

E. I. DU PONT DE NEMOURS & COMPANY

NIAGARA FALLS, N.Y. 14302

cc: Y. Erk - DEC (Buf)

M. L. Doster - DEC (Buf)

C. P. Allen - DEC

M. Hopkins - NCHD

CHEMICALS AND PIGMENTS DEPARTMENT

August 18, 1988

John S. Tygert
NYS Dept. of
Environmental Conservation
Region 9
600 Delaware Avenue
Buffalo, New York 14202-1073

Dear Mr. Tygert:

EFFECTIVENESS OF ADAMS AVE. SEWER SLURRY WALL

Attached, please find three copies of an evaluation of the effectiveness of the Adams Avenue sewer slurry wall. Recommendations contained within this report are in the process of being inplemented.

Please call me at (716) 278-5344 if you have any questions.

Regards,

Cicl Maryews (i Richard D. Marczewski, P.E.

Area Manager

Waste Treatment

ANR 10

5120 Butler Pike Plymouth Meeting Pennsylvania 19462 215-825-3000 Telex 846-343

Woodward-Clyde Consultants

August 11, 1988 88C2075B-1

E. I. du Pont de Nemours and Company 26th Street and Buffalo Avenue Niagara Falls, New York 14302

Attention:

Mr. Rick Marczewski

Re:

Effectiveness Evaluation

Adams Avenue Sewer Slurry Wall

Gentlemen:

In response to your request, Woodward-Clyde Consultants (WCC) is pleased to present this evaluation of the effectiveness of the Adams Avenue sewer slurry wall. The slurry wall was installed to decrease the off-plant migration of contaminants from the Du Pont Niagara Plant along the bedding of the active Adams Avenue sewer. This evaluation was performed in response to recent questions posed by the NYSDEC in regards to the slurry wall effectiveness.

If you have any questions or comments regarding this report, please do not hesitate to contact us.

Sincerely,

WOODWARD-CLYDE CONSULTANTS

Timothy D. Glazar Senior Staff Geologist

Robert 11 111

Lynn Rubisch Penniman, CPSS

Project Manager

TDG/LRP/kcs/WM-8K



EFFECTIVENESS EVALUATION ADAMS AVENUE SLURRY WALL NIAGARA PLANT NIAGARA FALLS, NEW YORK

Prepared for:

E.I. DU PONT DE NEMOURS AND COMPANY, INC. Niagara Falls, New York

Prepared by:

WOODWARD-CLYDE CONSULTANTS
Plymouth Meeting, Pennsylvania

August, 1988

EXECUTIVE SUMMARY

Manmade passageways investigations have been conducted at the Du Pont Niagara Plant to address the potential for movement of contaminants through buried utilities, such as water, sewer or electrical lines. Data from these investigations suggested that the Adams Avenue sewer may have been a pathway for contaminant transport from the site. As a result, a low permeability underground barrier (slurry wall) was constructed across the Adams Avenue sewer line.

Utility wells are located on both sides of the slurry wall and water level data before and after construction of the wall has been tabulated and evaluated. From the information, it appears that groundwater flow in the shotrock backfill has been reduced by the low permeability slurry wall resulting in mitigation of off-plant contaminant transport. Flow in the sewer line itself is considered unlikely since the line was broken and the ends were plugged. Monitoring of groundwater levels and sampling should continue in order to verify that the slurry wall is maintaining its integrity as a hydraulic and contaminant barrier.

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TABLE OF CONTENTS

		Page Number
1.0	PREVIOUS INVESTIGATIONS AND DATA ANALYSES	1
2.0	SLURRY WALL DETAILS	2
3.0	EVALUATION OF SLURRY WALL EFFECTIVENESS	2
4.0	RECOMMENDATIONS	3

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LIST OF TABLES

	Table Number
SUMMARY OF DEPTH OF MATERIALS ENCOUNTERED IN TEST PITS	1
SUMMARY OF PERMEABILITY TESTS	2
WATER LEVELS IN NEARBY UTILITY WELLS	3
LIST OF FIGURES	
	Figure Number
LOCATION OF ADAMS AVENUE SLURRY WALL	1
EXCAVATION PROGRESS DIAGRAM	2
AS-BUILT PLAN AND SECTION OF SLURRY WALL	3
GRAIN-SIZE DISTRIBUTION CURVES OF BACKFILL SAMPLES	4
	, 4
LIST OF APPENDICES	
	Appendix
TEST PIT LOGS AND UTILITY WELL CONSTRUCTION DIAGRAMS	Α
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1.0 PREVIOUS INVESTIGATIONS AND DATA ANALYSES

WCC has prepared two reports: "Manmade Passageways Investigation," (dated February 17, 1984) and "Supplemental Manmade Passageways," (dated October 24, 1984) which addressed the potential for the movement of contaminants through manmade passageways. Manmade passageways are defined as those portions of the subsurface which have been excavated and refilled to accommodate the placement of buried utilities, such as water, sewer, or electrical lines. Exploratory test pits were excavated adjacent to suspect utility lines and soil samples were obtained for chemical analysis. Utility wells were installed in the test pits to permit monitoring and analysis of water flowing in the sewer trench backfill material.

Test pits TP-1 and TP-14 were excavated adjacent to the Adams Avenue sewer. A summary of depths of materials encountered in each pit is presented in Table 1. Utility well U-1 was installed in TP-1 and utility well U-14 was installed in TP-4 (Figure 1). Test pit logs and utility well construction diagrams are presented in Attachment A. The test pit logs indicate that the Adams Avenue sewer trench was cut into rock and appears to have been drilled and shot. The sewer pipe bedding was noted as a silty clay/clayey silt with coarse to fine sand and gravel size rock fragments. The pipe trench backfill was noted as predominantly shot rock and more permeable than the surrounding material. The utility wells were screened in the sewer trench backfill since the higher permeability shot rock backfill would be the preferential pathway for groundwater movement and subsequent contaminant transport.

After the test pit excavations were completed and the utility wells allowed to equilibrate, water levels and groundwater samples were obtained. The groundwater elevations observed in utility wells U-1 and U-14 were lower with respect to the nearby monitoring well 19A. This would indicate a hydraulic gradient towards the sewer trench. Groundwater concentrations of C-1 and C-2 compounds in utility wells samples were about two orders of magnitude greater than in groundwater samples from monitoring well 19A. These data suggested that the Adams Avenue sewer may be a pathway for contaminant transport from the site. As a result of the investigation, Du Pont requested that WCC prepare a report on the construction of a low permeability underground barrier (slurry wall) across the Adams Avenue sewer, west of Chemical Road (Figure 1).

2.0 SLURRY WALL DETAILS

The purpose of the slurry wall was to prevent the migration of contaminants through the sewer and sewer bedding material. Construction of the slurry wall was started on June 2, 1986, and was completed on June 13, 1986. An excavation progress diagram is presented in Figure 2. The slurry wall was constructed by excavating the unconsolidated overburden and sewer backfill and replacing with a soil bentonite backfill. An as-built plan and section of the slurry wall is presented in Figure 3. The backfill was composed of soil from a local borrow source, bentonite, and water to form a slurry. The completed slurry wall is about 35 feet long, ranges in thickness from 8 feet in the sewer trench to 3 feet on top-of-bedrock, and ranges in depth from 7 to 18 feet.

Two samples of the soil-bentonite backfill material were returned to WCC's Plymouth Meeting, Pennsylvania laboratory for permeability testing. The results of the permeability testing with water as the permeant indicated a backfill sample permeability of less than 6.5×10^{-8} cm/sec. The Summary of Permeability Tests is presented in Table 2, with the grain-size distribution of the backfill samples shown on Figure 4.

3.0 EVALUATION OF SLURRY WALL EFFECTIVENESS

Water level data before and after construction of the slurry wall is presented in Table 3. Prior to installation of the slurry wall, a relatively steep hydraulic gradient was noted between the utility wells with groundwater in the trench flowing to the west. After the slurry wall was installed, water levels in the upgradient utility well U-1 remained consistent, however, the downgradient well U-14 was dry. From this information it appears that groundwater flow in the shot rock backfill has been reduced by the low permeability slurry wall resulting in the mitigation of off-plant contaminant transport. Flow in the sewer line itself is considered unlikely since the line was broken and plugged with cinder brick, mortar, and "water plug" cement on both sides of the slurry wall.

4.0 RECOMMENDATIONS

Utility well U-1 was damaged in in the winter of 1987 and has since been inaccessible to sampling crews. WCC recommends that U-1 be repaired in order to complement U-14 in monitoring the effectiveness of the Adams Avenue slurry wall. Utility well U-14 should be checked to verify that the casing is intact and the bottom is clear of any obstructions which may cause a dry well reading. Monitoring of groundwater levels and sampling in U-1 and U-14 should continue in order to verify that the slurry wall is maintaining its integrity as a hydraulic and contaminant barrier.

Tables

TABLE 1

SUMMARY OF DEPTH OF MATERIALS
ENCOUNTERED IN TEST PITS
DU PONT NIAGARA PLANT
NIAGARA FALLS, NEW YORK

Underlying Material	Bedrock	Bedrock
Bedding Material	Gravelly sandy silty clay under shotrock	Gravelly sandy silty clay/ clayey silt under shot rock
Water Elevation	560.9	556.8
Water Level Below G.S. (feet)	8.5	12.1
Total Depth (feet)	14.5	14.8
Depth Bedrock (feet, elevation)	8.0(561.4)	6.0(562.9)
Depth Clay/Till (feet)	1.5-8.0	2.5-6.0
Depth Fill (feet)	0-1.5	0-2.5
Surf. Elev.	569.4	568.9
Location	-	14

TABLE 2

SUMMARY OF PERMEABILITY TEST ADAMS AVENUE SLURRY WALL DU PONT NIAGARA PLANT NIAGARA FALLS, NEW YORK

Permeability (cm/sec)	6.5×10^{-8}	5.8×10^{-8}
Final Degree of Saturation (%)	99.7	100.0
Final Moisture Content (%)	36.5	31.5
Confining Stress (TSF)	0.36	0.36
Initial Degree of Saturation (%)	100.0	92.4
Dry Unit Weight (pcf)	8.09	74.4
Initial Moisture Content (%)	66.1	43.7
Test No.	-	2

TABLE 3

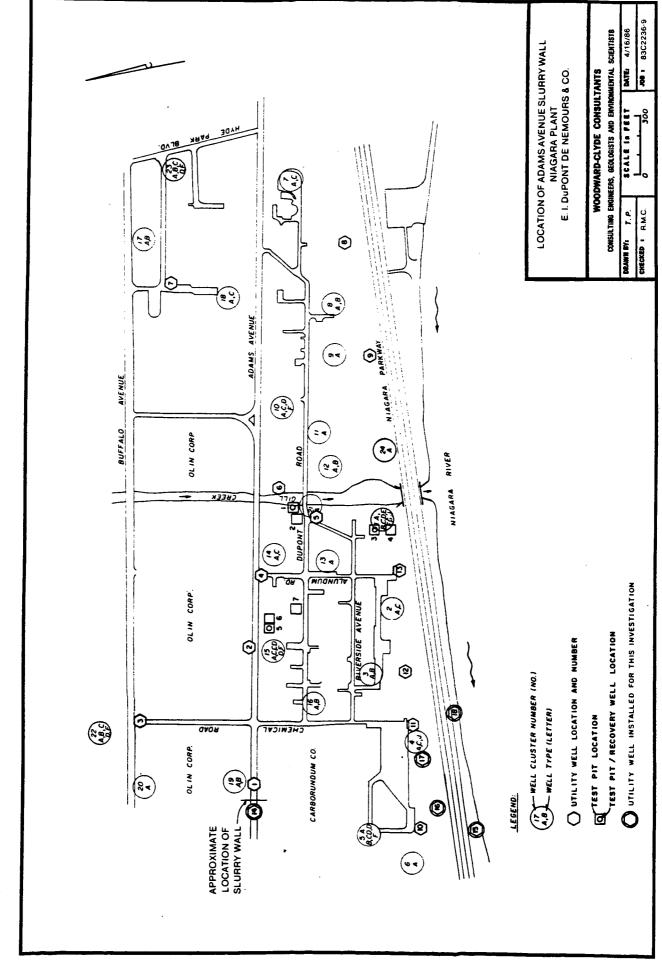
WATER LEVELS ADAMS AVENUE SLURRY WALL EVALUATION DU PONT NIAGARA PLANT NIAGARA FALLS, NEW YORK

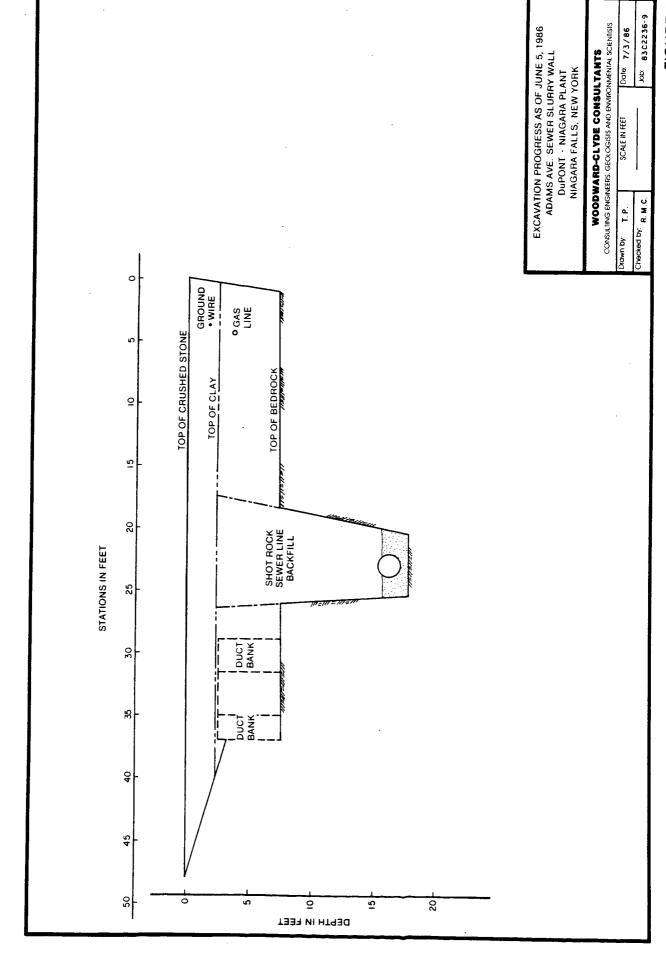
Date	Water Level (ft) U-1	Water Elevation (ft) U-1	Water Level (ft) U-14	Water Elevation (ft) U-14
01/23/84	8.5	560.4	U-14 Instal	led 5/17/84
05/10/84	7.8	561.1		
06/01/84	ND	ND	11.8	557.2
06/07/84	8.0	560.9	12.9	556.1
06/13/84	ND	ND	12.1	556.8
08/22/84	6.73	562.2	13.4	555.6
	SLURRY WALL INS	TALLED JUNE 2 THROU	GH 13, 1986	
06/19/86	6.8	562.1	Dry	< 554.4
12/01/86	8.2	560.3	Dry	<554.4
03/27/87	*	*	Dry	< 554.4
04/07/87	*	*	Dry	< 554.4
05/11/87	*	*	Dry	< 554.4
06/09/87	*	*	Dry	<554.4
07/01/87	*	*	Dry	< 554.4
08/13/87	*	*	Dry	< 554.4
09/02/87	*	*	Dry	< 554.4
10/05/87	*	*	Dry	< 554.4
11/16/87	*	*	Dry	< 554.4
12/07/87	*	*	Dry	< 554.4
01/04/88	*	*	Dry	< 554.4
02/02/88	*	*	Dry	< 554.4
03/03/88	*	*	Dry	< 554.4

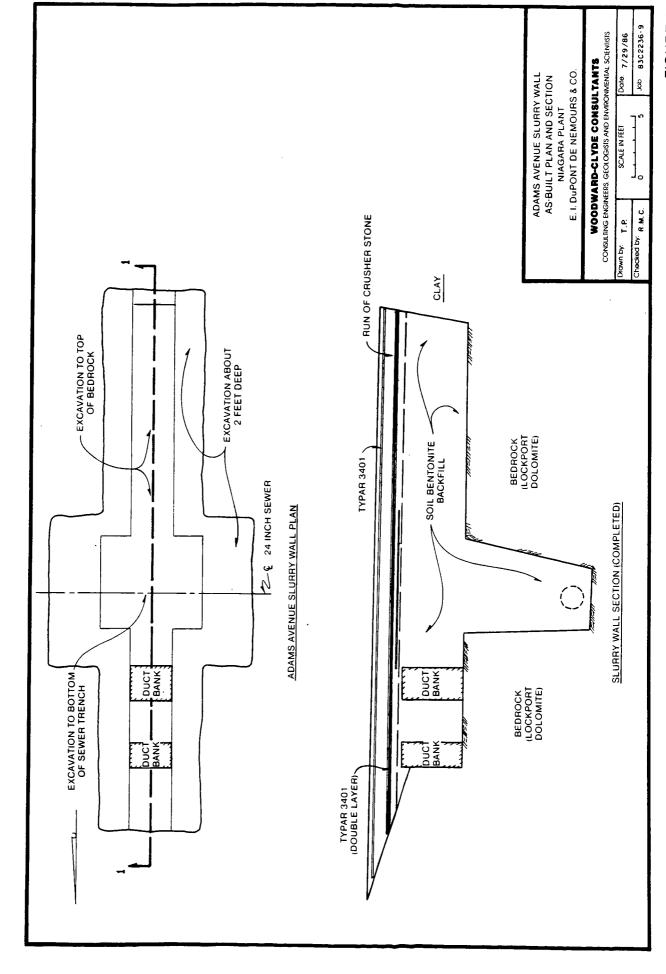
ND = No data obtained.

^{* =} Well casing bent or buried; no data obtained.

Figures







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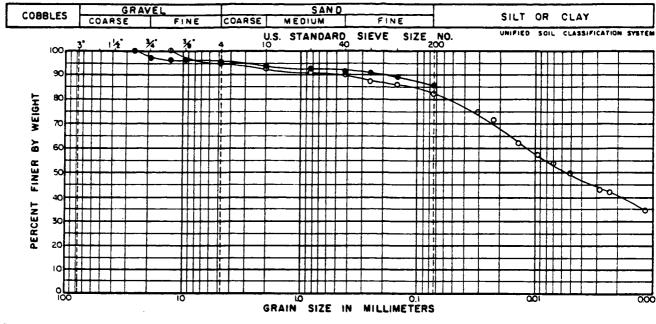
PROJECT

Sewer

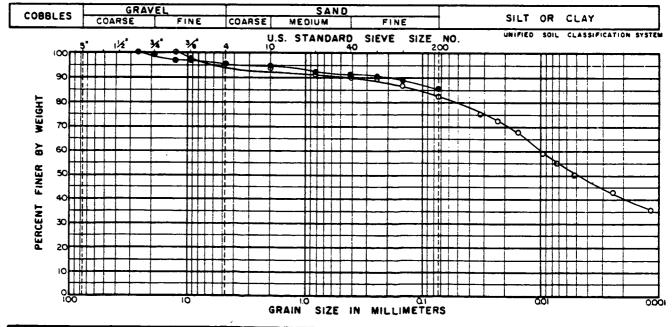
Avenue

Adams

Niagara Falls,



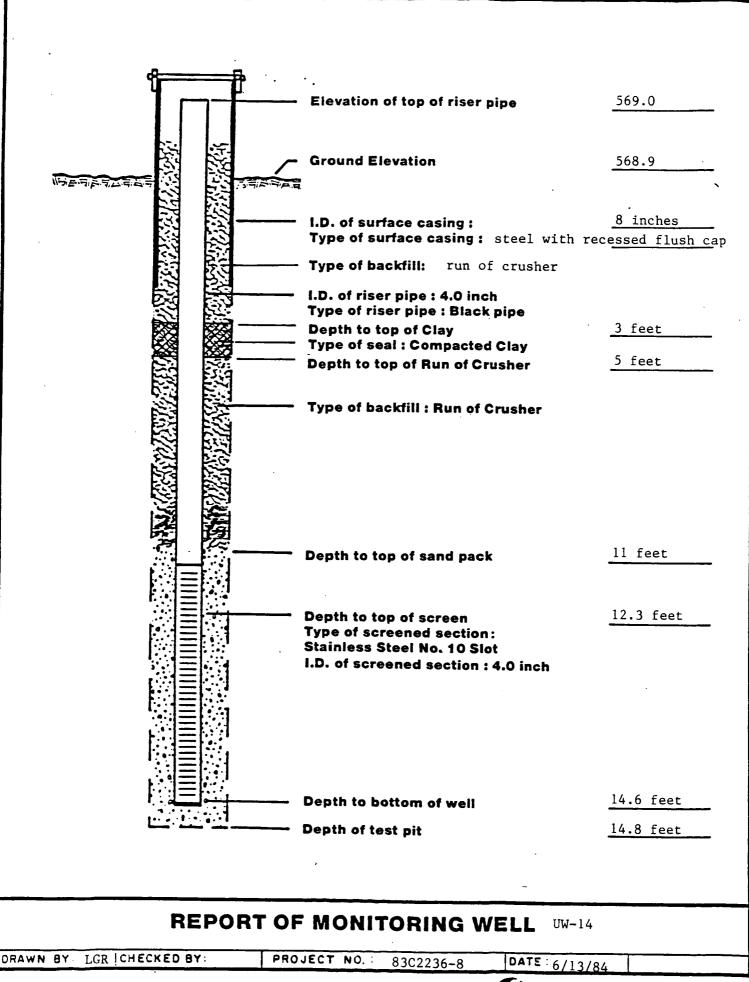
BORING	SAMPLE	DEPTH	SYMBOL	CLASSIFICATION	M C	LL	PL
	L&M		•	Brown coarse to fine sandy silty clay,	_		
				trace coarse to fine gravel (Borrow Source)			
	#1		0	Brown coarse to fine sandy silty clay,			
		· · · · · · · · · · · · · · · · · · ·		trace fine gravel (Backfill)			



BORING	SAMPLE	DEPTH	SYMBOL	CLASSIFICATION	MC	LL	PL
	UNK		•	Brown coarse to fine sandy silty clay,			
				trace fine gravel (Borrow Source)		1	
	#2		0	Brown coarse to fine sandy silty clay,			
				trace fine gravel (Backfill)			
L	<u> </u>		1				

Attachments

1 1 1 1 1 1 1 1 1 1		549 02
	Elevation of top of riser pipe	568.93
	_ Ground Elevation	569.4
	N=1.F	
<u> </u>	I.D. of surface casing 8.0 Inch	
	Type of surface casing Steel with reco	essed flush cap
	Type of Backfill Run of Crusher	
	4.0 lmah	
	I.D. of riser pipe 4.0 Inch Type of riser pipe Black Pipe	
<u> </u>	— Depth to Top of Clay	
	Type of Seal <u>Compacted Clay</u>	5'
2 2	— Depth to Top of Run of Crusher	7.
	. Type of backfill Run of Crusher	
	•	
	-	
	Depth to top of sand pack	11.1
	Depth to top of sand pack	11,1
	Depth to top of screen	12.3'
	Type of screened section	
	Stainless Steel # 10 Slot	
		
	I.D. of screened section 4.0 inch	
· · · · · · · · · · · · · · · · · · ·		4
- '劉章[3]		
	• • • • • • • • • • • • • • • • • • • •	14.3'
	Depth to bottom of well	14.5
1	Depth of Test Pit	14.5'
		··· ·····
	•	
REPORT	OF MONITORING WELL	
• • • • • • • • • • • • • • • • • •	OF MONITORING WELL UW-1	
RAWN BY: R.M.C. CHECKED BY: R.M.C. PROJ	ECT NO: 83C2236-5 DATE: 1/23	/84 FIGURE NO:
	UAIE: 1/23	704 FIGURE NO:



AUG 10 PO

49 # X9