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ATMOSPHERIC EMISSIONS DURING DEMONSTRATION OF THE CLEAN SOIL PROCESS® OF THE NORWICH, NEW YORK MANUFACTURED GAS PLANT SITE

From:

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Prepared by:

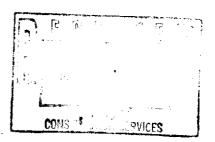
Atlantic Environmental Services, Inc. 188 Norwich Avenue • P.O. Box 297 Colchester, CT 06415

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ATLANTICCONFIDENTIAL

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ATMOSPHERIC EMISSIONS DURING DEMONSTRATION OF THE CLEAN SOIL PROCESS®

1.0 BACKGROUND

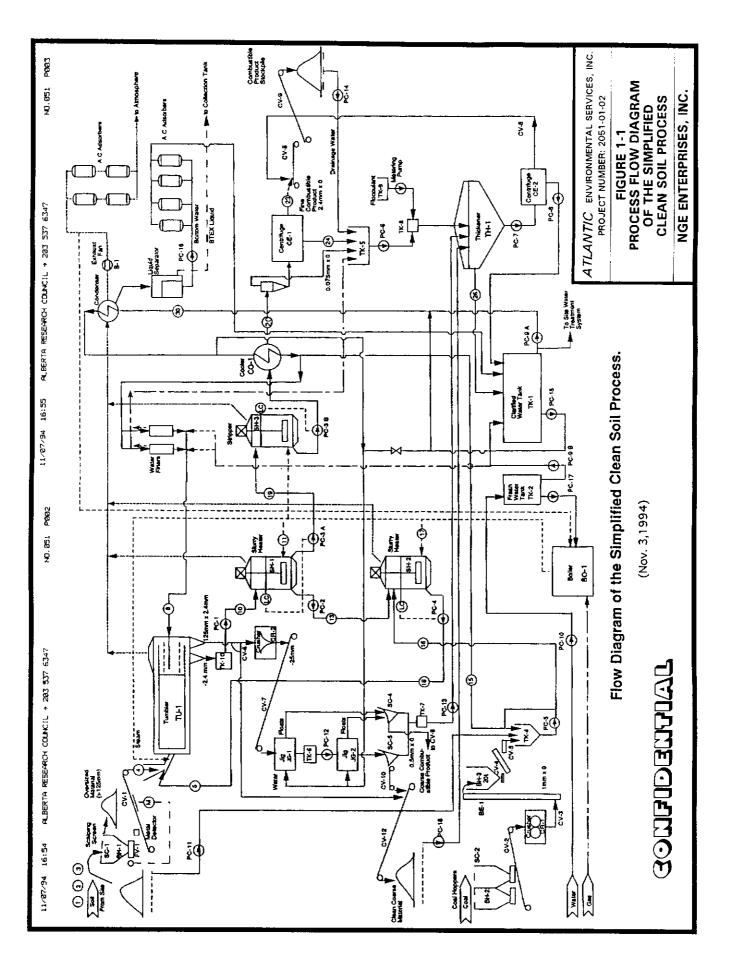
To evaluate the effectiveness, efficiency, reliability, and costs of the Clean Soil Process® (CSP) for partial remediation of wastes at former manufactured gas plant (MGP) sites, CSP will be tested during an interim remedial measure (IRM) to be completed by the New York State Electric and Gas Corporation (NYSEG) at its former MGP site in Norwich, New York. The demonstration is being conducted by NGE Enterprises, Inc. (NGE), a subsidiary of NYSEG. The IRM will involve two fundamental operations: (1) removal of MGP wastes (excavation) from designated locations, and (2) treatment of the excavated materials via CSP at predetermined operating conditions developed during pilot studies. The objective of the IRM is to reduce contamination in the MGP wastes to comply with New York State guidance regarding soil cleanup objectives. After satisfactory processing, the treated material will be backfilled and eliminated from further remedial treatment.

The overall objective of the NGE evaluation is to quantify the operation of CSP to assess its viability/feasibility for use in association with a program of remedial co-burning of MGP wastes in utility boilers. In transferring MGP contaminants to fine coal particles by adsorption via CSP, the coal is enriched with the combustible substances. By removing volatile organics as a product of CSP, including benzene, the combustible product is expected to qualify as nonhazardous material. Two NYSEG power plants, the Jennison and Hickling stations, are equipped and permitted for co-burning MGP-waste materials. The demonstration, using wastes from the Norwich MGP site, will provide the following specific objectives:

- (1) assessment of the CSP for commercial-scale applications;
- (2) comparison of the CSP treatment using results from different types of typical MGP wastes (e.g., relief holder and tar well contamination); and
- (3) cost analysis.

The planned demonstration of the CSP involves several potential sources of atmospheric emissions:

- the Sprung[™] structure, which will enclose portions of the operation (i.e., feed and output of the treated material);
- the CSP process downstream of the condenser (Figure 1-1); and
- a 200-hp boiler fueled by natural gas (Figure 1-1).



2.0 SPRUNG™ STRUCTURE

The Sprung[™] structure is not considered an emissions source subject to permitting, because it will be open with simple ventilation through open doors. No air treatment system is contemplated for organic emissions. Two relatively small stockpiles (80 tons each) of untreated material will be created and depleted simultaneously within the structure during operation of CSP. As one stockpile is used to feed CSP, a second small stockpile will be created for subsequent feed to CSP. The staging stockpile of covered, excavated material located outside the Sprung[™] structure will supply material for the 80 ton stockpiles.

3.0 CLEAN SOIL PROCESS® (CSP)

A principal function of CSP is the collection and management of the volatile hydrocarbons typically associated with MGP waste soils, i.e., benzene, toluene, ethylbenzene, and xylenes (BTEX). Within CSP, BTEX will be volatilized, captured, and condensed, resulting in a liquid solvent product. CSP is a closed system. Air flow entering the system is calculated based on the assumption of 25 percent pore space in the material to be treated and the rate of operation for the exhaust fan which draws vapors to the condenser. The range of air flow at a feed rate of 10 metric tons per hour is from 2 to 20 m³/hr.

The attached flow diagram of the Simplified Clean Soil Process (Figure 1-1) depicts the operation of CSP planned for the Norwich demonstration. Condensation of the captured volatiles, largely benzene, toluene, ethylbenzene and xylenes (BTEX), will minimize the amount of potential air emissions from the system. The capacity of the condenser will be 2.5 tons per hour. The operational efficiency of the condenser included with CSP is expected to be relatively high, but will vary with flow rate and BTEX concentration. Some residual BTEX vapor is expected downstream of the condenser, but it will be contained and managed in two ways: (1) recycling for combustion or (2) filtration through activated carbon. Benzene is expected to be the principal gaseous residual downstream of the condenser, because it is the most volatile of BTEX compounds.

During the demonstration, CSP will be operated in two modes to manage the potential emissions of residual organic volatiles. The emissions will be either:

- vented to the atmosphere after activated carbon filtration; or
- recycled to the boiler.

The solvent product will be handled by a reclamation contractor or manufacturer. Based on calculations shown in Appendix A, the estimated volume of solvent product will range from approximately 2 to 4 gallons per hour of operation at a feed rate of 10 metric tons per hour. The average detected concentrations of BTEX in the areas to be excavated during the IRM are the basis for this range:

Benzene	321	mg/kg
Toluene	471	mg/kg
Ethylbenzene	118	mg/kg
Xylene	498	mg/kg

From measurements of BTEX in soils to be used for the demonstration (Task II Site Investigation), the composition of the solvent product is expected to consist of chiefly toluene and xylenes.

4.0 BOILER

A boiler will generate steam during operation of CSP. During boiler output from 25 to 100 percent, it will be fueled with natural gas at an estimated range of 55 to 220 m³/hr. and the combustion air demand will range from 579 to 2,317 m³/hr. Because the unit uses natural gas as fuel, no permit is needed to operate it (6 NYCRR Part 201.6). The estimated maximum heat load resulting from the introduction of benzene to the boiler is 349,000 BTU/hr. (0.35 MBTU/hr.), as shown below.

Benzene High Heat Value = 18,188 BTU/lb = 3,687.5 BTU/ft

Assuming 20 m³/hr of air, mass flow of benzene = 8.71 Kg/hr (2,205 lb/Kg) = 19.205 lb/hr.

Benzene Heat Load = (19.205 lb/hr.)(18,188 BTU/lb)= 349,000 BTU/hr.

= 0.35 MBTU/hr.

5.0 <u>EMISSIONS CONTROL</u>

5.1 Atmospheric Venting through Activated Carbon Filters

The activated carbon filter system (Figure 1-1) is designed to work both sequentially and in parallel. Any residual vapor would pass through two pairs of filters before exiting to the atmosphere. A photoionization detector between the first and second pairs would detect breakthrough of the first pair should that occur before a scheduled substitution of fresh carbon canisters. The substitution sequence would remove the first pair of canisters and move the second pair into their place. Two fresh canisters would be installed at the second pair positions.

Information and calculations regarding the operation of the activated carbon filter system are provided in Form 76-19-3 for Process, Exhaust or Ventilation System (Appendix B).

5.2 Recycling

While operating CSP when recycling vapor to the boiler, an estimated maximum load of 8.71 kg/hr of residual benzene would be fed to the boiler combustion chamber with air flow from the system condenser. Because air introduced to the system will be limited to pore spaces in treated material, the air flow from the condenser will be relatively low; an estimated 2 to 20 m³/hr. is estimated based on an assumed 25 percent pore space. The combustion air demand far exceeds the flow from the condenser as shown in Appendix C.

Information and calculations regarding the operation of the boiler during the recycling mode are provided in Form 76-19-2 for Stationary Combustion Installation (Appendix C).

APPENDIX A VOLUME ESTIMATE FOR CONDENSED BTEX

VOLUME ESTIMATE FOR CONDENSED BTEX

Method

The volume of benzene, toluene, ethylbenzene, and xylene condensed and recovered by the Clean Soil Process® (CSP) was determined by estimating the mass flow rate of the compounds volatilized from the soil and then estimating the mass of compounds that pass through the condenser and remain in the vapor phase. The mass of compounds that pass through the condenser and remain in the vapor phase were determined to estimate potential vapor emissions from CSP (Appendix B). This calculation was based on the worst case assumption that the concentrations of BTEX are such that saturated conditions exist for each compound. This assumption is verified in the following calculations by determining the partial pressure of each compound at maximum and minimum soil concentrations (Phase III Investigation) and comparing the partial pressure to the vapor pressure of the compound at the condenser conditions. The partial pressure of each compound is a function of the compound's concentration in the air stream and the pressure in the condenser.

```
[Cs(mg/kg) \times ms (kg/hr)]/1,000,000 (mg/kg)
mt(kg/hr)
               =
where:
                      total mass loading of compound
       mt
               =
       Cs
                      concentration of compound in soil
               =
                      mass loading of soil = 10,000 \text{ kg/hr}
       ms
Ca(mg/m<sup>3)</sup>
               =
                      [Cs(mg/kg) \times ms(kg/hr)]/Qa(m^3/hr)
where:
       Ca
                      concentration of compound in the air stream to condenser
                      concentration of compound in soil
       Cs
               =
                      mass loading of soil = 10,000 \text{ kg/hr}
       ms
               =
                      volumetric flow rate of air through system
       Oa
Pi(psi)
                      [Ca(ppm) \times Patm (psi)]/1,000,000
               =
where
       Ρi
                      partial pressure of the compound
                      concentration of compound in the air stream to condenser
       Ca
       Patm
                      pressure in the condenser = 14.7 \text{ psi}
              =
       Note:
                     if Pi > vapor pressure (Pv), then saturated conditions exist
                      if Pi < Pv, then no condensation occurs for that specific
                     compound
mc(kg/hr)
                     mt(kg/hr) - ma(kg/hr)
where
```

mass of compound condensed in condenser

mass of compound passed through condenser at saturated conditions

total mass loading of compound

=

=

=

mc

mt

ma

APPENDIX A

Input Parameters

	Cs (max) (mg/kg)	Cs(min) (mg/kg)	Cs(Avg)	(mg/m3)/ppm	Pv @ 25C (psi)		ma (kg/hr) @ Qa = 20 m3/hr
Benzene	1250	0.002	321	3.25	1.84	0.87	8 71
Toluene	2000	0.002	471	3.83		0.3	3.04
Ethylbenzene	290	0.001	118	4.41	0.18	0.11	1 12
Xylenes	1600	0.005	498	4.41	0.13	0.09	0.85

RESULTS

Maximum soil concentrations and Qa = 2 m3/hr

	mt (kg/hr)	Ca (mg/m3)	Ca (ppm)	Pi (atm)	mc (kg/hr)	Vc (liters/hr)
Benzene	12.5	6.25E+06	1.92E+06	28.27	11.63	
Toluene	20	1.00E+07	2.61E+06	38.38	19.7	22.72
Ethylbenzene	2.9	1.45E+06	3.29E+05	4.83	 	
Xylenes	16	8.00E+06	1.81E+06	26.67	15.91	18.29
				Totals	50.03	57.50
					gal/hour	15.19

Maximum soil concentrations and Qa = 20 m3/hr

	mt (kg/hr)	Ca (mg/m3)	Ca (ppm)	Pi (atm)	mc (kg/hr)	Vc (liters/hr)
Benzene	12.5	6.25E+05	1.92E+05			4.32
Toluene	20	1.00E+06	2.61E+05	3.84	16.96	19.56
Ethylbenzene	2.9	1.45E+05	3.29E+04	0.48	1.77	2.04
Xylenes	16	8.00E+05	1.81E+05	2.67	15.15	17.41
				Totals	37.67	43.34
					gal/hour	11.45

Minimum soil concentrations and Qa = 2 m3/hr or 20 m3/hr

	mt (kg/hr)	Ca (mg/m3)	Ca (ppm)	Pi (atm)	mc (kg/hr)	Vc (liters/hr)
Benzene	0.00002	1.00E+01	3.08E+00	4.52E-05	0	0
Toluene	0.00002	1.00E+01	2.61E+00	3.84E-05	0	0
Ethylbenzene	0.00001	5.00E+00	1.13E+00	1.67E-05	0	0
Xylenes	0.00005	2.50E+01	5.67E+00	8.33E-05	0	0
				Totals	0	0

Average soil concentrations and Qa = 2 m3/hr

		Ca (mg/m3)	Ca (ppm)	Pi (atm)	mc (kg/hr)	Vc (liters/hr)
Benzene	3.21	1.61E+06	4.94E+05	7.26		2.67
Toluene	4.71	2.36E+06	6.15E+05	9.04	4.41	5.09
Ethylbenzene	1.18	5.90E+05	1.34E+05	1.97	1.07	1.23
Xylenes	4.98	2.49E+06	5.65E+05	8.30	4.89	5.62
				Totals	12.71	14.61
					gal/hour	3.86

Average soil concentrations and Qa = 20 m3/hr

	mt (kg/hr)	Ca (mg/m3)	Ca (ppm)	Pi (atm)	mc (kg/hr)	Vc (liters/hr)
Benzene	3.21		4.94E+04	0.73		
Toluene	4.71	2.36E+06	6.15E+04	0.90	1.67	1.93
Ethylbenzene	1.18	5.90E+05	1.34E+04	0.20	0.05	
Xylenes	4.98	2.49E+06	5.65E+04	0.83	4.13	
			*	Totals	5.85	6.73
					gal/hour	1,78

Note:

For the purposes of this calculation, the maximum concentration = 50% of the maximum measured concentrations in the soil from areas to be excavated. Average concentration = mean of detected concentrations in areas to be excavated.

APPENDIX B

FORM 76-19-3 FOR PROCESS, EXHAUST, OR VENTILATION SYSTEM

NEW YORK STATE DEPARTMENT OF ENVIRONMENTAL CONSERVATION

COPIES
WHOTE - ORIGINAL
GREEN - DIVISON OF AIR
WHITE - REGIONAL OFFICE
WHITE - PIELD REP

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The rationale for the approach applied to determine benzene stream exiting from the condenser is as follows

* According to Dalton's Law (at saturation conditions) gas leaving the condenser will contain

 $V_{benzene} = P_{benz}/P_{atmospheric} = 12.7/101.3 \ x100\% = 12.5\%$ $P_{benz} \cdot partial \ pressure \ for \ benzene$ 12.5 % (by volume) of benzene vapours.

** Molar mass of benzene (C6 H6) is 78 g/mole

1 kg of benzene contains $1000g/78g = 12.8 \text{ moles/}kg^{-1}$ and 1 mole of any gas occupies 22.4 liters (Avogadro's Law)

so 1kg of benzene (under standard conditions) occupies

$$V = 12.8 \times 22.4 = 287 \text{ liters/kg}$$

***The amount of benzene (at saturation conditions) will depend the flow rate of gas exiting the condenser and will be

For 2 m3/h flow rate

$$V_B = 2.0 \times 12.5\%/100\% = 0.25 \text{ m}^3 \text{ (250 liters)/hr,}$$

or $250/287 = 0.87 \text{ kg/hr.}$

Following that rule the data in Table 1 were obtained

Table 1

			· · · · · · · · · · · · · · · · · · ·	
BY KS DA	ATE 12/22/94	SUBJECT CLEAN SOIL P.	808 555 SHEET NO. 2 OF 5	
CHKD. BY DA				

ACTUAL WORSE CASE BENZENE LOADING BASED ON SOIL CONCENTRATION

Benzene Soil Concentration = 2500 mg/kg SOIL LONDING RATE = 10,000 mg/hr WORSE CASE BENZENE FLOW TO CONCENSER = 25 kg/hr

.. REGARDLESS OF AIR FIOW RATE BENZENE

CONCENTRATION EXITING CONVENSER COULD

NEVER EXCEED 25 Kg/Ar. BASED ON WORSE CHEE SOIL DAM.

A DOTTIONALLY IF THE BENZENE LOAD TO SYSTEM

IS BELOW SATURATION THE MASS LEAVING THE

CONDENSER WILL BE LOWER.

BY NO DATE 12/20104 SUBJECT Clean Soils France SHEET NO. 3. OF 5

CHKD. BY DATE TONICON FOR SINCE JOB NO. 7:51.01-02

MORES CASE TOLYENE PIK STIEFM EMISSIONS FROM THE CONDENSER

MORES CALCULATIONS BASED ON VENDORS APPROACH'

FOR BENZENE VAPOUR CALCULATIONS ATSATURATION CONVITIONS

TOLUENE VAPOR PRESSURE: PV = 0.55 10/1N2 @ 25 °C

- According to Caltons Law (at succession constitues):

1. gas leaving the constenser will contain 3.7% to some by volume

- Molar mass of Tollers = 92.14 Inole

For 1 kg of tollers: (1000) (1 mole) = 10.85 mole

1 mole 9as /22.4 liters: Upliese = (10,85 mole) 22.4 lites) = 243 liters

1 mole 9as /22.4 liters: Upliese = (10,85 mole) 22.4 liters

- The amount of Toloric (at saturation conditions) will depend on the flow rate: Votal

Versione = Valid (1037) $e \quad Valid = 20 \quad m^3/hr$ $Valuene = 0.74 \quad m^3/hr = 740 \quad liters/hr$ $Mass bloom = \frac{Value}{Valuene} = 740 \quad liters/hr = 3.04 Mg/hr$

BY KFS DATE 12/22/14 SUBJECT Clean soils from SS SHEET NO. 4 OF 5

CHKD. BY A DATE CONSERS PORTSOINSNIE JOB NO. 205/-01-02

WORSE CASE ETHYLBENGENE EMISSIONS FROM THE CONDENSER

WOTE: CALCULATIONS BASED ON VENIDOR APPROACH FOR BENZEIVE CALCULATIONS AT SATULATED CONDITIONS

Ethyl benzene Vapor Pressure: Pu = 0.18 B/m= @ 35 °C

- According to Dalltons Law (at saturation conclitions):

 $\frac{Ve8}{V + otal} = \frac{P_V}{Parm} = \frac{0.13}{14.7} = 0.012$

1. 925 leaving the constant will contain 1.2% ethyl sensere by volume

- molar mass of ethylbenzene = 106.17 9/mole

1. 9.42 moles/xa

Very/ Senzence = (9.42 note/2) (22.4 ters) = 211 1/405

- The amount of ethylbenzene at saturation conditions will depend on the Flow rate Unital

@ Vtotal = 20 m3/1000

Verhylderizere = (20 m/hr) (5,012) = 0,24 m/hr = 240 41/60/hr

Mass of Ethyloenzene = 340 11 ters/in = 1.13 halp

BY KES DATE 12/22/14 SUBJECT Class sale fores SHEET NO. 5 OF 5

CHKD. BY AF DATE CONSIDERS PORTSON JOB NO. 2051-31-32

WORSE CASE XYLENE EMISSIONS FROM THE CONFINSER

WOTE: CALCULATIONS CASED ON PENDOR APPROACH FOR

BENZENE CALCULATIONS AT SATURATED CONDITIONS

- XYLENUE Vapor Pressure: PU = 0.13 B/W= 8 25 0C

- According to Daltons Law (at saturation conslitions):

Vxy = Pv = 0.13 = 0.009

1. gas leaving the constancer will contain 0.9% "xyEENE" by volvine

- motor mass of xylewe = 106.17 % mote 1. 9.42 moto/kg $U_{xylewe} = (9.42 \text{ moto/kg})(22.4 \frac{1400}{\text{mote}}) = 211 \frac{11400}{\text{kg}}$

- The amount of xylene of submation conditions with depend on the Flow rate Vental

@ Vtotal = 20 m3/hour

V xyLENE = (20 m/hr) (5,009) = 0.18 m/hr = 180 4 m/hr

Mass of Xylene = 180 11 mas/or = 0.85 45/hr

									,
	DATE 12/22/94	SUBJECT	Clean	يئ رەي	Process_	<u>-</u>	SHEET NO.	_/_	. OF
		3000001	Carbon'	Las:10	مندلارد مندلارد		IOR NO	2051	-01-63
CHKD. BY	DATE		Carosio		-		100		

- ASSUME FLOW RATE TUROUGH SYSTEM = 20 m3/AC
- CARBON LOADING CAPACITIES FROM CALGON CO.
- Two 90 kg carson consisters will be used total 180 by

BENZENE

Constants above C 20 m/nr from constansor = 0.43 kg/m³ m = 8.71 kg/hrCarbon Capazity = 0.35 kg benzene /kg carbon

CARBON LIFE = (0.35)(180 kg or fine) = 7.2 hours

TOLUENE

Concentration @ 20 m3/hr = 0.152 48/m3 $\dot{m} = 3.04 \text{ Mg/hr}$ Carbon Capacity = 0,35 Mg tolucial kg carbon

Carbon Lege = (0.35) (180 Mg Carbon) = 20.7 hours

3.04 Mg tolucia

The carbon capacities for ethilbenzene and xylone are higher and the concentrations and mass loadings are lower. Therefore, the carbon life is significantly longer when evaluating for these companies and benzene is still worse case.

Exhaust Analysis Results

Input Data Summary

Boiler Size, hp:	200
Rated Input, Btu/hr:	8,388,750
Fuel Type:	Natural Gas
Boiler Type:	Steam
Steam Pressure, psig:	10
Stack Diameter, in:	16

Exhaust Data Summary

		Input (percent)			
		25%	50%	75%	100%
Input	Horsepower MM Btu/hr	50 2.09	100 4.18	150 6.28	200 8.37
Temp	erature Degrees, F	260	290	310	325
Exhau	ACFM SCFM Bo/br	656 483 2,172	1,154 816 3,669	1,777 1,224 5,503	2,415 1,831 7,338
Exhau	ust Velocity ft/sec ft/min	7.8 469.5	13.8 826.3	21.2 1,272.5	28.8 1,729.7

BOILER HP	200			
RATINGS - SEA LEVEL TO 5000 FT				
Rated Cap. Btu Output (1000 B tu/h)	6895			
APPROXIMATE FUEL CONSUMPTION AT RATED CAPACITY				
Light Oil				
Heavy Oil	•			
Gas MBtu - Natural Gas	8970			
POWER REQUIREMENTS - SEA LEVEL TO 3000 FT, 60 HZ				
Blower Motor Hp (except gas)	-			
Gas Modeis (only)	10			
Oil Pump Motor, Hp No. 2 Oil	1/2			
Oil Pump Motor, Hp. No. 6 Oil	1/2			
Oil Heaters NW No. 6 Oil	5			
Air Compressor Motor Hp (Oil Mixing Only)	Air Compressor Belt-Driven From Blower Motor			

APPENDIX C

FORM 76-19-2 FOR STATIONARY COMBUSTION INSTALLATION

Estimated Emission Levels Boiler Model: CB700-200-15

Fuel: Natural Gas

Emission Levels

Pollutant	Ib/MMBTU	lb/hr	tons/year
co	0.15	1.26	5.50
NOx	0.12	1.00	4.40
SOx	0.001	0.01	0.04
HC	0.016	0.13	0.59
PM	0.01	80.0	0.37

Notes:

1. The emission factors in Ib/MMBTU are based on the evaluation of laboratory and field test data.

The hourly emission rates are based on the maximum rated capacity of the boiler (8,369 MMBTU/hr).
 The annual emission levels in tons/year are based on the boiler firing 24 hours per day 365 per year.

NEW YORK STATE DEPARTMENT OF ENVIRONMENTAL CONSERVATION

COPIES WHITE ORIGINAL BLUE DIVISON OF AIR



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Exhau	st Velocity ft/sec ft/min	7.8 469.5	13.8 826.3	21.2 1,272.5	28.8 1,729.7	

BOILER HP	200				
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APPROXIMATE FUEL CONSUMPTION AT RATED CAPACITY					
Light Oil	•				
Heavy Oil	-				
Gas MBtu - Natural Gas	8970				
POWER REQUIREMENTS - SEA LEVEL TO 3000 FT, 60 HZ					
Blower Motor Hp (except gas)	-				
Gas Models (only)	10				
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Oil Pump Motor, Hp. No. 6 Oil	1/2				
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Fuel: Natural Gas

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