

DATE
 STARTED 5-16-88
 FINISHED 5-17-88
 SHEET 1 OF 2



SUBSURFACE LOG

HOLE NO. GMW-3
 SURF. ELEV. _____
 G. W. DEPTH See Note #1

PROJECT Monitor Well Installation

LOCATION Kingsbury Landfill

| DEPTH | SAMPLES | SAMPLE NO | BLOWS ON SAMPLER | | | | BLOW ON CASING C | SOIL OR ROCK CLASSIFICATION | NOTES |
|-------|---------|-----------|------------------|------|-------|-----|---|---|-------|
| | | | 0-6 | 6-12 | 12-18 | N | | | |
| 0 | | 1 | 1 | 1 | | 3 | Brown fine to medium SAND | Note #1: At completion of boring, a 2" PVC groundwater monitor well was installed per the attached "Monitor Well Detail" sheet. Note #2: WOH - indicates split spoon advanced six (6) inches by weight of drill rods and 140 lb. hammer. WOR - indicates split spoon advanced six (6) inches by weight of drill rods alone. | |
| | | 2 | 2 | 2 | | 6 | | | |
| | | 3 | 4 | 5 | | 8 | | | |
| 5 | | 4 | 4 | 5 | | 10 | -becomes wet | | |
| | | 5 | 3 | 3 | | 7 | | | |
| 10 | | 6 | 2 | 1 | | 4 | -grades Some Silt | | |
| | | 7 | 2 | 1 | | 3 | | | |
| | | 8 | 1 | WOH | | WOH | Gray CLAY | | |
| 15 | | 9 | 6 | 7 | | 14 | | | |
| | | 10 | 6 | 11 | | 21 | -grades CLAY and SILT, with seams of fine sand | | |
| 20 | | 11 | WOR | WOR | | 1 | -grades SILT and fine SAND | | |
| | | 12 | 3 | 3 | | 7 | | | |
| 25 | | 13 | 1 | 1 | | 3 | -grades gray SILT and CLAY, with seams of fine sand | | |
| | | 14 | 3 | 4 | | 7 | | | |
| | | 15 | 5 | 2 | | 6 | | | |
| 30 | | 16 | 2 | 2 | | 4 | | | |
| | | 17 | 3 | 1 | | 4 | | | |
| 35 | | 18 | 3 | 3 | | 6 | | | |
| | | 19 | 5 | 3 | | 7 | | | |
| | | 20 | 2 | 4 | | 8 | | | |
| 40 | | | 4 | 5 | | | | | |

N = No blows to drive 2 " spoon 12 " with 140 lb. pin wt. falling 30 "per blow. CLASSIFICATION Visual by

C = No blows to drive _____ " casing _____ " with _____ lb. weight falling _____ "per blow. Driller

METHOD OF INVESTIGATION 4 1/2" I.D. Hollow Stem Auger

DATE
 STARTED 5-16-88
 FINISHED 5-17-88
 SHEET 2 OF 2



SUBSURFACE LOG

HOLE NO. GMW-3
 SURF. ELEV. _____
 G. W. DEPTH _____

PROJECT Monitor Well Installation LOCATION Kingsbury Landfill

| DEPTH | SAMPLE NO | BLOWS ON SAMPLER | | | | BLOW ON CASING C | SOIL OR ROCK CLASSIFICATION | NOTES |
|-------|-----------|------------------|------|-------|-----|------------------|-----------------------------|-------|
| | | 0-6 | 6-12 | 12-18 | N | | | |
| 40 | 21 | WOH | 1 | | 3 | | | |
| | 2 | | 1 | | | | | |
| | 22 | 2 | 1 | | 2 | | | |
| | 1 | 1 | | | | | | |
| 45 | 23 | WOH | WOH | | WOH | | | |
| | | WOH | 1 | | | | | |
| | 24 | 1 | 2 | | 5 | | | |
| | | 3 | 3 | | | | | |
| | 25 | WOH | 3 | | 6 | | | |
| | | 3 | 3 | | | | (Wet-Very Soft to Medium) | |
| 50 | | | | | | | END OF BORING @ 50.0' | |
| 55 | | | | | | | | |

N = No blows to drive 2 " spoon 12 " with 140 lb. pin wt. falling 30 " per blow. CLASSIFICATION Visual by

C = No blows to drive _____ " casing _____ " with _____ lb. weight falling _____ " per blow. Driller

METHOD OF INVESTIGATION 4 1/2" I.D. Hollow Stem Auger

DATE

STARTED 5-17-88FINISHED 5-17-88SHEET 1 OF 1

SUBSURFACE LOG

HOLE NO. GMW-4

SURF. ELEV. _____

G. W. DEPTH See Note #1PROJECT Monitor Well InstallationLOCATION Kingbury Landfill

| DEPTH | SAMPLES | SAMPLE NO | BLOWS ON SAMPLER | | | | BLOW ON CASING C | SOIL OR ROCK CLASSIFICATION | NOTES |
|-------|---------|-----------|------------------|------|-------|----|---|--|-------|
| | | | 0-5 | 5-12 | 12-18 | N | | | |
| 0 | ✓ | 1 | 1 | 1 | | 3 | Brown fine to medium SAND | Note #1: At completion of boring, a 2" PVC groundwater monitor well was installed per the attached "Monitor Well Detail" sheet. | |
| | | 2 | 1 | | | | | | |
| | ✓ | 2 | 2 | 2 | | 3 | | | |
| | | 1 | 2 | | | | | | |
| 5 | ✓ | 3 | 3 | 4 | | 6 | -grades Some Silt, becomes wet | | |
| | | 2 | 2 | | | | | | |
| | ✓ | 4 | 2 | 3 | | 6 | | | |
| | | 3 | 3 | | | | | | |
| | ✓ | 5 | 6 | 5 | | 11 | -clay seams noted (Moist to Wet-Loose to Firm) | | |
| | | 6 | 6 | | | | | | |
| 10 | ✓ | 6 | 6 | 4 | | 11 | Brown SILT and CLAY | | |
| | | 7 | 7 | | | | | | |
| | ✓ | 7 | 8 | 5 | | 11 | | | |
| | | 6 | 8 | | | | | | |
| 15 | ✓ | 8 | 6 | 5 | | 11 | -seams of fine SAND noted | | |
| | | 6 | 8 | | | | | | |
| | ✓ | 9 | 4 | 3 | | 7 | -grades brown CLAY (Wet-Medium) | | |
| | | 4 | 4 | | | | | | |
| 20 | | | | | | | END OF BORING @ 18.0' | | |

N = No blows to drive 2 " spoon 12 " with 140 lb. pin wt. falling 30 " per blow. CLASSIFICATION Visual by

Driller

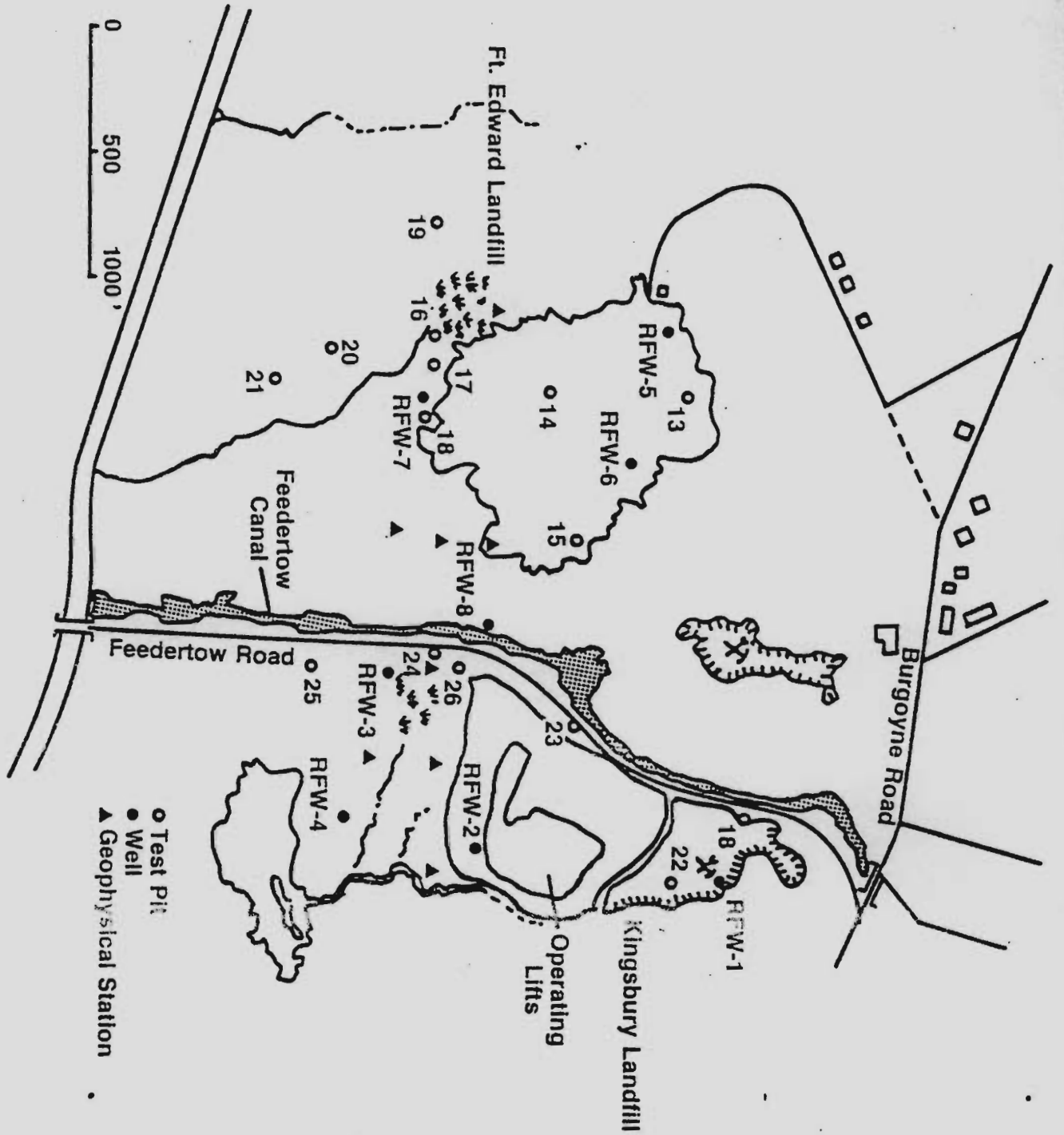


FIGURE 3A-12 GENERAL LOCATION MAP FT. EDWARD/KINGSBURY LANDFILL

RFW-3

| <u>Depth</u> | <u>Thickness</u> | <u>Description</u> |
|--------------|------------------|--|
| 0 - 20 | 20 | Light brown and gray clay |
| 20 | | Casing set with 10 feet of field slots |

RFW-4

| <u>Depth</u> | <u>Thickness</u> | <u>Description</u> |
|--------------|------------------|---|
| 0 - 20 | 20 | Blue-gray clay |
| 20 | | Set casing with 10 feet of field slots |

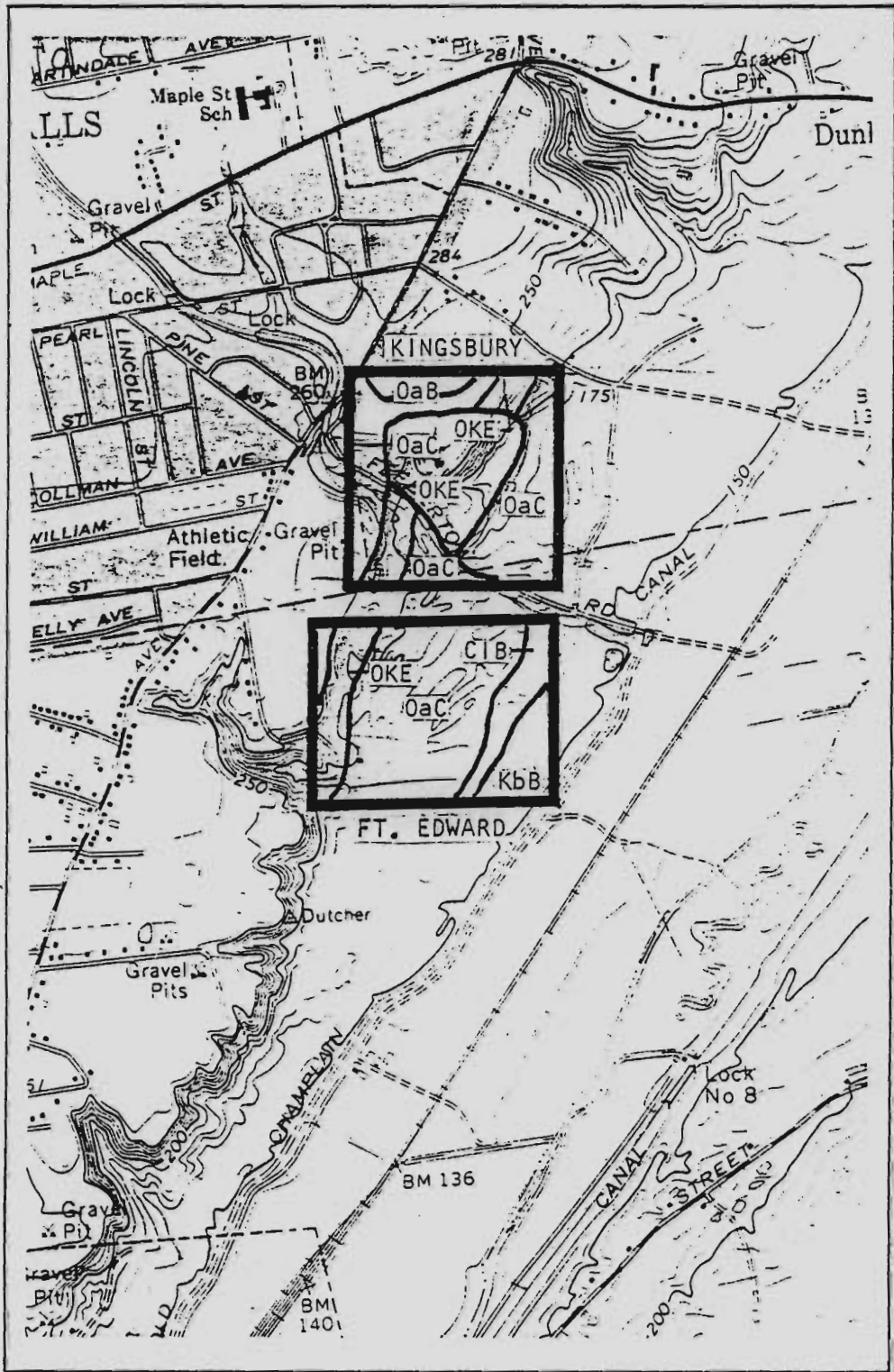


FIGURE 3A-13 DETAILED SOIL MAP OF FT. EDWARD/KINGSBURY LANDFILLS

E.C. JORDAN Co.

MW-90-14

| | | | | |
|--------------------------------------|---------------------|--------------------------------|---|---|
| Project KINGSBURY LANDFILL | | Site KINGSBURY, NEW YORK | | Project No. 6196-23 |
| Client NYSDEC | | Logged By LT | Checked By WGC | Ground Ele. 183.06 |
| Drilling Contractor MATHES | | Driller's Name S. KOVELESKY | Rig Type ATV | Start Date 11/29/90 |
| Drilling Method HOLLOW STEM AUGER | | Protection Level D DERMAL | P.I.D. (eV) 10.6 | Finish Date 11/29/90 |
| Soil Drilled 45.0' | Rock Drilled N/A | Total Depth 45.0' | Depth to Groundwater/Date 12.0' on 12/2/90 | Piez.Boring Well <input type="checkbox"/> <input type="checkbox"/> <input checked="" type="checkbox"/> |

| DEPTH (FEET) | SAMPLE NO. & PENETRATION / RECOVERY (FT) | SAMPLE TYPE | SPT BLOWS/6" OR CORE REC/RQD (%) | SPT-N (BLOWS/FT) | GRAPHIC LOG | SAMPLE DESCRIPTION | USCS GROUP SYMBOL | NOTES ON DRILLING | P. I. D. PPM | | WELL DIAGRAM | LAB TESTS |
|--------------|--|-------------|----------------------------------|------------------|-------------|---|-------------------|-------------------|---------------------|---------------------|--------------|-----------|
| | | | | | | | | | PI METER FIELD SCAN | PI METER HEAD SPACE | | |
| 0 - 2.0 | S-1 2.0/1.6 | [Pattern] | 1 1 2 6 | 3 | [Pattern] | Brown fine sandy <u>SILT</u> , little to trace organics, poorly-graded, non-plastic, very loose, moist (0.0' - 0.2') -TOPSOIL- Brown fine <u>SAND</u> , little to trace silt, poorly-graded, non-plastic, very loose, moist (0.2' - 0.8'), with brown silty clay lense with trace fine sand 0.8' - 1.3' -GLACIOLACUSTRINE- | ML SP SP | | BKG 2.3 | [Diagram] | | |
| 5 - 6.6 | S-2 2.0/1.8 | [Pattern] | 4 6 11 12 | 17 | [Pattern] | Brown fine <u>SAND</u> , little silt, poorly-graded, non-plastic, medium dense, wet, with clayey silt lenses (1/8" - 1/16") at 5.8', 6.0', and 6.6', color change to rust brown 6.4' - 6.6' -GLACIOLACUSTRINE- | SP | | BKG 3.6 | [Diagram] | | |
| 10 - 11.6 | S-3 2.0/1.5 | [Pattern] | 1 2 4 4 | 6 | [Pattern] | Brown fine <u>SAND</u> , some silt, poorly-graded, non-plastic, loose, saturated, rust brown pocket at 10.4', with gray silty clay lenses (1/8" - 1/4" at 11.2' and 11.6') -GLACIOLACUSTRINE- | SP-SM | | BKG 3.9 | [Diagram] | | |
| 15 - 16.6 | S-4 2.0/1.3 | [Pattern] | 2 4 8 16 | 12 | [Pattern] | Brown fine <u>SAND</u> , little to some silt, poorly-graded, non-plastic, medium dense, saturated (15.0' - 15.5') -GLACIOLACUSTRINE- | SP-SM | | BKG 4.6 | [Diagram] | | |
| 16.6 - 18.0 | S-5 2.0/1.2 | [Pattern] | 5 8 18 18 | 26 | [Pattern] | Gray fine <u>SAND</u> , little silt, poorly-graded, non-plastic, medium dense, saturated, with 1/16" brown silty clay lense at 18.0' -GLACIOLACUSTRINE- | SP | | BKG 3.2 | [Diagram] | | |
| 18.0 - 19.8 | S-6 | [Pattern] | 5 6 | 16 | [Pattern] | Gray fine <u>SAND</u> , little to some silt, poorly-graded, non-plastic, medium dense, saturated, silty from 19.8' | SP | | BKG 7.6 | [Diagram] | | |

E.C. JORDAN Co.

MW-90-14

Project

KINGSBURY LANDFILL

Site

KINGSBURY, NEW YORK

Project No.

6196-23

| DEPTH (FEET) | SAMPLE NO. & PENETRATION / RECOVERY (FT) | SAMPLE TYPE | SPT BLOWS/8" OR CORE REC/RQD (%) | SPT-N (BLOWS/FT) | GRAPHIC LOG | SAMPLE DESCRIPTION | USCS GROUP SYMBOL | NOTES ON DRILLING | P. I. D. PPM | | WELL DIAGRAM | LAB TESTS |
|--------------|--|-------------|----------------------------------|------------------|-------------|---|-------------------|-------------------|---------------------|---------------------|--------------|-----------|
| | | | | | | | | | PI METER FIELD SCAN | PI METER HEAD SPACE | | |
| | | | | | | | | | | | | |
| | 2.0/1.5 | | 10 13 | | | - 20.0', with 1/4" - 1/8" brown silty clay lense at 20.0' -GLACIOLACUSTRINE- | | | | | | |
| | S-7 2.0/0.9 | | 4 9 12 15 | 21 | | Brown fine SAND, little silt, poorly-graded, non-plastic, medium dense, saturated, with rust brown and gray streaks, silty zone 21.0' - 21.2' -GLACIOLACUSTRINE- | SP | | BKG | 9.3 | | |
| | S-8 2.0/1.0 | | 5 9 12 23 | 21 | | Brown fine SAND, little silt, poorly-graded, non-plastic, medium dense, saturated, with rust brown and gray streaks -GLACIOLACUSTRINE- | SP | | BKG | 7.5 | | |
| 25 | S-9 2.0/1.6 | | 6 10 16 14 | 26 | | Gray fine SAND, little to some silt, poorly-graded, non-plastic, medium dense, saturated, with silty clay lenses up to 1", stratified -GLACIOLACUSTRINE- | SP-SM | | BKG | 21.0 | | |
| | S-10 2.0/1.2 | | 5 7 15 26 | 22 | | Gray fine SAND, little to some silt, poorly-graded, non-plastic, medium dense, saturated, stratified -GLACIOLACUSTRINE- | SP-SM | | BKG | 5.6 | | |
| 30 | S-11 2.0/1.5 | | 9 9 16 20 | 25 | | Gray fine SAND, little to some silt, poorly-graded, non-plastic, medium dense, saturated, with silty clay lenses up to 1", stratified -GLACIOLACUSTRINE- | SP-SM | | BKG | 6.1 | | |
| | S-12 2.0/1.4 | | 10 15 25 31 | 40 | | Gray fine SAND, little to some silt, poorly-graded, non-plastic, dense, saturated, with silty clay lenses up to 1", stratified -GLACIOLACUSTRINE- | SP-SM | | BKG | 3.7 | | |
| | S-13 2.0/2.0 | | 13 11 15 19 | 26 | | Gray fine SAND, little to some silt, poorly-graded, non-plastic, dense, saturated, with silty clay lenses up to 1", stratified -GLACIOLACUSTRINE- | SP-SM | | BKG | 7.0 | | |
| 35 | S-14 2.0/2.0 | | 6 4 4 6 | 8 | | Gray fine SAND, little to some silt, poorly-graded, non-plastic, loose, saturated, with silty clay lenses up to 1", stratified -GLACIOLACUSTRINE- | CL | | BKG | 3.7 | | |
| | S-15 2.0/2.0 | | 2 2 3 3 | 5 | | Gray silty CLAY, poorly-graded, slightly-plastic, firm, saturated, with silty fine sand lenses 1/8" every 1" -GLACIOLACUSTRINE- | CL | | BKG | 7.1 | | |
| | S-16 2.0/2.0 | | 3 4 5 6 | 9 | | Gray silty CLAY, poorly-graded, slightly-plastic, soft to firm, saturated, with silty fine sand lenses 1/8" every 1" -GLACIOLACUSTRINE- | CL | | BKG | 5.2 | | |
| 40 | S-17 2.0/2.0 | | 5 4 6 6 | 10 | | Gray silty CLAY, poorly-graded, slightly-plastic, firm, saturated, with vertical silty fine sand lenses observed throughout sample -GLACIOLACUSTRINE- | CL | | BKG | 6.3 | | |
| | S-18 2.0/2.0 | | 2 2 2 4 | 4 | | Gray silty CLAY, poorly-graded, slightly-plastic, soft, saturated, with occasional silty fine sand lenses less than 1/16" every 1" - 2" -GLACIOLACUSTRINE- | CL | | BKG | 7.8 | | |

ENGINEERING REPORT

KINGSBURY SITE REMEDIAL PROGRAM

JULY 1990

**BLASLAND & BOUCK ENGINEERS, P.C.
6723 TOWPATH ROAD
SYRACUSE, NEW YORK 13214**

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TABLES

Table 1 - Kingsbury Site Contract Modifications

FIGURES

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- Figure 2 - Ground-Water Cutoff Wall Profile Record Drawing 0+00-6+00
(RD-1)
- Figure 3 - Ground-Water Cutoff Wall Profile Record Drawing 6+00-12+00
(RD-2)
- Figure 4 - Ground-Water Cutoff Wall Profile Record Drawing 12+00-18+00
(RD-3)
- Figure 5 - Ground-Water Cutoff Wall Profile Record Drawing 18+00-23+80
(RD-4)
- Figure 6 - Ground-Water Cutoff Wall Profile Record Drawing 23+80-34+40
(RD-5)

APPENDICES

- Appendix A - Material and Performance Specifications
- Appendix B - Field and Laboratory Test Results
- Appendix C - Monitoring and Relief Well Details
- Appendix D - Certificate of Substantial Completion

SECTION 1 - ENGINEERING REPORT

1.1 Introduction

This Engineering Report presents a summary of the construction services provided by Blasland & Bouck Engineers, P.C. (Blasland & Bouck), during the Kingsbury Site Remedial Program. This report also presents: 1) a listing of all contract modifications and associated costs incurred to date during construction of the Kingsbury site cap and ground-water cutoff wall; 2) a compilation of pertinent technical Quality Assurance/Quality Control (QA/QC) data for the landfill cap and ground-water cutoff wall; and 3) "as-built" drawings of the capped landfill and the installed monitoring wells and relief wells. The purpose of this report is to document the construction activities associated with implementation of the Remedial Program.

The Kingsbury Site includes a former landfill covering approximately 18 acres and is located in the village of Hudson Falls, New York. The contents of the landfill are reported to be municipal waste and a quantity of industrial waste which includes polychlorinated biphenyls (PCBs) and industrial solvents. Between 1987 and 1989, the Kingsbury Site underwent closure to isolate the landfill contents from the surrounding environment. Closure activities included the installation of a ground-water cutoff wall around the perimeter of the landfill and the placement of a low-permeability compacted soil cap over the entire 18-acre area.

1.2 Construction Services

In accordance with the Agreement for Engineering Services dated March 26, 1986, between the Owner [New York State Department of Environmental Conservation (NYSDEC)] and the Engineer [Blasland & Bouck], Blasland &

Bouck provided construction-related engineering services during the implementation of the Remedial Program at the Kingsbury Site. In general, the primary services performed by Blasland & Bouck during construction of the Remedial Program were field and office services.

1.2.1 Field Services

The field services provided by Blasland & Bouck during implementation of the Remedial Program included: 1) setting control lines and elevations; 2) reviewing all contractor submittals; 3) providing an on-site observer during construction; and 4) providing a geologist during the installation of the ground-water cutoff wall. The purpose of these services was to ensure that remedial activities were performed in accordance with the Contract Documents dated August 1986 for construction of the landfill cap and cutoff wall.

A summary of cutoff-wall quality assurance testing standards and the specifications followed by the Contractor during cap and cutoff wall construction have been included in Appendix A. The results of field and laboratory testing of the cap material, the cutoff wall slurry, and the cutoff wall backfill are presented in Appendix B.

1.2.2 Office Services

During cap and cutoff wall construction, events occurred which necessitated modifications to the original contract between the Owner and the Contractor [Yolam Construction, Inc., of Loudonville, New York]. In accordance with the Agreement for Engineering Services, Blasland & Bouck prepared contract modifications and cost estimates for these modifications. The overall cost impact of the modifications on the original contract is discussed in Section 1.4 - Contract Modification

Analysis. Contract modifications and their associated costs are summarized in Table 1.

1.2.3 Drawings

A record drawing depicting a plan view of the project site has been prepared in accordance with the Agreement for Engineering Services and is presented in Figure 1. Record drawings showing ground-water cutoff wall profiles are presented in Figures 2 through 6. Installation details of monitoring wells and relief wells (installed by a subcontractor, Empire Soils Investigations, Inc., of Albany, New York) are included in Appendix C.

1.3 Additional Construction Activities

During the construction phase of the Kingsbury Site Remedial Program, additional construction activities were necessary due to site conditions and requirements by the New York State Department of Transportation (NYSDOT). The following paragraphs provide a summary of each additional construction activity.

1.3.1 Additional Ground-Water Cutoff Wall Area

It was determined during construction of the ground-water cutoff wall that what was previously considered to be a significant clay stratum, based on a hydrogeologic investigation of the site performed by O'Brien & Gere Engineers, Inc., of Syracuse, New York (as specified in a February 1983 report for the General Electric Company), was actually an intermittent clay lense between wall stations 1+25 and 6+45. Therefore, the contractor was required to return to previously constructed sections of the cutoff wall and re-excavate to greater depths using a crane and clamshell. The additional excavation was necessary to obtain the

specified clay key invert for the cutoff wall. Subsequently, additional soil/bentonite was required to construct the cutoff wall to the deeper invert.

1.3.2 Construct Access Road Extension/Backfill Canal Lock No. 5

In a letter from NYSDEC dated December 9, 1986, Blasland & Bouck was informed of NYSDOT's request for access to the Glens Falls Feeder Canal for its maintenance equipment. To fulfill this request, the construction of an access road extension along the western section of the project site perimeter was required. The access road extension connected the previously designed northern, eastern, and southern access road sections, producing a continuous loop around the project site. The extension consists of a 20-foot wide clear section outside the site security fence which contains a 12-foot wide driving surface. The construction of the access road extension necessitated the modification of proposed final grade lines around the existing stone walls of historical Canal Lock No. 5 in the southwestern corner of the site. Modifications were required to protect the lock walls during the placement of backfill within the canal area. In addition, the drainage ditch on the western edge of the site was rerouted to avoid interference with the lock walls and to accommodate the access road installation.

1.3.3 Landfill Ground-Water Seepage Collection and Treatment

After completion of the ground-water cut-off wall, a ground-water seep area appeared within ten feet to the inside of the completed cutoff wall, between wall stations 1+00 and 6+00. To reduce the ground-water elevation within the landfill, a trench/drain system was installed during October and November 1988, along the seep area. The trench/drain system (designated the deep drain) consists of a six-inch diameter,

perforated, plastic pipe encapsulated with granular fill and filter fabric. The pipe is installed at elevation 190 (approximately 12 to 17 feet below the top of the cutoff wall) and slopes to a 6'- 6" diameter deep drain manhole.

Ground water collected by the deep drain system was pumped to a Temporary Leachate Treatment System (TLTS). The intent of the TLTS was to reduce/control the ground-water elevation within the landfill and prevent seepage of ground water over the cutoff wall. The TLTS was put into operation on March 6, 1989, and the process consisted of aeration, clarification, solids filtration, and carbon filtration to remove metals, volatile organics, and PCBs. Shortly thereafter, a flocculant feed system was installed to augment the solids settling in the clarifier. In addition, as per a NYSDEC request during the second week of April 1989, a second trench/drain system (designated as the shallow drain) was installed between April 24 and April 28, 1989, at elevation 198 (approximately 4 to 11 feet below the top of the cutoff wall). Piping for this system was "plowed in" and consisted of a six-inch diameter, flexible, perforated plastic pipe in a fabric sleeve. The shallow drain was installed to obtain better water quality in the TLTS influent, and on May 1, 1989, the shallow drain system was put in operation.

Based on a meeting on August 21, 1989, between NYSDEC and Blasland & Bouck, the existing TLTS was redesignated as the Interim Leachate Treatment System (ILTS). In January through April 1990, modifications requested by NYSDEC were made to the ILTS, including installation of a flocculation tank with a slow mixer, installation of two additional bag filters, installation of two clarifier solids collection tanks and a clarifier solids transfer pump, upgrading of the existing filter feed

pumps, installation of telephone and potable water service to the ILTS, upgrading of the existing electrical supply, and the addition of a recycle system to pump ILTS effluent back to the landfill during start-up procedures. Additionally, a structure was built onto the existing ILTS building to house all process equipment in order to winterize the ILTS. The basis of design and start-up and operating instructions for the ILTS are presented in a separate document entitled "Operation and Maintenance Manual - Kingsbury Site Interim Leachate Treatment System" (Blasland & Bouck, July 1990).

1.3.4 Drainage Ditch

In order to improve drainage and reduce future site maintenance, an upper drainage swale, a mid-slope stone ditch and a drainage ditch adjacent to the access road, all connected by three down-spout swales, were installed. The drainage ditch is comprised of rip-rap and geotextile fabric. This drainage system also expedited the establishment of vegetative growth and thus reduced site erosion.

1.4 Contract Modification Analysis

The original contract price between the owner and contractor was \$5,774,125.00. To date, a total of 24 contract modifications have been initiated during the Kingsbury Site Remedial Program. Of the 24 contract modifications, 5 were initiated by the Owner, 11 by the Contractor, and 2 by the Engineer. Additionally, 3 modifications have been declared void and 3 are pending at the time of this report.

To date, the total cost of the contract modifications is \$1,702,601.88 bringing the total project cost to \$7,476,762.88. The modifications represent

a 29 percent increase in total project cost. The cost of modifications associated with each initiator is as follows:

| <u>Initiator</u> | <u>Total Number of Modifications</u> | <u>Total Cost of Modifications to Date</u> |
|------------------|--------------------------------------|--|
| Contractor | 11 | \$1,202,423.74 |
| Engineer | 2 | 149,392.14 |
| Owner | <u>5</u> | <u>350,786.00</u> |
| Subtotal | 18 | \$1,702,601.88 |
| Void | 3 | |
| Pending | <u>3</u> | |
| Total | 24 | |

1.5 Certificate of Substantial Completion

The Certification of Substantial Completion of Contract No. 1 is found in Appendix D.



Tables

TABLE 1
KINGSBURY SITE CONTRACT MODIFICATIONS

TABLE 1
KINGSBURY SITE CONTRACT MODIFICATIONS

| <u>Modification No.</u> | <u>Reason for Modification</u> | <u>Initiated By</u> | <u>Contractor's Proposal Price</u> | <u>Net Cost</u> |
|-------------------------|---|---------------------|------------------------------------|-----------------|
| 1 | <ul style="list-style-type: none"> a. Delete one permanent air-monitoring station and add two temporary air-monitoring stations to provide better coverage during construction. b. Additional fencing and generator to protect the additional temporary monitoring station. c. Maintenance costs for air-monitoring equipment can best be paid for on a time and material basis. | Owner | \$4,369.68 | \$4,369.68 |
| 2 | NYS DOT had requested, after time of bid, access to the canal for its maintenance equipment. This caused grade changes to the site and additional culverts, fencing, and ditch excavation. | Owner | \$141,365.32 | \$6,116.32 |
| 3 | A previously unknown refuse area was discovered by Contractor during construction operations. | Contractor | \$34,235.00 | \$34,235.00 |
| 4 | A previously unknown refuse area was discovered by Contractor during construction operations. | Contractor | \$18,886.51 | \$18,886.51 |
| 5 | VOID | | | |
| 6 | PENDING - Addition liability insurance premiums. | Contractor | | |
| 7 | Recent OSHA Regulations call for special employee training. | Contractor | \$23,829.73 | \$23,102.54 |
| 8 | Test borings required along center line of proposed ground-water cutoff wall to verify whether or not the top of the clay stratum was at the elevation anticipated. | Engineer | \$3,268.14 | \$3,268.14 |

TABLE 1
KINGSBURY SITE CONTRACT MODIFICATIONS

| <u>Modification No.</u> | <u>Reason for Modification</u> | <u>Initiated By</u> | <u>Contractor's Proposal Price</u> | <u>Net Cost</u> |
|-------------------------|--|---------------------|------------------------------------|-----------------|
| 9 | It was determined during construction of the cutoff wall that what was previously considered to be a significant clay stratum was actually a clay lense between Stations 1 + 25 to Stations 6 + 45. The Contractor was subsequently required to return to previously constructed sections of the cutoff wall and re-excavate to greater depths using the crane and clamshell method. The backhoe which was leading the excavation operation and crews related to excavation procedures (mixing, transporting, placing backfill material) incurred idle time due to reduction in excavation production. | Contractor | \$244,154.56 | \$72,199.82 |
| 10 | Additional excavation was necessary during construction of ground-water cutoff wall to obtain an acceptable clay key invert. | Engineer | \$146,124.00 | \$146,124.00 |
| 11 | Provide access for ground-water level monitoring within the ground-water cutoff wall. | Owner | \$10,300.00 | \$10,300.00 |
| 12 | VOID | | | |
| 13 | Temporary ground-water treatment system installation | Contractor | \$373,353.28 | \$360,568.33 |
| 14 | VOID | | | |
| 15 | As a result of extra work provided for in Modification No. 2 resultant Contractor Unit Price Item credits were anticipated because of a reduction in the area of the ground-water cutoff wall. However, after construction of the cutoff wall no area reduction was realized. | Owner | -- | \$107,000.00 |

TABLE 1
KINGSBURY SITE CONTRACT MODIFICATIONS

| <u>Modification No.</u> | <u>Reason for Modification</u> | <u>Initiated By</u> | <u>Contractor's Proposal Price</u> | <u>Net Cost</u> |
|-------------------------|--|---------------------|------------------------------------|-----------------|
| 16 | Installation of an upper drainage swale, a mid-slope stone ditch and a drainage ditch adjacent to the access road, all connected by three down-spout swales to improve site drainage, to expedite establishment of vegetative growth, and to reduce future site erosion. | Contractor | \$97,853.13 | \$97,765.43 |
| 17 | Necessary to stabilize drainage ditch, though the addition of rip-rap and geotextile because of site conditions. | Contractor | \$36,502.03 | \$37,332.20 |
| 18 | Installation and interim operation (12/14/88-5/31/89) of a Temporary Leachate Treatment System | Contractor | \$254,821.47 | \$254,821.46 |
| 19 | Continued interim operations of the Temporary Leachate Treatment System (6/1/89-9/30/89) | Contractor | \$129,795.53 | \$129,795.53 |
| 20 | PENDING - construction time extension. | | | |
| 21 | a. Regrading of existing subgrade, replacement and compaction of existing stockpiled clay and installation of HDPE geogrid b. Investigation/Repair of east clay cap c. Investigation/Repair of north clay cap | Contractor | \$17,421.44 | \$17,421.45 |
| 22 | Continued ILTS operation (10/1/89 - 12/31/89). | Owner | \$223,000.00 | \$223,000.00 |
| 23 | ILTS winterization and equipment modifications. | Contractor | \$303,512.45 | \$303,512.45 |
| 24 | PENDING - final contract estimated quantity variance. | | | |



Figures

FIGURE 1

KINGSBURY SITE REMEDIAL PROGRAM
RECORD DRAWING

FIGURE 2

GROUND-WATER CUTOFF WALL PROFILE
RECORD DRAWING 0+00+6+00 (RD-1)

FIGURE 3

GROUND-WATER CUTOFF WALL PROFILE
RECORD DRAWING 6+00-12+00 (RD-2)

FIGURE 4

GROUND-WATER CUTOFF WALL PROFILE
RECORD DRAWING 12+00-18+00 (RD-3)

FIGURE 5

GROUND-WATER CUTOFF WALL PROFILE
RECORD DRAWING 18+00-23+80 (RD-4)

FIGURE 6

GROUND-WATER CUTOFF WALL PROFILE
RECORD DRAWING 23+80-34+40 (RD-5)



Appendices

APPENDIX A

KINGSBURY SITE REMEDIAL PROGRAM
MATERIAL AND PERFORMANCE SPECIFICATIONS FOR:

- CUTOFF WALL QUALITY ASSURANCE TESTING
- EMBANKMENT MATERIAL - SECTION 02004
- CAP MATERIALS AND INSTALLATION - SECTION 02006
- GROUND-WATER CUTOFF WALL - SECTION 02007
- TOPSOIL AND SEEDING - SECTION 02008

KINGSBURY SITE REMEDIAL PROGRAM
SUMMARY OF CUTOFF WALL
QUALITY ASSURANCE TESTING STANDARDS

KINGSBURY SITE REMEDIAL PROGRAM
SUMMARY OF CUTOFF WALL QUALITY ASSURANCE TESTING

| <u>MATERIAL</u> | <u>TEST</u> | <u>METHOD OF TESTING</u> | <u>LOCATION</u> | <u>FREQUENCY</u> | <u>STANDARD</u> |
|---------------------|-----------------------|--------------------------------------|---|--|---------------------------------|
| Fresh Slurry | Viscosity | API Code, RP 13B | Discharge to Trench Holding Ponds | Hourly Twice/Day | ≥ 40 sec. ≥ 40 sec. |
| | Density | Same as Above. | Discharge to Trench and Holding Ponds | Twice/Day Twice/Day | 65 PCF 65 PCF |
| | Fluid Loss | Same as Above. | Holding Ponds | Twice/Day | 15 ML/100 PSI In 30 Minutes |
| Trench Slurry | Fluid Loss | Same as Above. | Top mid-point and 10 ft. from bottom at a location in the vertical plane of the toe of backfill. | Three/Day | 15 ML/100 PSI In 30 Minutes |
| | Density | Same as Above. | Same as Above. | | Minimum 65 PCF, See NOTE [3] |
| Backfill | Slump | ASTM 143-74 | Mixing Pad | Two /Batch [1] | 4-6 inches |
| | Unit Weight | API Code RP 13B | Mixing Pad [2] | Once/Batch [1] | 100 to 115 PCF |
| | Permeability: | | | | |
| | o Field | | | | |
| | Permeability | Filter press to be per specs. | Mixing Pad | Once/Day | See NOTE [2] |
| | o Offsite | | | | |
| Permeability | | In Lab | Once/3,000 cy | 1x10 ⁻⁷ cm/sec | |
| Sieve Analysis | ASTM C117-76, C136-76 | Mixing Pad | Once/2Batch[1] | Design Mix | |
| Moisture Content | ASTM 02216-80 | Mixing Pad | Once/Batch [1] | Design Mix | |
| TRENCH ALIGNMENT | HORIZONTAL | ESTABLISHED SURVEY BASE LINE | | ONCE PER DAY Every 10 lf along completed | |
| | VERTICAL | APPROVED DEPTH MEASUREMENT DEVICE | | trench bottom, observation and sampling of trench cuttings from bottom every 20 lf and samples preserved every 200 lf. | Min. 6ft. into clay. |

- NOTES: [1] One Batch = 200 to 300/cy.
[2] Field permeability standard shall be established in the laboratory using the design mix.
[3] 85 PCF start desanding, at 90 PCF stop backfilling operations.

**KINGSBURY SITE REMEDIAL PROGRAM
CONTRACT SPECIFICATIONS**

MATERIALS AND PERFORMANCE~~SILTY LOAM MATERIAL AND INSTALLATION - SECTION 02017~~*EMBANKMENT - SECTION 02004
(ADDENDUM No. 2 subpart J)*PART 1 - GENERAL

1.01 DESCRIPTION

A. Work Specified

1. Earth embankments shall be constructed to establish lines and grades at the locations shown on the Contract Drawings and as directed by the Engineer. Embankment materials shall be obtained from acceptable soils within the Contract Work Area or approved off-site sources.
2. Embankment materials shall be free from frost, stumps, trees, roots, sods, muck, marl, vegetable matter or other unsuitable material and shall be suitable for compaction as described in the following provisions.
3. Embankments shall be constructed to such elevations as to make allowance for any settlement that may occur.
4. The embankment material source(s) may require Mining Permit(s) prior to removal of any material. If required, all provisions of the Permit(s) shall be adhered to by the Contractor. If not required, all disturbed borrow areas shall be, at a minimum, graded and reseeded at the completion of the work.

B. Related Work Specified Elsewhere

1. Cap Materials and Installation: Section 02006
2. Topsoil and Seeding: Section 02008
3. Embankment: Section 02004

1.02 TESTING

- A. All soil compaction testing including field and laboratory services required for completion of this Contract shall be provided by the Contractor under supervision of the Engineer.

1.03 SUBMITTALS

- A. Source(s) of borrow materials
- B. Location(s) of spoil area(s)

PART 3 - EXECUTION

3.01 PLACEMENT AND COMPACTION

- A. Surfaces on which embankments are to be placed shall be compacted to the required density of the embankment prior to any fill being placed.
- B. Materials shall be placed in lifts not greater than 12 inches of thickness unless greater thicknesses are allowed by the Engineer upon demonstration by the Contractor that the materials and compaction efforts are adequate to obtain the required density.

MATERIALS AND PERFORMANCE

CAP MATERIALS AND INSTALLATION - SECTION 02006

PART 1 - GENERAL

1.01 DESCRIPTION

- A. Work Specified
Excavation, backfilling, and compacting include the loosening, removing, working, transporting, storage, fill and disposal of all cap materials necessary for construction of the cap, as shown or specified, or as directed by the Engineer.
- B. Related Work Specified Elsewhere
 - 1. Ground-water Cutoff Wall: Section 02007
 - 2. Topsoil and Seeding: Section 02008

1.02 TESTING

- A. All soil testing services necessary for the Contractor to obtain an approved cap material shall be provided by the Contractor. All cap density testing including field and laboratory services required during cap installation shall be provided by the Contractor under the supervision of the Engineer.
- B. Each lift of cap material that is placed and compacted shall be tested for density and moisture content at a minimum of four tests per acre. No lift of cap material shall be covered by subsequent lifts without the Engineer's prior approval.

1.03 SUBMITTALS

- A. Source of borrow materials with final grading plans.
- B. Location of spoils area(s).
- C. Proposed soils testing laboratory.
- D. Laboratory certification of the capping material as specified herein.

PART 2 - PRODUCTS

2.01 CAP MATERIAL

- A. Capping material shall be obtained from a source approved by the Engineer.
- B. The capping material shall have a remolded saturated hydraulic conductivity (permeability) of a maximum of 1×10^{-7} cm/sec (0.0000001 cm/sec) as identified by laboratory permeability tests using triaxial apparatus with backpressure. A minimum of three (3) such permeability tests shall be required on representative samples taken from each borrow area. The compactive effort required on the soils prior to conducting the permeability tests shall be equivalent to a minimum of 90 percent of the maximum density achieved during the modified proctor density test.
- C. The Contractor shall submit testing methods (prior to conducting test), test results, and a certification from the approved soils testing laboratory that the cap material meets the requirements of B above. In addition, the Contractor shall submit compaction curves (ASTM D-698-78 Method C) for the proposed cap material. The results of all soils testing specified herein shall be submitted to the Department for approval.

MATERIALS AND PERFORMANCE

CAP MATERIALS AND INSTALLATION - SECTION 02006

2. Material shall be placed in a uniform lift and thoroughly compact to the specified modified proctor density using a sheepsfoot roller of sufficient weight to meet the compacted material density requirements. A minimum of two compaction coverages is required for each lift.
3. No cap material shall be placed where leachate is standing on the surface of the site where cap material is to be placed. Cap material shall not be compacted if leachate is standing on the surface of the site. A suitable working surface shall be obtained as outlined in Part 3 - Execution, Subpart 3.01 B. In addition, cap materials shall not be placed in a frozen condition or on top of frozen material.
4. Balls or clumps of cap material shall not exceed two inches in greatest diameter. Any materials exceeding these dimensions, measured along any face shall be removed from the cap materials prior to cap placement and shall be considered spoil.
5. Lifts which do not meet the compaction requirements of this Section shall be removed at the Contractor's expense.
6. Where required, the contractor shall add sufficient offsite water during the compaction effort to assure proper density. If due to rain or other causes, the material exceeds the optimum moisture content range for satisfactory compaction, it shall be allowed to dry, assisted by discing or harrowing, if necessary, before compaction is resumed.
7. If the compacted surface of any lift is too wet for proper compaction of the succeeding layer, the Contractor shall remove the lift, allow it to dry or work the material with suitable equipment to reduce the water content to the allowable water content range. The lift must then be recompacted before placement of a succeeding lift.
8. Where lifts of cap material are to be placed against a sloping surface or natural soil the Contractor shall bench the existing surface so that the new lifts overlie the existing material for a 12-inch horizontal distance.
9. The Contractor shall be required to seal the working surface from surface water infiltration at the end of each day or when a rain is expected. Sealing shall be accomplished by rolling the cap material with a smooth drum roller. Surface ponding of runoff on the cap surface will not be allowed.
10. Whenever the Contractor has sealed a lift, prior to placement of the next lift, the Contractor shall scarify the surface to a depth of 2 inches with a harrow scarifier or other suitable equipment to provide a satisfactory surface for each succeeding lift.
11. Compaction or consolidation achieved by traveling trucks, machines or other equipment shall not be accepted unless such procedures are approved by the Engineer and the compaction requirement of this Section are achieved.
12. Upon acceptance by the Engineer of the final lift of cap material in an area, the area shall immediately be covered with silty loam material in accordance with Section 02017.

MATERIALS AND PERFORMANCE

GROUND-WATER CUTOFF WALL - SECTION 02007

PART 1 - GENERAL

1.01 DESCRIPTION

- A. The Contractor shall construct a continuous, stable barrier consisting of either a mixture of soil and bentonite to the lines and grades indicated on the Contract Drawings. The cutoff wall shall have essentially vertical walls. The soil bentonite wall shall have a minimum width of 30 inches. The cutoff wall shall extend through all overburden materials to a depth of 6 feet into the underlying silt and clay subsoil. The resulting barrier shall have a permeability of less than 1×10^{-7} cm/sec (0.0000001 cm/sec). All efforts shall be made to provide a continuous, homogeneous soil and bentonite cutoff wall within the trench, and the occurrence of "windows" of materials having a permeability of greater than 1×10^{-7} cm/sec (0.0000001 cm/sec) shall not be allowed.

1.02 TESTING SERVICES

- A. All ground-water cutoff wall testing services including field and laboratory services required prior to and during installation of the ground-water cutoff wall shall be provided by the Contractor and shall be conducted under the supervision of the Department.

1.03 SOIL BENTONITE BACKFILL LABORATORY TESTING PROCEDURES

- A. The Contractor shall perform laboratory testing on the Contractor's proposed cutoff wall materials of construction. The purpose of this testing is to provide an evaluation of the permeability and to demonstrate to the Engineer that the proposed cutoff wall will meet the requirements of this Section.
- B. The Contractor shall have the testing performed using the actual types and mixtures of materials of construction to be used during installation of the ground-water cutoff wall including:
- Representative soils from the proposed location of the ground-water cutoff wall
 - Contractor's proposed bentonite
 - Contractor's proposed backfill
 - Contractor's proposed water source (Water)
 - Ground water from within the proposed location of the cutoff wall (Leachate)
- C. The Contractor shall be responsible for obtaining quantities of the representative soils, and leachate from the ground-water cutoff wall area, as noted above. The Engineer must approve the locations and times of all samples to be taken on the site.

MATERIALS AND PERFORMANCE

GROUND-WATER CUTOFF WALL - SECTION 02007

1.04 SUBMITTALS

- A. The Contractor shall submit a Field Quality Control Assurance Program detailing field quality control procedures with his Bid. The Field Quality Control Assurance Program shall insure that the cutoff wall is constructed in a manner which satisfies the design requirements set forth in this specification. For the soil bentonite cutoff wall, the program shall include, but not be limited to, checks on the excavation and backfilling procedures, cutoff wall depths and alignment, cutoff wall continuity, and testing of slurry and backfill for conformance with the proposed mix. (Submit with Bid.)
- B. Name of proposed testing laboratory or independent organization certifying laboratory test results.
- C. The Contractor may submit with his bid a proposal to utilize alternative methodology and/or materials of construction of the ground-water cutoff wall, if he can demonstrate that such alternative methods and/or materials would be more appropriate to this specific site.
- D. The Contractor is advised that remote mixing using auger-type equipment is required. The Contractor shall submit a proposed location and design of the remote mixing facility and auger mixing method.
- E. Proposed method of construction of the cutoff wall including types and sources of materials to be used to construct the cutoff wall, construction procedures and procedures for handling and disposing of contaminated materials (bentonite handling and disposing of contaminated materials (bentonite slurry, backfill, ground-water and/or soils removed during excavation of the slurry trench) (Submit with Bid.)
- F. After award of the Contract and prior to cutoff wall installation, the successful Contractor shall submit all laboratory test results to the Engineer for approval. , The Contractor shall also submit an independent certification that the laboratory tests were conducted in accordance with the specified laboratory testing program.
- G. If at any time during the contract the Engineer requests further testing to insure that the characteristics of the construction mate-

MATERIALS AND PERFORMANCE

GROUND-WATER CUTOFF WALL - SECTION 02007

PART 3 - EXECUTION

3.01 GENERAL REQUIREMENTS

- A. The ground-water cutoff wall shall be constructed to achieve a maximum permeability rate of 1×10^{-7} cm/sec (0.0000001 cm/sec) as determined by the specified laboratory testing program.

3.02 BATCHING PLANT

- A. A bentonite slurry batch plant and slurry hydration pond and/or tank shall be provided by the Contractor as necessary to meet the requirement of this Section. Each shall be placed at a location approved by the Engineer. Note: No slurry shall be made in the trench.
- B. The batching plant shall be of sufficient size not to cause an interruption of work.

3.03 BENTONITE SLURRY - BACKFILL MIXING

- A. Bentonite and backfill shall be mixed and blended using auger equipment into a soil bentonite mixture in such a manner as to meet the requirements of this Section. The soil bentonite backfill shall have the same bentonite content as utilized in the laboratory testing program and approved by the Engineer. The soil bentonite backfill shall have a slump (when tested by a conventional concrete slump cone test) as determined by the laboratory testing program and approved by the Engineer. The backfill shall not be mixed next to the trench, but at an on-site, remote location using auger-type equipment (refer to Paragraph 1.04 D. of this Section).

3.04 SLURRY TRENCH INSTALLATION

- A. A method for excavating the slurry trench shall be proposed as part of the Contractor's construction procedures to be submitted with his bid. Bentonite slurry shall be introduced into the slurry trench at the same time slurry trench excavation is begun and shall be maintained in the slurry trench during excavation until backfilled with soil bentonite backfill. The contractor shall maintain the stability of the excavated slurry trench at all times for its full depth. The level of the bentonite slurry in the slurry trench shall not be permitted to drop more than two feet below existing grade except as approved by the Engineer. Dilution of the bentonite slurry by surface waters shall be prevented.
- B. The Contractor shall waste the bottom six feet (6') of silt and clay soil excavated from the slurry trench to a location within the limits of the ground-water cutoff wall. Upon approval of the Engineer, this soil may be used in the soil bentonite backfill.

MATERIALS AND PERFORMANCE
TOPSOIL AND SEEDING - SECTION 02008

PART 1 - GENERAL

1.01 DESCRIPTION

- A. Work Specified
 - 1. The furnishing of topsoil, fertilizer, seed, and mulch; the preparation of the subgrade and the placing of the topsoil, fertilizer, seed and mulch.
 - 2. The maintenance required until acceptance.
- B. Related Work Specific Elsewhere
 - 1. Embankment: Section 02004
 - 2. Cap Materials and Installation: Section 02006

1.02 SUBMITTALS

- A. The Contractor shall submit for approval by the Engineer a written statement giving location of properties from which topsoil is to be obtained, names and addresses of owners, depth to be stripped and the crops grown during the past two years. The written statement shall include a laboratory certification of the actual gradation of the topsoil material.
- B. The Contractor shall submit seed vendor's certified statement for the grass seed mixture required, stating common name, percentage by weight, and percentages of purity and germination.
- C. The Contractor shall submit for approval by the Engineer all data concerning hydroseeding equipment (if used) including all material application rates.

PART 2 - PRODUCTS

2.01 TOPSOIL

Topsoil shall be unfrozen fertile, friable, natural loam. surface soil, and shall be free of subsoil, clay and clay lumps, brush, weeds, and other litter and free of roots, stumps, stones larger than 2 inches in any dimension, and other extraneous matter.

Topsoil shall meet the following requirements:

- 1. The pH of the material shall be between 5.5 and 7.6.
- 2. The organic content shall be not less than 2% nor more than 20%.
- 3. Gradation:

| <u>Sieve Size</u> | <u>Percent Passing by Weight</u> |
|-------------------|----------------------------------|
| 2 inch | 100 |
| 1 inch | 85 to 100 |
| 1/4 inch | 65 to 90 |
| No. 200 mesh | 20 to 80 |

The Contractor may amend natural topsoil with approved materials and by approved methods to meet the above specifications.

MATERIALS AND PERFORMANCE

TOPSOIL AND SEEDING - SECTION 02008

- C. The fertilizer shall be applied uniformly with a mechanical spreader at the rate of 20 pounds per 1000 square feet. Following the application of the fertilizer and prior to application of the seed, the surface shall be scarified to a depth of 2 inches with a disk or other suitable method.
- D. The seed mixture shall be applied uniformly upon the prepared surface with a mechanical spreader at a rate of not less than five pounds per 1000 square feet. The seed shall be raked lightly into the surface and rolled. Seeding shall be suspended when wind velocities exceed 5 miles per hour or as directed by the Engineer.
- E. Seeded areas shall then be covered by application of a uniform continuous 2" thick blanket of mulch. Excessive amounts or bunching of mulch will not be permitted. Mulch shall be left in place and allowed to disintegrate and shall be anchored as required by a method approved by the Engineer. Any anchorage or mulch that has not disintegrated at time of first mowing shall be removed.
- F. Following application of the mulch, the seed bed shall be moistened. A muddy soil condition will not be acceptable.
- G. Seeded areas shall be watered as often as required to obtain germination and to obtain and maintain a satisfactory growth. Watering shall be done in such a manner as to prevent washing out of seed and damaging of cap.
- H. The stand of grass resulting from the seeding shall not be considered satisfactory until accepted by the Engineer. If areas are determined to be unacceptable, the remaining mulch will be removed and all areas shall be reseeded, refertilized and remulched as per the above application procedures at the Contractor's expense. Any areas that are damaged by activities of the Contractor after topsoil and seeding shall be repaired to the satisfaction of the Engineer.
- I. Hydroseeding may be accepted as a method of applying fertilizer, seed and mulch. The Contractor must submit all data regarding materials and application rates to the Engineer for approval if hydroseeding is proposed by the Contractor.

3.03 MAINTENANCE

- A. The Contractor shall begin maintenance period immediately after planting of landscape materials.
- B. The Contractor shall maintain grass areas, for the periods required to establish an acceptable growth, but not less than 60 days, after date of substantial completion. If seeded in the fall and not given a full 60 days of maintenance, or if not considered acceptable by the Engineer at that time, continue maintenance during following spring until acceptable grass stand is established.
- C. Seeded areas shall be watered as often as required to obtain germination and to obtain and maintain a satisfactory sod growth. Watering shall be in such a manner as to prevent washing out of seed.

- END OF SECTION -

APPENDIX B

KINGSBURY SITE REMEDIAL PROGRAM
FIELD AND LABORATORY TEST RESULTS

- TRIAXIAL PERMEABILITY TESTING
- SLURRY QUALITY CONTROL TESTING
- SLURRY WALL BACKFILL TESTING
- IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP
- PROCTOR CURVES FOR CAP MATERIAL

**KINGSBURY SITE REMEDIAL PROGRAM
TRIAxIAL PERMEABILITY TEST RESULTS**

TRIAxIAL PERMEABILITY TEST RESULTS

| <u>Sample</u> | <u>Date</u> | <u>Normal Pressure (PSI)</u> | <u>Confining Pressure (PSI)</u> | <u>Back Pressure (PSI)</u> | <u>Permeability* (CM/SEC)</u> |
|---|-------------|--------------------------------------|---|------------------------------------|--|
| Slurry Wall Field Sample | 9/15/87 | 90 | 95 | 80 | 1.76×10^{-8} |
| Slurry Wall Field Sample | 8/31/87 | 90 | 95 | 80 | 1.20×10^{-8} |
| Slurry Wall Field Sample #1 Sta. 20 + 30 | | 90 85 | 95 95 | 80 80 | 1.23×10^{-8} 1.11×10^{-8} |
| Slurry Wall Field Sample #2 | | 90 | 95 | 80 | 1.47×10^{-8} |
| Slurry Wall Field Sample #3 | | 90 | 95 | 80 | 1.59×10^{-8} |
| Mix Design 85% "Soil," 15% Clay & Bentonite Slurry to Obtain 3 1/4" Slump | | 85 90 | 95 95 | 80 80 | 4.80×10^{-8} 4.74×10^{-8} |
| Proposed Cap Material - TP-1 @ 6' | | 85 90 | 95 95 | 80 85 | 2.25×10^{-9} 2.15×10^{-9} |
| Proposed Cap Material TP-3 @ 4' | | 85 90 | 95 95 | 80 80 | 2.65×10^{-9} 2.43×10^{-9} |
| Proposed Cap Material TP-4 @ 6.5' | | 85 90 | 95 95 | 80 80 | 1.84×10^{-9} 2.15×10^{-9} |
| Soil/Slurry Mix w/40% Natural Fines, 4" Slump | | 90 90 | 95 95 | 80 80 | 1.69×10^{-8} 2.97×10^{-8} |

*Note: Maximum allowable permeability = 1×10^{-7} cm/sec

**KINGSBURY SITE REMEDIAL PROGRAM
SLURRY QUALITY CONTROL TEST RESULTS**

SLURRY QUALITY CONTROL TESTING

| <u>Date</u> | <u>Time</u> | <u>Slurry Pond</u> | | | <u>Trench Slurry</u> | | | <u>Station</u> |
|-----------------|--------------|---------------------------|----------------------|----------------------|---------------------------|----------------------|----------------------|----------------|
| | | <u>Marsh Funnel (sec)</u> | <u>Filtrate Loss</u> | <u>Density (PCF)</u> | <u>Marsh Funnel (sec)</u> | <u>Filtrate Loss</u> | <u>Density (PCF)</u> | |
| <u>Required</u> | <u>Range</u> | <u>≥40</u> | <u>-</u> | <u>65-85</u> | <u>≥40</u> | <u>-</u> | <u>65-85</u> | |
| 7/28/87 | 12:30p | 44 | 9.5 | 65.5 | | | | |
| | 2:00p | 43 | - | - | | | | |
| | 2:45p | 41 | - | - | | | No Backfill Placed | |
| | 4:00p | 43 | - | - | | | | |
| | 4:45p | 40 | 10.5 | 65.0 | | | | |
| 7/29/87 | 8:00a | 43 | 10.0 | 65.0 | | | | |
| | 9:00a | 41 | - | - | | | | |
| | 10:00a | 40 | - | - | | | No Backfill Placed | |
| | 3:00p | 41 | - | - | | | | |
| | 4:00p | 40 | 10.5 | 65.0 | | | | |
| 7/30/87 | 7:30a | 42 | 9.5 | 65.0 | | | | |
| | 8:30a | 41 | - | - | | | | |
| | 9:30a | 40 | - | - | | | | |
| | 11:00a | 40 | - | - | | | No Backfill Placed | |
| | 1:00p | 41 | 10.0 | 65.0 | | | | |
| | 2:00p | 40 | - | - | | | | |
| | 3:00p | 40 | - | - | | | | |
| | 4:00p | 41 | - | - | | | | |
| | 4:30p | 40 | - | - | | | | |
| 7/31/87 | 7:15a | 40 | - | 65.0 | | | | |
| | 8:30a | 42 | - | - | | | | |
| | 9:30a | 40 | - | - | | | | |
| | 11:00a | 40 | - | - | | | | |
| | 3:00p | 44 | - | - | | | | |
| | 4:00p | 43 | - | - | | | | |
| | 5:00p | 43 | - | - | | | | |
| 8/3/87 | 7:15a | 41 | - | 65.0 | | | | |
| | 8:30a | 40 | - | - | | | | |
| | 9:30a | 41 | - | - | | | | |
| | 11:00a | 40 | - | - | | | | |
| | 1:00p | 40 | - | - | | | | |
| | 2:00p | 42 | - | - | | | | |
| | 3:00p | 41 | - | - | | | | |
| | 4:00p | 42 | - | - | | | | |
| | 5:00p | 42 | - | - | | | | |
| 8/4/87 | 7:30a | 42 | - | 65.5 | | | | |
| | 8:30a | 40 | - | - | | | | |
| | 9:30a | 40 | - | - | 51.0 | 10.5 | 71.8 | 22+20 |
| | 11:00a | 41 | - | - | | | | |

SLURRY QUALITY CONTROL TESTING
(Cont'd.)

| <u>Date</u> | <u>Time</u> | <u>Marsh Funnel</u> | <u>Slurry Pond</u> | | <u>Trench Slurry</u> | | | <u>Station</u> |
|-------------|-------------|---------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------|
| | | | <u>Filtrate Loss</u> | <u>Density (PCF)</u> | <u>Marsh Funnel</u> | <u>Filtrate Loss</u> | <u>Density (PCF)</u> | |
| Required | Range | ≥40 | - | 65-85 | ≥40 | - | 65-85 | |
| | 12:00p | 40 | - | - | | | | |
| | 1:15p | 42 | - | 65.0 | | | | |
| | 2:15p | 41 | - | - | 55.7 | 10.0 | 75.8 | 23+20 |
| | 4:30p | - | - | - | 56.3 | 10.7 | 75.3 | 23+00 |
| 8/5/87 | 8:00a | 40 | 11 | 65.0 | | | | |
| | 9:00a | 41 | - | - | 58.3 | | | |
| | 10:30a | 41 | - | - | | | | |
| | 11:30a | 41 | - | - | | | | |
| | 1:30p | 50 | - | 68.5 | | | | |
| | 2:00p | - | - | - | 57.7 | 10.7 | 79.5 | |
| | 4:00p | - | - | - | 58.3 | 10.5 | 79.7 | |
| 8/6/87 | 8:00a | 42 | 11.0 | 65.0 | 59.7 | 9.7 | 78.8 | |
| | 9:00a | 40 | - | - | | | | |
| | 10:00a | 40 | - | - | | | | |
| | 1:00p | 41 | - | - | 59.3 | 10.8 | 80.8 | 23+70 |
| | 3:00p | 40 | - | - | 59.3 | 10.5 | 80.8 | |
| 8/11/87 | 8:00a | 42 | 10.0 | 65.0 | 64.7 | 10.7 | 81.3 | |
| | 9:00a | 42 | - | - | | | | |
| | 10:00a | 43 | - | - | | | | |
| | 11:00a | 42 | - | - | 51.0 | 12.3 | 75.3 | |
| | 1:00p | 44 | - | - | | | | |
| | 2:00p | 42 | 10.0 | 65.0 | | | | |
| | 3:00p | 42 | - | - | 56.0 | 12.2 | 71.7 | |
| | 4:00p | 44 | - | - | | | | |
| 8/12/87 | 8:00a | 43 | 10.0 | 65.0 | 62.0 | 12.8 | 72.0 | |
| | 9:00a | 42 | - | - | | | | |
| | 10:00a | 42 | - | - | | | | |
| | 11:00a | 41 | - | - | | | | |
| | 1:00p | 44 | - | - | 50.0 | 12.0 | 74.3 | |
| | 2:00p | 43 | 10.0 | 65.0 | | | | |
| | 3:00p | 44 | - | - | | | | |
| 8/13/87 | 8:00a | 43 | - | 66.0 | | | | |
| | 9:00a | 42 | - | - | 53.3 | 12.2 | 73.7 | |
| | 10:00a | 44 | - | 66.5 | | | | |
| | 11:00a | 43 | - | - | | | | |
| | 1:00p | 42 | - | - | | | | |
| | 2:00p | - | - | - | 51.0 | 12.3 | 71.5 | |
| | 4:00p | - | - | - | 65.5 | 11.8 | 78.0 | |
| 8/14/87 | 8:00a | 41 | 10.0 | 65.0 | 55.0 | 11.8 | 83.5 | |
| | 9:00a | 42 | - | - | | | | |
| | 10:00a | 41 | - | - | | | | |

SLURRY QUALITY CONTROL TESTING
(Cont'd.)

| <u>Date</u> | <u>Time</u> | <u>Slurry Pond</u> | | | <u>Trench Slurry</u> | | | <u>Station</u> |
|-------------|-------------|---------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------|
| | | <u>Marsh Funnel</u> | <u>Filtrate Loss</u> | <u>Density (PCF)</u> | <u>Marsh Funnel</u> | <u>Filtrate Loss</u> | <u>Density (PCF)</u> | |
| Required | Range | ≥40 | - | 65-85 | ≥40 | - | 65-85 | |
| | 11:00a | 43 | - | - | | | | |
| | 1:00p | 42 | - | - | | | | |
| | 2:00p | 44 | 10.0 | 65.0 | 60.5 | 10.8 | 75.0 | |
| | 3:00p | 42 | - | - | | | | |
| | 4:00p | - | - | - | 54.3 | 11.3 | 75.7 | |
| | 5:00p | - | - | - | | | | |
| 8/17/87 | 8:00a | 41 | 10.5 | 65.0 | 45.0 | 12.5 | 71.5 | |
| | 9:00a | 41 | - | - | | | | |
| | 10:00a | 43 | - | - | | | | |
| | 11:00a | 42 | - | - | 49.5 | 13.5 | 81.0 | |
| | 1:00p | 43 | 10.0 | 66.0 | | | | |
| | 2:00p | 42 | - | - | | | | |
| | 3:00p | 44 | - | - | 54.0 | 13.3 | 80.3 | |
| 8/18/87 | 8:00a | 40 | 11.0 | 65.0 | 51.0 | 13.0 | 80.3 | |
| | 9:00a | 41 | - | - | | | | |
| | 10:00a | 41 | - | - | | | | |
| | 11:00a | 42 | - | - | 56.7 | 13.5 | 84.7 | |
| | 1:00p | 41 | - | - | | | | |
| | 2:00p | 43 | - | - | | | | |
| | 3:00p | 43 | 10.0 | 66.0 | | | | |
| | 4:00p | 42 | - | - | 56.7 | 12.7 | 85.0 | |
| | 5:00p | 42 | - | - | | | | |
| 8/19/87 | 8:00a | 43 | - | - | 60.0 | 50.3 | 80.3 | |
| | 9:00a | 42 | 10.0 | 65.0 | | | | |
| | 10:00a | 42 | - | - | | | | |
| | 11:00a | 41 | - | - | 56.3 | 12.0 | 82.3 | |
| | 4:00p | - | - | - | 48.3 | 12.0 | 78.3 | |
| 8/20/87 | 8:00a | 42 | - | - | 53.0 | 10.7 | 79.0 | |
| | 9:00a | 42 | - | - | | | | |
| | 10:00a | 41 | 10.0 | 65.0 | | | | |
| | 11:00a | 43 | - | - | 49.3 | 13.5 | 78.3 | |
| | 1:00p | 42 | - | - | | | | |
| | 2:00p | 41 | - | - | | | | |
| | 3:00p | 42 | 10.5 | 66.0 | 53.3 | 12.7 | 82.0 | |
| | 4:00p | 42 | - | - | | | | |
| 8/21/87 | 8:00a | - | - | - | 56.7 | 12.8 | 83.0 | |
| | 11:00a | - | 10.5 | 66.0 | 55.7 | 12.3 | 81.7 | 32+70 |
| | 3:00p | - | 11.5 | 66.0 | 57.3 | 12.3 | 83.0 | |
| 8/22/87 | 8:00a | 42 | - | - | 60.3 | 11.8 | 81.7 | 33+40 |
| | 9:00a | 42 | 12.0 | 65.0 | | | | |

SLURRY QUALITY CONTROL TESTING
(Cont'd.)

| <u>Date</u> | <u>Time</u> | <u>Marsh Funnel</u> | <u>Slurry Pond</u> | | <u>Trench Slurry</u> | | <u>Density (PCF)</u> | <u>Station</u> |
|-----------------|--------------|---------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------|
| | | | <u>Filtrate Loss</u> | <u>Density (PCF)</u> | <u>Marsh Funnel</u> | <u>Filtrate Loss</u> | | |
| <u>Required</u> | <u>Range</u> | ≥40 | - | 65-85 | ≥40 | - | 65-85 | |
| 8/24/87 | 8:00a | 42 | 11.5 | 66.0 | 58.7 | 12.5 | 82.7 | 33+70 |
| | 9:00a | 42 | - | - | - | - | - | - |
| | 10:00a | 41 | - | - | - | - | - | - |
| | 11:00a | 41 | - | - | 54.7 | 12.5 | 78.7 | 0+30 |
| | 1:00p | 42 | - | - | - | - | - | - |
| | 2:00p | 43 | - | - | - | - | - | - |
| | 3:00p | 43 | - | - | - | - | - | - |
| | 4:00p | 42 | 11.5 | 66.0 | 55.0 | 13.5 | 76.7 | - |
| | 5:00p | 42 | - | - | - | - | - | - |
| 8/25/87 | 8:00a | 42 | - | - | 64.3 | 12.0 | 80.7 | 0+50 |
| | 9:00a | 42 | - | - | - | - | - | - |
| | 10:00a | 43 | - | - | - | - | - | - |
| | 11:00a | 42 | 11.5 | 66.0 | 58.3 | 13.2 | 80.7 | 0+90 |
| | 1:00p | 41 | - | - | - | - | - | - |
| | 2:00p | 43 | - | - | - | - | - | - |
| | 3:00p | 43 | - | - | - | - | - | - |
| | 4:00p | 41 | 11.5 | 65.0 | 57.3 | 12.3 | 79.7 | 1+10 |
| | 5:00p | 42 | - | - | - | - | - | - |
| 8/26/87 | 8:00a | 43 | - | - | - | - | - | - |
| | 9:00a | 42 | 11.5 | 66.0 | 53.0 | 13.2 | 79.0 | 1+20 |
| | 10:00a | 42 | - | - | - | - | - | - |
| | 11:00a | 43 | - | - | 59.7 | 12.8 | 80.0 | 1+20 |
| | 1:00p | 41 | - | - | - | - | - | - |
| | 2:00p | 42 | 11.5 | 66.0 | - | - | - | - |
| | 3:00p | 42 | - | - | 56.0 | 12.5 | 80.7 | - |
| | 4:00p | 43 | - | - | - | - | - | - |
| 8/27/87 | 8:00a | 42 | - | - | 62.3 | 11.7 | 80.7 | 1+60 |
| | 9:00a | 41 | - | - | - | - | - | - |
| | 10:00a | 42 | 11.5 | 65.0 | - | - | - | - |
| | 11:00a | 42 | - | - | 62.3 | 11.2 | 81.3 | 2+40 |
| | 1:00p | 43 | - | - | - | - | - | - |
| | 2:00p | 42 | - | - | - | - | - | - |
| | 3:00p | 42 | 11.5 | 65.0 | 53.7 | 12.2 | 80.7 | - |
| | 4:00p | 41 | - | - | - | - | - | - |
| | 5:00p | - | - | - | - | - | - | - |
| 8/28/87 | 11:00a | 42 | 10.5 | 66.0 | - | - | - | - |
| | 1:00p | 42 | 10.5 | 66.0 | - | - | - | - |
| 8/31/87 | 8:00a | 41 | - | - | 50.7 | 12.0 | 78.7 | 2+20 |
| | 9:00a | 41 | - | - | - | - | - | - |
| | 10:00a | 42 | 10.5 | 66.0 | - | - | - | - |
| | 11:00a | 41 | - | - | 51.7 | 13.2 | 79.0 | 3+20 |
| | 1:00p | 43 | - | - | - | - | - | - |

SLURRY QUALITY CONTROL TESTING
(Cont'd.)

| <u>Date</u> | <u>Time</u> | <u>Marsh Funnel</u> | <u>Slurry Pond</u> | | <u>Trench Slurry</u> | | | <u>Station</u> |
|-----------------|--------------|---------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------|
| | | | <u>Filtrate Loss</u> | <u>Density (PCF)</u> | <u>Marsh Funnel</u> | <u>Filtrate Loss</u> | <u>Density (PCF)</u> | |
| <u>Required</u> | <u>Range</u> | ≥40 | - | 65-85 | ≥40 | - | 65-85 | |
| | 2:00p | 42 | - | - | | | | |
| | 3:00p | 42 | 11.0 | 66.0 | | | | |
| | 4:00p | 43 | - | - | 54.0 | 12.7 | 80.3 | 3+20 |
| | 5:00p | 42 | - | - | | | | |
| 9/1/87 | 8:00a | 40 | - | - | 52.7 | 13.2 | 81.0 | 3+20 |
| | 9:00a | 40 | - | - | | | | |
| | 10:00a | 41 | 10.0 | 65.0 | | | | |
| | 11:00a | 42 | - | - | 52.3 | 13.3 | 81.0 | 3+50 |
| | 1:00p | 41 | - | - | | | | |
| | 2:00p | 41 | - | - | | | | |
| | 3:00p | 42 | 10.5 | 66.0 | | | | |
| | 4:00p | 42 | - | - | | | | |
| 9/2/87 | 8:00a | 41 | - | - | 58.3 | 11.8 | 83.0 | 3+50 |
| | 9:00a | 41 | - | - | | | | |
| | 10:00a | 42 | 10.5 | 66.0 | | | | |
| | 11:00a | 42 | - | - | 57.0 | 11.8 | 83.0 | |
| | 1:00p | 41 | - | - | | | | |
| | 2:00p | 42 | 10.5 | 66.0 | | | | |
| | 3:00p | 42 | - | - | 54.5 | 11.3 | 80.5 | |
| | 4:00p | 42 | - | - | | | | |
| 9/3/87 | 8:00a | 43 | - | - | 53.5 | 11.8 | 81.5 | 4+00 |
| | 9:00a | 43 | - | - | | | | |
| | 10:00a | 42 | 10.5 | 66.0 | | | | |
| | 11:00a | 42 | - | - | 58.0 | 12.5 | 84.3 | 4+10 |
| | 1:00p | 41 | - | - | | | | |
| | 2:00p | 41 | - | - | | | | |
| | 3:00p | 41 | 10.0 | 65.0 | | | | |
| | 4:00p | 41 | - | - | 50.5 | 11.8 | 82.5 | 4+00 |
| 9/4/87 | 9:00a | 41 | - | - | 49.3 | 13.0 | 80.3 | 4+50 |
| | 10:00a | 43 | - | - | | | | |
| | 11:00a | 42 | 10.5 | 66.0 | | | | |
| | 1:00p | 41 | - | - | | | | |
| | 2:00p | 42 | - | - | 49.3 | 12.5 | 80.0 | |
| 9/8/87 | 8:00a | 41 | - | - | 50.7 | 12.7 | 81.3 | 4+70 |
| | 9:00a | 41 | 10.5 | 65.0 | | | | |
| | 10:00a | 41 | - | - | | | | |
| | 11:00a | 42 | - | - | 51.3 | 12.7 | 82.3 | 4+90 |
| | 1:00p | 42 | 10.5 | 66.0 | | | | |
| | 2:00p | 43 | - | - | | | | |
| | 3:00p | 42 | - | - | | | | |
| | 4:00p | 43 | - | - | 50.7 | 13.3 | 82.7 | 4+90 |

SLURRY QUALITY CONTROL TESTING
(Cont'd.)

| <u>Date</u> | <u>Time</u> | <u>Marsh Funnel</u> | <u>Slurry Pond</u> | | <u>Trench Slurry</u> | | | <u>Station</u> |
|-------------|-------------|-------------------------|--------------------------|--------------------------|-------------------------|--------------------------|--------------------------|----------------|
| | | | <u>Filtrate Loss</u> | <u>Density (PCF)</u> | <u>Marsh Funnel</u> | <u>Filtrate Loss</u> | <u>Density (PCF)</u> | |
| Required | Range | ≥40 | - | 65-85 | ≥40 | - | 65-85 | |
| 9/10/87 | 9:00a | 40 | 10.0 | 65.0 | 44.0 | 13.3 | 76.7 | 5+00 |
| | 10:00a | 40 | - | - | - | - | - | |
| | 11:00a | 40 | - | - | 45.7 | 13.8 | 79.3 | |
| | 1:00p | 40 | - | - | - | - | - | |
| | 2:00p | 40 | - | - | - | - | - | |
| | 3:00p | 41 | 10.5 | 66.0 | - | - | - | |
| | 4:00p | 42 | - | - | 44.7 | 13.8 | 80.0 | |
| 9/11/87 | 9:00a | 42 | - | - | - | - | - | |
| | 10:00a | 42 | 10.5 | 66.0 | 46.0 | 13.0 | 78.7 | |
| | 11:00a | 43 | - | - | - | - | - | |
| | 12:00p | 43 | - | - | - | - | - | |
| | 1:00p | 43 | - | - | - | - | - | |
| | 2:00p | 43 | - | - | 47.0 | 12.7 | 79.3 | |
| 9/14/87 | 9:00a | 42 | - | - | 47.3 | 12.8 | 79.0 | 6+40 |
| | 10:00a | 43 | - | - | - | - | - | |
| | 11:00a | 42 | 10.5 | 66.0 | 45.0 | 13.3 | 79.7 | |
| | 12:00p | 43 | - | - | - | - | - | |
| | 1:00p | 43 | - | - | - | - | - | |
| | 2:00p | 42 | 10.5 | 66.0 | 44.0 | 13.3 | 80.3 | |
| | 3:00p | 43 | - | - | - | - | - | |
| 9/15/87 | 9:00a | 42 | - | - | 49.3 | 13.2 | 82.3 | 7+30 |
| | 10:00a | 42 | - | - | - | - | - | |
| | 11:00a | 43 | 10.5 | 65.0 | - | - | - | |
| | 12:00p | 43 | - | - | 49.7 | 13.5 | 83.7 | |
| | 1:00p | 43 | - | - | - | - | - | |
| | 2:00p | 42 | 10.5 | 65.0 | - | - | - | |
| | 3:00p | 43 | - | - | - | - | - | |
| | 4:00p | 43 | - | - | 52.0 | 13.5 | 85.3* | |
| 9/16/87 | 9:00a | 43 | - | - | 52.7 | 13.8 | 86.0* | 7+60 |
| | 10:00a | 43 | 10.5 | 65.0 | - | - | - | |
| | 11:00a | 43 | - | - | 53.3 | 14.0 | 87.3* | |
| | 1:00p | 42 | - | - | - | - | - | |
| | 2:00p | 42 | 10.0 | 65.0 | - | - | - | |
| | 3:00p | 43 | - | - | - | - | - | |
| | 4:00p | 42 | - | - | 51.7 | 13.2 | 87.0* | |
| 9/17/87 | 8:00a | 43 | - | - | 51.2 | 13.7 | 85.5* | 8+20 |
| | 9:00a | 43 | - | - | - | - | - | |
| | 10:00a | 42 | 10.5 | 65.0 | 45.7 | 13.5 | 84.5 | |
| | 11:00a | 43 | - | - | - | - | - | |
| | 1:00p | 43 | 10.5 | 66.0 | - | - | - | |
| 2:00p | 42 | - | - | - | - | - | | |

*Outside required range
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SLURRY QUALITY CONTROL TESTING
(Cont'd.)

| <u>Date</u> | <u>Time</u> | <u>Marsh Funnel</u> | <u>Slurry Pond</u> | | <u>Trench Slurry</u> | | | <u>Station</u> |
|-------------|-------------|---------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------|
| | | | <u>Filtrate Loss</u> | <u>Density (PCF)</u> | <u>Marsh Funnel</u> | <u>Filtrate Loss</u> | <u>Density (PCF)</u> | |
| Required | Range | ≥40 | - | 65-85 | ≥40 | - | 65-85 | |
| | 3:00p | 42 | - | - | | | | |
| | 4:00p | 42 | - | - | | | | |
| 9/21/87 | 9:00a | 43 | - | - | | | | |
| | 10:00a | 42 | 10.5 | 66.0 | 43.7 | 14.2 | 82.0 | 9+00 |
| | 11:00 | 42 | - | - | | | | |
| | 1:00p | 42 | - | - | 49.3 | 14.0 | 83.3 | 8+50 |
| | 2:00p | 43 | - | - | | | | |
| | 3:00p | 42 | - | - | | | | |
| | 4:00p | 43 | - | - | | | | |
| 9/22/87 | 8:00a | 42 | - | - | 48.7 | 13.7 | 85.0 | 9+00 |
| | 9:00a | 42 | 10.5 | 66.0 | | | | |
| | 10:00a | 42 | - | - | | | | |
| | 11:00a | 43 | - | - | | | | |
| | 1:00p | 43 | - | - | 54.0 | 10.0 | 82.0 | 21+00 |
| | 2:00p | 43 | - | - | | | | |
| | 3:00p | 43 | 10.0 | 66.0 | | | | |
| | 4:00p | 42 | - | - | | | | |
| 9/23/87 | 8:00a | 43 | - | - | | | | |
| | 9:00a | 43 | 10.0 | 66.0 | 61.0 | 10.5 | 83.5 | 19+80 |
| | 10:00a | 43 | - | - | | | | |
| | 11:00a | 42 | - | - | | | | |
| | 1:00p | 42 | - | - | | | | |
| | 2:00p | 43 | - | - | 59.0 | 10.3 | 83.5 | 19+60 |
| | 3:00p | 43 | - | - | | | | |
| | 4:00p | 42 | 10.5 | 65.0 | | | | |
| 9/24/87 | 8:00a | 43 | - | - | 51.5 | 12.3 | 83.5 | 19+60 |
| | 9:00a | 42 | 10.0 | 65.0 | | | | |
| | 10:00a | 43 | - | - | 63.5 | 11.0 | 88.0* | 19+40 |
| | 11:00a | 43 | - | - | | | | |
| | 1:00p | 43 | - | - | 56.0 | - | 92.0* | 8+70 |
| | 2:00p | 42 | 10.0 | 65.0 | | | | |
| | 3:00p | 42 | - | - | | | | |
| | 4:00p | 42 | - | - | 50.0 | 14.0 | 87.3* | 9+00 |
| 9/25/87 | 8:00a | 42 | - | - | | | | |
| | 9:00a | 42 | 10.5 | 65.0 | | | | |
| | 10:00a | 42 | - | - | | | | |
| | 11:00a | 43 | - | - | 48.5 | 10.8 | 85.0 | 18+90 |
| | 1:00p | 43 | - | - | | | | |
| | 2:00p | 43 | - | - | | | | |
| | 3:00p | 43 | 10.5 | 66.0 | | | | |
| | 4:00p | 43 | - | - | | | | |

SLURRY QUALITY CONTROL TESTING
(Cont'd.)

| <u>Date</u> | <u>Time</u> | <u>Marsh Funnel</u> | <u>Slurry Pond</u> | | <u>Trench Slurry</u> | | <u>Density (PCF)</u> | <u>Station</u> |
|-----------------------|-------------|-------------------------|--------------------------|--------------------------|-------------------------|--------------------------|--------------------------|----------------|
| | | | <u>Filtrate Loss</u> | <u>Density (PCF)</u> | <u>Marsh Funnel</u> | <u>Filtrate Loss</u> | | |
| <u>Required Range</u> | | ≥40 | - | 65-85 | ≥40 | - | 65-85 | |
| 9/28/87 | 8:00a | 41 | - | - | | | | |
| | 9:00a | 41 | - | - | 50.5 | 10.3 | 84.0 | 18+90 |
| | 10:00a | 42 | 10.5 | 65.0 | | | | |
| | 11:00a | 42 | - | - | 48.0 | 13.2 | 83.0 | 18+90 |
| | 1:00p | 42 | 10.5 | 65.0 | 45.5 | | 77.5 | 18+90 |
| | 2:00p | 41 | - | - | 44.0 | 11.5 | 76.7 | 8+90 |
| | 3:00p | 43 | - | - | 43.0 | | 78.0 | 8+90 |
| | 4:00p | 43 | - | - | 43.3 | 11.7 | 75.3 | 9+00 |
| 9/29/87 | 8:00a | 43 | - | - | 45.0 | 12.8 | 76.0 | 9+00 |
| | 9:00a | 43 | - | - | 47.0 | 12.8 | 81.0 | 9+00 |
| | 11:00a | 43 | 10.0 | 66.0 | 50.3 | 13.2 | 76.0 | 9+20 |
| | | | | | 53.0 | 12.3 | 78.5 | 18+20 |
| 9/30/87 | 9:00a | 43 | - | - | 49.0 | 12.2 | 80.0 | 9+30 |
| | 11:00a | 43 | 10.5 | 66.0 | | | | |
| 10/6/87 | - | - | - | - | 43.0 | 11.8 | 72.3 | 17+20 |
| 10/7/87 | - | - | - | - | 44.7 | 13.2 | 73.0 | 9+80 |
| | - | - | - | - | 44.7 | 13.1 | 73.3 | 9+80 |
| | - | - | - | - | 46.5 | 10.2 | 76.0 | 17+20 |
| | - | - | - | - | 44.7 | 13.2 | 79.7 | 10+20 |
| 10/8/87 | - | - | - | - | 49.0 | 12.5 | 76.3 | 9+80 |
| | - | - | - | - | 43.0 | 13.0 | 75.0 | 16+60 |
| | - | - | - | - | 52.3 | 13.5 | 80.0 | 9+80 |
| | - | - | - | - | 42.5 | 13.5 | 75.0 | 16+30 |
| | - | - | - | - | | | 87.0* | 9+50 |
| 10/9/87 | - | - | - | - | 58.0 | | 87.0* | 10+20 |
| | - | - | - | - | 69.0 | | 95.0* | 10+00 |
| | - | - | - | - | 44.3 | 13.2 | 76.7 | 16+20 |
| | - | - | - | - | 43.0 | 13.8 | 77.0 | 15+10 |
| 10/10/87 | 10:00a | 43 | 10.5 | 65.0 | | | 84.0 | 9+60 |
| | - | - | - | - | 43.2 | 12.7 | 79.0 | 15+10 |
| | - | - | - | - | 42.7 | 14.2 | 75.7 | 15+10 |
| 10/12/87 | - | - | - | - | 49.7 | 11.7 | 77.3 | 9+70 |
| | - | - | - | - | 49.7 | 12.2 | 77.7 | 10+00 |
| | - | - | - | - | 48.7 | 11.3 | 80.0 | 10+00 |
| | - | - | - | - | 44.7 | 12.2 | 77.7 | 15+40 |
| 10/13/87 | - | - | - | - | 46.3 | 13.0 | 74.3 | 10+50 |
| | - | - | - | - | 50.7 | 11.5 | 77.7 | 10+50 |
| | - | - | - | - | 44.0 | 13.7 | 76.7 | 15+40 |

*Outside required range
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5/10/89
289171J

SLURRY QUALITY CONTROL TESTING
(Cont'd.)

| <u>Date</u> | <u>Time</u> | <u>Marsh Funnel</u> | <u>Slurry Pond</u> | | <u>Trench Slurry</u> | | | <u>Station</u> |
|-------------|-------------|-------------------------|--------------------------|--------------------------|-------------------------|--------------------------|--------------------------|----------------|
| | | | <u>Filtrate Loss</u> | <u>Density (PCF)</u> | <u>Marsh Funnel</u> | <u>Filtrate Loss</u> | <u>Density (PCF)</u> | |
| Required | Range | ≥40 | - | 65-85 | ≥40 | - | 65-85 | |
| 10/14/87 | - | - | - | - | 52.5 | 11.5 | 84.5 | 10+50 |
| | - | - | - | - | 48.3 | 11.3 | 86.0 | 10+70 |
| | - | - | - | - | 43.0 | 11.8 | 83.0 | 15+00 |
| | - | - | - | - | 47.0 | 12.5 | 87.5 | 15+90 |
| 10/16/87 | - | - | - | - | 46.0 | | 85.5 | 15+00 |
| | - | - | - | - | 43.0 | 9.7 | 84.0 | 11+10 |
| 10/19/87 | - | - | - | - | 48.0 | 13.2 | 84.0 | 11+20 |
| | - | - | - | - | 44.3 | 13.2 | 84.7 | 11+20 |
| | - | - | - | - | 44.0 | 14.0 | 85.3* | 11+20 |
| 10/20/87 | - | - | - | - | 47.7 | 13.7 | 84.0 | 11+60 |
| | - | - | - | - | 43.3 | 14.8 | 82.7 | 12+10 |
| | - | - | - | - | 45.7 | | 85.7* | 12+50 |
| 10/21/87 | - | - | - | - | 48.7 | 14.7 | 86.0* | 13+50 |
| | - | - | - | - | 47.0 | 14.3 | 88.3* | 13+50 |
| | - | - | - | - | 46.0 | | 86.3* | 14+10 |
| 10/22/87 | - | - | - | - | 47.7 | 13.2 | 85.7* | 13+70 |
| | - | - | - | - | 50.0 | 14.2 | 85.0 | 13+70 |
| 10/23/87 | - | - | - | - | 50.3 | | 87.0* | |
| 10/26/87 | - | - | - | - | 53.5 | 12.3 | 89.0* | 12+70 |
| | - | - | - | - | 47.0 | | 84.5 | 12+70 |
| 10/27/87 | - | - | - | - | 52.0 | 14.0 | 89.0* | 12+00 |
| | - | - | - | - | 54.5 | 13.8 | 84.5 | |
| 10/29/87 | - | - | - | - | 46.0 | 14.3 | 84.5 | 10+50 |
| | - | - | - | - | 53.5 | 14.8 | 89.5* | 10+50 |
| 10/30/87 | - | - | - | - | 61.0 | | 94.0* | 10+30 |

*Outside required range
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**KINGSBURY SITE REMEDIAL PROGRAM
SLURRY WALL BACKFILL TESTING RESULTS**

BACKFILL TESTING

| Date | AM/PM | Gradation - % Passing | | | Average Slump (IN) | Filtrate Loss (%) | Moisture Content (%) | Wet Density (PCF) |
|----------------|-------|-----------------------|-------|-------|--------------------|-------------------|----------------------|-------------------|
| | | 3/8" | #40 | #200 | | | | |
| Required Range | | 65-100 | 30-70 | 20-40 | 4-6 | | | ≥100 |
| 8/3/87 | AM | 100 | 68 | 35.4 | 4 | - | - | 110 |
| 8/3/87 | PM | 100 | 66 | 36.0 | 5 1/2 | - | - | 110 |
| 8/4/87 | AM | 96 | 66 | 22.9 | 4 | - | - | 109 |
| 8/5/87 | AM | 98 | 69 | 29.0 | 4 | - | - | 110 |
| 8/5/87 | PM | 100 | 68 | 30.7 | 3 3/4* | - | - | 110 |
| 8/6/87 | AM | 100 | 67 | 33.2 | 4 1/2 | - | - | 113 |
| 8/6/87 | PM | 100 | 69 | 35.1 | 4 | - | - | 113 |
| 8/11/87 | AM | 94 | 69 | 34.7 | 4 1/4 | - | 24.0 | 109 |
| 8/12/87 | AM | 100 | 66 | 27.0 | 4 1/4 | - | 26.5 | - |
| 8/12/87 | PM | 100 | 68 | 40.0 | 4 1/4 | - | 23.4 | - |
| 8/13/87 | AM | 100 | 70 | 40.3 | 4 1/2 | - | 27.0 | 112 |
| 8/13/87 | PM | 99 | 66 | 35.2 | 4 1/2 | - | 27.0 | 100 |
| 8/14/87 | AM | 100 | 68 | 30.4 | 4 1/2 | - | 26.7 | 112 |
| 8/14/87 | PM | 99 | 67 | 39.0 | 4 1/2 | - | 26.5 | 111 |
| 8/17/87 | AM | 100 | 67 | 40.0 | 4 1/2 | - | 25.9 | 115 |
| 8/17/87 | PM | 100 | 67 | 38.2 | 4 1/2 | - | 26.0 | 115 |
| 8/18/87 | AM | 100 | 69 | 36.2 | 4 3/4 | - | 28.7 | 110 |
| 8/18/87 | PM | 100 | 63 | 36.5 | 4 3/4 | - | 28.7 | 110 |
| 8/19/87 | AM | 99 | 70 | 26.0 | 4 1/2 | - | 26.0 | 110 |
| 8/19/87 | PM | 100 | 69 | 38.6 | 4 1/2 | - | 26.0 | 110 |
| 8/20/87 | AM | 100 | 68 | 31.4 | 5 | - | 24.9 | 115 |
| 8/21/87 | AM | 100 | 65 | 38.2 | 5 1/2 | - | 28.7 | 114 |

BACKFILL TESTING
(Cont'd.)

| Date | AM/PM | Gradation - % Passing | | | Average Slump (IN) | Filtrate Loss (%) | Moisture Content (%) | Wet Density (PCF) |
|----------------|-------|-----------------------|-------|-------|--------------------|-------------------|----------------------|-------------------|
| | | 3/8* | #40 | #200 | | | | |
| Required Range | | 65-100 | 30-70 | 20-40 | 4-6 | | | ≥100 |
| 8/21/87 | PM | 100 | 69 | 27.1 | 5 1/2 | - | 29.0 | 114 |
| 8/22/87 | PM | 99 | 67 | 39.5 | - | - | - | - |
| 8/24/87 | AM | 100 | 67 | 39.8 | 4 3/4 | - | 31.5 | 116 |
| 8/24/87 | PM | 100 | 68 | 32.2 | 4 3/4 | - | 28.3 | 116 |
| 8/25/87 | AM | 100 | 66 | 39.3 | 5 1/4 | - | 27.6 | 114 |
| 8/25/87 | PM | 99 | 69 | 28.4 | 5 1/4 | - | 30.7 | 114 |
| 8/26/87 | | 100 | 67 | 39.4 | 4 7/8 | - | 27.8 | - |
| 8/27/87 | AM | 100 | 67 | 29.4 | 4 1/2 | - | 26.7 | 114 |
| 8/27/87 | PM | 100 | 69 | 27.0 | 5 | - | 29.6 | 114 |
| 8/31/87 | AM | 100 | 64 | 30.8 | 5 1/2 | - | 30.0 | 115 |
| 8/31/87 | PM | 100 | 68 | 27.3 | 5 1/2 | - | 25.7 | 115 |
| 9/1/87 | AM | 100 | 64 | 23.0 | 4 1/2 | - | 26.5 | 114 |
| 9/1/87 | PM | 100 | 66 | 23.5 | 4 1/4 | - | 24.2 | 114 |
| 9/2/87 | AM | 100 | 68 | 26.5 | 4 1/4 | - | 23.4 | 115 |
| 9/2/87 | PM | 100 | 67 | 24.8 | 3* | - | 22.8 | 115 |
| 9/3/87 | AM | 100 | 68 | 26.9 | 4 | - | 24.6 | 115 |
| 9/3/87 | PM | 99 | 66 | 24.6 | 4 1/2 | - | 24.6 | 115 |
| 9/4/87 | AM | 94 | 65 | 30.3 | 3 3/4* | - | 25.9 | - |
| 9/8/87 | AM | 100 | 70 | 29.7 | 4 1/4 | - | 27.2 | 115 |
| 9/10/87 | AM | 98 | 69 | 39.9 | 4 3/4 | 9.5 | 27.4 | 112 |
| 9/10/87 | PM | 99 | 69 | 39.7 | 4 1/2 | - | - | 112 |
| 9/11/87 | AM | 100 | 68 | 34.0 | 4 1/4 | 8.0 | 28.8 | 114 |
| 9/14/87 | AM | 100 | 69 | 31.2 | 4 1/2 | 6.5 | 27.3 | 114 |

BACKFILL TESTING
(Cont'd.)

| Date | AM/PM | Gradation - % Passing | | | Average Slump (IN) | Filtrate Loss (%) | Moisture Content (%) | Wet Density (PCF) |
|----------------|-------|-----------------------|-------|-------|--------------------|-------------------|----------------------|-------------------|
| | | 3/8" | #40 | #200 | | | | |
| Required Range | | 65-100 | 30-70 | 20-40 | 4-6 | | | ≥100 |
| 9/14/87 | PM | 100 | 66 | 37.5 | 5 3/4 | - | 24.9 | 114 |
| 9/15/87 | AM | 100 | 70 | 37.4 | 4 | 7.0 | 26.5 | 115 |
| 9/15/87 | PM | 100 | 69 | 26.4 | 5 | - | 23.0 | - |
| 9/15/87 | PM | 100 | 68 | 35.1 | 5 | - | 30.2 | - |
| 9/16/87 | AM | 98 | 69 | 25.1 | 4 1/4 | 16.5 | 22.6 | 115 |
| 9/16/87 | PM | 95 | 61 | 24.2 | 4 1/4 | - | 22.0 | - |
| 9/17/87 | AM | 98 | 69 | 31.5 | 4 | 9.5 | 26.4 | 115 |
| 9/17/87 | PM | 99 | 69 | 29.1 | 4 1/2 | - | 27.6 | - |
| 9/21/87 | AM | 99 | 68 | 36.5 | 4 1/2 | - | 27.4 | 115 |
| 9/22/87 | AM | 99 | 68 | 35.8 | 4 | 16.5 | 23.8 | 114 |
| 9/23/87 | AM | 100 | 69 | 39.7 | 4 | 13.0 | 24.3 | 115 |
| 9/23/87 | PM | 100 | 68 | 39.2 | 4 1/2 | - | 24.9 | - |
| 9/23/87 | PM | 99 | 68 | 26.4 | 4 3/4 | - | 24.3 | - |
| 9/24/87 | AM | 100 | 63 | 23.6 | 4 | 12.5 | 16.1 | 115 |
| 9/24/87 | PM | 100 | 63 | 23.8 | 4 3/4 | - | 22.3 | - |
| 9/25/87 | AM | 100 | 65 | 24.8 | 4 3/4 | 8.5 | 24.7 | 114 |
| 9/25/87 | PM | 100 | 69 | 27.5 | 4 3/4 | - | 21.3 | - |
| 9/28/87 | AM | 97 | 67 | 27.7 | 4 | 11.0 | 21.5 | 114 |
| 9/28/87 | PM | 100 | 70 | 39.0 | 4 3/4 | - | 23.8 | - |
| 9/29/87 | AM | 100 | 67 | 24.6 | 4 1/8 | 15.0 | 21.9 | - |
| 9/29/87 | PM | 99 | 59 | 21.6 | 4 | - | 21.9 | - |
| 9/30/87 | PM | 99 | 62 | 25.1 | 4 3/4 | 11.0 | 22.7 | 115 |
| 10/1/87 | AM | 99 | 65 | 27.3 | 4 1/4 | 12.5 | 27.5 | 115 |

BACKFILL TESTING
(Cont'd.)

| Date | AM/PM | Gradation - % Passing | | | Average Slump (IN) | Filtrate Loss (%) | Moisture Content (%) | Wet Density (PCF) |
|----------------|-------|-----------------------|-------|-------|--------------------------|-------------------------|----------------------------|-------------------------|
| | | 3/8" | #40 | #200 | | | | |
| Required Range | | 65-100 | 30-70 | 20-40 | 4-6 | | | ≥100 |
| 10/1/87 | PM | 100 | 65 | 29.2 | 4 3/4 | - | 23.7 | - |
| 10/5/87 | AM | 100 | 65 | 25.4 | 4 1/2 | - | 24.7 | 115 |
| 10/5/87 | PM | 100 | 64 | 24.9 | 4 1/2 | - | 23.9 | 115 |
| 10/6/87 | AM | 100 | 64 | 24.5 | 4 1/4 | - | 25.7 | 115 |
| 10/6/87 | PM | 100 | 64 | 23.9 | 4 1/2 | - | 24.9 | - |
| 10/7/87 | AM | 100 | 65 | 27.6 | 4 1/4 | 10.0 | 23.9 | 115 |
| 10/7/87 | PM | 99 | 55 | 21.5 | 4 3/8 | - | 20.8 | 115 |
| 10/8/87 | AM | 99 | 64 | 23.6 | 4 3/8 | 19.0 | 21.4 | 115 |
| 10/8/87 | PM | 100 | 66 | 31.4 | 4 3/8 | - | 25.6 | - |
| 10/9/87 | AM | 100 | 63 | 27.6 | 4 | 9.5 | 25.2 | 115 |
| 10/9/87 | PM | 100 | 58 | 21.7 | 4 1/8 | - | 20.6 | - |
| 10/10/87 | AM | 100 | 69 | 26.6 | 4 | 14.0 | 20.9 | 115 |
| 10/10/87 | PM | 99 | 68 | 26.8 | 4 | - | 23.1 | - |
| 10/12/87 | AM | 99 | 66 | 22.5 | 4 1/4 | 19.0 | 20.8 | 115 |
| 10/12/87 | PM | 99 | 68 | 24.4 | 4 1/8 | 19.0 | 24.1 | - |
| 10/13/87 | AM | 99 | 61 | 21.0 | 4 1/4 | 13.5 | 19.5 | 115 |
| 10/13/87 | PM | 100 | 63 | 23.7 | 4 1/2 | - | 20.9 | - |
| 10/13/87 | PM | 100 | 66 | 22.0 | 4 | - | 20.7 | - |
| 10/14/87 | AM | 100 | 63 | 23.6 | 4 1/2 | 22.0 | 20.4 | 115 |
| 10/14/87 | PM | 100 | 64 | 21.3 | 4 | - | 20.7 | - |
| 10/14/87 | PM | 99 | 62 | 24.1 | 4 1/4 | - | 23.0 | - |
| 10/15/87 | AM | 100 | 69 | 23.2 | 4 | 19.0 | 20.6 | 114 |
| 10/15/87 | PM | 100 | 67 | 25.4 | 4 3/8 | - | 21.9 | - |
| 10/16/87 | AM | 100 | 64 | 28.3 | 4 1/4 | 17.0 | 23.6 | 115 |

BACKFILL TESTING
(Cont'd.)

| Date | AM/PM | Gradation - % Passing | | | Average Slump (IN) | Filtrate Loss (%) | Moisture Content (%) | Wet Density (PCF) |
|----------------|-------|-----------------------|-------|-------|--------------------|-------------------|----------------------|-------------------|
| | | 3/8* | #40 | #200 | | | | |
| Required Range | | 65-100 | 30-70 | 20-40 | 4-6 | | | ≥100 |
| 10/16/87 | PM | 99 | 62 | 22.0 | 4 1/4 | - | 19.9 | - |
| 10/19/87 | AM | 99 | 63 | 22.6 | 4 1/8 | 16.0 | 20.8 | 115 |
| 10/19/87 | PM | 99 | 65 | 22.9 | 3 7/8* | - | 20.5 | - |
| 10/20/87 | AM | 99 | 67 | 28.6 | 4 1/4 | 9.5 | 22.7 | 115 |
| 10/20/87 | PM | 100 | 65 | 23.9 | 4 1/2 | - | 21.7 | - |
| 10/21/87 | AM | 100 | 64 | 22.9 | 4 1/4 | 17.0 | 20.7 | 115 |
| 10/21/87 | PM | 100 | 66 | 22.0 | 4 1/4 | - | 21.5 | - |
| 10/21/87 | PM | 100 | 66 | 24.7 | 3 7/8* | - | 20.9 | - |
| 10/22/87 | AM | 100 | 67 | 27.4 | 3 7/8* | 13.5 | 21.4 | 114 |
| 10/22/87 | PM | 98 | 64 | 23.9 | 4 | - | 23.9 | - |
| 10/22/87 | PM | 99 | 64 | 26.8 | 4 1/4 | - | 19.8 | - |
| 10/26/87 | AM | 100 | 66 | 28.9 | 3 7/8* | 9.0 | - | 115 |
| 10/27/87 | AM | 99 | 67 | 31.8 | 3 7/8* | 8.0 | 25.1 | 114 |
| 10/27/87 | PM | 99 | 67 | 31.8 | 4 | - | 22.3 | - |
| 10/29/87 | AM | 100 | 63 | 26.3 | 4 1/4 | 10.5 | 24.0 | 115 |
| 10/29/87 | PM | 99 | 64 | 30.6 | 4 1/8 | - | 24.9 | - |
| 10/30/87 | AM | 100 | 64 | 30.4 | 4 1/8 | - | - | 115 |

**KINGSBURY SITE REMEDIAL PROGRAM
IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP**

IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|--------|---------------|-------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 5/8/87 | 1+65 | 17+15 | Elev. 192 | 112.4 | 1.3 | 118.0 | 12.9 | 95.3 |
| 5/8/87 | 2+40 | 17+60 | Elev. 194 | 114.6 | 2.0 | 118.0 | 12.9 | 97.1 |
| 5/8/87 | 3+45 | 17+10 | Elev. 196 | 113.8 | 3.0 | 118.0 | 12.9 | 96.4 |
| 5/8/87 | 4+75 | 17+05 | Elev. 197 | 115.8 | 3.6 | 118.0 | 12.9 | 98.2 |
| 5/8/87 | 5+95 | 17+20 | Elev. 200 | 114.5 | 2.3 | 118.0 | 12.9 | 97.0 |
| 5/8/87 | 6+80 | 16+80 | Elev. 201 | 108.3 | 3.1 | 118.0 | 12.9 | 91.8 |
| 5/8/87 | 7+80 | 16+00 | Elev. 202 | 114.2 | 1.9 | 118.0 | 12.9 | 96.8 |
| 5/8/87 | 8+85 | 16+20 | Elev. 204 | 111.8 | 2.5 | 118.0 | 12.9 | 94.7 |
| 5/8/87 | 9+75 | 15+40 | Elev. 205 | 114.0 | 2.8 | 118.0 | 12.9 | 96.9 |
| 5/8/87 | 10+35 | 14+70 | Elev. 204 | 114.8 | 2.3 | 118.0 | 12.9 | 97.3 |
| 5/8/87 | 10+45 | 14+00 | Elev. 204 | 112.9 | 2.8 | 118.0 | 12.9 | 95.7 |
| 5/4/87 | 2+40 | 17+40 | Elev. 193 | 111.0 | 2.6 | 118.0 | 12.9 | 94.0 |
| 5/4/87 | 3+30 | 17+60 | Elev. 193 | 118.2 | 2.1 | 118.0 | 12.9 | 100.0 |
| 5/4/87 | 4+60 | 16+90 | Elev. 194 | 107.9 | 3.0 | 118.0 | 12.9 | 91.4 |
| 5/4/87 | 5+90 | 16+90 | Elev. 195 | 114.2 | 1.8 | 118.0 | 12.9 | 96.7 |
| 5/4/87 | 7+10 | 16+20 | Elev. 197 | 109.5 | 2.1 | 118.0 | 12.9 | 92.7 |
| 5/4/87 | 7+80 | 15+90 | Elev. 198 | 108.0 | 1.9 | 118.0 | 12.9 | 92.2 |
| 5/4/87 | 8+75 | 16+15 | Elev. 199 | 117.7 | 4.7 | 118.0 | 12.9 | 99.7 |
| 5/4/87 | 9+50 | 15+85 | Elev. 200 | 109.6 | 4.3 | 118.0 | 12.9 | 92.9 |
| 5/4/87 | 10+25 | 15+80 | Elev. 201 | 118.8 | 3.0 | 118.0 | 12.9 | 100.0 |
| 5/4/87 | 10+50 | 14+70 | Elev. 201 | 117.6 | 2.3 | 118.0 | 12.9 | 99.6 |
| 5/4/87 | 10+90 | 14+10 | Elev. 202 | 112.0 | 1.9 | 118.0 | 12.9 | 94.9 |
| 5/6/87 | 1+80 | 17+00 | Elev. 195 | 108.4 | 5.2 | 118.0 | 12.9 | 91.9 |

IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|---------|---------------|-------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 5/6/87 | 2+55 | 17+35 | Elev. 195 | 113.8 | 2.7 | 118.0 | 12.9 | 96.4 |
| 5/6/87 | 3+50 | 17+20 | Elev. 197 | 109.6 | 3.2 | 118.0 | 12.9 | 92.8 |
| 5/6/87 | 4+70 | 17+00 | Elev. 197 | 107.2 | 4.7 | 118.0 | 12.9 | 90.8 |
| 5/6/87 | 5+90 | 16+95 | Elev. 199 | 111.2 | 2.5 | 118.0 | 12.9 | 94.2 |
| 5/6/87 | 7+25 | 16+30 | Elev. 199 | 114.6 | 3.6 | 118.0 | 12.9 | 97.1 |
| 5/6/87 | 8+60 | 15+90 | Elev. 200 | 115.4 | 4.7 | 118.0 | 12.9 | 97.7 |
| 5/6/87 | 9+25 | 15+55 | Elev. 200 | 114.0 | 2.9 | 118.0 | 12.9 | 96.6 |
| 5/6/87 | 10+60 | 14+90 | Elev. 201 | 120.4 | 3.0 | 118.0 | 12.9 | 100.0 |
| 5/6/87 | 10+85 | 14+10 | Elev. 205 | 118.6 | 2.1 | 118.0 | 12.9 | 100.0 |
| 5/6/87 | 1+80 | 17+00 | Elev. 195 | 108.4 | 5.2 | 118.0 | 12.9 | 91.9 |
| 5/6/87 | 2+55 | 17+35 | Elev. 195 | 113.8 | 2.7 | 118.0 | 12.9 | 96.4 |
| 5/6/87 | 3+50 | 17+20 | Elev. 197 | 109.6 | 3.2 | 118.0 | 12.9 | 92.8 |
| 5/6/87 | 4+70 | 17+00 | Elev. 197 | 107.2 | 4.7 | 118.0 | 12.9 | 90.8 |
| 5/6/87 | 5+90 | 16+95 | Elev. 199 | 111.2 | 2.5 | 118.0 | 12.9 | 94.2 |
| 5/6/87 | 7+25 | 16+30 | Elev. 199 | 114.6 | 3.6 | 118.0 | 12.9 | 97.1 |
| 5/6/87 | 8+60 | 15+90 | Elev. 200 | 115.4 | 4.7 | 118.0 | 12.9 | 97.7 |
| 5/6/87 | 9+25 | 15+55 | Elev. 200 | 114.0 | 2.9 | 118.0 | 12.9 | 96.6 |
| 5/6/87 | 10+60 | 14+90 | Elev. 201 | 120.4 | 3.0 | 118.0 | 12.9 | 100.0 |
| 5/6/87 | 10+85 | 14+10 | Elev. 205 | 118.6 | 2.1 | 118.0 | 12.9 | 100.0 |
| 4/28/87 | 1+35 | 17+30 | Elev. 191 | 108.0 | 1.3 | 118.0 | 12.9 | 91.5 |
| 4/28/87 | 2+50 | 17+70 | Elev. 192 | 108.7 | 4.2 | 118.0 | 12.9 | 92.1 |
| 4/28/87 | 3+25 | 17+20 | Elev. 193 | 110.2 | 5.1 | 118.0 | 12.9 | 93.4 |
| 4/28/87 | 4+35 | 17+10 | Elev. 193 | 110.8 | 5.5 | 118.0 | 12.9 | 93.8 |

IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|---------|---------------|---------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 4/28/87 | 5+40 | 16+80 | Elev. 193 | 110.7 | 4.4 | 118.0 | 12.9 | 93.8 |
| 4/28/87 | 6+30 | 16+95 | Elev. 193 | 113.2 | 2.4 | 118.0 | 12.9 | 95.9 |
| 4/28/87 | 7+55 | 16+50 | Elev. 194 | 112.6 | 4.1 | 118.0 | 12.9 | 95.4 |
| 4/28/87 | 8+80 | 15+80 | Elev. 195 | 114.7 | 4.8 | 118.0 | 12.9 | 97.2 |
| 4/28/87 | 9+35 | 15+25 | Elev. 195 | 115.3 | 3.5 | 118.0 | 12.9 | 97.7 |
| 4/28/87 | 10+55 | 15+25 | Elev. 193 | 114.0 | 3.1 | 118.0 | 12.9 | 96.6 |
| 4/30/87 | 1+30 | 17+70 | Elev. 192 | 113.8 | 4.1 | 118.0 | 12.9 | 96.4 |
| 4/30/87 | 1+90 | 17+00 | Elev. 192 | 110.4 | 3.2 | 118.0 | 12.9 | 93.5 |
| 4/30/87 | 3+15 | 17+20 | Elev. 192 | 113.0 | 2.3 | 118.0 | 12.9 | 95.8 |
| 4/30/87 | 4+60 | 16+70 | Elev. 194 | 111.0 | 3.1 | 118.0 | 12.9 | 94.1 |
| 4/30/87 | 5+35 | 17+25 | Elev. 194 | 112.2 | 1.7 | 118.0 | 12.9 | 95.1 |
| 4/30/87 | 6+65 | 16+40 | Elev. 194 | 115.6 | 4.4 | 118.0 | 12.9 | 97.9 |
| 4/30/87 | 7+45 | 16+05 | Elev. 195 | 115.1 | 6.2 | 118.0 | 12.9 | 97.5 |
| 4/30/87 | 8+60 | 16+40 | Elev. 195 | 112.1 | 5.2 | 118.0 | 12.9 | 95.0 |
| 4/30/87 | 9+80 | 15+90 | Elev. 196 | 115.4 | 3.6 | 118.0 | 12.9 | 97.8 |
| 4/30/87 | 10+60 | 14+90 | Elev. 197 | 113.2 | 5.2 | 118.0 | 12.9 | 95.9 |
| 4/30/87 | 10+45 | 14+15 | Elev. 198 | 112.2 | 4.3 | 118.0 | 12.9 | 95.1 |
| 4/8/87 | 12+10 | 0+20 | 18.0 | 115.6 | 5.6 | 118.0 | 12.9 | 98.0 |
| 4/8/87 | 8+40 | 15+80 | 18.0 | 117.0 | 7.9 | 118.0 | 12.9 | 99.1 |
| 4/8/87 | 8+00 | 16+00 | 18.0 | 115.5 | 6.5 | 118.0 | 12.9 | 97.9 |
| 4/8/87 | 7+30 | 16+00 | 18.0 | 114.4 | 5.0 | 118.0 | 12.9 | 96.9 |
| 4/8/87 | 8+90 | on wall | 18.0 | 106.5 | 5.7 | 118.0 | 12.9 | 90.2 |
| 4/8/87 | 8+35 | on wall | 18.0 | 113.5 | 5.2 | 118.0 | 12.9 | 96.2 |

IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|---------|---------------|---------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 4/8/87 | 7+75 | on wall | 18.0 | 112.4 | 4.0 | 118.0 | 12.9 | 95.2 |
| 4/20/87 | 1+70 | 17+30 | Elev. 182 | 112.2 | 3.7 | 118.0 | 12.9 | 95.1 |
| 4/20/87 | 3+85 | 17+10 | Elev. 185 | 108.5 | 3.7 | 118.0 | 12.9 | 92.0 |
| 4/20/87 | 4+85 | 16+35 | Elev. 186 | 113.9 | 1.4 | 118.0 | 12.9 | 96.5 |
| 4/20/87 | 6+20 | 16+90 | Elev. 187 | 111.2 | 3.1 | 118.0 | 12.9 | 94.2 |
| 4/20/87 | 7+10 | 16+65 | Elev. 188 | 108.6 | 1.7 | 118.0 | 12.9 | 92.0 |
| 4/20/87 | 8+00 | 16+25 | Elev. 190 | 111.5 | 1.4 | 118.0 | 12.9 | 94.4 |
| 4/20/87 | 8+60 | 15+90 | Elev. 193 | 113.6 | 3.0 | 118.0 | 12.9 | 96.3 |
| 4/20/87 | 10+05 | 15+25 | Elev. 192 | 118.0 | 1.7 | 118.0 | 12.9 | 100.0 |
| 4/20/87 | 1+75 | 17+20 | Elev. 182 | 111.9 | 2.9 | 118.0 | 12.9 | 94.8 |
| 4/22/87 | 2+60 | 17+75 | Elev. 183 | 112.8 | 1.9 | 118.0 | 12.9 | 95.6 |
| 4/22/87 | 3+95 | 16+85 | Elev. 184 | 109.8 | 9.2 | 118.0 | 12.9 | 93.0 |
| 4/22/87 | 5+00 | 16+45 | Elev. 184 | 111.0 | 4.2s | 118.0 | 12.9 | 94.0 |
| 4/22/87 | 6+60 | 16+45 | Elev. 184 | 108.6 | 8.2 | 118.0 | 12.9 | 92.0 |
| 4/22/87 | 7+70 | 16+05 | Elev. 184 | 112.2 | 6.9 | 118.0 | 12.9 | 95.0 |
| 4/22/87 | 8+75 | 16+05 | Elev. 184 | 113.9 | 3.9 | 118.0 | 12.9 | 96.5 |
| 4/22/87 | 10+00 | 15+85 | Elev. 184 | 112.9 | 9.0 | 118.0 | 12.9 | 95.6 |
| 4/24/87 | 1+30 | 17+70 | Elev. 184 | 111.7 | 2.0 | 118.0 | 12.9 | 94.7 |
| 4/24/87 | 2+70 | 17+65 | Elev. 184 | 113.0 | 2.2 | 118.0 | 12.9 | 95.8 |
| 4/24/87 | 3+25 | 17+50 | Elev. 186 | 110.5 | 5.5 | 118.0 | 12.9 | 94.6 |
| 4/24/87 | 4+30 | 17+25 | Elev. 187 | 109.6 | 3.5 | 118.0 | 12.9 | 92.9 |
| 4/24/87 | 5+40 | 16+90 | Elev. 188 | 109.3 | 4.3 | 118.0 | 12.9 | 92.6 |
| 4/24/87 | 6+50 | 16+70 | Elev. 189 | 112.3 | 2.3 | 118.0 | 12.9 | 95.2 |

IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|---------|---------------|-------------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 4/24/87 | 7+80 | 16+15 | Elev. 193 | 112.4 | 5.5 | 118.0 | 12.9 | 95.3 |
| 4/24/87 | 9+00 | 15+80 | Elev. 196.5 | 110.7 | 3.4 | 118.0 | 12.9 | 93.0 |
| 4/24/87 | 10+10 | 15+80 | Elev. 194 | 109.8 | 2.0 | 118.0 | 12.9 | 93.0 |
| 4/24/87 | 10+90 | 15+10 | Elev. 194.0 | 109.8 | 2.6 | 118.0 | 12.9 | 93.0 |
| 4/17/87 | 1+50 | 17+90 | 21.0 | 111.6 | 2.0 | 118.0 | 12.9 | 94.5 |
| 4/17/87 | 2+25 | 17+40 | 21.0 | 109.8 | 1.5 | 118.0 | 12.9 | 93.0 |
| 4/17/87 | 3+00 | 17+15 | 18.0 | 114.9 | 1.4 | 118.0 | 12.9 | 97.4 |
| 4/17/87 | 3+90 | 17+45 | 21.0 | 114.6 | 2.4 | 118.0 | 12.9 | 97.1 |
| 4/17/87 | 5+50 | 16+95 | 21.0 | 104.8 | 1.4 | 118.0 | 12.9 | 88.8 |
| 4/17/87 | 6+20 | 16+35 | 21.0 | 115.8 | 2.0 | 118.0 | 12.9 | 98.1 |
| 4/17/87 | 7+35 | 16+60 | 21.0 | 105.2 | 1.2 | 118.0 | 12.9 | 89.2 |
| 4/17/87 | 8+00 | 16+50 | 21.0 | 108.4 | 1.5 | 118.0 | 12.9 | 91.8 |
| 4/17/87 | 8+75 | 15+90 | 21.0 | 113.2 | 2.8 | 118.0 | 12.9 | 95.9 |
| 4/17/87 | 10+25 | 15+50 | 21.0 | 112.1 | 1.8 | 118.0 | 12.9 | 95.0 |
| 4/17/87 | 8+75 | 8+25 | 25.3 | 110.1 | 2.3 | 118.0 | 12.9 | 93.3 |
| 4/17/87 | 9+75 | 9+50 | 25.3 | 106.2 | 1.2 | 118.0 | 12.9 | 90.0 |
| 4/17/87 | 7+75 | 7+60 | 25.3 | 110.2 | 2.0 | 118.0 | 12.9 | 93.4 |
| 6/2/88 | 4+00-6+00 | 11+00-13+00 | 4.5 | 99.9 | 17.5 | 106.9 | 21.3 | 93.4 |
| 6/2/88 | 4+00-6+00 | 11+00-13+00 | 4.5 | 96.0 | 18.7 | 106.9 | 21.3 | 89.8 |
| 6/2/88 | 4+00-6+00 | 11+00-13+00 | 4.5 | 94.4 | 19.3 | 106.9 | 21.3 | 88.3 |
| 6/2/88 | 4+00-6+00 | 11+00-13+00 | 4.5 | 101.8 | 17.1 | 106.9 | 21.3 | 95.2 |
| 6/2/88 | 4+00-6+00 | 9+00-11+00 | 4.5 | 98.4 | 18.1 | 106.9 | 21.3 | 92.0 |
| 6/2/88 | 4+00-6+00 | 9+00-11+00 | 4.5 | 99.5 | 12.6 | 106.9 | 21.3 | 93.1 |

IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|--------|---------------|-------------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 6/2/88 | 4+00-6+00 | 9+00-11+00 | 4.5 | 89.6 | 21.6 | 106.9 | 21.3 | 83.8 |
| 6/2/88 | 4+00-6+00 | 9+00-11+00 | 4.5 | 93.6 | 20.2 | 106.9 | 21.3 | 87.5 |
| 6/2/88 | 4+00-6+00 | 7+00-9+00 | 4.5 | 98.5 | 16.8 | 106.9 | 21.3 | 92.2 |
| 6/2/88 | 4+00-6+00 | 7+00-9+00 | 4.5 | 91.9 | 20.0 | 106.9 | 21.3 | 85.9 |
| 6/2/88 | 4+00-6+00 | 7+00-9+00 | 4.5 | 92.9 | 20.1 | 106.9 | 21.3 | 86.8 |
| 6/2/88 | 4+00-6+00 | 7+00-9+00 | 4.5 | 92.8 | 19.7 | 106.9 | 21.3 | 86.7 |
| 6/2/88 | 3+00-6+00 | 6+00-7+00 | 4.5 | 87.6 | 27.9 | 106.9 | 21.3 | 81.9 |
| 6/2/88 | 3+00-6+00 | 6+00-7+00 | 4.5 | 90.1 | 23.5 | 106.9 | 21.3 | 84.3 |
| 6/2/88 | 3+00-6+00 | 6+00-7+00 | 4.5 | 90.1 | 25.1 | 106.9 | 21.3 | 84.3 |
| 6/2/88 | 3+00-6+00 | 6+00-7+00 | 4.5 | 95.1 | 18.4 | 106.9 | 23.0 | 89.0 |
| 6/2/88 | 3+00-4+00 | 7+00-11+00 | 4.5 | 91.8 | 19.7 | 106.9 | 23.0 | 85.9 |
| 6/2/88 | 3+00-4+00 | 7+00-11+00 | 4.5 | 91.3 | 19.7 | 106.9 | 23.0 | 85.4 |
| 6/2/88 | 3+00-4+00 | 7+00-11+00 | 4.5 | 88.8 | 18.6 | 106.9 | 23.0 | 83.0 |
| 6/2/88 | 3+00-4+00 | 7+00-11+00 | 4.5 | 91.2 | 19.0 | 106.9 | 23.0 | 85.3 |
| 6/2/88 | 2+00-4+00 | 11+00-13+00 | 4.5 | 84.8 | 23.7 | 106.9 | 23.0 | 79.3 |
| 6/2/88 | 2+00-4+00 | 11+00-13+00 | 4.5 | 91.1 | 22.1 | 106.9 | 23.0 | 85.2 |
| 6/2/88 | 2+00-4+00 | 11+00-13+00 | 4.5 | 89.8 | 25.6 | 106.9 | 23.0 | 84.0 |
| 6/2/88 | 2+00-4+00 | 11+00-13+00 | 4.5 | 95.1 | 19.3 | 106.9 | 23.0 | 89.0 |
| 6/2/88 | 6+00-8+00 | 11+00-13+00 | 4.5 | 99.6 | 16.1 | 106.9 | 23.0 | 93.1 |
| 6/2/88 | 6+00-8+00 | 11+00-13+00 | 4.5 | 96.7 | 23.3 | 106.9 | 23.0 | 90.5 |
| 6/2/88 | 6+00-8+00 | 11+00-13+00 | 4.5 | 101.3 | 16.5 | 106.9 | 23.0 | 94.7 |
| 6/2/88 | 6+00-8+00 | 11+00-13+00 | 4.5 | 99.8 | 18.0 | 106.9 | 23.0 | 93.4 |
| 6/2/88 | 6+00-8+00 | 9+00-11+00 | 4.5 | 94.9 | 20.3 | 106.9 | 23.0 | 88.7 |

IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|---------|---------------|-------------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 6/2/88 | 6+00-8+00 | 9+00-11+00 | 4.5 | 91.2 | 25.9 | 106.9 | 23.0 | 85.2 |
| 6/2/88 | 6+00-8+00 | 11+00-9+00 | 4.5 | 101.4 | 19.0 | 106.9 | 21.3 | 94.8 |
| 6/2/88 | 6+00-8+00 | 11+00-9+00 | 4.5 | 100.9 | 17.5 | 106.9 | 21.3 | 94.3 |
| 6/2/88 | 8+00-10+00 | 13+00-11+00 | 4.5 | 96.6 | 21.9 | 106.9 | 21.3 | 90.4 |
| 6/2/88 | 8+00-10+00 | 13+00-11+00 | 4.5 | 97.9 | 16.3 | 106.9 | 21.3 | 91.5 |
| 6/2/88 | 8+00-10+00 | 13+00-11+00 | 4.5 | 99.5 | 20.3 | 106.9 | 21.3 | 93.0 |
| 6/2/88 | 8+00-10+00 | 13+00-11+00 | 4.5 | 97.2 | 18.5 | 106.9 | 21.3 | 90.9 |
| 6/2/88 | 6+00-8+00 | 11+00-9+00 | 4.0 | 101.7 | 18.2 | 106.9 | 21.3 | 95.1 |
| 6/7/88 | 6+00-8+00 | 11+00-9+00 | 4.0 | 96.6 | 16.6 | 106.9 | 21.3 | 90.3 |
| 6/7/88 | 6+00-8+00 | 11+00-9+00 | 4.0 | 101.3 | 21.0 | 106.9 | 21.3 | 94.8 |
| 6/7/88 | 6+00-8+00 | 11+00-9+00 | 4.0 | 97.7 | 19.6 | 106.9 | 21.3 | 91.4 |
| 6/7/88 | 7+00-9+00 | 13+00-11+00 | 4.0 | 97.5 | 18.4 | 106.9 | 21.3 | 91.2 |
| 6/7/88 | 7+00-9+00 | 13+00-11+00 | 4.0 | 101.0 | 15.3 | 106.9 | 21.3 | 94.4 |
| 6/7/88 | 7+00-9+00 | 13+00-11+00 | 4.0 | 90.0 | 24.1 | 106.9 | 21.3 | 84.2 |
| 6/7/88 | 7+00-9+00 | 13+00-11+00 | 4.0 | 97.2 | 18.7 | 106.9 | 21.3 | 91.5 |
| 6/11/88 | 5+50-9+50 | 10+00-11+00 | 3.0 | 94.1 | 18.7 | 104.8 | 22.6 | 89.8 |
| 6/11/88 | 5+50-2+50 | 11+00-12+00 | 3.5 | 93.9 | 25.9 | 104.8 | 22.6 | 89.6 |
| 6/11/88 | 5+50-2+50 | 12+00-13+00 | 3.5 | 96.9 | 22.4 | 104.8 | 22.6 | 92.5 |
| 6/11/88 | 5+50-2+50 | 12+00-13+00 | 3.5 | 95.3 | 21.9 | 104.8 | 22.6 | 90.9 |
| 6/11/88 | 5+50-2+50 | 12+00-13+00 | 3.5 | 93.8 | 17.4 | 104.8 | 22.6 | 89.4 |
| 6/11/88 | 5+50-2+50 | 12+00-13+00 | 3.5 | 95.8 | 21.3 | 104.8 | 22.6 | 90.4 |
| 6/11/88 | 5+50-2+00 | 14+00-15+00 | 4.0 | 104.3 | 14.0 | 104.8 | 22.6 | 104.3 |
| 6/11/88 | 5+50-2+00 | 14+00-15+00 | 4.0 | 105.4 | 16.3 | 104.8 | 22.6 | 100.6 |

IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|---------|---------------|-------------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 6/11/88 | 5+50-2+00 | 14+00-15+00 | 4.0 | 98.3 | 19.2 | 104.8 | 22.6 | 93.8 |
| 6/11/88 | 5+50-2+00 | 14+00-15+00 | 4.0 | 101.4 | 18.5 | 104.8 | 22.6 | 96.7 |
| 6/11/88 | 2+00-5+00 | 15+00-16+50 | 4.0 | 100.6 | 17.9 | 104.8 | 22.6 | 96.0 |
| 6/11/88 | 2+00-5+00 | 15+00-16+50 | 4.0 | 93.3 | 21.7 | 104.8 | 22.6 | 89.0 |
| 6/11/88 | 2+00-5+00 | 15+00-16+50 | 4.0 | 94.7 | 23.4 | 104.8 | 22.6 | 90.4 |
| 6/11/88 | 2+00-5+00 | 15+00-16+50 | 4.0 | 101.0 | 16.8 | 104.8 | 22.6 | 96.3 |
| 6/13/88 | 5+50-8+50 | 16+00-14+50 | 4.0 | 105.8 | 16.7 | 104.8 | 22.6 | 100 |
| 6/13/88 | 5+50-8+50 | 16+00-14+50 | 4.0 | 96.3 | 15.7 | 104.8 | 22.6 | 91.9 |
| 6/11/88 | 5+50-9+50 | 10+00-11+00 | 3.0 | 93.4 | 20.8 | 104.8 | 22.6 | 89.1 |
| 6/11/88 | 5+50-9+50 | 10+00-11+00 | 3.0 | 93.8 | 23.0 | 104.8 | 22.6 | 89.5 |
| 6/11/88 | 5+50-9+50 | 10+00-11+00 | 3.0 | 95.2 | 21.7 | 104.8 | 22.6 | 90.8 |
| 6/11/88 | 9+50-5+50 | 9+00-10+00 | 3.0 | 94.6 | 25.7 | 104.8 | 22.6 | 90.2 |
| 6/11/88 | 9+50-5+50 | 9+00-10+00 | 3.0 | 96.1 | 21.7 | 104.8 | 22.6 | 91.7 |
| 6/11/88 | 9+50-5+50 | 9+00-10+00 | 3.0 | 96.2 | 27.0 | 104.8 | 22.6 | 91.8 |
| 6/11/88 | 9+50-5+50 | 9+00-10+00 | 3.0 | 94.0 | 27.0 | 104.8 | 22.6 | 89.7 |
| 6/11/88 | 3+00-5+50 | 9+00-10+00 | 3.5 | 94.0 | 23.2 | 104.8 | 22.6 | 89.7 |
| 6/11/88 | 3+00-5+50 | 9+00-10+00 | 3.5 | 96.8 | 19.2 | 104.8 | 22.6 | 92.3 |
| 6/11/88 | 3+50-5+50 | 10+00-11+00 | 3.5 | 95.0 | 22.4 | 104.8 | 22.6 | 90.7 |
| 6/11/88 | 3+50-5+50 | 10+00-11+00 | 3.5 | 96.2 | 21.8 | 104.8 | 22.6 | 91.8 |
| 6/11/88 | 3+50-5+50 | 10+00-11+00 | 3.5 | 96.1 | 21.5 | 104.8 | 22.6 | 91.7 |
| 6/11/88 | 5+50-2+50 | 11+00-12+00 | 3.5 | 95.3 | 24.6 | 104.8 | 22.6 | 90.9 |
| 6/11/88 | 5+50-2+50 | 11+00-12+00 | 3.5 | 93.4 | 22.1 | 104.8 | 22.6 | 93.4 |
| 6/11/88 | 5+50-2+50 | 11+00-12+00 | 3.5 | 97.5 | 19.9 | 104.8 | 22.6 | 93.0 |

IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|---------|---------------|-------------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 6/13/88 | 5+50-8+50 | 14+50-16+00 | 4.0 | 84.9 | 17.7 | 104.8 | 22.6 | 81.0 |
| 6/13/88 | 5+50-8+50 | 14+50-16+00 | 4.0 | 96.1 | 11.0 | 104.8 | 22.6 | 91.7 |
| 6/13/88 | 7+50-6+00 | 9+00-6+50 | 3.5 | 100.7 | 17.7 | 104.8 | 22.6 | 96.1 |
| 6/13/88 | 7+50-6+00 | 9+00-6+50 | 3.5 | 94.9 | 19.8 | 104.8 | 22.6 | 90.5 |
| 6/13/88 | 7+50-6+00 | 9+00-6+50 | 3.5 | 89.9 | 23.5 | 104.8 | 22.6 | 85.7 |
| 6/13/88 | 7+50-6+00 | 9+00-6+50 | 3.5 | 85.8 | 27.8 | 104.8 | 22.6 | 81.9 |
| 6/14/88 | 5+50-8+50 | 16+00-14+50 | 4.0 | 97.8 | 16.1 | 104.8 | 22.6 | 93.2 |
| 6/14/88 | 7+50-6+00 | 9+00-6+50 | 3.0 | 95.1 | 22.9 | 104.8 | 22.6 | 90.7 |
| 6/14/88 | 7+50-6+00 | 9+00-6+50 | 3.0 | 94.8 | 20.8 | 104.8 | 22.6 | 90.4 |
| 6/14/88 | 3+00-6+00 | 6+00-9+00 | 3.0 | 89.1 | 20.9 | 104.8 | 22.6 | 85.0 |
| 6/14/88 | 3+00-6+00 | 6+00-9+00 | 3.0 | 96.8 | 18.9 | 104.8 | 22.6 | 92.3 |
| 6/14/88 | 3+00-6+00 | 6+00-9+00 | 3.0 | 96.7 | 18.7 | 104.8 | 22.6 | 92.2 |
| 6/14/88 | 3+00-6+00 | 6+00-9+00 | 3.0 | 94.7 | 19.4 | 104.8 | 22.6 | 90.4 |
| 6/14/88 | 3+00-6+00 | 6+00-9+00 | 3.0 | 93.6 | 25.3 | 104.8 | 22.6 | 89.3 |
| 6/14/88 | 3+00-6+00 | 6+00-9+00 | 3.0 | 94.3 | 17.3 | 104.8 | 22.6 | 90.0 |
| 6/14/88 | 3+00-6+00 | 6+00-9+00 | 3.0 | 94.2 | 15.1 | 104.8 | 22.6 | 89.9 |
| 6/15/88 | 5+00-2+50 | 9+00-11+00 | 3.0 | 97.0 | 17.2 | 104.8 | 22.6 | 92.5 |
| 6/15/88 | 5+00-2+50 | 9+00-11+00 | 3.0 | 94.4 | 16.2 | 104.8 | 22.6 | 90.0 |
| 6/15/88 | 5+00-2+50 | 9+00-11+00 | 3.0 | 93.3 | 20.7 | 104.8 | 22.6 | 89.0 |
| 6/15/88 | 5+00-2+50 | 9+00-11+00 | 3.0 | 101.0 | 19.2 | 104.8 | 22.6 | 96.4 |
| 6/15/88 | 5+00-2+50 | 11+00-13+00 | 3.0 | 96.8 | 14.5 | 104.8 | 22.6 | 92.3 |
| 6/15/88 | 5+00-2+50 | 11+00-13+00 | 3.0 | 97.5 | 19.8 | 104.8 | 22.6 | 93.0 |
| 6/15/88 | 5+00-2+50 | 11+00-13+00 | 3.0 | 98.1 | 22.9 | 104.8 | 22.6 | 93.6 |

IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|---------|---------------|-------------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 6/15/88 | 5+00-2+50 | 11+00-13+00 | 3.0 | 98.1 | 22.6 | 104.8 | 22.6 | 93.6 |
| 6/16/88 | 3+00-6+50 | 13+00-15+00 | 3.5 | 97.8 | 23.2 | 104.8 | 22.6 | 93.3 |
| 6/16/88 | 3+00-6+50 | 13+00-15+00 | 3.5 | 97.6 | 18.7 | 104.8 | 22.6 | 93.1 |
| 6/16/88 | 3+00-6+50 | 13+00-15+00 | 3.5 | 101.4 | 16.4 | 104.8 | 22.6 | 96.7 |
| 6/16/88 | 3+00-6+50 | 13+00-15+00 | 3.5 | 97.7 | 20.2 | 104.8 | 22.6 | 93.2 |
| 6/16/88 | 3+00-6+50 | 13+00-15+00 | 3.5 | 94.8 | 21.5 | 104.8 | 22.6 | 90.4 |
| 6/16/88 | 3+00-6+50 | 13+00-15+00 | 3.5 | 95.0 | 20.8 | 104.8 | 22.6 | 90.6 |
| 6/16/88 | 5+50-9+50 | 12+50-10+50 | 2.25 | 88.3 | 18.7 | 104.8 | 22.6 | 84.2 |
| 6/16/88 | 5+50-9+50 | 12+50-10+50 | 2.25 | 86.1 | 35.1 | 104.8 | 22.6 | 82.1 |
| 6/16/88 | 5+50-9+50 | 12+50-10+50 | 2.25 | 89.3 | 32.0 | 104.8 | 22.6 | 85.2 |
| 6/16/88 | 5+50-9+50 | 12+50-10+50 | 2.25 | 90.3 | 31.2 | 104.8 | 22.6 | 86.1 |
| 6/16/88 | 5+50-9+50 | 12+50-10+50 | 2.25 | 87.1 | 27.8 | 104.8 | 22.6 | 83.1 |
| 6/16/88 | 5+50-9+50 | 12+50-10+50 | 2.25 | 88.1 | 21.7 | 104.8 | 22.6 | 84.0 |
| 6/17/88 | 3+00-8+00 | 15+00-16+50 | 3.5 | 96.0 | 19.2 | 104.8 | 22.6 | 91.5 |
| 6/17/88 | 3+00-8+00 | 15+00-16+50 | 3.5 | 95.6 | 23.3 | 104.8 | 22.6 | 91.2 |
| 6/17/88 | 3+00-8+00 | 15+00-16+50 | 3.5 | 97.0 | 19.0 | 104.8 | 22.6 | 92.6 |
| 6/17/88 | 3+00-8+00 | 15+00-16+50 | 3.5 | 94.1 | 19.5 | 104.8 | 22.6 | 89.7 |
| 6/17/88 | 3+00-8+00 | 15+00-16+50 | 3.5 | 97.7 | 20.5 | 104.8 | 22.6 | 93.2 |
| 6/17/88 | 3+00-8+00 | 15+00-16+50 | 3.5 | 95.2 | 25.0 | 104.8 | 22.6 | 90.8 |
| 6/17/88 | 5+50-9+50 | 10+50-9+50 | 2.25 | 86.7 | 24.0 | 104.8 | 22.6 | 82.7 |
| 6/17/88 | 5+50-9+50 | 10+50-9+50 | 2.25 | 86.7 | 25.4 | 104.8 | 22.6 | 82.7 |
| 6/17/88 | 5+50-9+50 | 10+50-9+50 | 2.25 | 90.0 | 27.0 | 104.8 | 22.6 | 85.9 |
| 6/17/88 | 5+50-9+50 | 10+50-9+50 | 2.25 | 88.9 | 27.0 | 104.8 | 22.6 | 84.8 |

IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|---------|---------------|-------------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 6/10/88 | 3+00-5+00 | 7+50-9+50 | 2.25 | 86.1 | 21.6 | 104.8 | 22.6 | 82.2 |
| 6/10/88 | 3+00-5+00 | 7+50-9+50 | 2.25 | 84.4 | 13.3 | 104.8 | 22.6 | 80.5 |
| 6/10/88 | 3+00-5+00 | 7+50-9+50 | 2.25 | 84.5 | 16.0 | 104.8 | 22.6 | 80.6 |
| 6/10/88 | 3+00-5+00 | 7+50-9+50 | 2.25 | 85.1 | 13.9 | 104.8 | 22.6 | 81.2 |
| 6/10/88 | 3+00-5+00 | 9+50-11+50 | 2.25 | 84.9 | 21.1 | 104.8 | 22.6 | 81.0 |
| 6/10/88 | 3+00-5+00 | 9+50-11+50 | 2.25 | 89.3 | 24.2 | 104.8 | 22.6 | 85.2 |
| 6/10/88 | 3+00-5+00 | 9+50-11+50 | 2.25 | 84.9 | 18.1 | 104.8 | 22.6 | 80.9 |
| 6/10/88 | 3+00-5+00 | 9+50-11+50 | 2.25 | 88.6 | 18.0 | 104.8 | 22.6 | 84.5 |
| 6/21/88 | 3+00-wall | 13+50-16+50 | 3.5 | 94.7 | 21.5 | 104.8 | 22.6 | 90.3 |
| 6/21/88 | 3+00-wall | 13+50-16+50 | 3.5 | 97.0 | 16.7 | 104.8 | 22.6 | 92.6 |
| 6/21/88 | 3+00-wall | 13+50-16+50 | 3.5 | 101.6 | 20.9 | 104.8 | 22.6 | 96.9 |
| 6/21/88 | 3+00-wall | 13+50-16+50 | 3.5 | 97.2 | 17.1s | 104.8 | 22.6 | 92.8 |
| 6/21/88 | 3+00-5+00 | 14+50-wall | 3.0 | 95.7 | 19.8 | 104.8 | 22.6 | 91.3 |
| 6/21/88 | 3+00-5+00 | 14+50-wall | 3.0 | 97.0 | 22.6 | 104.8 | 22.6 | 92.6 |
| 6/21/88 | 3+00-5+00 | 14+50-wall | 3.0 | 94.9 | 24.3 | 104.8 | 22.6 | 90.5 |
| 6/21/88 | 3+00-5+00 | 14+50-wall | 3.0 | 95.3 | 21.3 | 104.8 | 22.6 | 90.9 |
| 6/21/88 | 5+00-7+00 | 14+50-wall | 3.0 | 95.7 | 19.5 | 104.8 | 22.6 | 91.3 |
| 6/21/88 | 5+00-7+00 | 14+50-wall | 3.0 | 97.0 | 24.0 | 104.8 | 22.6 | 92.5 |
| 6/21/88 | 5+00-7+00 | 14+50-wall | 3.0 | 94.3 | 24.4 | 104.8 | 22.6 | 89.9 |
| 6/21/88 | 5+00-7+00 | 14+50-wall | 3.0 | 102.2 | 21.3 | 104.8 | 22.6 | 97.5 |
| 6/22/88 | 6+00-9+00 | 6+00-9+00 | 2.25 | 84.7 | 25.3 | 104.8 | 22.6 | 80.8 |
| 6/22/88 | 6+00-9+00 | 6+00-9+00 | 2.25 | 83.9 | 17.4 | 104.8 | 22.6 | 80.0 |
| 6/22/88 | 6+00-9+00 | 6+00-9+00 | 2.25 | 89.9 | 17.9 | 104.8 | 22.6 | 85.7 |

IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|---------|---------------|-------------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 6/22/88 | 6+00-9+00 | 6+00-9+00 | 2.25 | 89.5 | 13.5 | 104.8 | 22.6 | 85.4 |
| 6/22/88 | 6+00-9+00 | 6+00-9+00 | 2.25 | 89.4 | 17.5 | 104.8 | 22.6 | 85.3 |
| 6/22/88 | 6+00-9+00 | 6+00-9+00 | 2.25 | 87.8 | 20.6 | 104.8 | 22.6 | 83.8 |
| 6/22/88 | 6+00-9+00 | 3+00-6+00 | 2.25 | 86.7 | 14.1 | 104.8 | 22.6 | 82.7 |
| 6/22/88 | 6+00-9+00 | 3+00-6+00 | 2.25 | 87.0 | 30.1 | 104.8 | 22.6 | 83.0 |
| 6/22/88 | 6+00-9+00 | 3+00-6+00 | 2.25 | 86.6 | 31.1 | 104.8 | 22.6 | 82.6 |
| 6/22/88 | 6+00-9+00 | 3+00-6+00 | 2.25 | 89.7 | 13.2 | 104.8 | 22.6 | 85.6 |
| 6/22/88 | 6+00-9+00 | 3+00-6+00 | 2.25 | 88.3 | 15.8 | 104.8 | 22.6 | 84.2 |
| 6/22/88 | 6+00-9+00 | 3+00-6+00 | 2.25 | 85.2 | 33.2 | 104.8 | 22.6 | 81.3 |
| 6/22/88 | 3+00-wall | 13+50-16+50 | 3.0 | 89.5 | 29.7 | 104.8 | 22.6 | 85.7 |
| 6/22/88 | 3+00-wall | 13+50-16+50 | 3.0 | 96.1 | 25.5 | 104.8 | 22.6 | 91.7 |
| 6/22/88 | 3+00-wall | 13+50-16+50 | 3.0 | 91.2 | 26.9 | 104.8 | 22.6 | 87.0 |
| 6/24/88 | 3+00-wall | 13+50-16+50 | 3.0 | 96.9 | 21.2 | 104.8 | 22.6 | 92.4 |
| 6/24/88 | 3+00-wall | 13+50-16+50 | 3.0 | 94.2 | 22.1 | 104.8 | 22.6 | 89.8 |
| 6/24/88 | 3+00-wall | 13+50-16+50 | 3.0 | 99.2 | 20.1 | 104.8 | 22.6 | 94.6 |
| 6/24/88 | 3+00-wall | 13+50-16+50 | 3.0 | 95.4 | 21.0 | 104.8 | 22.6 | 91.0 |
| 6/24/88 | 3+00-5+00 | 14+50-wall | 3.0 | 84.4 | 23.8 | 104.8 | 22.6 | 80.5 |
| 6/24/88 | 3+00-5+00 | 14+50-wall | 3.0 | 83.1 | 20.3 | 104.8 | 22.6 | 79.8 |
| 6/24/88 | 3+00-5+00 | 14+50-wall | 3.0 | 85.9 | 19.1 | 104.8 | 22.6 | 81.9 |
| 6/24/88 | 3+00-5+00 | 14+50-wall | 3.0 | 89.1 | 21.5 | 104.8 | 22.6 | 85.0 |
| 6/24/88 | 5+00-7+00 | 14+50-wall | 3.0 | 86.0 | 16.7 | 104.8 | 22.6 | 82.0 |
| 6/24/88 | 5+00-7+00 | 14+50-wall | 3.0 | 84.4 | 18.8 | 104.8 | 22.6 | 80.5 |
| 6/24/88 | 5+00-7+00 | 14+50-wall | 3.0 | 89.4 | 25.7 | 104.8 | 22.6 | 85.3 |

IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|---------|---------------|-------------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 6/24/88 | 5+00-7+00 | 14+50-wall | 3.0 | 88.9 | 21.5 | 104.8 | 22.6 | 84.8 |
| 6/27/88 | 7+00-wall | 14+50-wall | 4.0 | 94.1 | 23.0 | 104.8 | 22.6 | 89.8 |
| 6/27/88 | 7+00-wall | 14+50-wall | 4.0 | 94.3 | 24.9 | 104.8 | 22.6 | 89.9 |
| 6/27/89 | 10+00 | 15+00 | 4.0 | 89.8 | 25.9 | 104.8 | 22.6 | 85.7 |
| 6/27/88 | 3+00-wall | 13+00-16+50 | 2.25 | 89.7 | 26.8 | 104.8 | 22.6 | 85.5 |
| 6/27/88 | 3+00-wall | 13+00-16+50 | 2.25 | 87.8 | 30.5 | 104.8 | 22.6 | 83.7 |
| 6/27/88 | 3+00-wall | 13+00-16+50 | 2.25 | 89.1 | 21.8 | 104.8 | 22.6 | 85.0 |
| 6/27/88 | 3+00-wall | 13+00-16+50 | 2.25 | 83.6 | 23.0 | 104.8 | 22.6 | 79.7 |
| 6/29/88 | 3+50-7+50 | 12+50-10+50 | 1.5 | 85.5 | 20.6 | 104.8 | 22.6 | 81.5 |
| 6/29/88 | 3+50-7+50 | 12+50-10+50 | 1.5 | 83.7 | 20.1 | 104.8 | 22.6 | 79.9 |
| 6/29/88 | 3+50-7+50 | 12+50-10+50 | 1.5 | 89.6 | 23.5 | 104.8 | 22.6 | 85.4 |
| 6/29/88 | 3+50-7+50 | 12+50-10+50 | 1.5 | 88.6 | 23.7 | 104.8 | 22.6 | 84.5 |
| 6/29/88 | 7+50-9+50 | 12+50-10+50 | 1.5 | 89.2 | 21.2 | 104.8 | 22.6 | 85.1 |
| 6/29/88 | 7+50-9+50 | 12+50-10+50 | 1.5 | 87.9 | 20.4 | 104.8 | 22.6 | 83.9 |
| 6/29/88 | 7+50-9+50 | 12+50-10+50 | 1.5 | 89.8 | 19.6 | 104.8 | 22.6 | 85.6 |
| 6/29/88 | 7+50-9+50 | 12+50-10+50 | 1.5 | 87.8 | 24.2 | 104.8 | 22.6 | 83.1 |
| 6/29/88 | 5+50-7+50 | 10+50-8+50 | 1.5 | 88.6 | 18.8 | 104.8 | 22.6 | 84.5 |
| 6/29/88 | 5+50-7+50 | 10+50-8+50 | 1.5 | 86.0 | 20.9 | 104.8 | 22.6 | 82.0 |
| 6/29/88 | 5+50-7+50 | 10+50-8+50 | 1.5 | 85.7 | 21.8 | 104.8 | 22.6 | 81.8 |
| 6/29/88 | 5+50-7+50 | 10+50-8+50 | 1.5 | 88.5 | 16.2 | 104.8 | 22.6 | 84.4 |
| 7/6/88 | wall-7+50 | 14+50-wall | 4.0 | 97.0 | 21.6 | 104.8 | 22.6 | 92.5 |
| 7/6/88 | wall-7+50 | 14+50-wall | 4.0 | 97.2 | 20.7 | 104.8 | 22.6 | 92.7 |
| 7/6/88 | 15+00 | 10+50 | 4.0 | 88.4 | 23.0 | 104.8 | 22.6 | 84.3 |

IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|---------|---------------|-------------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 7/6/88 | 15+00 | 9+50 | 4.0 | 91.6 | 19.8 | 104.8 | 22.6 | 87.3 |
| 7/6/88 | 5+00-9+00 | 6+00-9+00 | 1.5 | 84.0 | 12.5 | 104.8 | 22.6 | 80.1 |
| 7/6/88 | 5+00-9+00 | 6+00-9+00 | 1.5 | 84.3 | 14.0 | 104.8 | 22.6 | 80.3 |
| 7/6/88 | 5+00-9+00 | 6+00-9+00 | 1.5 | 88.3 | 16.6 | 104.8 | 22.6 | 84.2 |
| 7/6/88 | 5+00-9+00 | 6+00-9+00 | 1.5 | 83.9 | 21.1 | 104.8 | 22.6 | 80.1 |
| 7/8/88 | 5+50-7+50 | 14+50-16+50 | 1.5 | 89.1 | 29.6 | 104.8 | 22.6 | 85.0 |
| 7/8/88 | 5+50-7+50 | 14+50-16+50 | 1.5 | 88.2 | 28.7 | 104.8 | 22.6 | 84.1 |
| 7/8/88 | 5+50-7+50 | 14+50-16+50 | 1.5 | 85.3 | 22.0 | 104.8 | 22.6 | 81.4 |
| 7/8/88 | 5+50-7+50 | 14+50-16+50 | 1.5 | 87.9 | 22.2 | 104.8 | 22.6 | 83.8 |
| 7/8/88 | 3+50-5+50 | 14+50-16+50 | 1.5 | 90.6 | 29.5 | 104.8 | 22.6 | 86.4 |
| 7/8/88 | 3+50-5+50 | 14+50-16+50 | 1.5 | 88.0 | 18.3 | 104.8 | 22.6 | 83.9 |
| 7/8/88 | 3+50-5+50 | 14+50-16+50 | 1.5 | 89.3 | 29.4 | 104.8 | 22.6 | 85.2 |
| 7/8/88 | 3+50-5+50 | 14+50-16+50 | 1.5 | 83.1 | 20.2 | 104.8 | 22.6 | 79.2 |
| 7/8/88 | wall-3+50 | 12+50-16+50 | 1.5 | 89.5 | 17.3 | 104.8 | 22.6 | 85.4 |
| 7/8/88 | wall-3+50 | 12+50-16+50 | 1.5 | 86.2 | 16.9 | 104.8 | 22.6 | 82.3 |
| 7/8/88 | wall-3+50 | 12+50-16+50 | 1.5 | 86.5 | 19.0 | 104.8 | 22.6 | 82.5 |
| 7/8/88 | wall-3+50 | 12+50-16+50 | 1.5 | 87.2 | 19.5 | 104.8 | 22.6 | 83.1 |
| 7/8/88 | wall-3+50 | 12+50-16+50 | 1.5 | 90.0 | 18.5 | 104.8 | 22.6 | 85.8 |
| 7/11/88 | 1+50-wall | 14+50-wall | 3.5 | 99.9 | 21.8 | 104.8 | 22.6 | 95.7 |
| 7/11/88 | 1+50-wall | 14+50-wall | 3.5 | 98.9 | 19.2 | 104.8 | 22.6 | 94.4 |
| 7/11/88 | 1+50-wall | 14+50-wall | 3.5 | 96.1 | 20.8 | 104.8 | 22.6 | 91.7 |
| 7/11/88 | 1+50-wall | 14+50-wall | 3.5 | 98.0 | 22.0 | 104.8 | 22.6 | 93.5 |
| 7/11/88 | 5+00-wall | 14+50-15+50 | 1.5 | 89.8 | 13.9 | 104.8 | 22.6 | 85.7 |

IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|---------|---------------|-------------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 7/11/88 | 5+00-wall | 14+50-15+50 | 1.5 | 84.8 | 19.8 | 104.8 | 22.6 | 80.9 |
| 7/11/88 | 5+00-wall | 14+50-15+50 | 1.5 | 86.6 | 15.3 | 104.8 | 22.6 | 82.6 |
| 7/11/88 | 5+00-wall | 14+50-15+50 | 1.5 | 89.2 | 14.3 | 104.8 | 22.6 | 85.1 |
| 7/11/88 | 5+00-wall | 13+50-12+50 | 1.5 | 84.8 | 15.2 | 104.8 | 22.6 | 80.9 |
| 7/11/88 | 5+00-wall | 13+50-12+50 | 1.5 | 86.5 | 15.4 | 104.8 | 22.6 | 82.5 |
| 7/11/88 | 5+00-wall | 13+50-12+50 | 1.5 | 87.0 | 17.3 | 104.8 | 22.6 | 83.0 |
| 7/11/88 | 5+00-wall | 13+50-12+50 | 1.5 | 88.2 | 19.1 | 104.8 | 22.6 | 84.1 |
| 7/11/88 | 5+00-wall | 12+50-11+50 | 1.5 | 86.6 | 15.9 | 104.8 | 22.6 | 82.6 |
| 7/11/88 | 5+00-wall | 12+50-11+50 | 1.5 | 87.6 | 14.9 | 104.8 | 22.6 | 83.5 |
| 7/11/88 | 5+00-wall | 12+50-11+50 | 1.5 | 88.9 | 15.3 | 104.8 | 22.6 | 84.8 |
| 7/11/88 | 5+00-wall | 12+50-11+50 | 1.5 | 84.2 | 14.8 | 104.8 | 22.6 | 80.3 |
| 7/11/88 | 5+00-wall | 11+50-10+50 | 1.5 | 87.5 | 11.6 | 104.8 | 22.6 | 83.5 |
| 7/11/88 | 5+00-wall | 11+50-10+50 | 1.5 | 87.1 | 13.6 | 104.8 | 22.6 | 83.1 |
| 7/11/88 | 5+00-wall | 11+50-10+50 | 1.5 | 89.1 | 13.6 | 104.8 | 22.6 | 85.0 |
| 7/11/88 | 5+00-wall | 11+50-10+50 | 1.5 | 86.0 | 14.1 | 104.8 | 22.6 | 82.1 |
| 7/11/88 | 5+00-wall | 10+50-9+50 | 1.5 | 83.8 | 14.1 | 104.8 | 22.6 | 80.0 |
| 7/11/88 | 5+00-wall | 10+50-9+50 | 1.5 | 86.9 | 12.1 | 104.8 | 22.6 | 82.9 |
| 7/11/88 | 5+00-wall | 10+50-9+50 | 1.5 | 89.3 | 16.8 | 104.8 | 22.6 | 85.2 |
| 7/11/88 | 5+00-wall | 10+50-9+50 | 1.5 | 87.0 | 18.8 | 104.8 | 22.6 | 83.0 |
| 7/12/88 | 7+50-wall | 14+50-wall | 3.0 | 99.9 | 15.9 | 104.8 | 22.6 | 95.3 |
| 7/12/88 | 7+50-wall | 14+50-wall | 3.0 | 94.9 | 22.1 | 104.8 | 22.6 | 90.5 |
| 7/12/88 | 7+50-wall | 14+50-wall | 3.0 | 96.2 | 21.0 | 104.8 | 22.6 | 91.7 |
| 7/12/88 | 7+50-wall | 14+50-wall | 3.0 | 97.1 | 20.5 | 104.8 | 22.6 | 92.6 |

IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|---------|---------------|-------------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 8/2/88 | 9+50-15+50 | 12+50-10+50 | 0.5 | 112.3 | 14.0 | 126.5 | 10.2 | 88.8 |
| 8/2/88 | 9+50-15+50 | 12+50-10+50 | 0.5 | 116.8 | 7.5 | 126.5 | 10.2 | 92.3 |
| 8/2/88 | 9+50-15+50 | 12+50-10+50 | 0.5 | 116.3 | 7.7 | 126.5 | 10.2 | 91.9 |
| 8/2/88 | 9+50-15+50 | 12+50-10+50 | 0.5 | 118.1 | 8.2 | 126.5 | 10.2 | 93.3 |
| 8/10/88 | 8+00-wall | 14+50-wall | 1.5 | 83.9 | 23.7 | 104.8 | 22.6 | 80.0 |
| 8/10/88 | 8+00-wall | 14+50-wall | 1.5 | 87.8 | 27.5 | 104.8 | 22.6 | 83.7 |
| 8/10/88 | 8+00-wall | 14+50-wall | 1.5 | 86.1 | 21.7 | 104.8 | 22.6 | 82.2 |
| 8/10/88 | 8+00-wall | 14+50-wall | 1.5 | 87.6 | 23.7 | 104.8 | 22.6 | 83.6 |
| 8/10/88 | 5+00-7+00 | 12+50-10+50 | 0.5 | 111.4 | 9.4 | 126.5 | 10.2 | 88.1 |
| 8/10/88 | 5+00-7+00 | 12+50-10+50 | 0.5 | 116.7 | 8.9 | 126.5 | 10.2 | 92.2 |
| 8/10/88 | 5+00-7+00 | 12+50-10+50 | 0.5 | 109.1 | 11.7 | 126.5 | 10.2 | 86.3 |
| 8/10/88 | 5+00-7+00 | 12+50-10+50 | 0.5 | 118.6 | 7.4 | 126.5 | 10.2 | 93.7 |
| 8/10/88 | 7+00-wall | 12+50-10+50 | 0.5 | 119.5 | 6.9 | 126.5 | 10.2 | 94.4 |
| 8/10/88 | 7+00-wall | 12+50-10+50 | 0.5 | 115.1 | 9.1 | 126.5 | 10.2 | 90.9 |
| 8/10/88 | 7+00-wall | 12+50-10+50 | 0.5 | 110.8 | 9.2 | 126.5 | 10.2 | 87.6 |
| 8/10/88 | 7+00-wall | 12+50-10+50 | 0.5 | 110.0 | 10.5 | 126.5 | 10.2 | 86.9 |
| 8/10/88 | 5+00-7+00 | 10+50-8+50 | 0.5 | 116.2 | 6.3 | 126.5 | 10.2 | 91.8 |
| 8/10/88 | 5+00-7+00 | 10+50-8+50 | 0.5 | 115.1 | 8.6 | 126.5 | 10.2 | 91.0 |
| 8/10/88 | 5+00-7+00 | 10+50-8+50 | 0.5 | 114.1 | 8.0 | 126.5 | 10.2 | 90.1 |
| 8/10/88 | 5+00-7+00 | 10+50-8+50 | 0.5 | 117.6 | 7.1 | 126.5 | 10.2 | 92.9 |
| 8/10/88 | 7+00-wall | 10+50-8+50 | 0.5 | 118.2 | 6.0 | 126.5 | 10.2 | 93.4 |
| 8/10/88 | 7+00-wall | 10+50-8+50 | 0.5 | 115.4 | 10.9 | 126.5 | 10.2 | 91.2 |
| 8/10/88 | 7+00-wall | 10+50-8+50 | 0.5 | 116.2 | 11.6 | 126.5 | 10.2 | 91.8 |

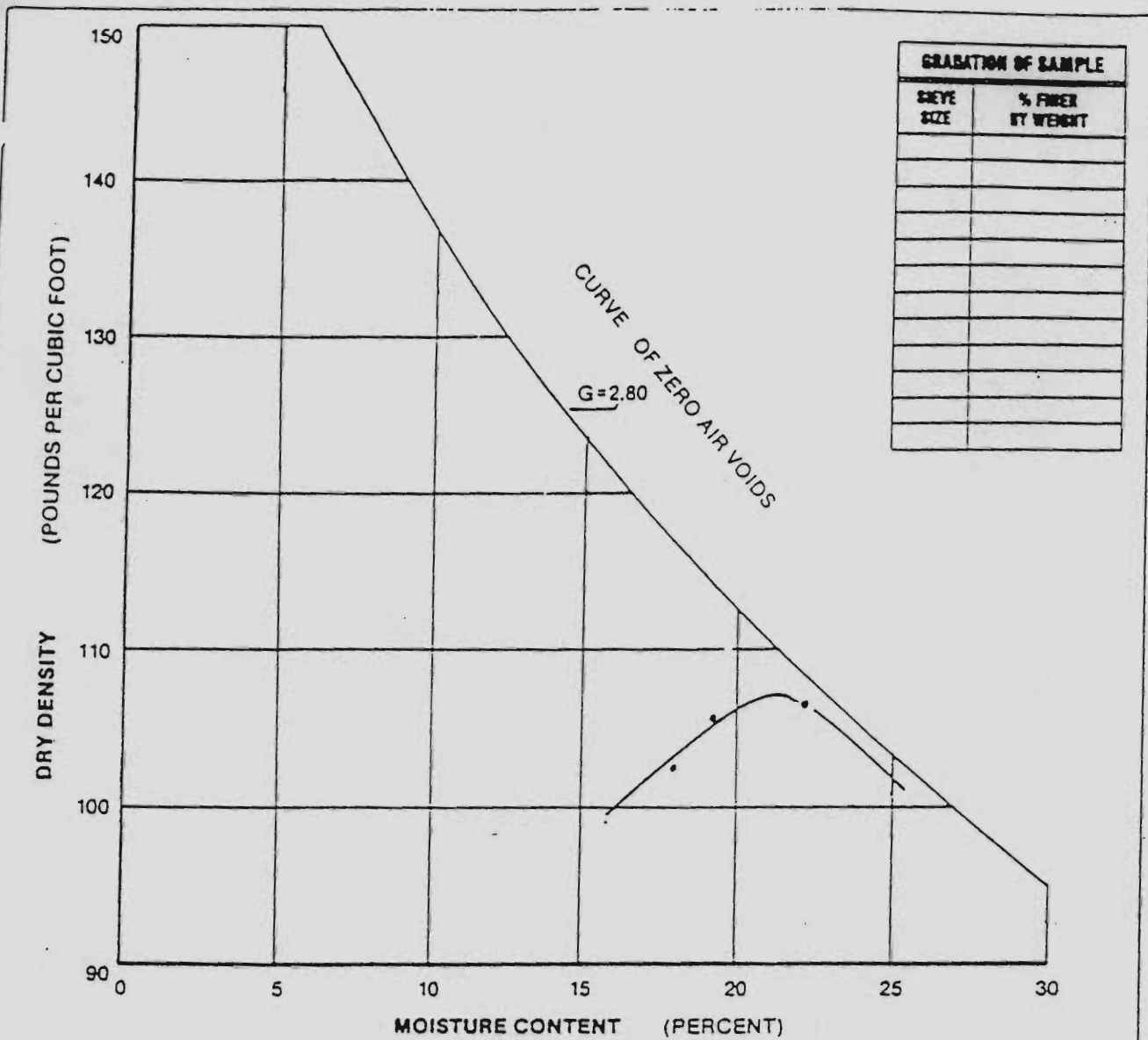
IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|---------|---------------|------------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 8/10/88 | 7+00-wall | 10+50-8+50 | 0.5 | 113.7 | 11.2 | 126.5 | 10.2 | 89.8 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 115.3 | 8.2 | 126.5 | 10.2 | 91.1 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 112.2 | 11.1 | 126.5 | 10.2 | 88.7 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 109.6 | 12.5 | 126.5 | 10.2 | 86.6 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 117.8 | 11.2 | 126.5 | 10.2 | 93.1 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 111.4 | 11.9 | 126.5 | 10.2 | 88.0 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 113.5 | 9.5 | 126.5 | 10.2 | 89.7 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 110.9 | 9.4 | 126.5 | 10.2 | 87.6 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 114.6 | 9.3 | 126.5 | 10.2 | 90.6 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 110.1 | 11.1 | 126.5 | 10.2 | 87.0 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 112.0 | 7.7 | 126.5 | 10.2 | 88.5 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 116.1 | 9.0 | 126.5 | 10.2 | 91.7 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 110.0 | 10.6 | 126.5 | 10.2 | 86.9 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 115.4 | 8.3 | 126.5 | 10.2 | 91.2 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 110.5 | 11.1 | 126.5 | 10.2 | 87.3 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 107.8 | 10.4 | 126.5 | 10.2 | 85.0 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 108.6 | 10.9 | 126.5 | 10.2 | 85.7 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 109.7 | 10.7 | 126.5 | 10.2 | 86.7 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 112.3 | 9.4 | 126.5 | 10.2 | 88.7 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 113.1 | 10.1 | 126.5 | 10.2 | 89.3 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 108.7 | 11.4 | 126.5 | 10.2 | 85.9 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 109.5 | 12.1 | 126.5 | 10.2 | 86.5 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 112.4 | 11.1 | 126.5 | 10.2 | 88.8 |

IN-PLACE DENSITY/MOISTURE TESTING OF LANDFILL CAP

| Date | Grid Location | | Depth Below Final Grade (ft) | In-Place Density (PCF) | In-Place Moisture (%) | Maximum Density (PCF) | Optimum Moisture Content (%) | Percent Compaction |
|---------|---------------|-------------|------------------------------------|------------------------------|-----------------------------|-----------------------------|---------------------------------------|-----------------------|
| | North | East | | | | | | |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 110.1 | 11.7 | 126.5 | 10.2 | 87.0 |
| 8/18/88 | 1+00-5+00 | 6+00-13+00 | 0.5 | 117.5 | 6.7 | 126.5 | 10.2 | 92.9 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 117.6 | 5.5 | 126.5 | 10.2 | 93.0 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 118.0 | 6.1 | 126.5 | 10.2 | 93.2 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 113.5 | 5.3 | 126.5 | 10.2 | 89.7 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 108.7 | 5.9 | 126.5 | 10.2 | 85.9 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 109.6 | 8.0 | 126.5 | 10.2 | 86.6 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 119.8 | 6.1 | 126.5 | 10.2 | 94.7 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 118.0 | 5.6 | 126.5 | 10.2 | 93.3 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 115.4 | 6.4 | 126.5 | 10.2 | 91.2 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 113.0 | 5.7 | 126.5 | 10.2 | 89.3 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 116.8 | 6.5 | 126.5 | 10.2 | 92.3 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 114.0 | 4.6 | 126.5 | 10.2 | 90.1 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 114.1 | 5.9 | 126.5 | 10.2 | 90.2 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 118.1 | 7.1 | 126.5 | 10.2 | 93.4 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 117.7 | 7.9 | 126.5 | 10.2 | 93.0 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 114.5 | 6.0 | 126.5 | 10.2 | 90.5 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 115.7 | 10.0 | 126.5 | 10.2 | 91.4 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 116.0 | 7.7 | 126.5 | 10.2 | 91.6 |
| 9/8/88 | 1+00-5+00 | 13+00-16+00 | 0.5 | 113.3 | 7.0 | 126.5 | 10.2 | 89.5 |

KINGSBURY SITE REMEDIAL PROGRAM
PROCTOR CURVES FOR CAP MATERIAL



SAMPLE DESCRIPTION

TEST RESULTS

Material CLAY, trace gravel Maximum Dry Density 106.9 pcf
Hillview Drive
 Color Dark Brown Source Borrow Site Optimum Water Content 21.3 %
 Sampled By RA At TP-3, 4'

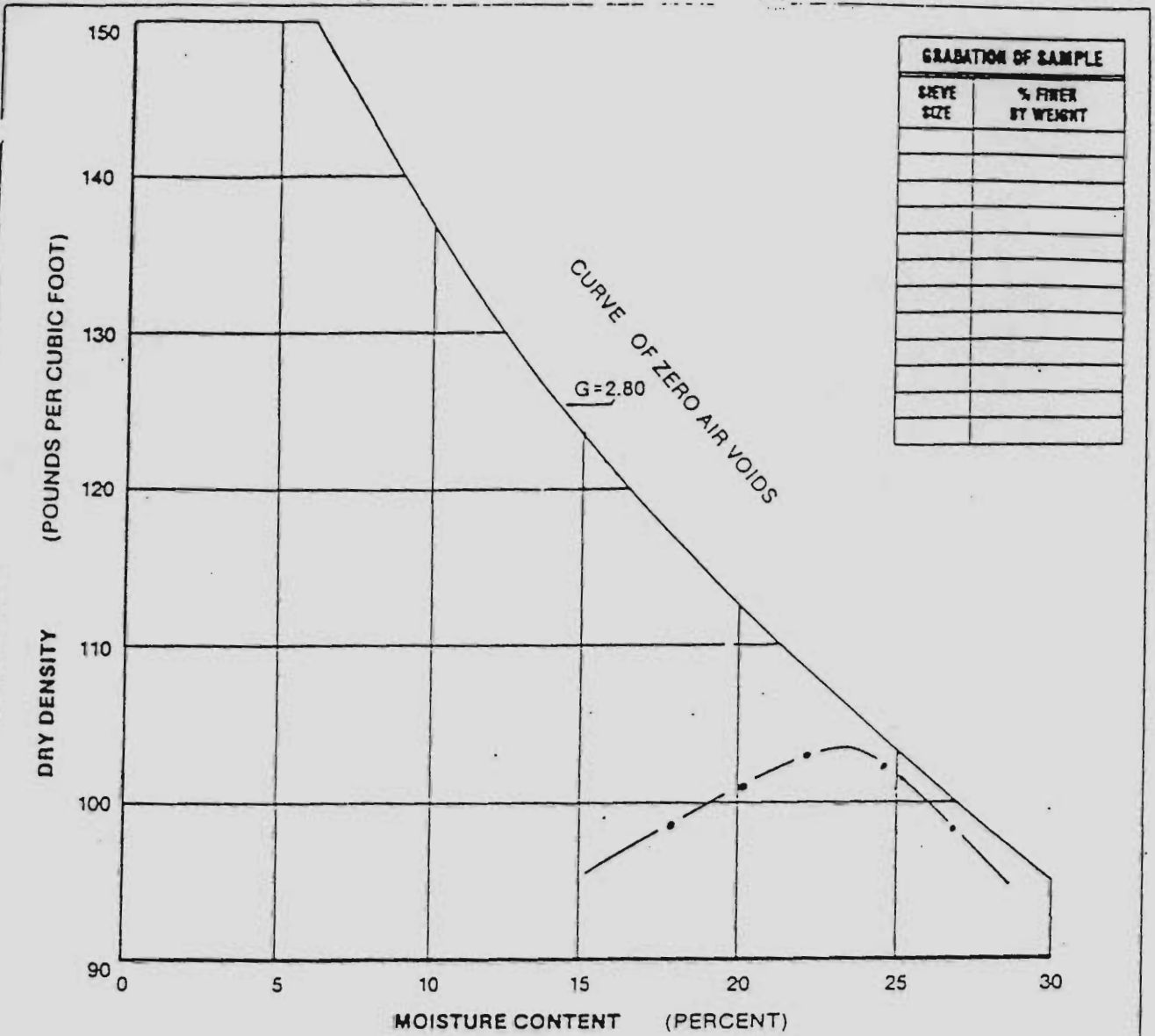
| METHOD OF TEST | |
|----------------------|----------|
| STANDARD | METHOD |
| ASTM <u>D1557-78</u> | <u>A</u> |
| AASHTO _____ | _____ |
| MILITARY _____ | _____ |
| OTHER _____ | _____ |



OPTIMUM MOISTURE—MAXIMUM DENSITY


KINGSBURY LANDFILL
 TOWN OF KINGSBURY, NEW YORK

DR. BY: SB | DATE SAMPLED: _____ | PROJ. NO. ATA-87-37



| | | | |
|---------------------------|-------------------------------|-----------------------|-----------|
| SAMPLE DESCRIPTION | | TEST RESULTS | |
| Material | CLAY | Maximum Dry Density | 103.5 pcf |
| Color | Dark Brown | Optimum Water Content | 23.2 % |
| Source | Hillview Drive Borrow Site | | |
| Sampled By | RA At TP-1, 6' | | |

| METHOD OF TEST | |
|----------------|--------|
| STANDARD | METHOD |
| ASTM D1557-78 | A |
| AASHTO | |
| MILITARY | |
| OTHER | |



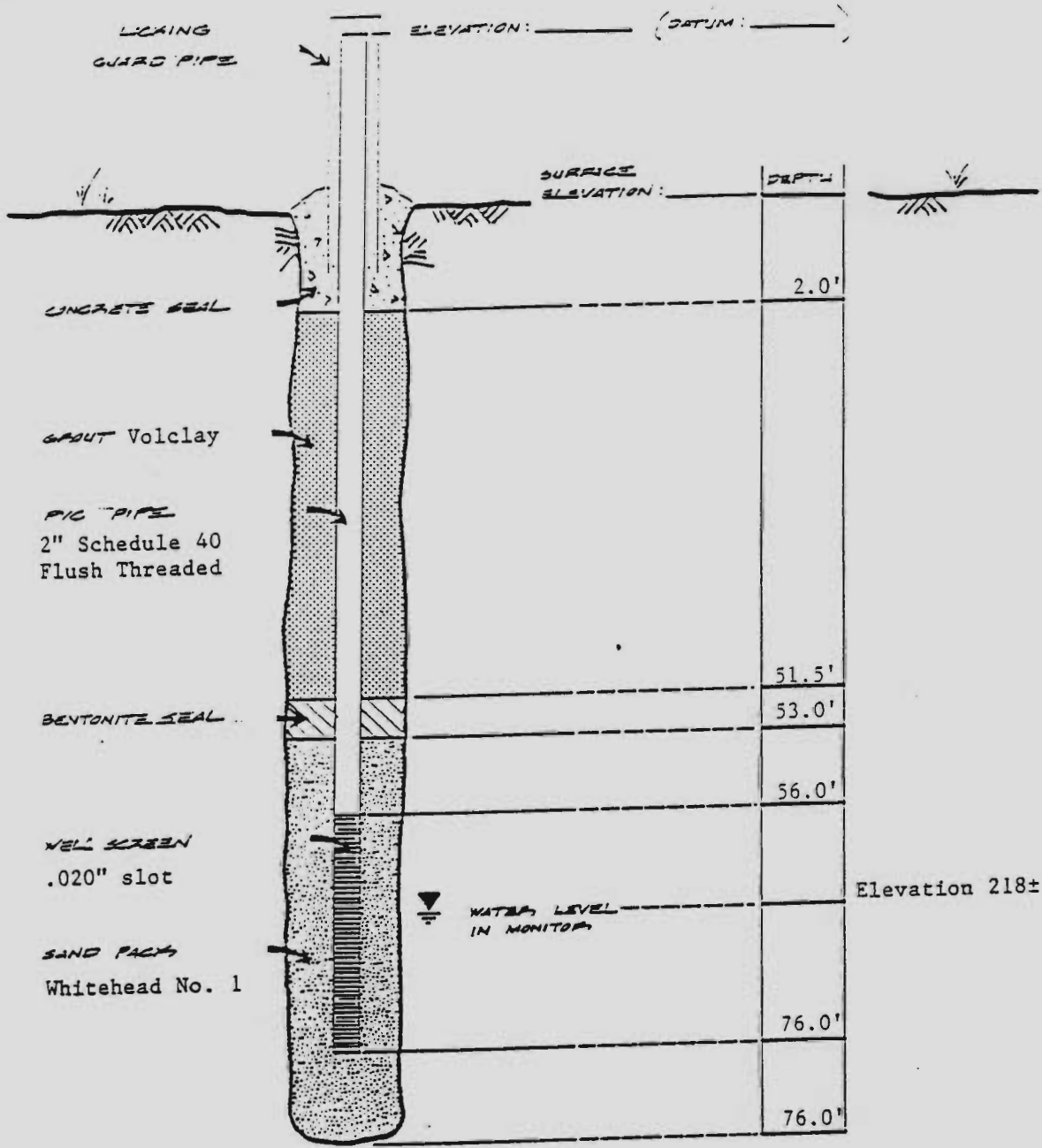
OPTIMUM MOISTURE—MAXIMUM DENSITY

KINGSBURY LANDFILL
TOWN OF KINGSBURY, NEW YORK

| | | |
|---------------|---------------|---------------------|
| DR. BY: SB | DATE SAMPLED: | PROJ. NO. ATA-87-37 |
| TESTED BY: TW | CURVE NO. 3 | |

APPENDIX C

KINGSBURY SITE REMEDIAL PROGRAM
MONITORING AND RELIEF WELL DETAILS



WELL No.

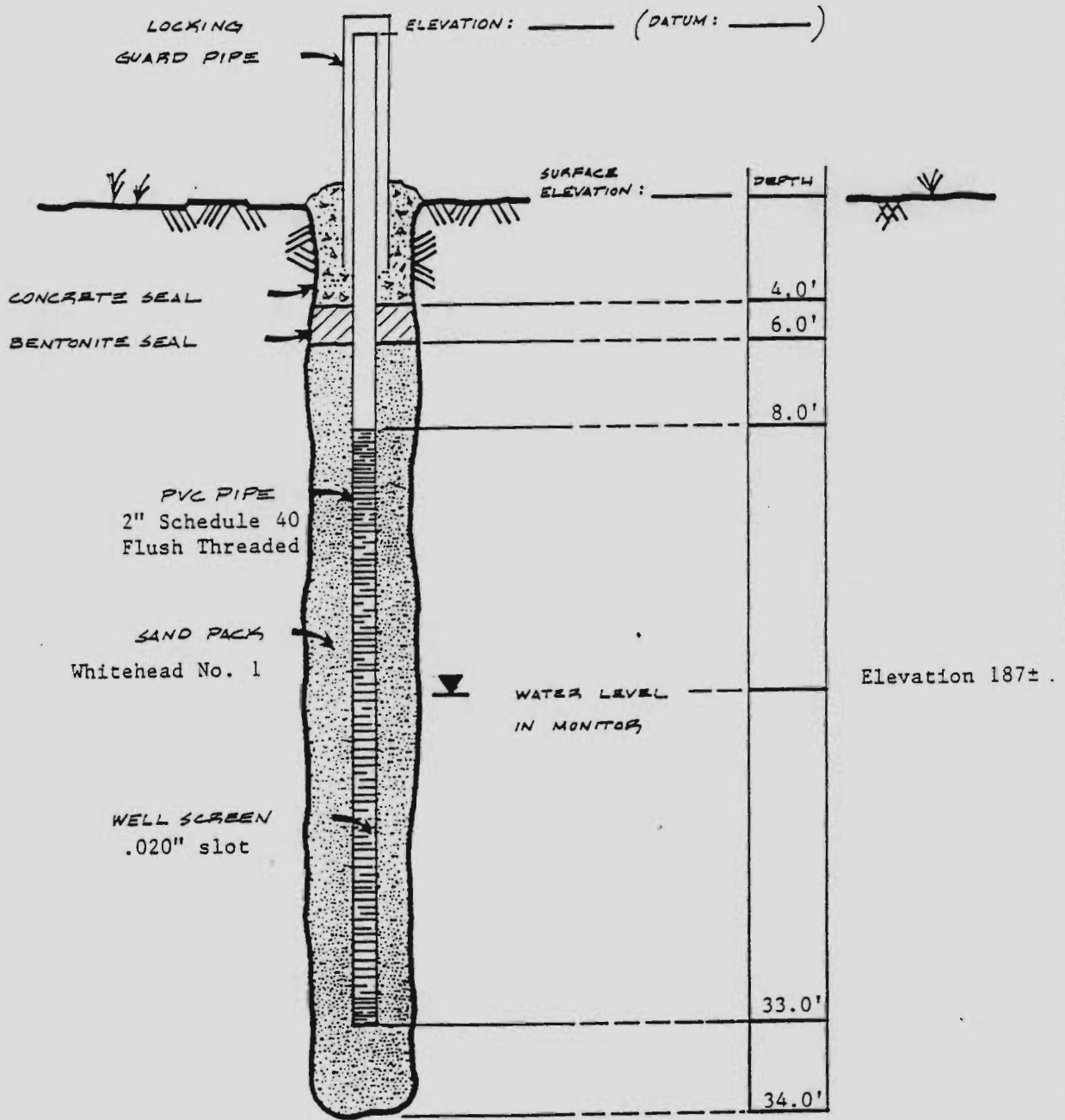
GMW-1



MONITORING WELL DETAILS

KINGSBURY LANDFILL

| | | | | | |
|---------|-----|--------|---------|----------|----------|
| DR BY | JH | SCALE: | N.T.S. | PROJ. NO | AD-86-90 |
| CK'D BY | RWD | DATE: | 6-15-88 | DRWG NO | |



WELL N \varnothing

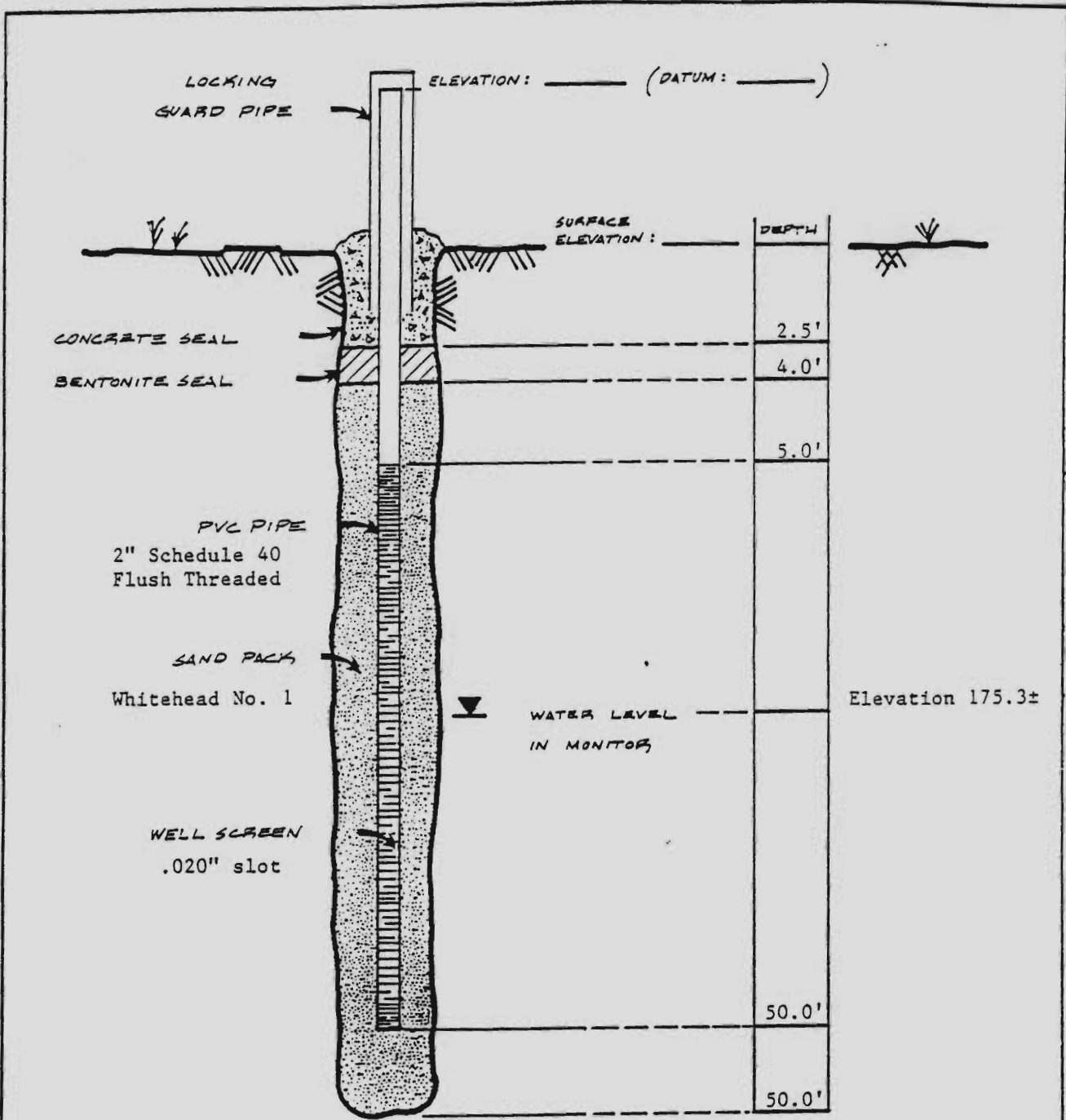
GMW-2



MONITORING WELL DETAILS

KINGSBURY LANDFILL

| | | |
|-------------|--------------|------------------|
| DR BY JH | SCALE N.T.S. | PROJ NO AD-86-90 |
| CK'D BY RWD | DATE 6-15-88 | DRWG NO |



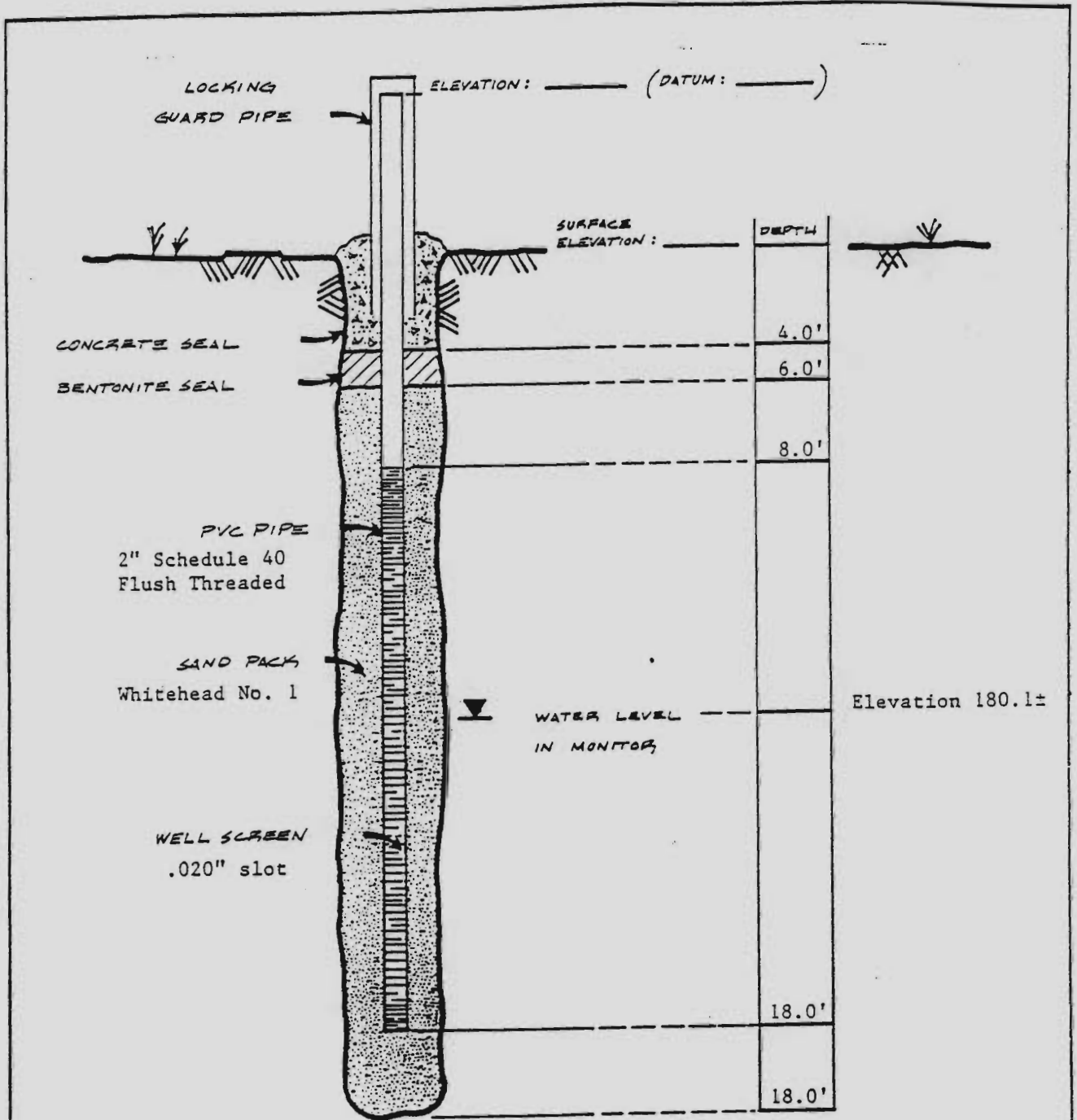
WELL N \varnothing

GMW-3



MONITORING WELL DETAILS
KINGSBURY LANDFILL

| | | | | | |
|---------|-----|-------|---------|---------|----------|
| DR BY | JH | SCALE | N.T.S. | PROJ NO | AD-86-90 |
| CX O BY | RWD | DATE | 6-15-88 | DRWG NO | |



WELL N^o

GMW-4



MONITORING WELL DETAILS

KINGSBURY LANDFILL

DR BY JH

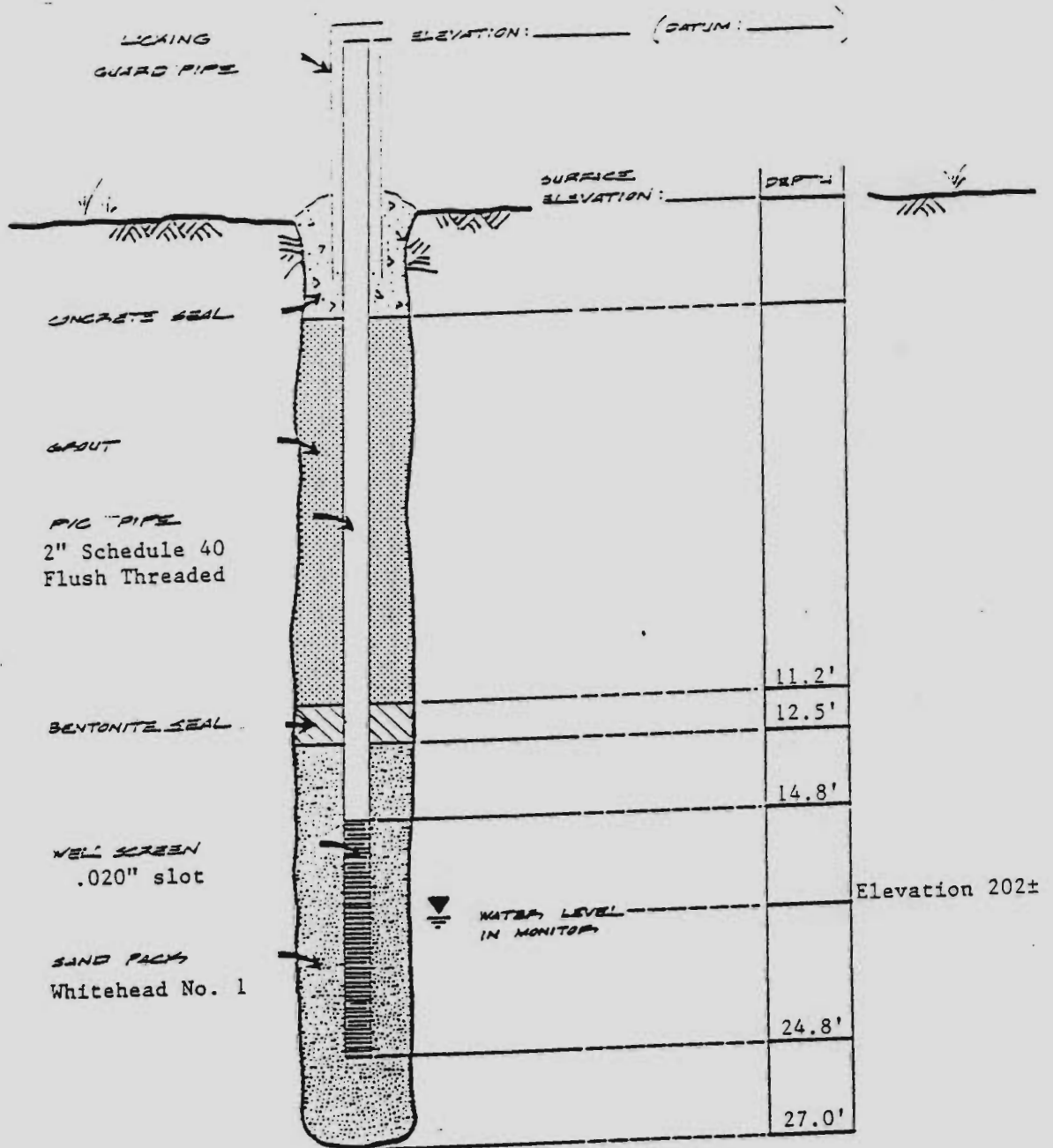
SCALE N.T.S.

PROJ NO. AD-86-90

CK'D BY RWD

DATE 6-15-88

DRWC NO



WELL No.

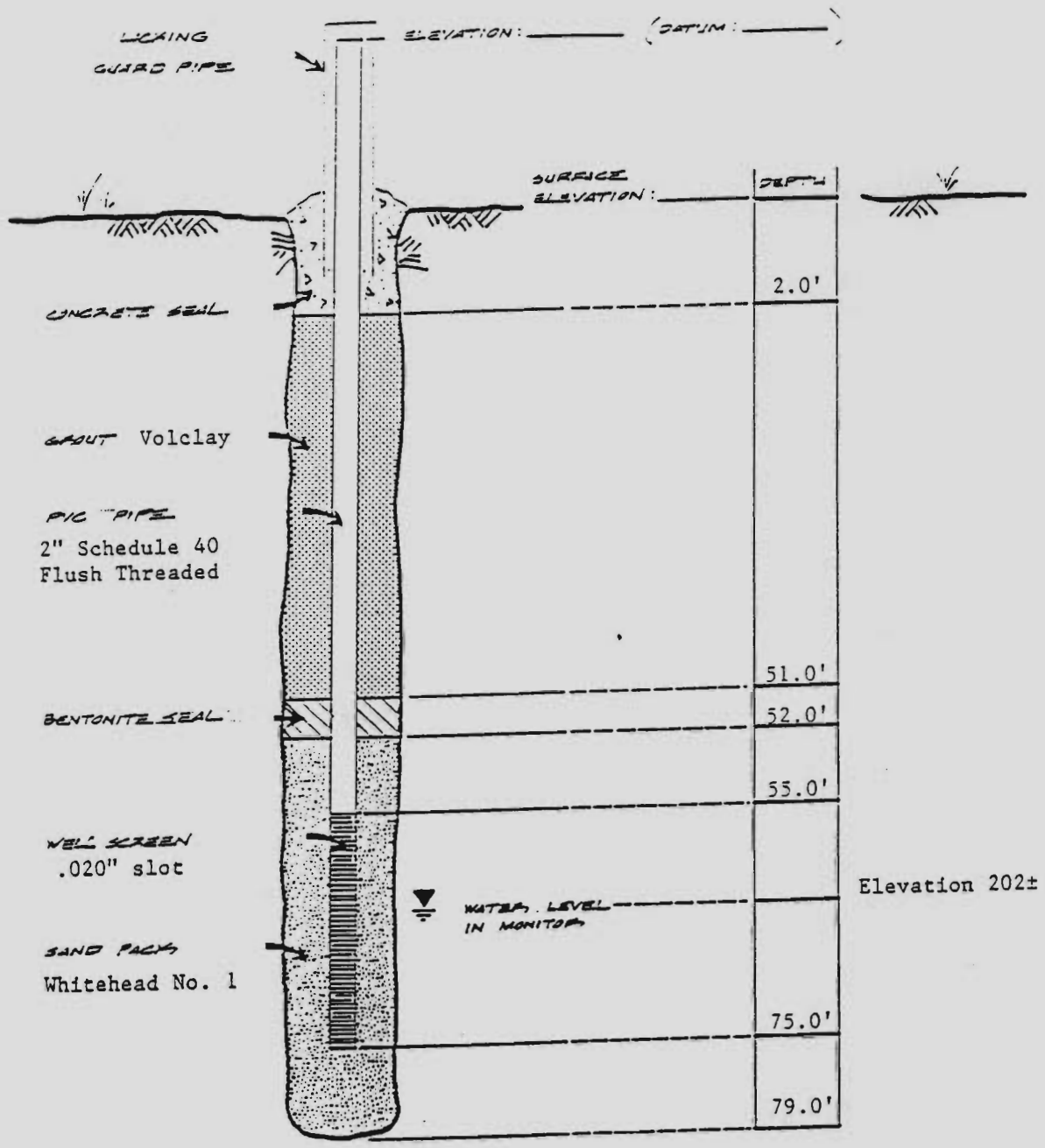
GMW-5



MONITORING WELL DETAILS

KINGSBURY LANDFILL

| | | | | | |
|-------|---------|---------|--------|----------|----------|
| DR BY | JH | SCALE: | N.T.S. | PROJ. NO | AD-86-90 |
| DATE: | 6-16-88 | DRWG NO | | | |



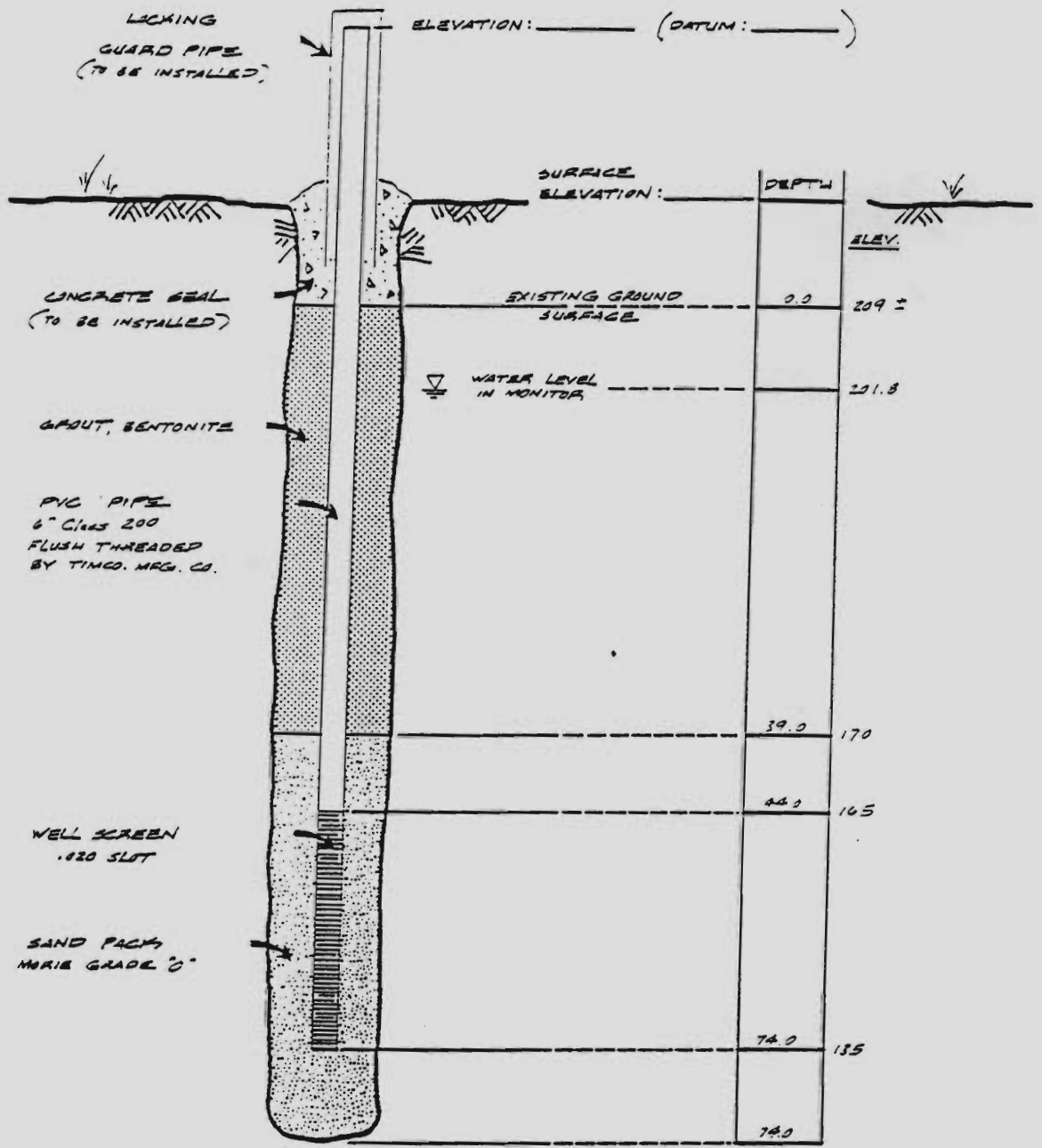
WELL No.

GMW-6



MONITORING WELL DETAILS
KINGSBURY LANDFILL

| | | |
|-----------|---------------|--------------------|
| DR BY JH | SCALE: N.T.S. | PROJ. NO. AD-86-90 |
| CK BY RWD | DATE: 6-15-88 | ORWC NO |



LOCKING
GUARD PIPE
(TO BE INSTALLED)

ELEVATION: _____ (DATUM: _____)

CONCRETE SEAL
(TO BE INSTALLED)

SURFACE
ELEVATION:

DEPTH

ELEV.

EXISTING GROUND
SURFACE

0.0

209.2

WATER LEVEL
IN MONITOR

211.8

GROUT, BENTONITE

PVC PIPE
6" Class 200
FLUSH THREADED
BY TIMCO. MFG. CO.

39.0

170

44.0

165

WELL SCREEN
.020 SLOT

74.0

135

SAND PACK
MORIS GRADE 2"

74.0

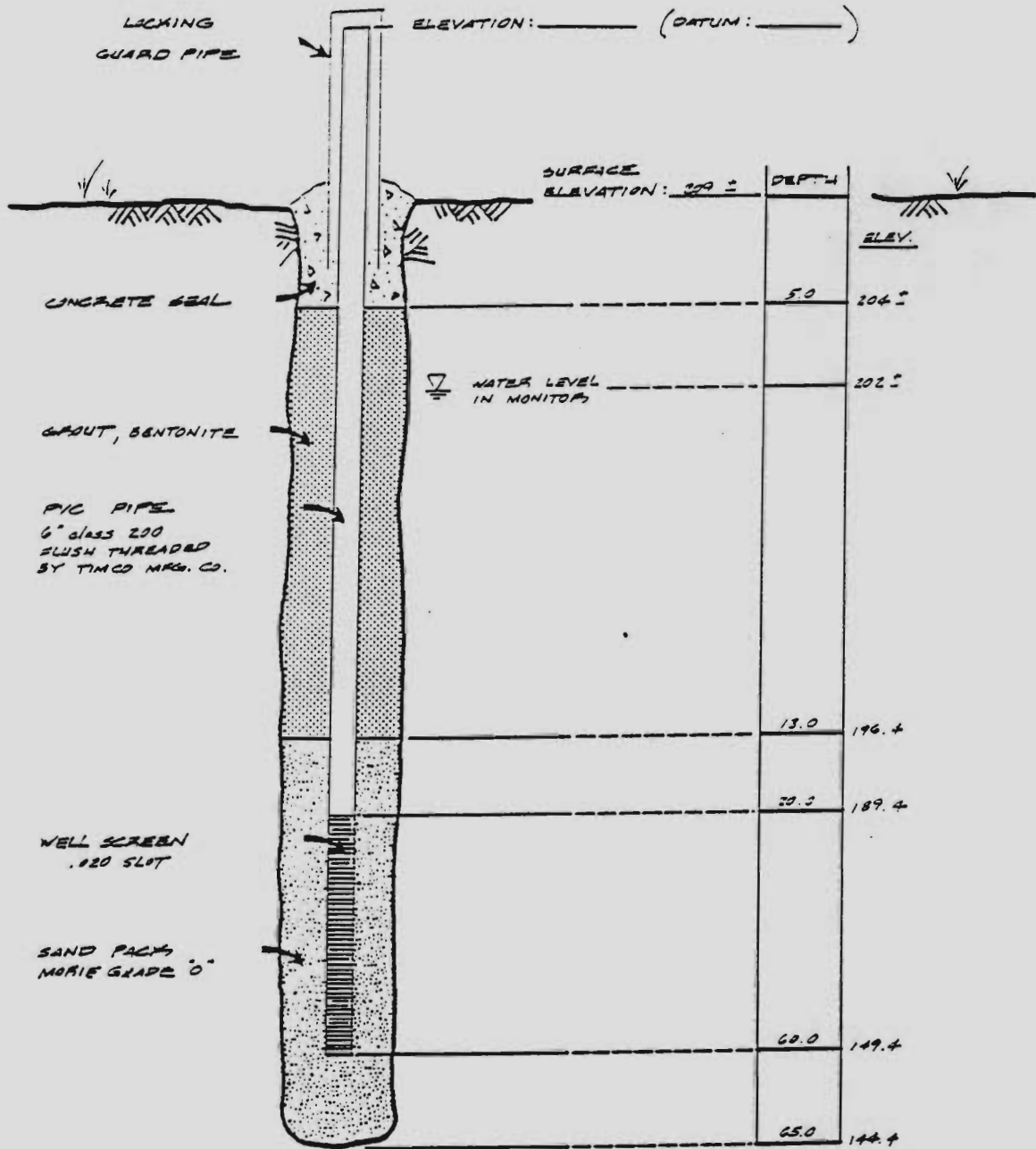


WELL No.

BW-1

RELIEF WELL DETAILS
KINGSBURY LANDFILL

| | | | | | |
|--------|-----|-------|---------|---------|----------|
| DR BY | JW | SCALE | N.T.S. | PROJ NO | 10-86-90 |
| CKD BY | AWD | DATE | 6-21-88 | DRWG NO | |



WELL No.

BW-2



RELIEF WELL DETAILS
KINGSBURY LANDFILL

| | | | | | |
|--------|-----|-------|---------|-----------|----------|
| DR BY | JW | SCALE | N.T.S. | PROJ. NO. | AD-86-90 |
| CHK BY | AWD | DATE | 6-21-88 | DRWG NO. | |

APPENDIX D

KINGSBURY SITE REMEDIAL PROGRAM
CERTIFICATE OF SUBSTANTIAL COMPLETION

CERTIFICATE OF SUBSTANTIAL COMPLETION

OWNER: New York State Department of
Environmental Conservation

PROJECT: Kingsbury Site Remedial Program

CONTRACTOR: Yolam Construction, Inc.

ENGINEER: Blasland & Bouck Engineers, P.C.

CONTRACT: No. 1

PROJECT NO: 92.01

Project or Specified Part shall include: Substantial Completion of Contract No. 1.

Definition of Substantial Completion: Substantial Completion is defined to be the date when the Owner and the Contractor reach mutual agreement that the work is substantially complete.

Date of Substantial Completion: October 31, 1989

Written, mutual agreements upon which the date of Substantial Completion has been mutually agreed to are as follows:

1. Agreement to Substantial Completion by the Owner will in no way affect the obligations of the Contractor under the terms and provisions of the Contract with respect to uncompleted work.
2. The Contractor shall subsequently complete or correct all unfinished items in the work accepted by the Owner as substantially complete.
3. The Owner, Engineer and Contractor made an inspection of the work on November 1, 1989 and, following this inspection, the Engineer advised the Contractor of remaining items to be completed or corrected and provided the Contractor with an Estimate of Work Remaining, (attached). The Contractor shall endorse said Estimate of Work Remaining as evidence of agreement and provide the Owner with a mutually acceptable schedule for completion of the Estimate of Work Remaining.

CERTIFICATE OF SUBSTANTIAL COMPLETION

4. Warrantee/Guarantee Periods, as stipulated in the Contract Documents, are to begin upon the date of Substantial Completion.

YOLAM CONSTRUCTION, INC.

By: *[Signature]*
Title: *[Signature]*
Date: *Jan. 23, 1990*

BLASLAND & BOUCK ENGINEERS, P.C.

By: *Joseph A. Otto*
Title: *Director of Construction Services*
Date: *Jan. 18, 1990*

NEW YORK STATE DEPARTMENT OF ENVIRONMENTAL CONSERVATION

By: *James Van Hoese*
Title: *Assoc. San. Const. Engin.*
Date: *1-24-90*

92.01
1/18/90

Kingsbury Site Remedial Program

Estimate of Work Remaining

1. Demobilization of Engineer's and Contractor's Field Offices
(2 x \$1,000 = \$2,000)

2. Repair and maintain eroded cap areas and mid-slope stone ditch as required to correct and prevent further erosion. Repairs shall include reseeding and maintenance of slopes and ditches until establishment of final vegetative growth.
(2 x \$4,000 = \$8,000)