPME
2	12	5-7	Lse brn m-c snd w/slt, f-m ang gvl Outwash, dry		0.0 PPME
3	23	11-13	Lse-frn c snd w/slt, f-c ang-rnd sh frags, dry Outwash		0.0 PPME
4	95	19- 20.2	No recovery, wet		
Competent bedrock at 20.2' as determined by split spoon.					

GRAIN SIZE DISTRIBUTION TEST REPORT



Test	%+3"	% GRAVEL	% SAND	% SILT	% CLAY
5	0.0	37.8	53.8	8.4	

LL	PI	D ₈₅	D ₆₀	D ₅₀	D ₃₀	D ₁₅	D ₁₀	C _c	C _u
		14.74	4.25	2.56	0.963	0.2205	0.0930	2.34	45.7

MATERIAL DESCRIPTION	USCS	AASHTO
○ Brown SAND & GRAVEL, trace silt	SW-SM	

Project No.: AT-89-363
 Project: STORONSKE COOPERAGE CO. INC. EAST GREENBUSH
 ○ Location: 6A(CB)-SAMPLE DEPTH= 1-3ft

Date: 01-18-90

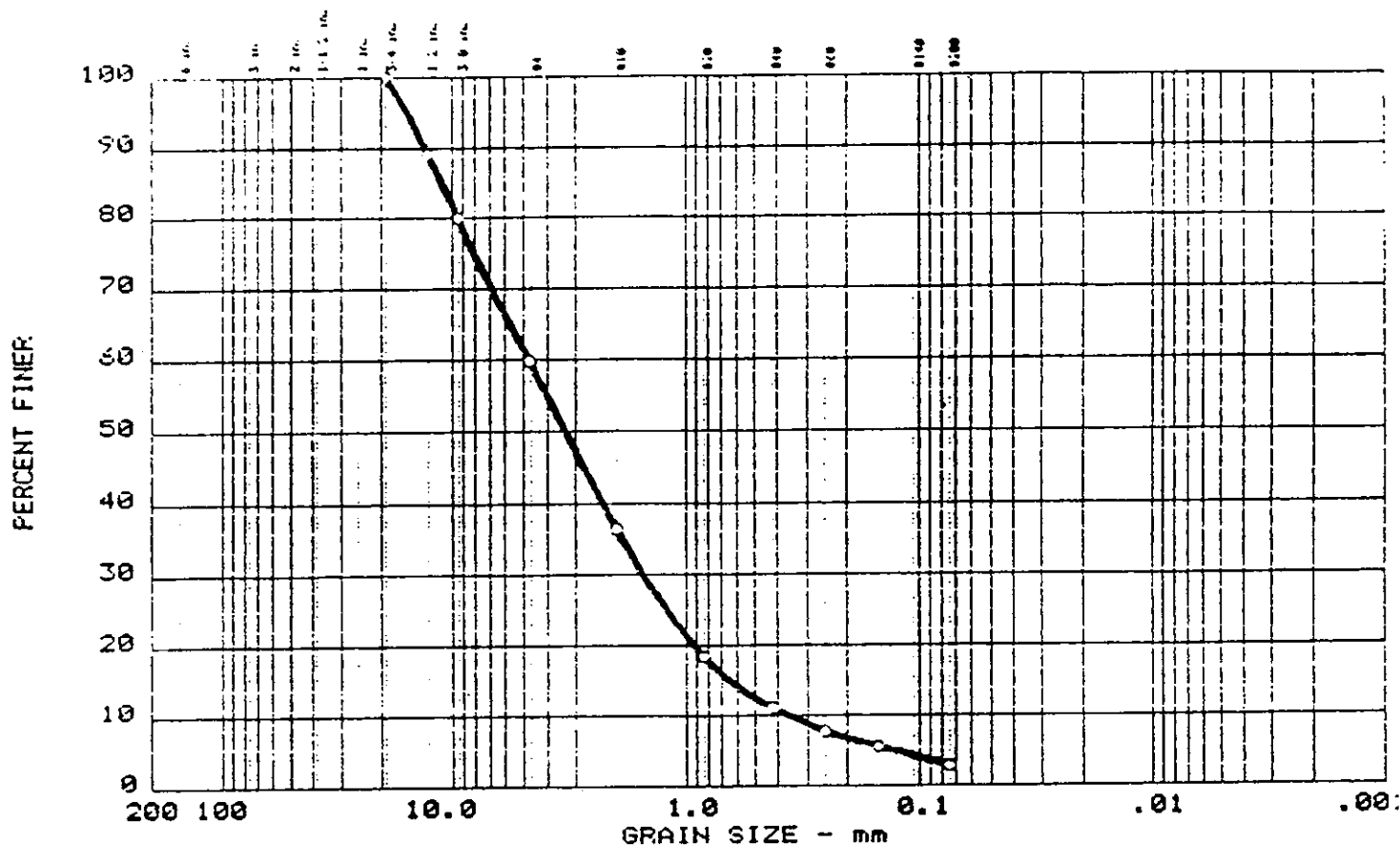
Remarks:
 CLIENT: MALCOLM PIRNIE

LAB. NO. 288.005

GRAIN SIZE DISTRIBUTION TEST REPORT
 EMPIRE SOILS INVESTIGATIONS, INC.

Fig. No.

GRAIN SIZE DISTRIBUTION TEST REPORT



Test	%+3"	% GRAVEL	% SAND	% SILT	% CLAY
4	0.0	40.2	57.0	2.9	

LL	PI	D ₈₅	D ₆₀	D ₅₀	D ₃₀	D ₁₅	D ₁₀	C _c	C _u
		11.09	4.79	3.31	1.531	0.6393	0.3548	1.38	13.5

MATERIAL DESCRIPTION	USCS	AASHTO
o Brown SAND & GRAVEL, trace silt	SW	

Project No.: AT-89-363
 Project: STORONSKE COOPERAGE CO. INC. EAST GREENBUSH
 o Location: 6C(CB)-SAMPLE DEPTH=11-13 ft

Date: 01-18-90

GRAIN SIZE DISTRIBUTION TEST REPORT
 EMPIRE SOILS INVESTIGATIONS, INC.

Remarks:
 CLIENT: MALCOLM PIRNIE

LAB. NO. 288.004






Fig. No.

PROJECT NAME : N.Storonske Cooperage
 DATE : 8/10-8/11/89
 CONTRACTOR : Empire Soils Invest.
 DRILL. METHOD: 4.25" I.D. H.S.A.

BORING NUMBER: CB-7
 PROJECT NO. : 0852-13-1
 LOCATION : Schodack, N.Y.
 INSPECTOR : N.Thompson & A.Murtaugh
 SAMP. METHOD : Split spoon

SURFACE ELEV.: 356.45

DATUM : Ground level

SAMPLE		SOIL DESCRIPTION		STR.	Field screening of split spoon with 11.7 Hnu
No.	N- Value	Depth (ft.)	Density, color, SOIL, admixtures moisture, other, CONTAMINATION		
1	3	2-4	Lse brn f-m snd, mod w srt, ltl slt Fill, dry		0.0 PPME
2	14	4-6	Lse brn f-c snd, f-c ang-rnd gvl Outwash at 4.2', dry		0.0 PPME
3	19	8-10	Frm brn slt w/f-m snd, some ang f- m gvl, tr sh frag, Outwash, dry-moist		0.0 PPME
4	39	10-12	Lse gry brn f-c snd w/ang-rnd gvl some slt, Outwash, moist		
Competent bedrock at 14.7' as determined by hollow stem auger.					

SURFACE ELEV.: 358.21 DATUM :Ground level

PAGE 1 OF 1

PROJECT NAME : N.Storonske Cooperage	BORING NUMBER: CB-10
DATE : 8/11/89	PROJECT NO. : 0852-13-1
CONTRACTOR : Empire Soils Invest.	LOCATION : Schodack, N.Y.
DRILL. METHOD: 4.25" I.D. H.S.A.	INSPECTOR : N.Thompson & A.Murtaugh
	SAMP. METHOD : Split spoon
SURFACE ELEV.: 357.84	DATUM : Ground level

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SAMPLE		SOIL DESCRIPTION			
No.	N- Value	Depth (ft.)	Density, color, SOIL, admixtures moisture, other, CONTAMINATION	STR.	Field screening of split spoon with

1	23	1-3	Lse -frm brn slt,snd,gvl,Fill,dry		
2	13	5-7	Lse brn f-c snd,f-c gvl,Outwash, dry		
3	91	11.5- 13	Grn gry weathered bedrock,broken & ang Argillite w/rock fines.		



Weathered bedrock at 11.5 as
determined by hollow stem augers and
split spoon.

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PROJECT NAME : N.Storonske Cooperage
 DATE : 8/10/89
 CONTRACTOR : Empire Soils Invest.
 DRILL. METHOD: 4.25" I.D. H.S.A.

BORING NUMBER: CB-11
 PROJECT NO. : 0852-13-1
 LOCATION : Schodack, N.Y.
 INSPECTOR : N.Thompson & A.Murtaugh
 SAMP. METHOD : Split spoon

SURFACE ELEV.: 354.56

DATUM : Ground level

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SAMPLE		SOIL DESCRIPTION		Field screening of split spoon with 11.7 Hnu
No.	N- Value	Depth (ft.)	Density, color, SOIL, admixtures moisture, other, CONTAMINATION	
1	5	1-3	Lse-frn brn slt & f snd, tr f-m ang -rnd gvl, tr sh frags, Fill, dry	0.2 PPME
		3-5	Lse or brn f snd, Fill, dry	
2	5	5-7	Lse brn f-m snd, tr ang-subrnd f-m gvl, Fill, dry	0.8 PPME
3	12	9-11	Frm-hd brn slt & snd matrix w/f-c ang-rnd gvl, tr sh frags, Outwash, dry	0.0 PPME
4	36	11-13	Frm-lse brn c-snd, f-c ang-rnd gvl some slt Outwash, dry-moist Note: Hd dns lt brn dry Till found on auger.	
Competent bedrock at 13.9' as determined by hollow stem auger.				




PROJECT NAME : N.Storonske Cooperage
 DATE : 8/11/89
 CONTRACTOR : Empire Soils Invest.
 DRILL. METHOD: 4.25" I.D. H.S.A.

BORING NUMBER: CB-12
 PROJECT NO. : 0852-13-1
 LOCATION : Schodack, N.Y.
 INSPECTOR : N.Thompson & A.Murtaugh
 SAMP. METHOD : Split spoon

SURFACE ELEV.: 357.29

DATUM : Ground level

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SAMPLE		SOIL DESCRIPTION		STR.	Field screening of split spoon with 11.7 Hnu
No.	N- Value	Depth (ft.)	Density, color, SOIL, admixtures moisture, other, CONTAMINATION		
1	10	1-3	Lse brn slt, snd, gvl, Fill, dry		
2	23	5-7	Lse-frn brn f-c snd w/gvl, Outwash dry		
3	100/.2	9.5 11.5	No recovery		
4	100/.4	12.5- 13.8	No recovery		
Competent bedrock at 12.8' as determined by hollow stem augers and split spoon.					

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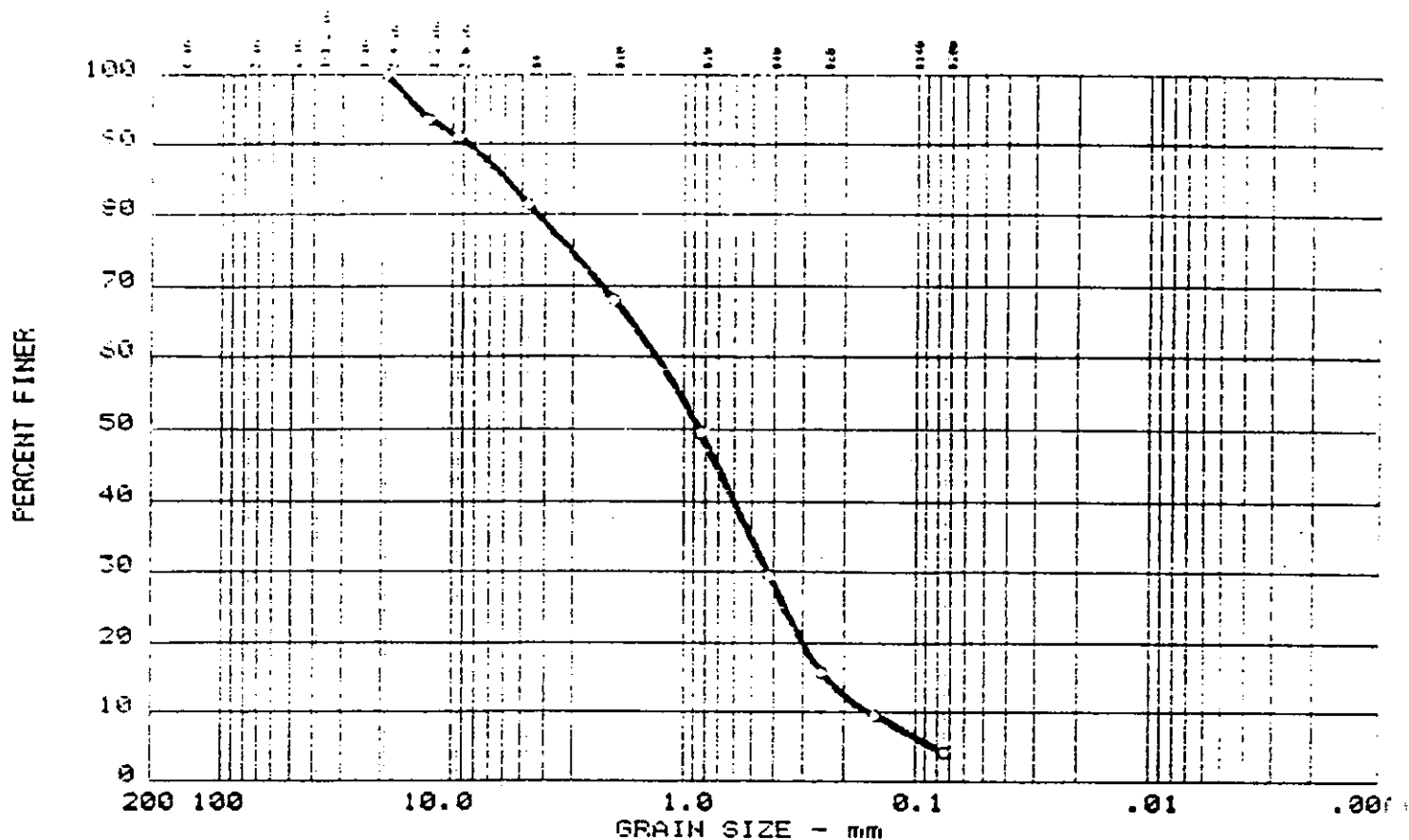
PROJECT NAME : N.Storonske Cooperage	BORING NUMBER: CB-13
DATE : 8/10/89	PROJECT NO. : 0852-13-1
CONTRACTOR : Empire Soils Invest.	LOCATION : Schodack, N.Y.
DRILL. METHOD: 4.25" I.D. H.S.A.	INSPECTOR : N.Thompson & A.Murtaugh
	SAMP. METHOD : Split spoon
SURFACE ELEV.: 356.65	DATUM : Ground level

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SAMPLE		SOIL DESCRIPTION		STR.	Field screening of split spoon with 11.7 Hnu
N- No.	Depth Value (ft.)	Density, color, SOIL, admixtures moisture, other, CONTAMINATION			
1	3	1-3 Lse-frn tan-br slt & f snd some f-m rnd-ang gvl, fiil, dry			0.0 PPME
2	6	5-7 Frn brn c snd, some f-m snd & slt some f-m ang-subrnd gvl, Outwash, dry			0.0 PPME
3	23	9-11 Lse brn f-m snd w/ang-rnd gvl, slt, Outwash, dry			0.0 PPME
4	10	11-13 Same as above, abundant gvl, dry			0-4.0 PPME
5	41	13-15 No recovery			
6	16	15-17 Lse brn c snd w/gvl, some slt & f snd, Outwash, moist-wet			

Competent bedrock at 19.7 as
determined by hollow stem augers.
Note: Till found on bottom of augers.

GRAIN SIZE DISTRIBUTION TEST REPORT



Test	%+3"	% GRAVEL	% SAND	% SILT	% CLAY
9	0.0	18.6	77.2	4.2	

LL	PI	D ₈₅	D ₆₀	D ₅₀	D ₃₀	D ₁₅	D ₁₀	C _c	C _u
		5.96	1.30	0.85	0.427	0.2399	0.1567	0.89	8.3

MATERIAL DESCRIPTION	USCS	AASHTO
o Brown SAND, little gravel, trace silt	SP	

Project No.: AT-89-363
 Project: STORONSKE COOPERAGE CO. INC. EAST GREENBUSH
 o Location: 18A (CB) - SAMPLE DEPTH = 1-3 ft

Date: 01-18-90

GRAIN SIZE DISTRIBUTION TEST REPORT
 EMPIRE SOILS INVESTIGATIONS, INC.



Remarks:
 CLIENT: MALCOLM PIRNIE

LAB. NO. 238.009

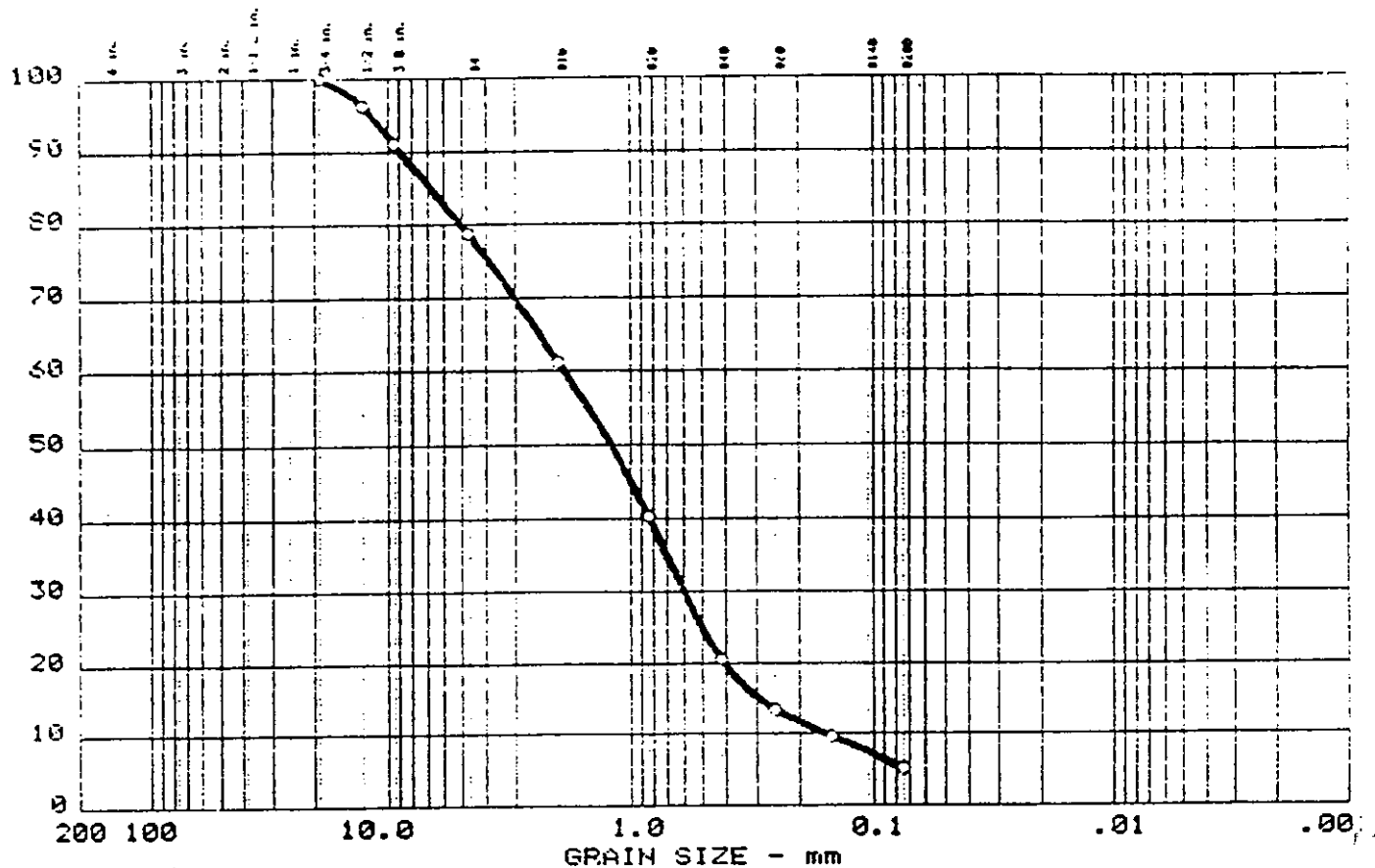
Fig. No.

PROJECT NAME : N.Storonske Cooperage	BORING NUMBER: CB-17
DATE : 8/7/89	PROJECT NO. : 0852-13-1
CONTRACTOR : Empire Soils Invest.	LOCATION : Schodack, N.Y.
DRILL. METHOD: 4.25" I.D. H.S.A.	INSPECTOR : N.Thompson & A.Murtaugh
	SAMP. METHOD : Split spoon
SURFACE ELEV.: 354.47	DATUM : Ground level

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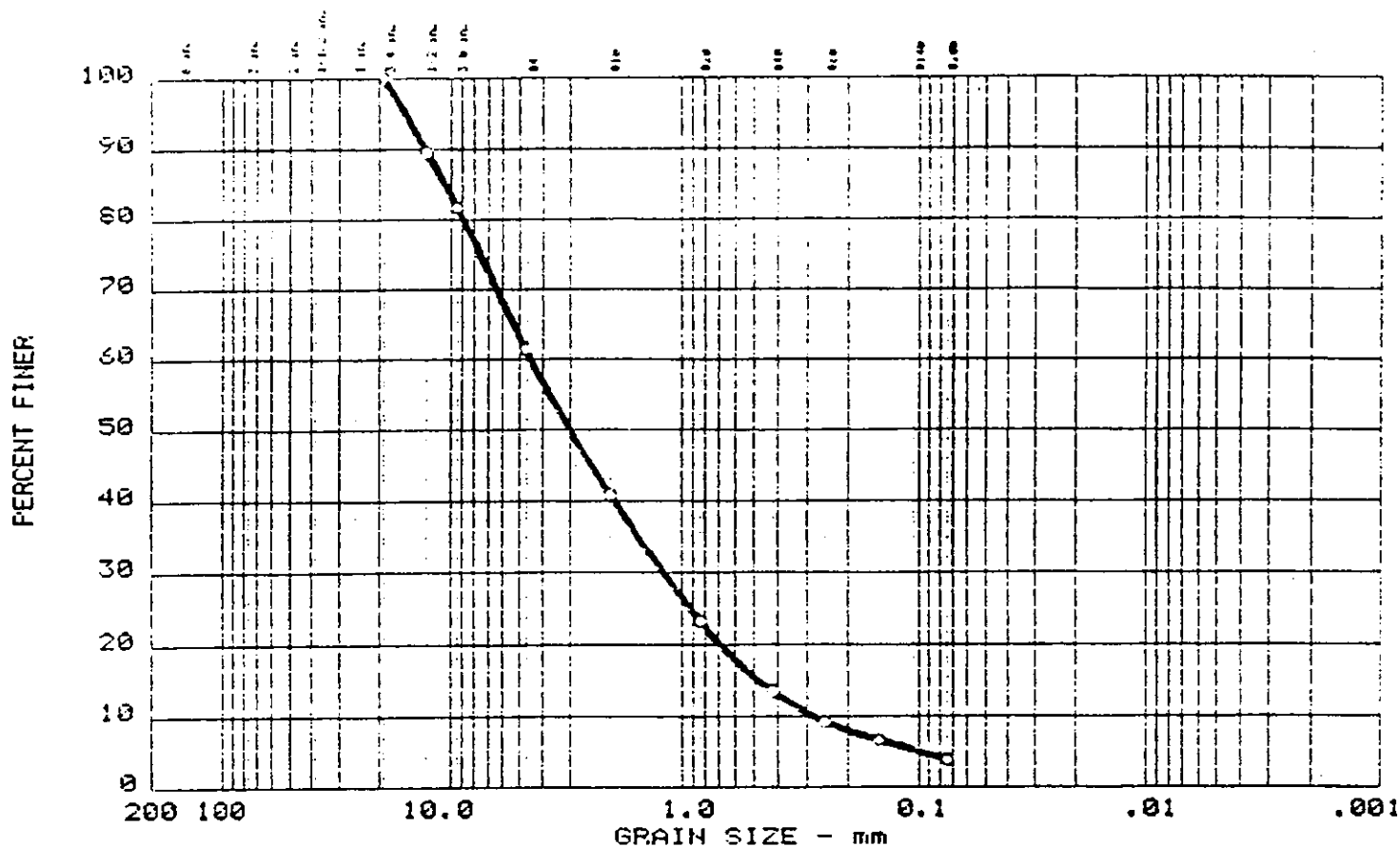
SAMPLE		SOIL DESCRIPTION		STR.	Field screening of split spoon with 11.7 Hnu
No.	N- Value	Depth (ft.)	Density, color, SOIL, admixtures moisture, other, CONTAMINATION		
1	3	1-3	Lse brn f-c snd w/slt & f-c gvl Fill, dry		11.0 PPME
2	12	5-7	Lse brn f-c snd, slt, ang gvl, Fill, dry		6.0 PPME
3	17	11-13	Lse brn m-c snd w/slt & gvl Outwash, dry		
4	37	19-21	Hd grn tan slt matrix w/f-c snd, sh frags, Till, dry		
Competent bedrock at 22.4' as determined by hollow stem augers.					

PERCENT FINER

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Project No.: AT-89-363	Remarks:
Project: STORONSKE COOPERAGE CO.INC. EAST GREENBUSH	CLIENT: MALCOLM PIRNIE
o Location: 17A / 17B(CB)- SAMPLE DEPTH A:1-3ft B:5-7ft	
Date: 01-18-90	LAB. NO. 288.006
GRAIN SIZE DISTRIBUTION TEST REPORT	
EMPIRE SOILS INVESTIGATIONS, INC.	Fig. No.

GRAIN SIZE DISTRIBUTION TEST REPORT



Test	%+3"	% GRAVEL	% SAND	% SILT	% CLAY
7	0.0	38.5	57.6	3.0	

LL	PI	D ₈₅	D ₆₀	D ₅₀	D ₃₀	D ₁₅	D ₁₀	C _c	C _u
		10.72	4.51	3.01	1.199	0.4775	0.2812	1.14	18.0

MATERIAL DESCRIPTION	USCS	AASHTO
o Brown SAND & GRAVEL, trace silt	SW	

Project No.: AT-89-363
 Project: STORONSKE COOPERAGE CO. INC. EAST GREENBUSH
 o Location: 17C (CB) - SAMPLE DEPTH = 11-13 ft

Date: 01-18-90

GRAIN SIZE DISTRIBUTION TEST REPORT
EMPIRE SOILS INVESTIGATIONS, INC.


Remarks:
 CLIENT: MALCOLM PIRNIE

LAB. NO. 288.007

Fig. No.


PROJECT NAME : N.Storonske Cooperage	BORING NUMBER: CB-21
DATE : 8/14/89	PROJECT NO. : 0852-13-1
CONTRACTOR : Empire Soils Invest.	LOCATION : Schodack, N.Y.
DRILL. METHOD: 4.25" I.D. H.S.A.	INSPECTOR : N.Thompson & A.Murtaugh
	SAMP. METHOD : Split spoon
SURFACE ELEV.: 354.88	DATUM : Ground level

=====

SAMPLE		SOIL DESCRIPTION		Field screening of split spoon with STR. 11.7 Hnu
No.	N- Value	Depth (ft.)	Density, color, SOIL, admixtures moisture, other, CONTAMINATION	
1	11	1-3	Frm brn slt w/ c snd gvl,pooly srt Fill,dry	
2	20	5-7	Lse brn c snd w/ang-rnd gvl,some f snd & slt,Outwash,dry	
3	100/.412-14		Boulder,no recovery	
4	20	15-17	Frm gry-brn c snd,f-m gvl w/slt Outwash,moist-wet	
5	43	18-20	Stf-hd grn-brn slt w/snd & gvl Till,wet	
6	100/.3	20- 20.8	Same as above,Till,wet	
Competent bedrock at 20.8' as determined by split spoon.				




PROJECT NAME : N.Storonske Cooperage
 DATE : 8/3/89
 CONTRACTOR : Empire Soils Invest.
 DRILL. METHOD: 4.25" I.D. H.S.A.
 BORING NUMBER: CB-22
 PROJECT NO. : 0852-13-1
 LOCATION : Schodack, N.Y.
 INSPECTOR : N.Thompson & A.Murtaugh
 SAMP. METHOD : Split spoon
 SURFACE ELEV.: 352.56
 DATUM : Ground level

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SAMPLE		SOIL DESCRIPTION			STR.	Field screening of split spoons with 11.7 Hnu
No.	N- Value	Depth (ft.)	Density, color, SOIL, admixtures moisture, other, CONTAMINATION			
1	13	1-3	Frm brn-gry slt,snd,f-m ang gvl, Fill,dry			
2	70	5-7	Lse brn slt w/f-c snd,some f ang gvl,Fill,dry		1.0 PPME	
3	16	7-9	7-8' same as above 8-9' Lse-frn brn c snd w/ f-c ang gvl,Outwash,dry		1.2 PPME	
4	20	11-13	Stf-hd grn brn slt & snd matrix w/ ang-rnd f gvl,Outwash,dry			
5	14	13-15	Lse gry brn c snd w/some f snd & f ang gvl,Outwash,dry		0.0 PPME	
6	75	18-20	No recovery			
7	30	20-22	Frm tan-lt brn f.snd & slt matrix ltl cl,some f gvl,Till, moist-wet			
			Competent bedrock at 21' as determined by split spoon			


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PROJECT NAME : N.Storonske Cooperage		BORING NUMBER: CB-23
DATE : 8/1/89	PROJECT NO. : 0852-13-1	
CONTRACTOR : Empire Soils Investigati	LOCATION : Schodack, N.Y.	
DRILL. METHOD: 4.25" I.D. H.S.A.	INSPECTOR : N.Thompson & A.Murtaugh	
	SAMP. METHOD : Split spoon	
SURFACE ELEV.: 353.30	DATUM : Ground level	

SAMPLE		SOIL DESCRIPTION			STR.	Well Construction
No.	N-Value	Depth (ft.)	Density, color, SOIL, admixtures moisture, other, CONTAMINATION			
1	4	2-4	Frm br slt w/some f-c snd,f ang-rnd gvl,Fill,moist			
2	12	4-6	Frm brn slt w/f-c snd,some f-m ang gvl,dry-moist,Fill			
3	68	8-10	Frm brn slt,snd,c ang gvl,Fill			
4	24	10-12	Lse -frm brn f-c snd matrix w/f-c ,ang-rnd gvl,Fill			
5	84	14-16	14-15' Tan-brn slt & snd w/f-c ang gvl,dry 15-16' Stf slt,snd matrix w/m rnd gvl tr cl,Till,moist			
6	50	16-17.8	Frm grn slt w/sh frags,moist-wet Till			
						

Competent bedrock at 17.8' as determined by split spoon

PROJECT NAME : N.Storonske Cooperage	BORING NUMBER: CB-24
DATE : 8/8/89	PROJECT NO. : 0852-13-1
CONTRACTOR : Empire Soils Investigati	LOCATION : Schodack, N.Y.
DRILL. METHOD: 4.25" I.D. H.S.A.	INSPECTOR : N.Thompson & A.Murtaugh
	SAMP. METHOD : Split spoon
SURFACE ELEV.: 354.92	DATUM : Ground level

SAMPLE		SOIL DESCRIPTION		STR.	Field screening of split spoon with 11.7 Hnu
No.	N-Value	Depth (ft.)	Density, color, SOIL, admixtures moisture, other, CONTAMINATION		
1	6	2-4	Lse dk brn-blk silt, sand, gravel, Fill, moist		
2	5	4-6	Sft lt tan-brn clay silt w/few pebbles Fill, moist-wet		7.0 PPME
3	10	8-10	Sft-firm grn-brn clay silt w/rock frags, Fill, moist		7.4 PPME
4	8	14-16	Sft-firm grn gry silt, sand, clay, w/some gravel, v poorly sorted, Outwash moist-wet		5 PPME
Competent bedrock at 23.2' as determined by hollow stem auger.					

