

**Division of Environmental Remediation** 

## Hydrogeologic Evaluation Report

Niagara Sanitation Landfill Wheatfield, Niagara County, New York Site Number 932054

**December 2024** 

New York State Department of Environmental Conservation Region 9 700 Delaware Avenue Buffalo, New York 14209

# **Special Report**

Hydrogeologic Evaluation of the Niagara Sanitation Landfill in the Town of Wheatfield, Niagara County, **New York** 



NEW YORK STATE Conservation



Prepared by:

New York State Department of Environmental Conservation **Division of Environmental Remediation** 700 Delaware Avenue Buffalo, New York 14209

> Glenn M. May, PG **Professional Geologist I**

|--|

SEC7	ΓΙΟΝ	PAGE
1.0	INTRODUCTION	
2.0	SITE HISTORY AND BACKGROUND	
2.1		2
2.1	SITE DESCRIPTION	3 າ
2.2		
2.3		
3.0	SURFACE WATER HYDROLOGY	
3.1	PRECIPITATION	7
3.2	EVAPOTRANSPIRATION	8
3.3	SITE DRAINAGE CHARACTERISTICS	9
4.0	GEOLOGY	
41	REGIONAL GEOLOGY	11
	11 Nverhurden Geology	
4	1.1.2 Redrock Geology	
42	SITE GEOLOGY	14
4	121 Surface Soils	14 15
4	12.2 Fill Material	
1	12.2 Claciolacustrine Denosit	10 17
г	4231 Brown Silt and Clay	17 17
	4.2.3.2 Unner Sand Deposit	
	4.2.3.3 Gray-Brown Silty Clay Deposit	
	4.2.3.4 Red-Gray Layered Clay Deposit	
	4.2.3.5 Lower Sand Deposit	
4	P.2.4 Glacial Till Deposit	20
4	P.2.5 Bedrock	21
5.0	HYDROGEOLOGY	22
5.1	REGIONAL HYDROGEOLOGY	22
5	5.1.1 Regional Groundwater Flow	
5.2	SITE HYDROGEOLOGY	
5	5.2.1 Fill/Upper Sand Water-Bearing Zone	
5	5.2.2 Upper Clay Aquitard	
5	5.2.3 Lower Sand Water-Bearing Zone	
5	5.2.4 Glacial Till Aguitard	
5	5.2.5 Unner Bedrock Water-Bearing Zone	
6.0	GROUNDWATER GEOCHEMISTRY	
<i>C</i> 1		
6.1 6.2	GENERAL	35 25
63	GEOCHEMICAL EVALUATION METHODS	
0.5	531 Piner Plats	
64	CONCEPTIAL GEOCHEMICAL MODEL FOR THE NIACARA SANITATION LANDELL	
65	GENCER FORE RESULTS	20 20
0.5	551 Surface Water	20
U	Sol Sulface Water management	

6.	.5.2 Fill Wells	
6.	.5.3 Upper Sand Water-Bearing Zone	
6.	.5.4 Upper Clay Aquitard	
6.	.5.5 Lower Sand Water-Bearing Zone	
6.	.5.6 Glacial Till Aquitard	
6.	.5.7 Upper Bedrock Water-Bearing Zone	
7.0	SUMMARY	
7.0	SUMMARY	
<b>7.0</b> 7.1	GEOLOGY	
7.0 7.1 7.2	GEOLOGY Hydrogeology	
7.0 7.1 7.2 7.3	GEOLOGY Hydrogeology Geochemistry	

## LIST OF FIGURES (Following Text)

- Figure 1-1 Site Location Map
- Figure 2-1 Niagara Sanitation Landfill Property Map
- Figure 2-2 Site Boundary Map Showing Wetlands
- Figure 2-3 Ground Surface Topography
- Figure 2-4 2013 Site Characterization Sample Location Map
- Figure 3-1 Precipitation Data for Western New York
- Figure 4-1 Soil Boring Location Map
- Figure 4-2 Cross-Section Location Map 1985 Phase II
- Figure 4-3 Cross-Section Location Map 2017 Remedial Investigation
- Figure 4-4 Geological Cross Section A-A' 1985 Phase II
- Figure 4-5 Geological Cross Section B-B' 1985 Phase II
- Figure 4-6 Cross Section A-A' 2017 Remedial Investigation
- Figure 4-7 Cross Section B-B' 2017 Remedial Investigation
- Figure 4-8 Cross Section C-C' 2017 Remedial Investigation
- Figure 4-9 Cross Section D-D' 2017 Remedial Investigation
- Figure 4-10 Upper Sand Surface Contour Map
- Figure 4-11 Upper Sand Thickness Map
- Figure 4-12 Depth to the Gray-Brown Silty Clay Deposit Contour Map
- Figure 4-13 Lower Sand Thickness Map
- Figure 4-14 Depth to the Glacial Till Contour Map
- Figure 4-15 Depth to the Bedrock Surface Contour Map
- Figure 4-16 Bedrock Surface Elevation Contour Map
- Figure 5-1 Monitoring Well and Staff Gauge Location Map
- Figure 5-2 Hydrograph for the Fill/Upper Sand Wells
- Figure 5-3 Hydrograph for the Fill/Upper Sand Wells
- Figure 5-4 Hydrograph for the Fill/Upper Sand Wells
- Figure 5-5 Hydrograph for the Fill/Upper Sand Wells-Staff Gauge Couplets
- Figure 5-6 Groundwater Elevation Contour Map, Fill/Upper Sand: August 2, 2013 (GES Survey)
- Figure 5-7 Groundwater Elevation Contour Map, Fill/Upper Sand: August 2, 2013 (LiRo Survey)
- Figure 5-8 Groundwater Elevation Contour Map, Fill/Upper Sand: May 19, 2014
- Figure 5-9 Groundwater Elevation Contour Map, Fill/Upper Sand: August 2, 2017

## LIST OF FIGURES (continued)

- Figure 5-10 Groundwater Elevation Contour Map, Fill/Upper Sand: August 8, 2017
- Figure 5-11 Groundwater Elevation Contour Map, Fill/Upper Sand: August 22, 2017
- Figure 5-12 Groundwater Elevation Contour Map, Fill/Upper Sand: August 30, 2017
- Figure 5-13 Groundwater Elevation Contour Map, Fill/Upper Sand: September 12, 2017
- Figure 5-14 Groundwater Elevation Contour Map, Fill/Upper Sand: September 25, 2017
- Figure 5-15Groundwater Elevation Contour Map, Fill/Upper Sand: October 17, 2017
- Figure 5-16 Difference in Groundwater Elevations: September 25 to October 17, 2017
- Figure 5-17Groundwater Elevation Contour Map, Fill/Upper Sand: October 20, 2017
- Figure 5-18Groundwater Elevation Contour Map, Fill/Upper Sand: October 27, 2017
- Figure 5-19Groundwater Elevation Contour Map, Fill/Upper Sand: November 7, 2017
- Figure 5-20Groundwater Elevation Contour Map, Fill/Upper Sand: November 21, 2019
- Figure 5-21 Groundwater Elevation Contour Map, Fill/Upper Sand: April 3, 2020
- Figure 5-22 Groundwater Elevation Contour Map, Fill/Upper Sand: November 23, 2021
- Figure 5-23Hydrograph for the Upper Clay Aquitard Well
- Figure 5-24 Hydrograph for Select Wells and Staff Gauges
- Figure 5-25 Hydrograph for the Lower Sand Wells
- Figure 5-26Hydrograph for the Glacial Till Wells
- Figure 5-27Groundwater Elevation Contour Map, Glacial Till: Phase II Report
- Figure 5-28 Groundwater Elevation Contour Map, Glacial Till: October 20, 2017
- Figure 6-1 The Three Components of the Piper Plot
- Figure 6-2 Interpretation of the Diamond Plot
- Figure 6-3A Plot of the Major Cations for the Various Hydrogeologic Zones Underlying the Niagara Sanitation Landfill
- Figure 6-38 Plot of the Major Anions for the Various Hydrogeologic Zones Underlying the Niagara Sanitation Landfill
- Figure 6-4 Piper Plot of Surface Water at the Niagara Sanitation Landfill
- Figure 6-5 Piper Plot of Fill Wells at the Niagara Sanitation Landfill
- Figure 6-6 Piper Plot of Upper Sand Deposit Wells at the Niagara Sanitation Landfill
- Figure 6-7 Piper Plot of the Upper Clay Aquitard Well at the Niagara Sanitation Landfill
- Figure 6-8 Piper Plot of Lower Sand Deposit Wells at the Niagara Sanitation Landfill
- Figure 6-9 Piper Plot of Glacial Till Deposit Wells at the Niagara Sanitation Landfill
- Figure 6-10 Piper Plot of Upper Camillus Shale Bedrock Wells in the Tonawanda Area
- Figure 6-11 Piper Plot of Lockport Dolostone Bedrock Wells in the Niagara Falls Area
- Figure 7-1 Hydrograph for Representative Wells from All Hydrogeologic Zones

## LIST OF TABLES (Following Text)

- Table 3-1Average Monthly Precipitation and Evapotranspiration Data
- Table 4-1Stratigraphic Sequence of Western New York
- Table 4-2Stratigraphic Summary of the Niagara Sanitation Landfill
- Table 4-3Summary of Grain Size Analyses
- Table 5-1Construction Summary of Existing Wells at the Niagara Sanitation Landfill
- Table 5-2Summary of Water Level Measurements

## LIST OF TABLES (continued)

Table 5-3Summary of Hydraulic Conductivity Testing Results

## LIST OF APPENDICES

- Appendix A Soil Boring Logs
- Appendix B Well Construction Diagrams
- Appendix C Well Development Logs
- Appendix D Groundwater Purge and Sample Logs
- Appendix E Select Hydrographs with Precipitation Data
- Appendix F Grain Size Analysis Test Data
- Appendix G Hydraulic Conductivity Test Data
- Appendix H Geochemical Data

## **1.0 INTRODUCTION**

The Niagara Sanitation Landfill is an inactive landfill located on Nash Road in the Town of Wheatfield, Niagara County, New York (Figure 1-1). During implementation of a State Superfund Remedial Investigation at the site in 2017, groundwater flow in the shallow fill/upper sand unit underlying the site was to the south toward Forbes Street. This flow pattern, however, was opposite to that identified in studies completed in 2013 & 2014. As a result, in 2022 the New York State Department of Environmental Conservation (NYSDEC) began a detailed evaluation of the geology, hydrogeology, and groundwater geochemistry of the Niagara Sanitation Landfill to evaluate groundwater in the various water-bearing zones underlying the site. A primary objective was to further evaluate groundwater flow patterns in the water-bearing zones underlying the site. A complete understanding of the groundwater flow patterns, especially in the fill/upper sand water-bearing zone, is critical for evaluating the potential for contaminants in groundwater to migrate from the site. The remaining sections of this report are organized as follows:

- Section 2.0, Site History and Background: This section describes the site and various site features, and discusses the history and previous investigations completed at the site;
- Section 3.0, Surface Water Hydrology: This section describes the surface water hydrology of the site, which includes precipitation, evapotranspiration, drainage, and infiltration characteristics.
- **Section 4.0, Geology:** This section describes regional and site geology. The characteristics and areal extent of the geologic strata are discussed;
- Section 5.0, Hydrogeology: This section describes regional and site hydrogeology. Groundwater flow patterns and the hydrogeologic properties of the various water-bearing zones are discussed;
- Section 6.0, Groundwater Geochemistry: This section describes the general geochemistry data from the various hydrogeologic zones underlying the site, and evaluates the results against a conceptual geochemical model for the Niagara Sanitation Landfill;
- Section 7.0, Summary: This section summarizes the findings of Sections 4.0 through 6.0;

and

• Section 8.0, References: This section contains a list of references utilized or cited in this report.

#### 2.1 Site Description

The Niagara Sanitation Company Site, also known as the Nash Road or Niagara Sanitation Landfill, is an inactive landfill located on Nash Road in the Town of Wheatfield, Niagara County, New York (Figure 1-1). The property is owned by the Town of Wheatfield and is adjacent to the municipal boundary that separates the Town of Wheatfield from the City of North Tonawanda (Figure 2-1). The landfill is located approximately 1,400 feet east of Nash Road (Figures 1-1 and 2-1). The majority of historic landfilling operations took place on the portion of the property that is rectangular in shape, which consists of approximately 18.7 acres of the 20.8-acre parcel (Figure 2-2). The property is zoned for Public Service use.

The site is bordered by the Society of Catholic Apostolate property to the north; a property that contains a former motel and livery service to the east; a utility right-of-way (both overhead electric and underground natural gas and brine lines) and residential properties to the south; and Nash Road and residential properties to the west (Figures 1-1 and 2-1).

#### 2.2 Site Features

The Niagara Sanitation property is vacant and overgrown with mature trees, dense brush, and marsh vegetation (e.g., phragmites). The site is poorly drained and contains delineated wetlands in the western, northern, and eastern portions of the property (Figure 2-2). These wetlands, however, are dry during the summer and early fall months. In December 2017, the Town of Wheatfield installed a 6-foot-tall perimeter fence with locking gates that encompasses most of the landfill. Prior to that time access to the site was not restricted.

Historic landfilling activities have resulted in an irregular ground surface topography at the site, with relief being less than 10 feet (Figure 2-3). Numerous soil/debris mounds predominate in the western two-thirds of the site but can be observed throughout the site, with general municipal (i.e., non-hazardous) waste protruding at most mounded locations. During a site reconnaissance completed for the 2013 NYSDEC Site Characterization Study and during the 2017 Remedial Investigation, evidence of residential/municipal waste, either partially buried or lying directly on the ground surface was observed in discrete areas across the site. Identifiable municipal wastes found

at the surface typically include used/discarded clothing, shoes, children's toys, sports equipment, household appliances, containers for residential cleaning supplies, food containers, dishes, glassware, silverware, tires, and battery casings along with generally unidentifiable metal, glass, rubber, plastic debris, and in a few locations, whole vehicles. There is also evidence of industrial wastes at the site (e.g., empty steel drums and 4-inch diameter carbon core samples) mixed within the predominately residential/municipal waste.

## 2.3 Site History

Available records indicate that the site was operated as a landfill by the Niagara Sanitation Company from approximately 1955 to 1968. The landfill accepted both municipal and industrial solid wastes, including caustic materials, plating tank sludge, fly ash, salt solids, graphite, carbon, scrap adhesives, and miscellaneous laboratory chemicals. Records from the NYSDEC indicate that Bell Aerospace, Carborundum, and Graphite Specialties disposed of waste at the site.

In June 1968, shortly before the site's formal disposal operations were discontinued, the New York State Department of Transportation (NYSDOT) discovered waste while constructing the LaSalle Expressway in Niagara Falls. This material was excavated from the area that later became known as Love Canal. Niagara Sanitation Landfill records indicate that approximately 1,600 cubic yards of excavated materials were placed into a 30-foot wide by 100-foot long by 27-foot-deep trench at the eastern end of the landfill. The waste was reportedly placed from the bottom of the trench to 15 feet below ground surface and covered with 12 feet of excavated native soil.

The NYSDEC completed a Phase I Investigation (historical records review and site walk over) of the site in 1983, a Phase II Investigation (on-site data collection) in 1985, and a Supplemental Phase II Investigation in 1989. In association with these investigations, the New York State Department of Health (NYSDOH) completed surface soil sampling in 1991 to evaluate potential exposure risks. At that time, it was determined that the site did not pose a significant threat to public health or the environment because the exposure was limited; the wastes were buried, contained, or sufficiently covered to avoid significant exposure. Groundwater as a potential exposure pathway was also limited because the area was served by public water and the closest private well was approximately one mile away. As a result, the site was designated as Class 3 (action can be deferred) in the NYSDEC Registry of Inactive Hazardous Waste Disposal Sites. These reports can be found online at <a href="https://www.dec.ny.gov/data/DecDocs/932054/">https://www.dec.ny.gov/data/DecDocs/932054/</a>.

NYSDEC continuously monitors and evaluates sites on the Registry of Inactive Hazardous Waste Disposal Sites. In 2013, as part of these efforts, the NYSDEC completed a Site Characterization Study to re-evaluate the Class 3 NYSDEC Registry designation for the site, to confirm the location of the wastes from the LaSalle Expressway project, and to re-evaluate the potential for direct contact exposures. The Site Characterization was heavily focused on the eastern portion of the site where the wastes associated with the construction of the LaSalle Expressway were placed (Figure 2-4). This report can be found online at <a href="https://www.dec.ny.gov/data/DecDocs/932054/">https://www.dec.ny.gov/data/DecDocs/932054/</a>.

Later in 2013, Glenn Spring Holdings, an affiliate of the Occidental Chemical Corporation, began an Interim Remedial Measure (IRM) to characterize and remove the LaSalle Expressway wastes. These wastes were excavated from the site during the Fall/Winter of 2014 and the Winter/Spring of 2015 and transported out of state for incineration. The IRM Closure Report can be found online at <a href="https://www.dec.ny.gov/data/DecDocs/932054/">https://www.dec.ny.gov/data/DecDocs/932054/</a>.

In 2014, the NYSDEC conducted a Supplemental Site Characterization Study to characterize the municipal and industrial waste in the remainder of the landfill. While most of the site contained contaminant concentrations typical of non-hazardous municipal/industrial waste, three locations were identified that contained hazardous concentrations of lead or PCBs. Several surface soil samples exceeded residential soil cleanup objectives (SCOs) for polycyclic aromatic hydrocarbons (PAHs) and metals. Groundwater within the footprint of the landfill contained elevated concentrations of volatile organic compounds, semi-volatile organic compounds, pesticides, and metals that exceeded the NYSDEC groundwater standards or guidance values. These results are described in more detail in the Supplemental Site Characterization Study Report (GES, 2014), which can be found online at <a href="https://www.dec.ny.gov/data/DecDocs/932054/">https://www.dec.ny.gov/data/DecDocs/932054/</a>.

Based upon the results of the Site Characterization and Supplemental Site Characterization Studies, the NYSDEC reclassified the site to Class 2 (represents a significant threat to public health and/or the environment) and completed a comprehensive, state funded Remedial Investigation of the site in 2017. A more detailed history of the Niagara Sanitation Landfill, along with the analytical results of the samples collected, are presented in the Remedial Investigation Report (LiRo, 2019). This report can be found online at https://www.dec.ny.gov/data/DecDocs/932054/.

Between October 22, 2019 and January 9, 2020, the NYSDEC completed additional groundwater and surface water sampling activities at the site to evaluate current groundwater and surface water conditions, and to supplement the results contained in the Remedial Investigation

Report (LiRo, 2019). The 2019/20 results are discussed in the Groundwater & Surface Water Monitoring Report (NYSDEC, 2022), which can be found online at <a href="https://www.dec.ny.gov/data/DecDocs/932054/">https://www.dec.ny.gov/data/DecDocs/932054/</a>.

In an ongoing effort by the NYSDEC to investigate the Niagara Sanitation Landfill, groundwater samples were collected from the site between October 29, 2021 and November 8, 2021. These sampling activities were completed to evaluate current groundwater conditions at the site, and to supplement the results contained in the Remedial Investigation Report (LiRo, 2019) and the 2019/20 Groundwater & Surface Water Monitoring Report (NYSDEC, 2022). The 2021 results are discussed in the 2021 Groundwater Monitoring Report (NYSDEC, 2023), which can be found online at <a href="https://www.dec.ny.gov/data/DecDocs/932054/">https://www.dec.ny.gov/data/DecDocs/932054/</a>.

In its continued effort to investigate the Niagara Sanitation Landfill, the NYSDEC completed additional groundwater and surface water sampling activities at the site between October 15 and 23, 2023. These sampling activities were completed to evaluate current groundwater and surface water conditions at the site, and to supplement the results contained in the Remedial Investigation Report (LiRo, 2019), the 2019/20 Groundwater & Surface Water Monitoring Report (NYSDEC, 2022), and the 2021 Groundwater Monitoring Report (NYSDEC, 2023). The report describing the 2023 sampling event is currently being drafted.

## 3.0 SURFACE WATER HYDROLOGY

Surface water runoff is a potential pathway for the migration of contaminants from the Niagara Sanitation Landfill. In addition, infiltration of surface water and precipitation recharges shallow groundwater, and in the process, can leach contaminants from the waste material through which it passes. Surface water hydrology, therefore, is an important aspect of this study. This section describes the surface water hydrology of the Niagara Sanitation Landfill, which includes precipitation, evapotranspiration, and site drainage characteristics.

## 3.1 Precipitation

Infiltration, and hence groundwater recharge, depends upon the amount of precipitation falling on an area and the amount of water lost through evapotranspiration (discussed below) and runoff. Precipitation data for the Niagara Sanitation Landfill is not available so the precipitation measured at the National Weather Service Station at the Buffalo Niagara International Airport are used as a proxy for on-site precipitation amounts. The National Weather Service Station is located approximately 11 miles southeast of the Niagara Sanitation Landfill in the Town of Cheektowaga, New York.

The average annual precipitation between 1985 and 2015 as measured at the National Weather Service Station at the Buffalo Niagara International Airport is 40.62 inches (Table 3-1), which equates to an average monthly precipitation of 3.39 inches. This precipitation is fairly evenly distributed throughout the year (Table 3-1; Figure 3-1), although slightly larger amounts fall in September and October, and slightly lower amounts fall in February and March. Severe droughts are rare, but periods of low precipitation and relatively high temperatures are common, sometimes causing at least temporary concern over declining water levels and moisture stress in crops and other vegetation. Precipitation generally falls as rain from April through November, and as snow from December through March. The mean annual snowfall between 1985 and 2015 as measured at the National Weather Service Station is 94.61 inches, with ¾ of this total falling between December and February. The snowpack generally reaches its maximum depth in February, and decreases in March and early April (Dethier, 1966). During this snowmelt period, there is a significant increase in both surface water runoff and groundwater recharge via infiltration.

The average annual precipitation at the National Weather Service Station between 2016 and

2022 was 41.81 inches (Table 3-1), which is slightly above the long-term annual average. In contrast to these totals, the annual precipitation for 2017 and 2019 was 48.48 inches and 47.82 inches, respectively (Table 3-1). This represents a 19.4% increase over the long-term average for 2017 and a 17.7% increase for 2019.

The largest increases in 2017 occurred during April and May, which exhibited increases in precipitation of 3.18 inches and 2.92 inches, respectively, over the long-term averages for those months. March, July, October, and November were also substantially wetter than normal (i.e., >1.0 inch above the long-term average for those months), while June was substantially drier (1.43 inches below the long-term average for that month). Graphs showing daily precipitation between August 2 and October 27, 2017 are presented in Appendix E.

In contrast, the largest increases in 2019 occurred during January and September, which exhibited increases in precipitation of 2.57 inches and 2.34 inches, respectively, over the long-term averages for those months. October and December were also substantially wetter than normal (i.e., >1.0 inch above the long-term average for those months), while July and November were substantially drier (1.39 inches and 1.73 inches, respectively, below the long-term average for those months).

The annual precipitation for 2020 (39.67 inches) and 2021 (40.33 inches) were close to the long-term annual average (Table 3-1).

## 3.2 Evapotranspiration

Evapotranspiration is defined as the sum of the water loss attributable to evaporation from soil and surface water bodies (e.g., lakes, rivers, wetlands) and to transpiration by plants (Staubitz and Miller, 1987). Since quantifying the contribution to water loss by each mechanism is generally not possible, potential evapotranspiration is generally used, which is defined as the maximum evapotranspiration that would occur if the quantity of water available in soil was unlimited (Freeze and Cherry, 1979). Under actual field conditions where soil moisture is limited, evapotranspiration will always be less than the potential evapotranspiration.

Specific estimates of potential evapotranspiration rates are generally not completed during environmental investigations. A literature search, however, found that annual evapotranspiration rates have been estimated for the Ashland 1 and 2 sites in nearby Tonawanda, New York. In addition,

Staubitz and Miller (1987) report monthly potential evapotranspiration rates for the Clarence-Newstead area of northeastern Erie County (Table 3-1). The annual evapotranspiration rates for the Ashland 1 and 2 sites were estimated at 29.4 inches, 28.2 inches and 29.2 inches for the years 1987, 1988 and 1989, respectively (Bechtel, 1993). These rates are slightly higher than the 25.74-inch annual estimate for the Clarence-Newstead area (Staubitz and Miller, 1987). In the current study, the monthly potential evapotranspiration rates reported by Staubitz and Miller (1987) are used as a proxy for on-site potential evapotranspiration rates at the Niagara Sanitation Landfill.

The data in Table 3-1 shows that the potential evapotranspiration rates for June, July, and August are higher than the long-term precipitation for those months. This suggests that shallow groundwater underlying the Niagara Sanitation Landfill would decrease during those months. This relationship is described in more detail in Section 5.0 of this report.

## 3.3 Site Drainage Characteristics

Before landfilling activities began, the property was believed to be a low-lying swampy area with natural on-site ponds. At the present time, most surface water bodies occur in small, enclosed depressions less than 3 feet deep. In contrast to the small ponds, a large, shallow pond is located at the northeast portion of the site (Figure 2-3). Most of these swampy areas and ponds contain marsh vegetation (e.g., phragmites).

The occurrence and location of surface water bodies on the Niagara Sanitation property is variable and seasonal. They are formed by either snow meltwater or rainfall, and generally disappear during the summer months due to lower amounts of precipitation and elevated rates of potential evapotranspiration. During 2021 and 2023, surface water bodies at the site were still dry in mid-October of those years. In the spring, however, approximately one-third of the site may be under water (Figure 2-2).

On-site overland flow in the eastern portion of the site is generally into the large, shallow pond at the northeast portion of the site (Figure 2-3). When surface water elevations in this pond are relatively high it will discharge to the north via a small swale into the Northern Boundary Ditch (Figure 2-3). At the northeast corner of the site, the Northern Boundary Ditch makes a "dogleg" turn and continues to the south (Figure 2-3). The Northern Boundary Ditch also extends to the west along the northern boundary of the site, shallows in the center of the site (the area where wetlands are not shown on Figure 2-3), then deepens slightly as it continues to the west.

During a significant rain event (i.e., >1.0 inches of precipitation within 24 hours) during the Remedial Investigation field activities, LiRo directly observed and recorded surface overland flow and channel flow in the eastern portion of the site, which terminated at the Northern Boundary Ditch (Figure 2-3). Surface water runoff from the neighboring property to the north was channeled southward into shallow drainage swales and small (i.e., <4") buried drain lines that discharged directly into the Northern Boundary Ditch. Flow from a pond on the neighboring property to the east (Figure 1-1) was carried by a buried 8-inch diameter pipe directly into the Northern Boundary Ditch (Figure 2-3). Surface water runoff from the south followed a shallow off-site ditch east of the site property boundary. This ditch initially flowed to the east and then north to feed directly into the Northern Boundary Ditch.

The 1989 Supplemental Phase II Investigation Report suggested that the Northern Boundary Ditch drained into Sawyer Creek, which is less than one-quarter mile northeast of the site along Niagara Falls Boulevard. During the GES and LiRo site visits, however, no surface water outlets were observed for the Northern Boundary Ditch, and it is believed that all impounded water is lost by a combination of evapotranspiration during the hot, drier months and infiltration into subsurface soils throughout the year.

## 4.0 GEOLOGY

One objective of this study was to establish the characteristics, areal extent and hydrogeologic properties of strata underlying the Niagara Sanitation Landfill. This is important as these attributes govern the occurrence and flow of groundwater at the site. These attributes also govern the potential for contaminant migration and determine the rate and extent of this migration. As a result, a detailed evaluation of the geology of the Niagara Sanitation Landfill is essential. Before completing such a detailed evaluation, however, it is important to first describe the regional geologic history of the western New York area as a general knowledge of this history is critical to a complete understanding of the complex interrelationships between the various geologic strata and their hydrogeologic properties. This section, therefore, describes regional and site geology, along with the characteristics and areal extent of the strata underlying the Niagara Sanitation Landfill.

## 4.1 Regional Geology

The Niagara Sanitation Landfill is located in the Erie-Ontario Lowland physiographic province of New York State, which can be characterized as the areas of low relief that border Lakes Erie and Ontario (Muller, 1965). The lowland region extends from the Onondaga escarpment located about eight miles south of the site to Lake Ontario.

#### 4.1.1 Overburden Geology

Geologic evidence suggests that at least four major glacial episodes covered parts of North America during the Pleistocene Epoch (Buehler and Tesmer, 1963). In western New York, however, there is evidence of only two such episodes. The last glacial event in the area, the Wisconsin, eroded and modified the earlier glacial deposits to such an extent that little evidence of their existence remains. These glacial events widened the preexisting valleys and basins and led to the development of the present-day drainage system in western New York (La Sala, 1968).

During the final retreat of the Wisconsin ice sheet from the region, meltwater formed a complex sequence of proglacial lakes in front of the ice margin. These lakes inundated an extensive area of western New York. This succession originated in the Erie-Huron Basin prior to 14,000 years ago as the ice sheet retreated from the basin and ended approximately 9,800 years ago with the formation of Lake Tonawanda (Calkins and Brett, 1978). This lake sequence was responsible for the deposition of the stratified lacustrine clays, silts, sands, and gravels that now cover much of western

New York.

Lake Tonawanda was one of the largest of these lakes. It was an elongated lake that occupied an east-west trending basin between the Onondaga and Niagara escarpments and drained to the north into Lake Iroquois. Sediments deposited in this lake consist of blanket sands and beach ridges that are occasionally interlayered with lacustrine silts and clays. Parts of this sequence are "…very regularly bedded with cyclic alternation of clay and silt laminae; moderately permeable along bedding surfaces…" (Muller, 1977). The Niagara Sanitation Landfill is located on property that was inundated by this lake.

The Pleistocene Epoch presented a variety of environments that resulted in the deposition of unconsolidated deposits. In southwestern Niagara County these deposits include the following (GTC, 1983; Engineering Science, 1989; URS, 1991; Ecology and Environment, 1992):

- Glacial till consisting of a non-sorted, non-stratified mixture of sand, silt, clay, gravel, and rock fragments deposited directly from glacial ice;
- Glaciolacustrine deposits consisting primarily of silt, sand and clay deposited in lakes that formed during melting and retreat of the ice sheets;
- Glaciofluvial deposits consisting of sand and gravel deposited either by glacial meltwater streams or by the reworking of till and other glacial deposits along the shore of former glacial lakes; and
- Alluvial deposits consisting of silt, sand and gravel deposited by streams during comparatively recent geologic time.

La Sala (1968) reports that glacial till is the most widespread deposit in the Erie-Niagara Basin, ranging in thickness from 2 to 200 feet. Glaciolacustrine clay is also widespread, reaching thicknesses of 300 feet in some valleys within the basin (La Sala, 1968).

#### 4.1.2 Bedrock Geology

The bedrock underlying western New York is characterized as a thick sequence of shales, sandstones, limestones and dolostones deposited in ancient seas during the Silurian and Devonian Periods (Buehler and Tesmer, 1963). This stratigraphic sequence is summarized in Table 4-1. Bedrock bedding generally strikes in an east-west direction, approximately paralleling the Niagara

and Onondaga escarpments, and dips to the south at approximately 30 to 40 feet per mile (Johnson, 1964; La Sala, 1968; Yager and Kappel, 1987). Erosion and weathering, however, have produced local differences in the bedrock surface configuration (Snyder Engineering, 1987).

The uppermost bedrock unit underlying the Niagara Sanitation Landfill is unknown. The 1985 Phase II investigation (Engineering Science, 1985) identified bedrock as "dolostone" of the Lockport Group. A published geologic map of the western New York area, however, suggests that bedrock beneath the site is the Salina Group (Rickard and Fisher, 1970). In addition, an EPA report (EPA, 1985) stated that bedrock at the site is the Camillus Shale, a member of the Salina Group. None of the borings completed at the Niagara Sanitation Landfill have cored into bedrock for positive identification. As a result, both the Camillus Shale and Lockport Group are briefly discussed below.

The Camillus Shale Formation of the Salina Group was deposited in a shallow sea environment during the Late Silurian Period (Rickard and Fisher, 1970). This formation extends across northern Erie County/southern Niagara County in an east-west trending belt approximately 6 to 8 miles wide (Conestoga-Rovers & Associates, 1998). Exposures of this formation are rare because of the low relief of the outcrop area and the mantle of glacial deposits. Buehler and Tesmer (1963, page 30) describe the Camillus Shale as a "thin bedded shale to massive mudstone. Color is gray or brownish gray with some beds showing a red or green tinge. Gypsum and anhydrite are present throughout the formation in Erie County," and occur in beds and lenses up to 5 feet thick (La Sala, 1968). Subsurface data indicate, however, that a considerable quantity of gray limestone and dolostone is interbedded within the shale (Stanley Consultants, 1981; GZA, 1983; URS, 1992; Woodward-Clyde, 1993; Parsons Engineering Science, 1995). The upper 10 to 25 feet of this formation can be heavily weathered and often contains abundant bedding planes and vertical fractures enlarged by dissolution and glacial scour (La Sala, 1968). Buehler and Tesmer (1963) report that the maximum thickness of the Camillus Shale is 400 feet. Within the Erie-Niagara Basin, however, the thickness of this formation ranges from approximately 80 to 100 feet (Rickard, 1966).

The Lockport Group varies in thickness from 20 to 175 feet (Johnson, 1964; Brett et al., 1995), and is described by Brett et al (1995, page 45) as a "massive- to medium-bedded, argillaceous dolomite with minor amounts of dolomite and shale." The uppermost bedrock formation of the Lockport Group is the Guelph Dolostone (Table 4-1), which was deposited in a shallow sea environment during the Middle Silurian Period (Brett et al., 1995). In Ontario, Canada the Guelph Dolostone is between 200 and 300 feet thick; however, only a thin wedge of the formation extends

into Niagara County where it is only 33 to 36 feet thick (Brett et al., 1995). Brett et al (1995, page 59) describe the Guelph Dolostone as a "medium-gray to dark-gray, light-gray to tan weathering, laminated, fine-grained, commonly oolitic dolomite." The upper 10 to 25 feet of the Lockport Group contains abundant bedding planes and vertical fractures enlarged by dissolution and glacial scour (Miller and Kappel, 1987).

## 4.2 Site Geology

The stratigraphy of the Niagara Sanitation Landfill has been evaluated by examining seventyseven (77) stratigraphic logs obtained from soil borings completed at the site. The locations of the soil borings evaluated during this study are shown on Figure 4-1. The stratigraphic logs for these soil borings are given in Appendix A, while a stratigraphic summary of these logs is provided as Table 4-2.

These stratigraphic logs indicate that most investigation activities have been confined to the fill material and the upper glaciolacustrine deposits underlying the site. Several borings, however, have completely penetrated the native deposits, with 5 borings having encountered the underlying bedrock (Table 4-2).

An evaluation of the stratigraphic logs compiled for this study (Table 4-2) reveals that there are eight (8) distinct stratigraphic units underlying the Niagara Sanitation Landfill, which are summarized as follows:

- Fill: General refuse (e.g., glass, plastic, cloth, etc.) mixed with native fine sand and clay that ranges in thickness from 0.5 to >12.0 feet;
- Silt and Clay: An upper brown silt & clay deposit that ranges in thickness from 0.5 to 4.0 feet;
- Upper Sand: An upper yellow-brown sand deposit that ranges in thickness from 0.4 to 11.0 feet;
- Silty Clay: A gray-brown lacustrine silty clay deposit that ranges in thickness from 2.0 to 8.0 feet;
- Layered Clay: A red-gray layered lacustrine clay deposit containing thin sand seams. This

deposit ranges in thickness from 18.5 to 33.0 feet;

- Lower Sand: A lower red-brown sand deposit that ranges in thickness from 0.2 to 5.0 feet;
- Glacial Till: A dense reddish brown to gray till that ranges in thickness from 22.0 to 42.2 feet; and
- Bedrock: Dolostone bedrock encountered at depths ranging from 66.0 to 70.3 feet below ground surface.

The gray-brown silty clay deposit and underlying red-gray layered clay act as a groundwater aquitard that prevents the downward migration of groundwater and contaminants from the upper sand and fill water bearing unit to the lower water-bearing zones.

The stratigraphic relationship between these units can be seen on the various cross-sections prepared from the stratigraphic logs (Figures 4-4 through 4-9). The cross-sections shown in Figures 4-4 and 4-5 are from the 1985 Phase II Report, while the cross-sections shown in Figures 4-6 through 4-9 are from the 2019 Remedial Investigation Report. The locations of the Phase II cross-sections are shown on Figure 4-2, while the locations of the RI cross-sections are shown on Figure 4-3. These cross-sections are referenced in the following discussion where appropriate.

## 4.2.1 Surface Soils

The following discussion regarding surface soils at the Niagara Sanitation Landfill was included in the 1989 Supplemental Phase II Report completed by Engineering-Science for the NYSDEC. This discussion is based on soil borings completed at the site and information from the Niagara County Soil Survey (USDA, 1972). The soils mapped for the site include the Raynham silt loam and the Canandaigua silt loam. The Raynham soils are somewhat poorly drained, medium textured silt loam occurring on slopes ranging from 0% to 6%. These soils formed from calcareous silty sediments deposited by glacial Lake Tonawanda. The permeability of the Raynham silt loam is estimated at  $1 \times 10^{-3}$  to  $4 \times 10^{-4}$  cm/sec (USDA, 1972).

The Canandaigua silt loam is a very poorly drained, medium to moderately fine textured soil. These soils are level or depressional and occupy areas where water remains ponded or runs off very slowly. These soils formed in lacustrine deposits of silt, very fine sand, and clay. The permeability of Canandaigua silt loam is estimated at  $4 \times 10^{-3}$  to  $4 \times 10^{-4}$  cm/sec (USDA, 1972).

#### 4.2.2 Fill Material

Fill material overlies the native deposits throughout most of the Niagara Sanitation Landfill but is discontinuous across the site (Table 4-2; Figures 4-4 through 4-9). Where fill material is absent, native deposits are generally encountered at ground surface (Table 4-2). The fill material encountered contains varying degrees of re-worked native soils (i.e., silt, clay, and sand) and municipal landfill waste, the latter consisting primarily of glass, plastic, wood, cloth/canvas, and metal. Rubber, ash, cinders, slag, tile, and bricks were also observed at some locations. Photos of typical fill material found at the site are provided in Appendix I. It is believed that these materials were typically disposed in natural low-lying areas or within shallow pits and trenches excavated into the native deposits for disposal purposes.

Grain size analyses were completed on 3 different types of reworked soil encountered at the site (Table 4-3). These soils are quite variable, ranging from 0.1% to 26.9% gravel, 20.8% to 66.9% sand, 25.3% to 66.8% silt, and 4.6% to 21.2% clay (Table 4-3).

Fill material was encountered in 44 borings completed at the site (Table 4-2). Where encountered, fill material was observed at the ground surface and extended to depths typically ranging from 2.0 to 6.0 feet below ground surface. Thicker fill (i.e., > 6.0 feet) was observed at borings completed in the disposal pit that was excavated for the Lasalle Expressway wastes (Table 4-2). Where completely penetrated, the thickness of the fill material ranges from 0.5 to 10.0 feet (Table 4-2). The average thickness of the fill material is 4.1 feet.

While shallow soil observed at boring SB-B was not initially classified as fill material by GES, based upon previous site investigations, observed solvent odors, the softness of the material relative to other shallow native silty clay, and a review of historical documents, the clay is believed to be reworked native soil that was used to backfill the LaSalle Expressway disposal pit. This material was also observed at boring SB-M. These reworked soils are included with the fill material in Table 4-2.

Boring SB-AA was advanced from the top of a prominent mound west of the landfill and traversed by the gravel access road. The mound was estimated to be 8 to 10 feet high relative to the surrounding land surface. The samples collected from this boring consisted entirely of clay with no fill material observed. It is likely that this mound is man-made and may have been part of the landfill operations in the 1960s.

#### 4.2.3 Glaciolacustrine Deposit

The native soils underlying the Niagara Sanitation Landfill include a glaciolacustrine deposit and glacial till. With increasing depth, the glaciolacustrine deposit consists of a brown silt and clay unit, an upper sand unit, a gray-brown silty clay unit, a red-gray layered clay unit, and a lower sand unit (Figures 4-4 through 4-9). These units were deposited in glacial lakes that covered the area during the Wisconsin Glacial Stage.

The full thickness of the glaciolacustrine deposit was only penetrated at 7 borings completed at the site (Table 4-2). The total thickness of this deposit was quite variable, ranging from 21.5 to 45.0 feet. It should be noted, however, that at 6 of the 7 locations the thickness of the glaciolacustrine deposit was 36.0 feet or greater.

#### 4.2.3.1 Brown Silt and Clay

The 1985 Phase II Report states that "in the eastern part of the site, the upper sand is overlain by a layered silt" (Engineering Science, 1985). This deposit was only encountered in one boring completed during the Supplemental Phase II Investigation (Table 4-2) so was not included in the stratigraphic column generated for the site nor discussed in the report (Engineering Science, 1989). This deposit was also encountered during the GES and LiRo investigations (Table 4-2) but again was not discussed in their respective reports (GES, 2013; GES, 2014, LiRo, 2019).

When adding this unit to the site's stratigraphic discussion, it was necessary to determine if this unit was a reworked soil related to landfilling operations or native soils of the glaciolacustrine deposit. An evaluation of Table 4-2 reveals that the brown silt and clay deposit either underlies the fill material or is encountered at the ground surface. In addition, this deposit directly overlies the upper sand deposit where the upper sand is present. This suggests that the brown silt and clay deposit is native, and it has been included with the glaciolacustrine deposit. The occurrence of this fine-grained deposit may suggest a deepening of glacial Lake Tonawanda.

The brown silt and clay deposit is described as a light brown silt and clay, a light brown stiff silt, or a gray silt and clay with a trace of fine sand (Engineering Science, 1985). Engineering Science (1989) describes this deposit as a brown clay with some silt. In contrast, LiRo (2019) describes this deposit as a dark brown silt and sand and include it with the fill/topsoil layer on their geologic cross-sections (Figures 4-4 through 4-9).

A grain size analysis of the brown silt and clay deposit shows that it contains 18% sand, 59%

silt and 23% clay (Table 4-3). During testing, a suspension of the silt was extremely frothy and had a soapy odor.

The brown silt and clay deposit was encountered in 30 borings completed at the site (Table 4-2). Depth to this deposit ranged from 0.0 to 4.0 feet below ground surface, with its thickness ranging from 0.5 to 4.0 feet (Table 4-2). The average thickness of brown silt and clay deposit is 2.0 feet.

#### 4.2.3.2 Upper Sand Deposit

The first encountered native deposit that is areally extensive across the Niagara Sanitation Landfill is the upper sand deposit (Figures 4-4 through 4-9). This deposit is described as a medium to coarse grained, well sorted, orange-brown sand (Engineering Science, 1989). GES (2013), however, described this sand as fine to coarse grained, gray to black in some borings, and tan to brown in others. LiRo (2019) described the sand as light brown-yellowish brown to light gray. This deposit likely originated as a late deposit of Lake Tonawanda. Photos of the upper sand deposit underlying the site are provided in Appendix I.

Grain size analyses of the upper sand deposit show that it contains 74.4% to 87.6% sand with the remaining percentage being silt and clay (Table 4-3).

The upper sand deposit was encountered in 61 borings completed at the site (Table 4-2). Depth to this deposit was quite variable, ranging from 0.0 to 10.0 feet below ground surface. Where completely penetrated, the thickness of the upper sand deposit was also quite variable, ranging from 0.4 to 11.0 feet (Table 4-2). The average thickness of this deposit is 4.4 feet.

The upper sand deposit is thickest in the southwest portion of the site and thins to the north and east (Figure 4-11). There also appears to be a thick "ridge" of sand that trends northwest-southeast in the northeastern portion of the site that is roughly centered on borings OW-14A, OW-14BR, and SB-J (Figure 4-11). A surface elevation contour map of the upper sand deposit (Figure 4-10) shows a series of ridges and circular to ovoid depressions. This topography may be related to the excavation of disposal pits and trenches during landfill operations.

## 4.2.3.3 Gray-Brown Silty Clay Deposit

Underlying the upper sand deposit is a stiff, gray-brown silty clay deposit (Figures 4-4 and 4-

**5**). Photos of this deposit underlying the site are provided in Appendix I. Very fine sand beds about one inch thick are present in this deposit. This silty clay deposit was often less saturated than the overlying upper sand deposit, suggesting that it is an aquitard as discussed in previous site investigations. This deposit may be the regularly bedded cyclic laminae of clay and silt described by Muller (1977) as being typical of the lacustrine sediments deposited in Lake Tonawanda. The lower portion of this lacustrine unit is slightly higher in clay content (86%), but in general, this deposit contains 93% to 100% silt and clay (Table 4-3).

The gray-brown silty clay deposit was encountered in 63 borings completed at the Niagara Sanitation Landfill (Table 4-2). Depth to this deposit was quite variable, ranging from 3.0 to 15.0 feet below ground surface. This deposit was only completely penetrated at 11 locations, with the thickness ranging from 2.0 to 8.0 feet (Table 4-2). The average thickness of the gray-brown silty clay deposit is 4.8 feet.

Figure 4-12 is a contour map showing the depth to the gray-brown silty clay deposit. This contour shows a deep ( $\approx$ 6 feet) north-south trending trough in the southwestern portion of the site that shallows to the west, north and east. A heart-shaped depression is located in the west-central portion of the site and is defined by borings OW-32, OW-33, SB-U, SB-V, SB-X, and SB-JJ. A circular depression centered roughly on the disposal pit is located in the eastern portion of the site, with depths becoming shallower to the north, south, and west.

#### 4.2.3.4 Red-Gray Layered Clay Deposit

Underlying the gray-brown silty clay deposit and blanketing the site is a layered "fat" clay deposit (Figures 4-4 and 4-5). This deposit is described as a red-gray layered clay containing thin sand seams that is moist and highly plastic.

Grain size analyses of the red-gray layered clay deposit show that it contains 13.7% to 24.0% silt and 76.0% to 86.0% clay (Table 4-3). This deposit is a classic example of the Lake Tonawanda deposits as mapped by Muller (1977).

The red-gray layered clay deposit was encountered in 11 borings completed at the site (Table 4-2). Depth to this deposit was quite variable, ranging from 8.0 to 16.0 feet below ground surface. Where completely penetrated (8 borings), the thickness of the red-gray layered clay deposit was extremely variable, ranging from 18.5 to 33.0 feet (Table 4-2). The average thickness of this deposit is 25.6 feet. Neither the depth to this deposit, nor its thickness, have been contoured.

#### 4.2.3.5 Lower Sand Deposit

A relatively thin, red-brown sand deposit underlies the red-gray layered clay deposit and mantles the glacial till (Figures 4-4 through 4-9). Grain size analyses of this deposit show that it is predominantly a sand (30.4% to 65.0%) that also contains 0.0% to 18.3% gravel and 35.0% to 57.3% silt and clay (Table 4-3). Based on its lithology and stratigraphic position, this sand deposit is interpreted to be an early deposit of Lake Tonawanda.

The lower sand deposit was only encountered in 6 borings completed at the site (Table 4-2). Depth to this deposit was quite variable, ranging from 26.3 to 42.0 feet below ground surface. Where completely penetrated (5 borings), the thickness of this deposit was somewhat variable, ranging from 0.2 to 5.0 feet (Table 4-2). In 4 of these borings, however, the thickness of this deposit ranged from 3.0 to 5.0 feet (Table 4-2).

Figure 4-13 is a contour map showing the thickness of the lower sand deposit. This contour shows that this deposit is thickest in the north-central portion of the site and thins to the south and east. The lower sand deposit was absent in the easternmost (OW-1B) and westernmost (OW-6) borings that encountered the underlying glacial till deposit. These borings are shown on Figure 4-1. It should be noted, however, that it is possible that this deposit was missed due to the large sampling interval (i.e., 5 feet) utilized at depths greater than 20 feet below ground surface during the 1985 Phase II Investigation.

#### 4.2.4 Glacial Till Deposit

A relatively thick, continuous layer of glacial till underlies the lower sand deposit and mantles the underlying bedrock (Figures 4-4 through 4-9). The term "till" is used for a variety of non-sorted, non-stratified glacial deposits; however, because a till is so variable, caution must be exercised when describing its character and hydrogeologic properties. The till underlying the Niagara Sanitation Landfill consists predominantly of a dense, brown silt with fine to coarse sand and fine gravel.

Grain size analyses of the glacial till deposit show that it contains 50.5% to 66.0% silt and clay, 10.0% to 15.3% gravel, and 19.0% to 34.7% sand (Table 4-3).

The glacial till deposit was only encountered in 7 borings completed at the site. Depth to till was quite variable, ranging from 26.5 to 45.0 feet below ground surface. Where completely penetrated (5 borings), the thickness of this deposit ranged from 22.0 to 42.2 feet (Table 4-2). The average thickness of the glacial till deposit is 29.0 feet.

Figure 4-14 is a contour map showing the depth to the glacial till deposit. This contour shows that the glacial till is shallowest in the southeast portion of the landfill and gradually deepens to the northwest to form a trough under the western portion of the landfill. The maximum relief of the till surface across the Niagara Sanitation Landfill is 18.5 feet (Figure 4-14).

#### 4.2.5 Bedrock

As stated in Section 4.1.2, the uppermost bedrock unit underlying the Niagara Sanitation Landfill is unknown. Available information suggests that it could be dolostone of the Lockport Group or the Camillus Shale of the Salina Group. None of the borings completed at the Niagara Sanitation Landfill cored into bedrock for positive identification.

Bedrock was only encountered in 5 borings completed at the site (Table 4-2). The boring logs, however, do not describe this bedrock, only stating that it is dolostone (see boring logs in Appendix A). Depth to bedrock beneath the Niagara Sanitation Landfill was relatively consistent, ranging from 66.0 to 70.3 feet below ground surface (Table 4-2).

Figure 4-15 is a contour map showing the depth to bedrock. This contour shows that bedrock is deepest in the central portion of the landfill and shallows to the east and west. The maximum relief of the bedrock surface across the Niagara Sanitation Landfill is 4.3 feet (Figure 4-15).

Figure 4-16 is a contour map showing the surface elevation of the bedrock underlying the site. This contour shows a bedrock trough in the central portion of the site that shallows slightly to the east and more substantially to the west.

## 5.0 HYDROGEOLOGY

In Section 4.0 the geology of the Niagara Sanitation Landfill was described in detail. In this section the hydrogeologic properties of these strata are evaluated. As part of this evaluation, a series of hydrographs and groundwater contour maps were produced and are examined. Before completing such a detailed evaluation, however, it is important to first describe the regional hydrogeologic setting of southwestern Niagara County.

## 5.1 Regional Hydrogeology

Many site investigations and hydrogeologic studies have been completed in southwestern Niagara County. These studies indicate that there are four principal hydrogeologic zones in the area described as follows:

- Shallow alluvium, glaciofluvial, and glaciolacustrine sand deposits, which can be characterized as either unconfined (water table) or perched aquifers;
- The glaciolacustrine silty clay deposit, which can be characterized as an aquitard, confining groundwater from the underlying Lockport Dolostone or Camillus Shale;
- The glacial till deposit, which can also be characterized as an aquitard; and
- The Lockport Dolostone or Camillus Shale bedrock, which can be characterized as confined aquifers.

Of these zones, the principal aquifers include the sands of the recent alluvium, glaciofluvial, and glaciolacustrine deposits, and the upper bedrock of the Lockport Dolostone or Camillus Shale. In southwestern Niagara County, unconfined groundwater is encountered largely within the alluvium, glaciofluvial, and glaciolacustrine sand deposits. Where these deposits overlie glaciolacustrine silty clay, perched groundwater conditions occur. Well yields from these deposits in southwestern Niagara County are generally unknown, although wells installed in highly permeable outwash deposits in the Tonawanda Creek valley have yields ranging from 1,000 to 1,400 gallons per minute (gpm) (La Sala, 1968).

The glaciolacustrine silty clay and glacial till deposits separate the unconfined and/or perched aquifers from the confined upper bedrock aquifer. The hydraulic conductivities of these

deposits are generally low, typically ranging from 10<sup>-6</sup> to 10<sup>-8</sup> cm/sec. The glaciolacustrine silty clay and glacial till deposits, therefore, can be considered aquitards, preventing the vertical movement of shallow groundwater to the underlying Lockport Dolostone or Camillus Shale. Some vertical movement, however, can occur through desiccation cracks in the upper glaciolacustrine silty clay, although such cracks have not been documented at the Niagara Sanitation Landfill. Horizontal groundwater flow within this deposit is severely limited. In fact, the glaciolacustrine deposit is generally not water bearing, yielding only small quantities of water, which is primarily interstitial pore water that is tightly bound to the soil particles. This deposit, however, frequently contains horizontal laminations and sand seams. These internal features facilitate localized horizontal groundwater flow through otherwise low permeability materials.

La Sala (1968) reports that the Camillus Shale is "by far the most productive bedrock aquifer" in the Erie-Niagara Basin, with individual well yields ranging from 300 to 1,200 gpm. The production well at the Dunlop Tire Corporation in the Town of Tonawanda yields 600 to 900 gpm (Pyanowski, 1990), although yields of 1,800 gpm were observed during a 1995 Hydrogeologic Evaluation Study (May, 2007).

Groundwater within the Camillus Shale occurs primarily in the following types of openings: (1) weathered surface fractures, (2) horizontal beds widened by dissolution, (3) vertical joints, and (4) small cavities and vugs. The availability of groundwater within the Camillus Shale results largely from the dissolution of thin (up to 5 feet in thickness; La Sala, 1968) gypsum seams and layers interbedded throughout the formation. Since the solubility of gypsum is high compared to the shales, limestones and dolostones that constitute the Camillus Shale, circulating groundwater will more readily dissolve the gypsum, producing migration pathways that can transmit large quantities of groundwater. The most prolific water-bearing zones, therefore, are generally horizontal because gypsum typically occurs in horizontal beds and thin zones of gypsiferous shale and dolostone (La Sala, 1968). These water bearing zones have been encountered at varying depths and stratigraphic horizons within the Camillus Shale, with individual dissolution zones ranging up to several miles in lateral extent (La Sala, 1968). The larger solution openings most likely occur in discharge areas near Tonawanda Creek and the Niagara River, where groundwater flow is greatest. Some horizontal groundwater flow, however, may also occur through small cavities and vugs.

Vertical movement of groundwater also occurs within the Camillus Shale, especially in the upper several feet of bedrock where vertical fractures, created by stress relief from tectonic events

and glacial rebound (Gross and Engelder, 1991), have been enlarged by glacial scour, dissolution, and other weathering processes. In general, however, vertical movement of groundwater within the Camillus Shale is limited. La Sala (1968) reports that this weathered and fractured zone is in hydraulic communication with the overlying glacial till throughout the area. Collectively, these zones can yield small quantities of water to wells but are generally not used for domestic or industrial purposes.

Although the hydraulic conductivity of the Camillus Shale is typically very low, the dissolution of gypsum produces zones of high transmissivity within the formation. Reported transmissivity values for the Camillus Shale based upon specific-capacity tests range from 7,000 to 70,000 gallons per day per feet (gpd/ft) (La Sala, 1968). Because of these yields, groundwater from the Camillus Shale is commonly utilized for industrial purposes (i.e., non-contact cooling). This water, however, is not utilized as a source of drinking water because of naturally occurring high mineral content and the close proximity of the Niagara River, an important and easily accessed source of municipal drinking water throughout the Western New York area.

Groundwater within the Lockport Dolostone occurs primarily in the following types of openings: (1) weathered surface fractures, (2) bedding joints, (3) vertical joints, and (4) small cavities and vugs. Although the Lockport Dolostone consists predominantly of dolostone, thin beds of limestone and shaly dolostone, and small irregularly shaped masses of gypsum are common. These thin beds and masses are subject to dissolution by groundwater, resulting in the enlargement of fractures and the formation of migration pathways that transmit large quantities of groundwater. The principal control on groundwater flow, however, is the vertical and horizontal bedding plane fractures. The latter are the primary groundwater flow pathways in the Lockport Dolostone and are areally extensive over several miles (Johnson, 1964; Yager and Kappel, 1987). Johnson (1964) identified seven such zones in the Niagara Falls area. Some horizontal groundwater flow, however, also occurs through small cavities and vugs (Woodward-Clyde and Conestoga-Rovers & Associates, 1992).

Vertical movement of groundwater also occurs, especially in the upper 10 to 25 feet of rock where vertical fractures, created by stress relief from tectonic events and glacial rebound (Gross and Engelder, 1991) have been enlarged by dissolution and/or glacial scour. Vertical movement of groundwater within the Lockport Group is quite prevalent, with both upward and downward gradients observed (Woodward-Clyde and Conestoga-Rovers & Associates, 1992). Where horizontal

and vertical fractures intersect, the water bearing capacity of the bedrock is substantially increased. Such areas have been identified in the Niagara Falls area.

Groundwater wells completed in the Lockport Group have yields commonly ranging from 10 to 100 gpm (Miller and Kappel, 1987), with yields up to 950 gpm reported (Yager and Kappel, 1987). Reported transmissivity values range from 330 to 68,000 gpd/ft (Johnson, 1964). Groundwater in the Lockport Group is very hard and highly mineralized (Johnson, 1964; La Sala, 1968; NYSDEC, 1997). As a result, this groundwater is not extensively utilized as a source of drinking water. Because of significant well yields, however, Lockport Dolostone groundwater is commonly utilized for industrial purposes (i.e., non-contact cooling; quarry washing operations).

Most recharge to the Lockport Dolostone and Camillus Shale results from infiltration of rainfall, snowmelt, and surface water through the overburden deposits (Johnson, 1964; La Sala, 1968). The low permeability of the glacial deposits within southwestern Niagara County, however, only permit limited recharge to the upper bedrock aquifer. Subsurface flow of groundwater from areas of higher elevation (e.g., the Niagara Escarpment) also recharges the upper bedrock aquifer (Johnson, 1964; La Sala, 1968). Recharge of deeper unconsolidated deposits and the upper bedrock aquifer may also result from infiltration of Niagara River and Tonawanda Creek water through the recent alluvium and glaciofluvial deposits. In general, however, these water bodies are typically discharge zones, so recharge in these areas would be restricted to the small stagnant zone underlying these water bodies.

#### 5.1.1 Regional Groundwater Flow

Information regarding regional groundwater flow in the upper bedrock near the Niagara Sanitation Landfill is not available. Investigations completed at sites west of the landfill, however, indicate that upper bedrock groundwater flow is toward the Niagara River, the principal discharge zone in southwestern Niagara County (GTC, 1983; Golder Associates, 1991).

## 5.2 Site Hydrogeology

As discussed in Section 4.2, eight distinct stratigraphic units underlie the Niagara Sanitation Landfill. The hydrogeologic data compiled and generated during this study, however, indicate that five hydrogeologic zones underlie the site. These hydrogeologic zones are summarized as follows:

• Fill/Upper Sand Water-Bearing Zone: The fill/upper sand water-bearing zone includes

the following stratigraphic units, which act as a single water-bearing unit across the site:

- Fill: General refuse (glass, plastic, cloth, etc.) mixed with native fine sand and clay that ranges in thickness from 0.5 to >12 feet;
- Upper Sand: The upper yellow-brown sand deposit that ranges in thickness from 0.4 to 11.0 feet;
- Upper Clay Aquitard: The upper clay aquitard includes the following stratigraphic units:
  - Silty Clay: The gray-brown lacustrine silty clay that ranges in thickness from 2.0 to 8.0 feet;
  - Layered Clay: The red-gray layered lacustrine clay that ranges in thickness from 18.5 to 33.0 feet;
- Lower Sand Water-Bearing Zone: The lower red-brown sand deposit that ranges in thickness from 0.2 to 5.0 feet;
- Glacial Till Aquitard: The dense reddish brown to gray till that ranges in thickness from 22.0 to 42.2 feet; and
- Upper Bedrock Water-Bearing Zone: Dolostone bedrock encountered at depths ranging from 66.0 to 70.3 feet below ground surface.

The gray-brown silty clay and underlying red-gray layered clay units of the glaciolacustrine deposit are characterized as an aquitard, restricting the downward movement of groundwater from the shallow to the deeper hydrogeologic zones. In addition, the designation of the glacial till aquitard as a separate hydrogeologic unit is highly generalized as the lower portion of this deposit is hydraulically connected to the upper bedrock hydrogeologic zone (La Sala, 1968).

There are forty (40) existing monitoring wells and two (2) staff gauges installed at the Niagara Sanitation Landfill that have been utilized to monitor groundwater and surface water elevations (Figure 5-1). The surface completions and well casings at two historic monitoring wells (OW-13 and OW-14B) were found to be heaved/damaged due to frost action and were no longer considered accurate for groundwater and hydrogeologic data collection. During the 2017 Remedial Investigation field activities, monitoring well OW-13 was replaced by well LPZ-08S and monitoring

well OW-14B was replaced by well OW- 14BR.

A monitoring well construction summary table for the existing wells at the Niagara Sanitation Landfill is given in Table 5-1, while the well construction diagrams are given in Appendix B. Historic and recent groundwater and surface water elevation data are summarized in Table 5-2.

## 5.2.1 Fill/Upper Sand Water-Bearing Zone

Thirty-two (32) monitoring wells installed at the Niagara Sanitation Landfill screen either fill material or the upper sand deposit underlying the site (Figure 5-1; Table 5-1). These wells include 14 previously installed wells (OW-01, OW-13, OW-14B, OW-16, OW-21, OW-22, OW-23, and OW-31 through OW-37), 14 wells installed during the 2017 Remedial Investigation (LPZ-01S through LPZ-13S and OW-14BR), and 4 hand-drilled wells installed during the 2017 Remedial Investigation (LDP-01 through LDP-04). Hand-drilled wells LDP-01 through LDP-03 are located within the south gasline and brine-line right-of-way, while LDP-04 is located at the northwest corner of the landfill (Figure 5-1). Well LDP-02 was subsequently destroyed and not replaced.

Water level measurements in pre-RI wells have been collected on numerous occasions: four times during the Supplemental Phase II Investigation, once during the Site Characterization Study, and once during the Supplemental Site Characterization Study (Table 5-2A). During the Remedial Investigation, water levels in the fill/upper sand wells were measured on thirteen occasions (Tables 5-2B through 5-2]). Water level measurements were also completed in 2019 (Table 5-2K), 2020 (Table 5-2L), and 2021 (Table 5-2M). The water level measurements taken during the Supplemental Phase II Investigation suggested that water levels in the upper sand deposit were highest in the vicinity of the ponds over the reported disposal pit in the northeastern portion of the site. There was insufficient data, however, to construct a groundwater contour map or to determine the relationship between shallow groundwater and the ponds.

The water level data compiled during this study were utilized to construct hydrographs for the fill/upper sand wells (Figures 5-2 through 5-4). These hydrographs reveal that water levels fluctuated between August and November 2017, the period in which the water level measurements were taken. Water levels steadily decreased between August 22<sup>nd</sup> and September 25<sup>th</sup>, a period that was characterized by lower-than-normal rainfall (Figure 3-1; Table 3-1). In contrast, October and November 2017 were characterized by higher-than-normal rainfall (Figure 3-1; Table 3-1), and as a result, water levels increased substantially in all fill/upper sand wells (Figures 5-2 through 5-4) at

the Niagara Sanitation Landfill. The response in all fill/upper sand wells was similar, the difference being that water levels in some wells decreased more than in others, with these same wells generally showing a greater increase in water levels during October and November 2017 (Figures 5-2 through 5-4).

To further evaluate the relationship between the fill/upper sand wells and precipitation, Figure 5-5 is a hydrograph of the two staff gauges installed at the site along with the upper sand wells closest to those gauges. This hydrograph shows a strong correlation between surface water elevations at the Niagara Sanitation Landfill with those in the upper sand deposit.

The water level data compiled during this study were also utilized to construct a series of groundwater contour maps for the fill/upper sand wells (Figures 5-6 through 5-22). At the time of the 2013 GES Site Characterization Study, groundwater flow in the fill/upper sand water-bearing zone (hereinafter called the shallow zone) was to the north and northwest (Figure 5-6). It was suspected that groundwater flow was influenced by surface water hydrology, including the large pond in the northeastern portion of the site, as groundwater flow mimicked the surface drainage pattern. During the Remedial Investigation, these wells were resurveyed. The groundwater contour map generated from the recalculated water level elevations of 2013 is illustrated in Figure 5-7. This figure indicates that groundwater is mounded at well OW-13 and flows from this mound to the northeast, north, and northwest. This example shows that at sites with very shallow gradients (note that the contour interval is 0.10 feet for Figure 5-6 and 0.20 feet for Figure 5-7), survey and water level measurement errors can drastically impact groundwater flow patterns.

It was stated in the Supplemental Site Characterization Study (GES, 2014) that groundwater flow in the shallow zone was generally to the north. It is important to note, however, that due to seasonal overgrowth the top of riser (TOR) elevations could not be surveyed at wells OW-33 through OW-36. As a result, LiRo generated a groundwater contour map using the 2014 water level measurements and the 2017 survey elevations. This contour is provided as Figure 5-8 and shows that groundwater flows radially at a very shallow gradient into a depression centered on well OW-33.

Four groundwater contour maps were generated using water level data from August 2017. The RI wells were being installed during this time, so these contours use between 8 and 25 water level measurements each. Groundwater contour maps generated from these water level data are provided as Figures 5-9 through 5-12. These figures show that groundwater in the fill/upper sand

water-bearing zone generally flows to the south at gradients ranging from 0.003 to 0.005 foot per foot (ft/ft). Note that the contour interval for these figures is only 0.25 feet.

Figure 5-13 is a groundwater contour map generated from the water level data collected on September 12, 2017. This contour shows that groundwater is mounded in the north-east portion of the landfill and flows outward from this mound toward the south and east. By September 25, 2017, the groundwater mound was more defined with a smaller mound now present at the northwest corner of the landfill (Figure 5-14).

During the Remedial Investigation, groundwater elevations in the shallow zone were observed to fluctuate in direct response to significant (i.e., >1.0-inch within 24-hours) precipitation events. The September 25, 2017 elevation measurements were recorded at the end of an approximate 2-week long dry period with little to no precipitation (see charts in Appendix E). In fact, the hydrographs of Figures 5-2 through 5-4 show that the lowest groundwater elevations documented for 2017 were recorded on that date.

Subsequent water level measurements were collected on October 17, 2017 following a significant precipitation event (see charts in Appendix E). Figure 5-15 is a groundwater contour map generated from that data, which shows that the groundwater flow direction was generally inward toward the central portion of the landfill. As a result, groundwater flow in the southern portion of the landfill reversed and was now to the north. Groundwater flow to the east, however, was still observed at the eastern portion of the site.

Figure 5-16 is a map showing the difference in elevation between September 25, 2017, and October 17, 2017. The greatest elevation changes were generally observed along the southern and northern boundaries of the site. All fill/upper sand monitoring wells reported a positive net change in groundwater elevation (Figures 5-2 through 5-4), which ranged between 0.24 feet (LPZ-09S) and 3.05 feet (LDP-02). The duration of this inward flow condition is unknown but can still be observed in the west half of the landfill on the October 20, 2017 (Figure 5-17) and October 27, 2017 (Figure 5-18) contours. In the eastern portion of the landfill groundwater flow was generally to the east on October 20, 2017 (Figure 5-17) and October 27, 2017 (Figure 5-18) with a northeast flow component observed on October 20, 2017 (Figure 5-17). A small groundwater depression is observed around well LPZ-07S for both dates (Figures 5-17 and 5-18).

Figure 5-19 is a groundwater contour map generated from the water level data collected on

November 7, 2017 when groundwater elevations were high (compare to Figures 5-2 through 5-4). This contour shows that groundwater from the southern portion of the landfill was flowing to the north toward two groundwater sinks. The largest sink, located in the western portion of the landfill, is centered on wells OW-16, OW-32, OW-35, OW-37, LPZ-04S, and LPZ-09S. The smaller sink is located in the eastern portion of the landfill.

Water levels measurements were also collected on November 21, 2019, April 3, 2020, and November 23, 2021. Groundwater contour maps generated from these data are provided as Figures 5-20 through 5-22, respectively. Figure 5-20 is very similar to Figure 5-15 and shows that groundwater flow was inward toward a well-defined groundwater sink in the central portion of the landfill and centered on wells OW-32, OW-33, LPZ-09S, and LPZ-13S. Smaller sinks were observed in the western (e.g., well OW-16) and eastern (e.g., wells OW-21 and OW-22) portions of the landfill. As a result, groundwater flow in the southern portion of the landfill was to the north toward these sinks.

Figure 5-21 is a groundwater contour map generated from the water level data collected on April 3, 2020. This contour shows that groundwater flow was to the north with a northwest flow component at the eastern portion of the landfill.

Figure 5-22 is a groundwater contour map generated from the water level data collected on November 23, 2021. This contour is similar to Figure 5-21 and shows that groundwater flow was to the north with a northwest flow component at the eastern portion of the landfill.

An in-situ permeability test (slug test) was conducted on well OW-1 during the Phase II Investigation (Engineering Science, 1985). The hydraulic conductivity of this well was determined to be  $4.37 \times 10^{-4}$  cm/sec (Table 5-3), which is consistent with the rapid water level fluctuations observed in this well (Figure 5-2). Hydraulic conductivity tests have not been conducted on any other well that screens the fill/upper sand water-bearing zone.

## 5.2.2 Upper Clay Aquitard

Only one (1) monitoring well (OW-2) installed at the Niagara Sanitation Landfill screens the upper clay aquitard underlying the site (Figure 5-1; Table 5-1). This well is shallow and screens the gray-brown silty clay deposit and upper 2 feet of the underlying red-gray layered clay (Figure 4-4). Historically, water level measurements from this well have been collected on numerous occasions: once during the Supplemental Phase II Investigation, once during the Site Characterization Study,
and eleven times during the Remedial Investigation (Tables 5-2A through 5-2J).

The water level data compiled for this well were utilized to construct a hydrograph for the upper clay aquitard (Figure 5-23). This hydrograph reveals that water levels fluctuated between August and November 2017 in a pattern similar to that documented for the fill/upper sand wells (compare with Figures 5-2 through 5-4), with water levels ranging from 573.74 to 575.44 feet above mean sea level (Figure 5-22; Tables 5-2B through 5-2]).

To further evaluate the relationship between the upper clay aquitard well and the fill/upper sand wells, Figure 5-24 is the same hydrograph as Figure 5-5 (see Section 5.2.1 for details) with the hydrograph for well OW-2 added to it. This hydrograph shows that the response of well OW-2 is nearly identical to the response in the two upper sand wells and the staff gauges, indicating that well OW-2 is hydraulically connected to the upper sand deposit. It is important to note that the top of the filter pack for this well was at the upper sand/gray-brown silty clay interface, which supports the idea of a hydraulic connection.

Due to the presence of only one well in the upper clay aquitard, a groundwater contour map could not be generated.

An in-situ permeability test (slug test) was conducted on well OW-2 during the Phase II Investigation (Engineering Science, 1985). The hydraulic conductivity of this well was determined to be  $6.75 \times 10^{-4}$  cm/sec (Table 5-3). This value, however, is two to four orders of magnitude higher than typical hydraulic conductivities of the glaciolacustrine deposit, which usually range from  $10^{-6}$  to  $10^{-8}$  cm/sec (see Section 5-1). It is likely that the slug test was influenced by groundwater inflow from the upper sand deposit, so this hydraulic conductivity would not be representative of the upper clay aquitard underlying the Niagara Sanitation Landfill.

#### 5.2.3 Lower Sand Water-Bearing Zone

Only two (2) monitoring wells (OW-14A and OW-15) installed at the Niagara Sanitation Landfill screen the lower sand deposit underlying the site (Figure 5-1; Table 5-1). Historically, water level measurements from these wells have been collected on numerous occasions: four times during the Supplemental Phase II Investigation and ten times during the Remedial Investigation (Table 5-2).

The water level data compiled during this study were utilized to construct hydrographs for the lower sand wells (Figure 5-25). The hydrograph for well OW-15 reveals that there was very little

seasonal fluctuation in this well, with water levels ranging from 567.58 to 568.11 feet above mean sea level (Figure 5-25; Table 5-2). The hydrograph for well OW-14A, however, is completely different, having lower water levels and greater fluctuations prior to October 17, 2017. The lower groundwater elevations in early August 2017 (August 2<sup>nd</sup> and 8<sup>th</sup>) likely result from the screened interval (3 feet) having completely silted up since this well was last sampled in 1988. Redevelopment, which took place on 6 separate days between August 16 and September 12, 2017, likely accounts for the lower groundwater elevations between August 22 and September 25, 2017, the day the well was sampled (i.e., water levels in the well didn't fully recover between re-development events). Following well re-development, the response in well OW-14A mirrors that of well OW-15 (Figure 5-25).

Due to the presence of only two wells in the lower sand deposit, a groundwater contour map could not be generated, and the direction of groundwater flow through this deposit is unknown.

In-situ permeability tests (slug tests) have not been conducted on either well that screens the lower sand deposit.

#### 5.2.4 Glacial Till Aquitard

Five (5) monitoring wells installed at the Niagara Sanitation Landfill screen the glacial till deposit underlying the site (Figure 5-1; Table 5-1). Four of these wells screen the bottom of the glacial till deposit, while the remaining well screens the approximate midpoint of this deposit (Figures 4-4 and 4-5). Historically, water level measurements from these wells have been collected on numerous occasions: twice during the Supplemental Phase II Investigation and thirteen times during the Remedial Investigation (Table 5-2).

The water level data compiled during this study were utilized to construct hydrographs for the glacial till wells (Figure 5-26). These hydrographs reveal that there was very little seasonal fluctuation in the wells, with water levels ranging from 564.95 to 565.75 feet above mean sea level (Figure 5-26; Table 5-2). The lower groundwater elevations observed for well OW-1B in August 2017 are likely related to well re-development.

Figure 5-27 is a groundwater contour map for the glacial till deposit generated from the water level data collected during the Phase II Investigation (date not specified in the report). This contour shows that groundwater is mounded in the north-central portion of the landfill and flows outward from this mound toward the east, south, and west. This mound may be attributable to the overlying lower sand deposit that acts as a source of recharge to the glacial till deposit.

**Figure 5-28** is a groundwater contour map for the glacial till deposit generated from the water level data collected on October 20, 2017. This contour shows that groundwater in the glacial till flows across the site from east to west at a very shallow gradient. Note that the contour interval is only 0.05 feet.

In-situ permeability tests (slug tests) were conducted on all five glacial till wells during the Phase II Investigation (Engineering Science, 1985). The results of these tests are summarized in Table 5-3, and indicate that the hydraulic conductivity of the glacial till deposit is extremely variable, ranging from 7.50 x  $10^{-4}$  to 7.88 x  $10^{-7}$  cm/sec. Because of this extreme variability, the hydraulic conductivities for the glacial till deposit were separated into two groups (e.g., wells OW-1B, OW-03, and OW-04, and wells OW-05 and OW-06) based upon similar conductivities (Table 5-3). The arithmetic and geometric means for these groups are  $1.02 \times 10^{-6}$  and  $9.83 \times 10^{-7}$  cm/sec, and  $7.15 \times 10^{-4}$  and  $7.14 \times 10^{-4}$  cm/sec, respectively.

These results suggest that the tests for monitoring wells OW-05 and OW-06 may have been influenced by the degree of fracturing in the upper bedrock. Independent evidence of this comes from recharge and field parameter observations recorded during monitoring well re-development (Appendix C) during the 2017 Remedial Investigation, which suggest that monitoring wells OW-05 and OW-06 are hydraulically connected to the upper bedrock water-bearing zone. The well purging and sampling logs from the 2017 Remedial Investigation are included as Appendix D as they were not included in the 2019 Remedial Investigation Report.

The OW-05 well development logs from August 10, 2017 reported the extraction of 47 gallons of groundwater over a period of 62 minutes at an approximate rate of 0.75 gallons per minute (gpm). During re-development, the maximum drawdown in groundwater elevation was 9.46 feet, out of an available 56.48 feet of water column prior to pumping. The 47-gallons removed was greater than 4.5 times the calculated well volume. Additionally, the water was noted to have a sulfur odor, which is a typical characteristic of groundwater pumped from local bedrock due to the presence and dissolution of sulfur containing minerals (e.g., gypsum [calcium sulfate: CaSO<sub>4</sub>], pyrite [iron sulfide: FeS], and sphalerite [iron/zinc sulfide: Fe/ZnS]) in the bedrock.

Similarly, monitoring well OW-06 produced 50 gallons of water (i.e., 5.70 times the initial well volume) over 93 minutes at an approximate rate of 0.53 gpm with minimal drawdown noted.

Well development observations indicate that monitoring wells OW-1B, OW-03, and OW-04 are not hydraulically connected to the upper bedrock water-bearing zone. These wells went dry repeatedly during re-development, typically after the removal of only one well volume. At each of these locations, it was necessary to conduct re-development over several days due to poor recharge and to achieve acceptable field parameter results. The turbidity at OW-04, however, did not sustain readings below 800 Nephelometric Turbidity Units (NTUs) even after the removal of 67.5 gallons of water over six separate days of purging. The slow recharge of these wells is consistent with the lower hydraulic conductivities determined for them (Table 5-3).

### 5.2.5 Upper Bedrock Water-Bearing Zone

Upper bedrock monitoring wells have not been installed at the Niagara Sanitation Landfill, so the upper bedrock water-bearing zone was not evaluated.

#### 6.1 General

In Section 5.0 the hydrogeology of the Niagara Sanitation Landfill was described in detail. In this section the general geochemistry data from the various hydrogeologic zones are evaluated. Geochemical evaluation methods are based upon the principle that dissolved constituents in groundwater occur in predictable proportions, which are based upon the minerals present in the aquifer. In addition, the way in which dissolved constituents behave is known and predictable. As a result, if the minerals present are known, it is possible to predict the water quality resulting from the dissolution of these minerals. Geochemical evaluation methods, therefore, can be utilized to fingerprint different water types by the proportions of dissolved constituents present in the water.

### 6.2 Water Quality Database

During the 2017 Remedial Investigation thirty-eight (38) samples were collected for geochemical analyses from the four overburden hydrogeologic zones identified at the site along with one (1) surface water sample from the northern drainage ditch. These data are summarized in Appendix H. All samples were analyzed by TestAmerica, Inc. in Amherst, New York for calcium, magnesium, sodium, potassium, sulfate, chloride, and alkalinity. In addition, historic water quality data for wells that screen the Camillus Shale in Tonawanda, Erie County, New York (Table H-7), and the upper Lockport Dolostone in Niagara Falls, Niagara County, New York (Table H-8) were also compiled.

Prior to conducting geochemical evaluations, the general reliability of the data set must first be determined by completing charge balance calculations. These calculations consider the major dissolved species that account for most of the charge contribution to the solution. These species are divided into cations (i.e., calcium, magnesium, sodium, and potassium) and anions (i.e., alkalinity (or bicarbonate), chloride, and sulfate). Because most natural waters are electrically neutral, the sum of the positive cation charges should be approximately equal to the sum of the negative anion charges, with respect to the above seven ions. If there is a significant departure from neutrality (greater than 20 percent), there might be a problem with the analytical results and hence data reliability.

To calculate charge balance error, the concentration of each of the above seven ions is

converted to their respective charge contributions. Each of the ions has a positive or negative charge, as follows:

CATIONS (POSITIVE CHARGE)	ANIONS (NEGATIVE CHARGE)		
Calcium (+2) or Ca <sup>+2</sup>	Alkalinity/Bicarbonate (-1)		
Magnesium (+2) or Mg <sup>+2</sup>	or HCO <sub>3</sub> -1		
Sodium (+1) or Na <sup>+1</sup>	Sulfate (-2) or SO <sub>4</sub> - <sup>2</sup>		
Potassium (+1) or K <sup>+1</sup>	Chloride (-1) or Cl <sup>-1</sup>		

The amount of charge contributed by each ion is determined by taking the reported concentration of each ion (in parts per million [ppm]), dividing by its molecular weight, and multiplying by the ionic charge. For example, the amount of charge due to 100 ppm calcium is:

100 ppm	÷	40 mg/mmol	Х	2	=	5 meq/L.
(concentration)		(molecular weight)		(ionic charge)		(total charge)

The total charge is expressed in milliequivalents per liter (meq/L). This value is calculated for each of the seven ions, with the calculated meq/L values added separately for the positive and negative ions as follows:

 $\Sigma$ meg/L cations = meq/L calcium + meq/L magnesium + meq/L sodium + meq/L potassium;  $\Sigma$ meq/L anions = meq/L bicarbonate + meq/L sulfate + meq/L chloride.

The percent error is then calculated as follows:

 $(\Sigma meq/L \text{ cations} - \Sigma meq/L \text{ anions}) \div (\Sigma meq/L \text{ cations} + \Sigma meq/L \text{ anions}) \ge 100 = \% \text{ error.}$ 

There may be circumstances that will produce excessive charge balance errors even with good analytical data. For example, if there is a significant concentration of trace constituents in the water sample, the result will be an apparent imbalance. For typical natural water samples, however, trace constituents are rarely concentrated enough to result in an error exceeding 20 percent.

The error of the water quality database utilized in this study is less than 20 percent (Tables H-1 through H-8 in Appendix H), indicating that the data are reliable for evaluation with geochemical evaluation methods.

# 6.3 Geochemical Evaluation Methods

The geochemical evaluation method utilized in this study relied extensively on ion ratios, rather than comparisons of reported concentrations of natural occurring geochemical constituents typically observed in groundwater. This technique minimizes the effects of variability in reported concentrations between sampling locations. The graphical method utilized was the Piper plot. These plots were interpreted within the context of the known hydrogeology of the Niagara Sanitation Landfill.

#### 6.3.1 Piper Plots

A water's chemical character is determined by seven major ions (calcium, magnesium, sodium, potassium, chloride, sulfate, and bicarbonate); therefore, evaluating the relative abundance of these ions can be utilized to identify mineral or waste sources for these ions. As a result, Piper plots are an effective means of evaluating a large quantity of water quality data as numerous samples can be included on a single plot. Major ion groupings and mixing trends are clearly differentiated, while water quality changes for a given well over time can also be determined.

Piper plots are prepared by first calculating the relative proportion of each cation (calcium, magnesium, sodium, potassium) to the total cation concentration, and the relative proportion of each anion (chloride, sulfate, bicarbonate) to the total anion concentration. The cation chemistry for each sample is plotted on the lower left triangle of the Piper plot, while the anion chemistry is plotted on the lower right triangle (Figure 6-1). The corresponding data points in each triangle are then extrapolated up into the central diamond and plotted at the intersection of the extrapolations (Figure 6-1). Waters originating from different geologic materials will plot within distinct hydrogeochemical regions that will be characteristic of the associated aquifer (Figure 6-2). Waters that are mixtures will plot between these distinct facies. Thus, the origin of a given aquifer's water chemistry can be determined, along with mixing reactions between different aquifers or water types.

# 6.4 Conceptual Geochemical Model for the Niagara Sanitation Landfill

As groundwater flows through the subsurface environment, it evolves geochemically based upon the minerals present in the aquifer and the solubility of those minerals. As a general rule, the concentration of total dissolved solids (TDS) and most of the major ions will increase naturally with increased depth and/or residence time. This generalization suggests that shallow groundwater in recharge areas (i.e., areas with low depth and/or short residence time) will be lower in TDS and major ion concentrations than shallow groundwater in discharge areas, and further, will also be lower in TDS and major ion concentrations than groundwater deeper in the flow system (Freeze and Cherry, 1979). Combining this general principle with the known hydrogeology of the Niagara Sanitation Landfill, a conceptual geochemical model for the site was developed. The Piper plots generated during this study are then interpreted within the framework of this model.

As discussed in Section 5.0, the general stratigraphy of the site, with increasing depth, consists of miscellaneous fill, an upper sand deposit, glaciolacustrine silty clays, a lower sand deposit, glacial till, and Camillus Shale or Lockport Dolostone bedrock. For wells screened within the fill materials, groundwater quality would likely exhibit a wide range of characteristics relating to the chemistry of the fill. The presence of native soil intermixed with the fill material will also result in variable geochemistry.

Since limestone (predominantly CaCO<sub>3</sub>), dolostone (predominantly CaMg[CO<sub>3</sub>]<sub>2</sub>), and shale are the dominant rock types in western New York, the native overburden soils will be composed predominantly of the minerals present in these rocks. The exception to this may be the upper and lower sand deposits, as the source rock for these deposits is unknown. Since the upper sand deposit is encountered at such shallow depths, however, it is anticipated that groundwater in this deposit will be dominated by bicarbonate resulting from the interaction of atmospheric and soil CO<sub>2</sub> with carbonate present in local soils intermixed with the sand.

While the hydraulic conductivity of the underlying glaciolacustrine silty clay deposit is generally extremely low, the presence of vertical desiccation cracks increases the potential for precipitation to infiltrate into this deposit. Concentrations of calcium and magnesium would remain the dominant cations, but the concentrations of bicarbonate will decrease as the presence of atmospheric  $CO_2$  becomes less available to the system.

Groundwater in the underlying lower sand and glacial till deposit will continue to evolve but under closed-system conditions as atmospheric  $CO_2$  is no longer available to the system. The carbonate minerals are less soluble under closed-system conditions, giving rise to increased dissolution of other minerals in the soils. Since it is believed that Camillus Shale bedrock underlies the site, the presence of shale minerals would begin to play a significant role in the evolution of the deeper zone groundwater. Since sodium and sulfate are common ions in shale, groundwater in the lower sand and glacial till deposits should exhibit increasing concentrations of these ions. Groundwater within the upper bedrock hydrogeologic zone evolves differently than groundwater within the overburden deposits; upper bedrock groundwater evolves as it flows through the saturated media over greater distances and generally lower velocities. Groundwater in the bedrock recharge zone, which is believed to be located miles away from the Niagara Sanitation Landfill, would have characteristics similar to those in the shallow hydrogeologic zone; active flushing during recharge would be dominated by bicarbonate resulting from the interaction of atmospheric and soil  $CO_2$  with carbonate derived from the dissolution of limestone, dolostone, and shale in the recharge zone. As groundwater flows through the upper bedrock, the concentrations of the major ions will continue to increase, as will the concentration of TDS. Since the Camillus Shale contains abundant quantities of gypsum (CaSO<sub>4</sub>·H<sub>2</sub>O), groundwater within this formation will become concentrated in calcium and sulfate, while bicarbonate concentrations will decrease as limestone (CaCO<sub>3</sub>), which is also found in abundant quantities within the Camillus Shale, is less soluble under close-system (saturated) conditions. As a result, groundwater in the Camillus Shale is classified as a calcium-sulfate water.

It is also possible that the Lockport Dolostone underlies the Niagara Sanitation Landfill. Johnson (1964) reports that groundwater in the Lockport Dolostone contains significant concentrations of calcium (10.0 to 194.0 mg/l), magnesium (54.8 to 142.0 mg/l), sulfate (62.0 to 1,320 mg/l), and bicarbonate (119.0 to 429.0 mg/l), which are derived from the dissolution of dolostone (CaMg(C0<sub>3</sub>)<sub>2</sub>) and gypsum (CaS0<sub>4</sub>·2H<sub>2</sub>0) by percolating groundwater. As a result, groundwater in the Lockport Dolostone is typically either a calcium-sulfate or calcium-bicarbonate water, is very hard, and highly mineralized (Johnson, 1964; La Sala, 1968).

#### 6.5 Geochemical Results

#### 6.5.1 Surface Water

Only one surface water sample was collected from the Niagara Sanitation Landfill and analyzed for the major cations and anions (Table H-1 in Appendix H). These results indicate that surface water at the site contains higher concentrations of calcium (35.5 mg/l) and bicarbonate (146.3 mg/l) compared to the other major anions and cations (Table H-1). The percentage of calcium and bicarbonate in surface water compared to the total cations and anions, respectively, are shown on Figure 6-3.

The other major cations and anions are detected at much lower concentrations (Table H-1):

magnesium (8.9 mg/l), potassium (4.2 mg/l), sodium (2.3 mg/l), chloride (1.9 mg/l) and sulfate (6.7 mg/l). The percentages of these constituents are also shown on Figure 6-3. The Piper plot for these data (Figure 6-4) confirm that surface water at the Niagara Sanitation Landfill is classified as a calcium-bicarbonate water (compare Figure 6-4 with the diamond plot of Figure 6-2).

### 6.5.2 Fill Wells

As stated in Section 6.4, groundwater from wells that screen the fill materials likely exhibit a wide range of characteristics relating to the chemistry of the fill. As a result, these wells are described separately from wells that screen the upper sand deposit. During the Remedial Investigation, seven (7) groundwater samples from wells that screen the fill materials were collected and analyzed for the major cations and anions (Table H-2 in Appendix H). These results indicate that groundwater in fill at the site contains higher concentrations of calcium (124.0 to 373.0 mg/l) and bicarbonate (815.7 to 1,499.6 mg/l) compared to the other major anions and cations (Table H-2). The arithmetic means for calcium and bicarbonate are 216.86 mg/l and 1,091.73 mg/l, respectively (Table H-2). The percentage of calcium and bicarbonate in fill groundwater compared to the total cations and anions, respectively, are shown on Figure 6-3.

Concentrations of the other major cations and anions range as follows (Table H-2): magnesium (30.5 to 163.0 mg/l), potassium (9.2 to 42.0 mg/l), sodium (10.3 to 153.0 mg/l), chloride (6.9 to 127.0 mg/l) and sulfate (non-detect to 1,150 mg/l). The arithmetic and geometric means for these constituents are given in Table H-2. The percentages of these constituents are shown on Figure 6-3.

The Piper plot for the fill material wells (Figure 6-5) shows variability in the results but also shows that 5 of the 7 samples plot relatively close together in the calcium-bicarbonate section of the diamond (compare Figure 6-5 with the diamond plot of Figure 6-2). Only the sample from well OW-33 does not plot as calcium-bicarbonate water. This well plots as calcium-sulfate water (compare Figure 6-5 with the diamond plot of Figure 6-2).

# 6.5.3 Upper Sand Water-Bearing Zone

During the Remedial Investigation, twenty-three (23) groundwater samples from wells that screen the upper sand deposit were collected and analyzed for the major cations and anions (Table H-3 in Appendix H). These results indicate that groundwater from the upper sand deposit is highly variable, most likely affected by precipitation, seasonal fluctuations in water levels and the fill

materials found throughout the Niagara Sanitation Landfill. In general, water in this zone contains higher concentrations of calcium (148.0 to 780.0 mg/l) and bicarbonate (508.4 to 1,402.1 mg/l) compared to the other major anions and cations (Table H-3). The arithmetic means for calcium and bicarbonate are 338.00 mg/l and 895.02 mg/l, respectively (Table H-3). The percentage of calcium and bicarbonate in upper sand groundwater compared to the total cations and anions, respectively, are shown on Figure 6-3.

Concentrations of the other major cations and anions range as follows (Table H-3): magnesium (34.8 to 293.0 mg/l), sodium (13.8 to 500.0 mg/l), potassium (0.99 to 33.2 mg/l), chloride (11.3 to 664.0 mg/l) and sulfate (8.0 to 1,540.0 mg/l). The arithmetic and geometric means for these constituents are given in Table H-3. The percentages of these constituents are shown on Figure 6-3.

The Piper plot for the upper sand wells (Figure 6-6) shows variability in the results but indicates that groundwater in the upper sand deposit is best classified as a calcium-bicarbonate water (compare Figure 6-6 with the diamond plot of Figure 6-2). Several wells, however, plot as calcium-sulfate water (compare Figure 6-6 with the diamond plot of Figure 6-2). Three (3) specific wells are denoted in Figure 6-6. Well OW-31 is located along the eastern boundary of the landfill (Figure 5-1) but plots in a similar location to three (3) wells located within the landfill. This well plots as calcium-sulfate water. Well OW-21 (Figure 5-1) has the lowest sulfate concentration (8.0 mg/l) of all the upper sand deposit wells, the next lowest sulfate concentration being 84.3 mg/l (Table H-3). The low sulfate concentration in this well, however, is similar to the sulfate concentrations in 5 of the 7 fill wells (compare Tables H-2 and H-3). Well LPZ-04S is located along the southern boundary of the Niagara Sanitation Landfill (Figure 5-1). This well has a higher percentage of sodium and chloride than the other upper sand wells (Figure 6-6). It is interesting to note that this well is located close to the brine pipelines that border the site and may reflect leakage from one of the pipelines.

#### 6.5.4 Upper Clay Aquitard

As discussed in Section 5.2.2, only one (1) well screens the upper clay aquitard underlying the Niagara Sanitation Landfill, and that this well appears to be in hydraulic connection with the overlying upper sand deposit. To evaluate this connectivity further, Figure 6-7 is a Piper plot of well OW-2 along with two (2) nearby upper sand wells. The locations of these wells are shown on Figure 5-1. The Piper plot indicates that well OW-2 has a slightly higher percentage of magnesium than the

2 upper sand wells and a slightly lower percentage of bicarbonate. In general, however, groundwater from this well plots close to groundwater in the nearby upper sand wells and appears to confirm that this well is in hydraulic connection with the upper sand deposit. The major cation and anion results for this well are provided in Table H-4 in Appendix H. The percentages of the major cations and anions are shown on Figure 6-3.

#### 6.5.5 Lower Sand Water-Bearing Zone

As discussed in Section 5.2.3, only two (2) wells screen the lower sand deposit underlying the Niagara Sanitation Landfill. During the Remedial Investigation, both wells were sampled and analyzed for the major cations and anions (Table H-5 in Appendix H). These results indicate that groundwater in the lower sand deposit contains higher concentrations of sodium (50.8 and 64.5 mg/l) and sulfate (112.0 and 125.0 mg/l) compared to the other major anions and cations (Table H-5). The arithmetic means for sodium and sulfate are 57.65 mg/l and 118.50 mg/l, respectively (Table H-5). The percentage of sodium and sulfate in lower sand groundwater compared to the total cations and anions, respectively, are shown on Figure 6-3.

Concentrations of the other major cations and anions range as follows (Table H-5): calcium (16.8 and 18.2 mg/l), magnesium (3.2 and 8.3 mg/l), potassium (1.4 and 1.9 mg/l), bicarbonate (64.0 and 82.5 mg/l), and chloride (3.0 and 15.8 mg/l). The arithmetic and geometric means for these constituents are given in Table H-5. The percentages of these constituents are shown on Figure 6-3.

The Piper plot for the lower sand deposit is given as Figure 6-8, which shows that groundwater in this deposit is best classified as a sodium-chloride water (compare Figure 6-8 with the diamond plot of Figure 6-2). Figure 6-8 also shows that groundwater in the lower sand deposit is significantly different than groundwater encountered in the fill material, the upper sand deposit, and the upper clay aquitard. This indicates that the upper clay aquitard has prevented the downward migration of shallow groundwater to the lower sand deposit.

#### 6.5.6 Glacial Till Aquitard

As discussed in Section 5.2.4, five (5) wells screen the glacial till deposit underlying the Niagara Sanitation Landfill, and that wells OW-05 and OW-06 are hydraulically connected to the underlying upper bedrock. During the Remedial Investigation, all five (5) wells were sampled and analyzed for the major cations and anions (Table H-6A in Appendix H). A review of Table H-6A reveals that the concentrations of calcium, magnesium, and sulfate are significantly higher in well

OW-6 than in the other glacial till wells. As a result, the geochemistry of this well will be discussed separately from the other glacial till wells.

The major cation and anion results indicate that groundwater in glacial till wells OW-1B, OW-3, OW-4, and OW-5 contains higher concentrations of sodium (54.3 to 107.0 mg/l) and sulfate (261.0 to 491.0 mg/l) compared to the other major anions and cations (Table H-6B). The arithmetic means for sodium and sulfate are 84.85 mg/l and 348.50 mg/l, respectively (Table H-6B). The percentage of sodium and sulfate in glacial till groundwater compared to the total cations and anions, respectively, are shown on Figure 6-3.

Concentrations of the other major cations and anions range as follows (Table H-6B): calcium (36.8 to 88.7 mg/l), magnesium (25.1 to 46.7 mg/l), potassium (1.9 to 2.7 mg/l), bicarbonate (66.4 to 256.0 mg/l), and chloride (5.0 to 34.8 mg/l). The arithmetic and geometric means for these constituents are given in Table H-6B. The percentages of these constituents are shown on Figure 6-3.

The Piper plot for the glacial till is given as Figure 6-9, which shows that groundwater in this deposit is best classified as a calcium-sulfate water (compare Figure 6-9 with the diamond plot of Figure 6-2). Figure 6-9 also shows that groundwater in the glacial till deposit is quite variable, with only wells OW-1B, OW-4, and OW-5 plotting in a loose cluster. Well OW-3, which is located southeast of the IRM excavation area, contains groundwater that plots between the upper sand deposit wells and the glacial till wells (compare Figures 6-6 and 6-9) and could reflect migration of upper sand groundwater to the glacial till through the former disposal pit. The cross-section provided as Figure 4-7 shows that the reported depth of the disposal pit would have extended into the glacial till deposit, and that the top of the screen of well OW-3 is only about 5 feet lower. The concentration of bicarbonate in this well is also substantially higher than the other glacial till wells (Table H-6A), which is indicative of shallow groundwater.

Although the lower sand deposit wells did not show evidence of leakage from the shallow water-bearing zones (see Figure 6-8), the lower sand wells may not be located downgradient of the disposal pit and thus may not be impacted by leakage if it is in fact occurring.

Table H-6A shows that well OW-6 contains much higher concentrations of calcium, magnesium, and sulfate than the other glacial till wells. The geochemical difference of the groundwater in this well is clearly observed on the bar graph of Figure 6-3 (labelled as Bedrock?)

and the Piper plot of Figure 6-9. Well OW-6 will be further discussed in Section 6.5.7 below.

### 6.5.7 Upper Bedrock Water-Bearing Zone

**Camillus Shale**: Upper bedrock wells have not been installed at the Niagara Sanitation Landfill, and there is some question as to whether bedrock that underlies the site is the Camillus Shale or the Lockport Dolostone. To evaluate the Camillus Shale, water quality data from upper Camillus Shale bedrock wells in the Tonawanda area were compiled during this study (Table H-7 in Appendix H). These results indicate that groundwater in the upper Camillus Shale contains higher concentrations of calcium (389.0 to 612.0 mg/l) and sulfate (1,370 to 2,970 mg/l) compared to the other major anions and cations (Table H-7). The arithmetic means for calcium and sulfate are 472.13 mg/l and 2,242.12 mg/l, respectively (Table H-7). The percentage of calcium and sulfate in upper Camillus Shale groundwater compared to the total cations and anions, respectively, are shown on Figure 6-3.

Concentrations of the other major anions and cations range as follows (Table H-7): magnesium (35.7 to 232.0 mg/l), sodium (29.9 to 476.0 mg/l), potassium (2.8 to 64.7 mg/l), bicarbonate (21.7 to 474.3 mg/l), and chloride (3.6 to 420.0 mg/l). The arithmetic and geometric means for these constituents are given in Table H-7. The percentages of these constituents are shown on Figure 6-3.

The Piper plot for the upper Camillus Shale bedrock is given as Figure 6-10, which shows that groundwater in this formation is best classified as a calcium-sulfate water (compare Figure 6-10 with the diamond plot of Figure 6-2). The Piper plot, however, shows two distinct groups within the calcium-sulfate quadrant. The first group contains proportions of calcium and magnesium above 75%, while the second group contains proportions of these cations below 75% (Figure 6-10). The first group also contains slightly higher proportions of chloride and sulfate than the second group (Figure 6-10).

**Lockport Dolostone**: Since upper bedrock underlying the Niagara Sanitation Landfill could be the Lockport Dolostone, water quality data from upper Lockport Dolostone bedrock wells in the Niagara Falls area were compiled during this study (Table H-8 in Appendix H). These results indicate that groundwater in the upper Lockport Dolostone contains higher concentrations of calcium (72.0 to 620.0 mg/l), bicarbonate (231.7 to 607.2 mg/l), and sulfate (78.0 to 1,628 mg/l) compared to the other major anions and cations (Table H-8). The arithmetic means for calcium, bicarbonate, and sulfate are 265.43 mg/l, 369.82 mg/l, and 679.14 mg/l, respectively (Table H-8). The percentage of calcium, bicarbonate, and sulfate in upper Lockport Dolostone groundwater compared to the total cations and anions, respectively, are shown on Figure 6-3.

Concentrations of the other major anions and cations range as follows (Table H-8): magnesium (34.0 to 178.0 mg/l), sodium (3.9 to 161.0 mg/l), potassium (non-detect to 11.0 mg/l), and chloride (10.0 to 290.0 mg/l). The arithmetic and geometric means for these constituents are given in Table H-8. The percentages of these constituents are shown on Figure 6-3.

The Piper plot for the upper Lockport Dolostone bedrock is given as Figure 6-11, which shows that groundwater in this formation plots as two distinct clusters. Upper Lockport Dolostone groundwater is either a calcium-sulfate or calcium-bicarbonate water (compare Figure 6-11 with the diamond plot of Figure 6-2).

**Niagara Sanitation Landfill**: A comparison of the Piper plots for glacial till wells at the Niagara Sanitation Landfill (Figure 6-9), upper Camillus Shale bedrock wells in the Tonawanda area (Figure 6-10), and upper Lockport Dolostone bedrock wells in the Niagara Falls area (Figure 6-11) reveals that glacial till well OW-6 plots squarely within the first group of Camillus Shale wells. The concentrations of the major cations and anions in this well are also squarely within the ranges documented for the upper Camillus Shale wells (compare Tables H-6 and H-7). These results suggest that well OW-06 is hydraulically connected to the upper bedrock, and that the bedrock underlying the Niagara Sanitation Landfill is the Camillus Shale.

Although the results discussed in Section 5.2.4 suggest that glacial till well OW-5 is also hydraulically connected to upper bedrock underlying the Niagara Sanitation Landfill, the groundwater geochemistry does not support this (compare Figure 6-9 to Figures 6-10 and 6-11).

# 7.0 SUMMARY

During implementation of a State Funded Remedial Investigation at the Niagara Sanitation Landfill in 2017, groundwater flow in the fill/upper sand water-bearing zone was to the south toward Forbes Street. This flow pattern, however, was opposite to that identified in studies completed in 2013 & 2014. To further evaluate groundwater flow patterns at the site, a detailed study of the geology and hydrogeology of the Niagara Sanitation Landfill was completed, with the information utilized to develop a conceptual geochemical model for the site. Geochemical data obtained during the Remedial Investigation from the various water-bearing zones underlying the site were then evaluated within this framework.

# 7.1 Geology

The stratigraphy of the Niagara Sanitation Landfill was evaluated by examining seventyseven (77) stratigraphic logs obtained from soil borings completed at the site. These data suggest that eight (8) distinct stratigraphic units underlie the site: (1) fill material, (2) an upper brown silt and clay deposit, (3) an upper yellow-brown sand deposit, (4) a gray-brown lacustrine silty clay deposit, (5) a red-gray layered lacustrine clay deposit, (6) a relatively thin, lower red-brown sand deposit, (7) a relatively thick, reddish brown to gray glacial till deposit, and (8) bedrock. Most investigations completed at the site have been confined to the fill material, the upper sand deposit, and the upper brown silt and clay deposit.

Fill material overlies the native deposits throughout most of the Niagara Sanitation Landfill but is discontinuous across the site. Where fill material is absent, native deposits are generally encountered at ground surface. The thickness of the fill material typically ranges from 2.0 to 6.0 feet, although thicker areas of fill are associated with the former disposal pit. The average thickness of the fill material is 4.1 feet.

The native soils underlying the Niagara Sanitation Landfill include a glaciolacustrine deposit and glacial till. With increasing depth, the glaciolacustrine deposit consists of a brown silt and clay unit, an upper sand unit, a gray-brown silty clay unit, a red-gray layered clay unit, and a lower sand unit. These units were deposited in glacial lakes that covered the area during the last ice age.

The full thickness of the glaciolacustrine deposit was only penetrated at 7 borings completed at the site. The total thickness of this deposit was quite variable, ranging from 21.5 to 45.0 feet. At 6

of the 7 boring locations, however, the thickness of the glaciolacustrine deposit was 36.0 feet or greater.

The brown silt and clay deposit was encountered in 30 borings completed at the site. The depth to this deposit ranged from 0.0 to 4.0 feet below ground surface, while the thickness ranged from 0.5 to 4.0 feet. The average thickness of brown silt and clay deposit is 2.0 feet.

The upper sand deposit was encountered in 61 borings completed at the site. The depth to this deposit ranged from 0.0 to 10.0 feet below ground surface. Where completely penetrated, the thickness of the upper sand deposit was quite variable, ranging from 0.4 to 11.0 feet. The average thickness of this deposit is 4.4 feet.

The gray-brown silty clay deposit was encountered in 63 borings completed at the Niagara Sanitation Landfill. The depth to this deposit was quite variable, ranging from 3.0 to 15.0 feet below ground surface. This deposit was only completely penetrated at 11 locations, with the thickness ranging from 2.0 to 8.0 feet. The average thickness of the gray-brown silty clay deposit is 4.8 feet.

The red-gray layered clay deposit was encountered in 11 borings completed at the site. The depth to this deposit was quite variable, ranging from 8.0 to 16.0 feet below ground surface. Where completely penetrated, the thickness of the red-gray layered clay deposit was extremely variable, ranging from 18.5 to 33.0 feet. The average thickness of this deposit is 25.6 feet.

A relatively thin, red-brown sand deposit underlies the red-gray layered clay deposit and mantles the glacial till. Based on its lithology and stratigraphic position, this sand deposit is interpreted to be an early deposit of Lake Tonawanda. The lower sand deposit was only encountered in 6 borings completed at the site. The depth to this deposit was quite variable, ranging from 26.3 to 42.0 feet below ground surface, while the thickness was somewhat variable, ranging from 0.2 to 5.0 feet. In 4 borings, however, the thickness of this deposit ranged from 3.0 to 5.0 feet.

A relatively thick, continuous layer of glacial till underlies the lower sand deposit and mantles the underlying bedrock. The till underlying the Niagara Sanitation Landfill consists predominantly of a dense, brown silt with fine to coarse sand and fine gravel. The glacial till deposit was only encountered in 7 borings completed at the site. The depth to till was quite variable, ranging from 26.5 to 45.0 feet below ground surface. Where completely penetrated, the thickness of this deposit ranged from 22.0 to 42.2 feet. The average thickness of the glacial till deposit is 29.0 feet. The uppermost bedrock unit underlying the Niagara Sanitation Landfill is unknown. Available information suggests that it could be dolostone of the Lockport Group or the Camillus Shale of the Salina Group. None of the borings completed at the Niagara Sanitation Landfill cored into bedrock for positive identification. Bedrock was only encountered in 5 borings completed at the site. Depth to bedrock beneath the Niagara Sanitation Landfill was relatively consistent, ranging from 66.0 to 70.3 feet below ground surface.

# 7.2 Hydrogeology

A primary objective of this study was to further evaluate groundwater flow patterns in the water-bearing zones underlying the site. This was completed by generating a series of groundwater contour maps. A complete understanding of the groundwater flow patterns, especially in the fill/upper sand water-bearing zone, is critical for evaluating the potential for contaminants in groundwater to migrate from the site.

The hydrogeology of the Niagara Sanitation Landfill was evaluated by examining hydrogeologic data obtained during this study. These data suggest that five (5) hydrogeologic zones underlie the site: (1) the fill/upper sand water-bearing zone consisting of miscellaneous fill and the upper sand deposit, (2) the upper clay aquitard consisting of the gray-brown lacustrine silty clay and red-gray layered lacustrine clay deposits, (3) the lower sand water-bearing zone, (4) the glacial till deposit that acts an aquitard, and (5) the upper bedrock water bearing zone. Upper bedrock monitoring wells have not been installed at the Niagara Sanitation Landfill, so the upper bedrock water-bearing zone was not evaluated.

In Sections 5.2.1 through 5.2.4, hydrographs and groundwater contour maps for the various hydrogeologic zones underlying the Niagara Sanitation Landfill were presented and discussed. In this section, those hydrographs and groundwater contours are evaluated collectively to form a comprehensive picture of the hydrogeology at the site.

**Figure 7-1** is a hydrograph showing representative wells from all hydrogeologic zones at the site. As discussed in Section 5.2.1, water levels in the fill/upper sand wells fluctuated throughout the year in response to precipitation. Water levels steadily decreased between August 22<sup>nd</sup> and September 25<sup>th</sup>, a period that was characterized by lower-than-normal rainfall. Water levels then increased substantially in all fill/upper sand wells during October and November 2017, a period that was characterized by higher-than-normal rainfall. These fluctuations are clearly seen on Figure 7-1.

There is only one (1) monitoring well (OW-2) at the Niagara Sanitation Landfill that screens the upper clay aquitard that underlies either fill material or the upper sand deposit. As discussed in Section 5.2.2, the hydrogeologic data compiled for this study indicates that well OW-2 is hydraulically connected to the fill/upper sand water-bearing zone. The hydrograph for this well shows that water level fluctuations mirrored those in the fill/upper sand wells. This relationship is clearly seen on Figure 7-1.

There are only two monitoring wells (OW-14A and OW-15) at the Niagara Sanitation Landfill that screen the lower sand deposit that underlies the upper clay aquitard. As discussed in Section 5.2.3, the hydrograph for well OW-15 shows very little seasonal fluctuation, with water levels ranging from 567.58 to 568.11 feet above mean sea level. The relatively small fluctuations in this well are clearly seen on Figure 7-1.

Figure 7-1 indicates that water levels in the lower sand deposit are approximately 6 feet lower than water levels in the overlying hydrogeologic zones. This indicates the potential for vertical downward movement of groundwater from the fill/upper sand water-bearing zone to the lower sand deposit. This potential, however, is thought to be very limited due to the low permeability of the glaciolacustrine silty clay and clay deposits, which typically range from 10<sup>-6</sup> to 10<sup>-8</sup> cm/sec. In addition, the layered nature of the sediments on-site suggest that the vertical hydraulic conductivity could be orders of magnitude lower than the horizontal hydraulic conductivity.

There are five monitoring wells at the Niagara Sanitation Landfill that screen the glacial till deposit that underlies the lower sand deposit. As discussed in Section 5.2.4, the hydrographs for these wells reveal that there was very little seasonal fluctuation, with water levels ranging from 564.95 to 565.75 feet above mean sea level. The relatively small fluctuations in these wells are clearly seen on Figure 7-1.

Figure 7-1 indicates that water levels in the glacial till deposit are approximately 3 feet lower than water levels in the overlying upper sand deposit. This indicates the potential for vertical downward movement of groundwater from the lower sand deposit to deeper water-bearing zones. This potential, however, is again thought to be very limited due to the low permeability of the glacial till deposit. The hydraulic conductivity of the glacial till wells not influenced by the underlying bedrock ranged from  $1.43 \times 10^{-6}$  to  $7.88 \times 10^{-7}$  cm/sec (Table 5-3).

Numerous groundwater contour maps have been generated for the fill/upper sand water-

bearing zone (Figures 5-6 through 5-22). These contours, however, do not show a consistent pattern of groundwater flow across the Niagara Sanitation Landfill. Groundwater flow has been documented to the north (Figures 5-6, 5-7, 5-21 and 5-22), south (Figures 5-9, 5-10, 5-11, 5-12, 5-13, and 5-14), and inward (Figures 5-8, 5-15, 5-17, 5-18, 5-19, and 5-20). In the eastern portion of the site, an eastward component to groundwater flow was observed on August 2, 2013 (Figure 5-7), August 2, 2017 (Figure 5-9), August 22, 2017 (Figure 5-11), August 30, 2017 (Figure 5-12), September 12, 2017 (Figure 5-13), September 25, 2017 (Figure 5-14), October 17, 2017 (Figure 5-15), October 20, 2017 (Figure 5-17), and October 27, 2017 (Figure 5-18), while flow to the west or northwest in the eastern portion of the site was observed on November 7, 2017 (Figure 5-19), April 3, 2020 (Figure 5-21), and November 23, 2021 (Figure 5-22).

It is important to note that flow gradients are low, typically ranging from 0.003 to 0.005 ft/ft. Groundwater contour intervals are also low, ranging from 0.05 feet (0.6 inches) to 0.25 feet (3 inches). This suggests that an error in measurement, recording, or a slightly heaved well can drastically impact the contour. An example of the latter is documented by Figures 5-9 and 7-2. As stated in Section 5.2, well OW-14B was found to be heaved/damaged due to frost action and was no longer considered accurate for groundwater and hydrogeologic data collection. These figures show the groundwater contour for August 2, 2017 with (Figure 7-2) and without (Figure 5-9) the water level from this well. The groundwater flow patterns for these two contours are drastically different.

For sites with low flow gradients, the number of wells utilized to generate a groundwater contour can also have a huge influence. An example of this is documented by Figures 5-6 and 5-7. During the 2013 GES Site Characterization Study, water levels were measured in ten (10) monitoring wells. The contour generated from these data (Figure 5-6) showed that groundwater in the fill/upper sand water-bearing zone flowed to the north and northwest.

During the Remedial Investigation, these wells were resurveyed. The groundwater contour map generated from the new survey data is illustrated in Figure 5-7. It is important to note, however, that several wells had been removed during the Interim Remedial Measure completed by the Occidental Chemical Corporation, so this contour only includes water levels from five (5) wells. This contour indicates that groundwater is mounded at well OW-13 and flows from this mound to the northeast, north, and northwest. Once again, the groundwater flow patterns for these two contours are drastically different.

Due to the limited number of wells in the upper clay aquitard (1 well) and the lower sand

deposit (2 wells), groundwater contour maps for these hydrogeologic zones could not be generated.

Two (2) groundwater contour maps have been generated for the glacial till deposit (Figures 5-27 and 5-28). Figure 5-27 is a groundwater contour map for the glacial till deposit generated from the water level data collected during the Phase II Investigation (date not specified in the report). This contour shows that groundwater is mounded in the north-central portion of the landfill and flows outward from this mound toward the east, south, and west. Figure 5-28 is a groundwater contour map for the glacial till deposit generated from the water level data collected on October 20, 2017. This contour shows that groundwater in the glacial till flows across the site from east to west at a very low gradient.

# 7.3 Geochemistry

A conceptual geochemical model based upon the hydrogeology of the Niagara Sanitation Landfill was developed to provide a framework in which to further evaluate the five (5) hydrogeologic zones that underlie the site. During the 2017 Remedial Investigation thirty-eight (38) samples were collected for geochemical analyses from the four overburden hydrogeologic zones identified at the site. One (1) surface water sample from the northern drainage ditch was also collected and analyzed. These data were evaluated by using Piper plots.

The Piper plots presented in Section 6.5 reveal that distinct water types are present at the Niagara Sanitation Landfill. For example, surface water is best classified as a calcium-bicarbonate water (Figure 6-4), while water in the Camillus Shale bedrock is best classified as a calcium-sulfate water (Figure 6-10). In this section, the water types identified during this evaluation will be discussed in relation to the conceptual geochemical model described in Section 6.4.

Surface water at the Niagara Sanitation Landfill is best classified as a calcium-bicarbonate water (Figure 6-4). This type of water results from the dissolution of calcium that occurs naturally in soils of southwestern Niagara County and the interaction of atmospheric and soil  $CO_2$  with carbonate present in on-site soils. The presence of calcium-bicarbonate surface water at the site is consistent with the conceptual geochemical model.

Groundwater in the fill material at the Niagara Sanitation Landfill is best classified as a calcium-bicarbonate water (Figure 6-5). This groundwater generally contains low sulfate (5 of 7 samples), which is likely caused by the interaction of groundwater and fill material. Calcium is the

dominant cation in this groundwater, resulting from the dissolution of calcium carbonate from the native soils intermixed with the fill material. Bicarbonate is the dominant anion in this groundwater, resulting from the interaction of atmospheric and soil CO<sub>2</sub> with carbonate present in on-site soils. The presence of calcium-bicarbonate groundwater in the fill material at the site is consistent with the conceptual geochemical model.

Groundwater in the upper sand deposit is highly variable, most likely affected by precipitation, seasonal fluctuations in water levels and the fill materials found throughout the Niagara Sanitation Landfill. The Piper plot for the upper sand deposit (Figure 6-6) shows that groundwater in this deposit is best classified as a calcium-bicarbonate water, although several wells plot as calcium-sulfate water. Once again, the presence of calcium-bicarbonate groundwater in the upper sand deposit is consistent with the conceptual geochemical model.

There is only one well at the Niagara Sanitation Landfill that screens the upper clay aquitard. As previously stated, this well appears to be in hydraulic connection with the overlying upper sand deposit. As a result, groundwater in this well plots close to groundwater from nearby upper sand wells (Figure 6-7). Additional wells would need to be installed in this deposit to further evaluate the groundwater type in this zone.

Groundwater in the lower sand deposit at the Niagara Sanitation Landfill is best classified as a sodium-chloride water (Figure 6-8). Figure 6-8 also shows that groundwater in the lower sand deposit is significantly different than groundwater encountered in the overlying fill material, the upper sand deposit, the upper clay aquitard, and the underlying glacial till deposit (compare Figure 6-8 with Figures 6-5, 6-6, and 6-9). This suggests that the upper clay aquitard has prevented the downward migration of shallow groundwater to the lower sand deposit, while the glacial till deposit has prevented upward migration of upper bedrock groundwater into this zone. Since the areal extent of the lower sand deposit is unknown, the source of the groundwater in this deposit is also unknown.

Groundwater in the glacial till deposit at the Niagara Sanitation Landfill is best classified as a calcium-sulfate water (Figure 6-9). Figure 6-9 also shows that groundwater in the glacial till deposit is quite variable, with only wells OW-1B, OW-4, and OW-5 plotting in a loose cluster. The presence of calcium-sulfate groundwater in this deposit is consistent with the conceptual geochemical model; the carbonate minerals in the glacial till are less soluble under closed-system conditions, concentrations of bicarbonate decrease as the presence of atmospheric  $CO_2$  becomes less available to the system, and there is increased dissolution of other minerals in the soils.

Upper bedrock wells have not been installed at the Niagara Sanitation Landfill. Glacial till well OW-6, however, which appears to be in hydraulic connection with the upper bedrock, plots squarely within a group of Camillus Shale wells located in nearby Tonawanda, New York (Figure 6-10), but does plot within either of the Lockport Dolostone clusters (Figure 6-11). This highly suggests that bedrock underlying the Niagara Sanitation Landfill is the Camillus Shale. The higher concentrations of sodium and sulfate in the Camillus Shale wells are consistent with the conceptual geochemical model, i.e., as groundwater flows through the upper bedrock, the concentrations of the major ions will continue to increase. Since the Camillus Shale contains abundant quantities of gypsum (CaSO<sub>4</sub>·H<sub>2</sub>O), groundwater within this formation will become concentrated in calcium and sulfate, while bicarbonate concentrations will decrease as limestone (CaCO<sub>3</sub>), which is also found in abundant quantities within the Camillus Shale, is less soluble under close-system (saturated) conditions.

#### 8.0 **REFERENCES**

- Bechtel, 1993, Remedial Investigation Report for the Tonawanda Site: Bechtel National, Inc., Oak Ridge, Tennessee.
- Buehler, E.J., and Tesmer, I.H., 1963, Geology of Erie County, New York: Buffalo Society of Natural Sciences Bulletin, v. 21, no. 3, 118p.
- Brett, C.E., Tepper, D.H., Goodman, W.M., LoDuca, S.T., and Eckert, B.Y, 1995, Revised Stratigraphy and Correlations of the Niagaran Provincial Series (Medina, Clinton, and Lockport Groups) in the Type Area of Western New York: U.S. Geological Survey Bulletin 2086, 66p.
- Calkins, P.E., and Brett, C.E., 1978, Ancestral Niagara River Drainage: Stratigraphic and Paleontologic Setting: Geological Society of America Bulletin, v. 89, p. 1140-1154.
- Conestoga Rovers & Associates, 1998, RCRA Facility Investigation and Remedial Investigation Report, Spaulding Composites Company, Tonawanda, New York: Conestoga Rovers & Associates, Niagara Falls, New York.
- Dethier, B.E., 1966, Precipitation in New York State: Ithaca, N.Y., Cornell University Agricultural Experiment Station, Bulletin 1009, 78p.
- Ecology and Environment, 1992, Engineering Investigations at Inactive Hazardous Waste Disposal Sites, Phase II Report, Wurlitzer Site, Site No. 932041, City of North Tonawanda, Niagara County: Ecology and Environment Engineering, P.C., April 1992.
- Engineering-Science, 1983, Engineering Investigations and Evaluations at Inactive Hazardous Waste Disposal Sites, Phase I Report, Niagara Sanitation, Nash Road, Niagara County, NY: Engineering-Science in association with Dames & Moore, June 1983.
- Engineering-Science, 1985, Engineering Investigations and Evaluations at Inactive Hazardous Waste Sites, Phase II Report, Nash Road Landfill, Site No. 932054, Town of Wheatfield, Niagara County: Engineering Science in association with Dames & Moore, July 1985.
- Engineering Science, 1989, Engineering Investigations and Evaluations at Inactive Hazardous Waste Sites, Phase II Supplemental Investigation Report, Niagara Sanitation Company (Nash Road Landfill), Site No. 932054, Town of Wheatfield, Niagara County: Engineering Science, September 1989.
- EPA, 1985, Preliminary Evaluation of Chemical Migration to Groundwater and the Niagara River from Selected Waste-Disposal Sites: Great Lakes National Program Office, Report EPA-905/4-85-001.
- Freeze, R.A., and Cherry, J.A., 1979, Groundwater: Prentice-Hall, Inc., Englewood Cliffs, New Jersey, 604p.
- GES, 2013, Site Characterization Report, Former Nash Road Landfill, Town of Wheatfield, Niagara County, New York, NYSDEC Site #932054: Groundwater Environmental Services, Inc.,

November 2013.

- GES, 2014, Supplemental Site Characterization Report, Former Nash Road Landfill, Town of Wheatfield, Niagara County, New York, NYSDEC Site #932054: Groundwater Environmental Services, Inc., July 2014.
- Glenn Springs, 2016, Interim Remedial Measure Project Summary Report, NYSDEC Site #932054, Former Niagara Sanitation Site, Wheatfield, New York: Glenn Springs Holdings, Inc., January 2016.
- Golder Associates, 1991, Corrective Measures Study, Bell Aerospace Textron Wheatfield Plant: Golder Associates Inc, June 1991.
- Gross, M.R., and Engelder, T., 1991, a Case for Neotectonic Joints along the Niagara Escarpment: Tectonics, v. 10, no. 3, p 631-641.
- GTC, 1983, Love Canal Hydrogeologic Investigation: GTC Geologic Testing Consultants LTD., January 1983.
- GZA, 1983, Geotechnical Report for Niagara Mohawk Power Corporation C.R. Huntley Steam Station Wastewater Management Systems Project: Goldberg-Zoino Associates, Buffalo, New York.
- Johnson, R.H., 1964, Ground Water in the Niagara Falls Area, New York: State of New York Water Resources Commission Bulletin GW 53, 93p.
- La Sala, A.M., Jr., 1968, Ground-Water Resources of the Erie-Niagara Basin, New York: Water Resources Commission, Basin Planning Report ENB-3, New York State Conservation Department, Albany, New York, 114p.
- LiRo, 2019, Remedial Investigation Report, Niagara Sanitation/Nash Road Landfill Site, 7415 Nash Road, Town of Wheatfield, Niagara County, New York, NYSDEC Site Number 932054: LiRo Engineers, Inc., February 2019.
- May, G.M., 2007, Hydrogeologic and Geochemical Investigation of the Southwestern Portion of the Town of Tonawanda, Erie County, New York: New York State Department of Environmental Conservation, Division of Environmental Remediation, Buffalo, New York.
- Miller, T.S., and Kappel, W.M., 1987, Effect of Niagara Power Plant Project on Ground-Water Flow in the Upper Part of the Lockport Dolomite, Niagara Falls Area, New York: U.S. Geological Survey Water-Resources Investigation Report 86-4130, 31p.
- Muller, E.H., 1965, Bibliography of New York Quaternary Geology: New York State Museum and Science Service Bulletin Number 398.
- Muller, E.H., 1977, Quaternary Geology of New York, Niagara Sheet: New York State Museum and Science Service, Map and Chart Series Number 28, Scale 1:250,000.
- NYSDEC, 1997, Immediate Investigative Work Assignment, Vanadium Corporation of America Site, Town of Niagara, Niagara County, Site Number 9-32-001: New York State

Department of Environmental Conservation, Division of Environmental Remediation, Buffalo, New York, 95p. plus appendices.

- NYSDEC, 1998, Ambient Water Quality Standards and Guidance Values and Groundwater Effluent Limitations: New York State Department of Environmental Conservation, Division of Water Technical and Operational Guidance Series (1.1.1), Albany, New York.
- NYSDEC, 2006, 6 NYCRR Part 375: Environmental Remediation Programs, Soil Cleanup Objectives: New York State Department of Environmental Conservation, Division of Environmental Remediation, Albany, New York.
- NYSDEC, 2010, DER-10: Technical Guidance for Site Investigation and Remediation: New York State Department of Environmental Conservation, Division of Environmental Remediation, Albany, New York.
- Parsons Engineering Science, 1995, Remedial Investigation Report, Polymer Applications Site, Site No. 915044: Parsons Engineering Science, Inc., Liverpool, New York.
- Pyanowski, D., 1990, Memorandum to File, dated June 14, 1990: Dunlop Tire Corporation, Buffalo, New York.
- Rickard, L.V., 1966, Upper Silurian Cayugan Series, Niagara Frontier, New York in Buehler, E.J., (ed.), Geology of Western New York, Guidebook, New York State Geological Association 38th Annual Meeting: Department of Geological Sciences, State University of New York at Buffalo, New York.
- Rickard, L.V. and Fisher, D.W., 1970, Geologic Map of New York State, Niagara Sheet: New York State Museum and Science Service, Map and Chart Series No. 15.
- Snyder Engineering, 1987, Support Documentation for an Application to Construct and Operate Cell Number Three at the SKW Alloys, Inc. Witmer Road Solid Waste Management Facility: Snyder Engineering, Grand Island, New York.
- Stanley Consultants, 1981, Coal Pile Groundwater Monitoring Study, C.R. Huntley Steam Station: Stanley Consultants, Muscatine, Iowa.
- Staubitz, W.W., and Miller, T.S., 1987, Geology and Hydrology of the Onondaga Aquifer in Eastern Erie County, New York, with Emphasis on Ground-water Level Declines since 1982: U.S. Geological Survey Water-Resources Investigations Report 86-4317.
- URS, 1991, Remedial Investigation Report, Frontier Chemical-Pendleton Site, Site No. 932043, Town of Pendleton, Niagara County, New York: URS Consultants, Inc., June 1991.
- URS, 1992, Report of Field Investigation and Data Analysis, Inactive Disposal Sites, No's 915018A, B, C: URS Consultants, Inc., Buffalo, New York.
- USDA, 1972, Soil Survey of Niagara County, New York: U.S. Department of Agriculture, Soil Conservation Service in cooperation with Cornell University Agricultural Experiment Station, Washington, D.C., 199 p.

- Woodward-Clyde, 1993, Phase II Investigation Report, DuPont Yerkes Plant, Site No. 915019: Woodward-Clyde Consultants, North Tonawanda, New York.
- Woodward-Clyde Consultants and Conestoga Rovers and Associates, 1992, Niagara Falls Regional Ground-Water Assessment: Niagara Falls, N.Y., Conestoga Rovers and Associates, 126p plus appendices.
- Yager, R.M., and Kappel, W.M., 1987, Characterization of Fractures in the Lockport Dolomite, Niagara County, New York, in Khanbilvardi, R.M., and Fillos, J., (eds.), Pollution, Risk Assessment and Remediation in Groundwater Systems: Washington, D.C., Scientific Publications Co., p. 149-195.

# **FIGURES**













Figure 3-1. Precipitation Data for Western New York.






TOWN OF WHEATFIELD, NIAGARA COUNTY, NEW YORK	SHEET	OF
NYSDEC SITE NUMBER 932054		
DRAWING TITLE:	FIGURE NO.	
CROSS-SECTION LOCATION MAP 2017 REMEDIAL INVESTIGATION	4	-3



e 4

\$

Ľ.









NOTES:

- 1. ELEVATIONS IN FEET ABOVE MEAN SEA LEVEL.
- 2. WATER LEVELS MEASURED ON SEPTEMBER 25,



```
NOTES:
```

- 1. ELEVATIONS IN FEET ABOVE MEAN SEA LEVEL.
- 2. WATER LEVELS MEASURED ON SEPTEMBER 25, 2017 AND OCTOBER 17, 2017.
- 3. REFER TO TEXT FOR DESCRIPTION OF UNITS.

## LEGEND



\_\_\_\_

WATER LEVEL RECORDED SEPTEMBER 25, 2017

WATER LEVEL RECORDED OCTOBER 10, 2017

SCREENED INTERVAL

00

INFERRED GEOLOGICAL BOUNDARY (DATA NOT AVAILABLE)

80	80
HORIZONTAL SC	ALE IN FEET
5 0	5
VERTICAL SCA	LE IN FEET
JOB TITLE AND LOCATION: NIAGARA SANITATION / NASH ROAD LANDFILL SITE 7415 NASH ROAD	liro job no.: 17—013—0289
TOWN OF WHEATFIELD, NIAGARA COUNTY, NEW YORK NYSDEC SITE NUMBER 932054	SHEET OF
DRAWING TITLE:	FIGURE NO.
GEOLOGIC CROSS-SECTION D-D' 2017 REMEDIAL INVESTIGATION	4-9



	LEGEND				
	AREA OF INVESTIGATION				
<del></del>	1985 & 1989 PHASE II SOIL BORINGS				
۲	2013 & 2014 GES SOIL BORINGS				
<del>\$</del>	2017 & 2021 LIRO SOIL BORINGS				

	80 SCALI	0 80 E IN FEET
JOB TITLE AND LOCATION: NIAGARA SANITATION / NASH ROAD LANDFILL SITE 7415 NASH ROAD		<b>LIRO JOB NO.:</b> 17-013-0289
TOWN OF WHEATFIELD, NIAGARA COUNTY, NEW YORK NYSDEC SITE NUMBER 932054		SHEET OF
DRAWING TITLE:		FIGURE NO.
UPPER SAND SURFACE CONTOUR MAP		4-10



LEGEND				
	AREA OF INVESTIGATION			
$\ominus$	1985 & 1989 PHASE II SOIL BORINGS			
	2013 & 2014 GES SOIL BORINGS			
<del>•</del>	2017 & 2021 LIRO SOIL BORINGS			

8	SCALI	O E IN FEE	80 T
Job Title and location: NIAGARA SANITATION / NASH ROAD LANDFILL SITE 7415 NASH ROAD		<b>LIRO JOB NO</b> 17-013-	# -0289
TOWN OF WHEATFIELD, NIAGARA COUNTY, NEW YORK NYSDEC SITE NUMBER 932054		SHEET	OF
DRAWING TITLE:		FIGURE NO.	
UPPER SAND THICKNESS CONTOUR MAP		4-1	1



LEGEND				
	AREA OF INVESTIGATION			
	1985 & 1989 PHASE II SOIL BORINGS			
۲	2013 & 2014 GES SOIL BORINGS			
<del>\$</del>	2017 & 2021 LIRO SOIL BORINGS			

	SCALE IN FEET
JOB TITLE AND LOCATION: NIAGARA SANITATION / NASH ROAD LANDFILL SITE 7415 NASH ROAD TOWN OF WHEATFIELD, NIAGARA COUNTY, NEW YORK NYSDEC SITE NUMBER 932054	LIRO JOB NO.: 17-013-0289 SHEET OF
DRAWING TITLE: DEPTH TO GRAY-BROWN SILTY CLAY CONTOUR MAP	FIGURE NO. 4-12







P.P. 	681.46' DEED
BRINE MARKER	REPUTED OWNER IROQUOIS GAS CORPORATION L-1496, P-986
P.P. 1.2' SOUTH FENCE No 50 0.1' SOUTH 0.1' SOUTH 0.8' SC 0.8' SC	SHED FENCE UTH 1.8 SOUTH
ES TERRACI wide easement to texi orporation L-2072, p-	– – (60.0' WIDE) 15 –

	80 0 80 SCALE IN FEET
JOB TITLE AND LOCATION: NIAGARA SANITATION / NASH ROAD LAND 7415 NASH ROAD TOWN OF WHEATFIELD, NIAGARA COUNTY, N	LIRO JOB NO.:   17-013-0289   NEW YORK SHEET OF
DRAWING TITLE: LOWER SAND THICKNESS MAP	FIGURE NO. 4-13





BRINE MARKER 41 GAS MARKER 41 BRINE MARKER 41 P.P. 1.2' SOUTH FENCE NC FENCE 0.1' SOUTH NT SOR 0.1' SOUTH 1.8' SOUTH NT 62 0.1' SOUTH 1.8' SOUTH 1.		P.P. 1.1' SOUTH	681.46' DEED
P.P. 1.2' SOUTH FENCENG 50R FENCENG 62R FENCENG 62R NY 62 0.7' NORTH 0.6' SOUTH 1.8' SOUTH 0.6' SOUTH	1	BRINE MARKER	REPUTED OWNER IROQUOIS GAS CORPORATION L-1496, P-986
	4	P.P. 1.2' SOUTH FENCENG 0.7' NORTH 0.7' NORTH	SOR FENCE SOUTH 1.8" SOUTH

80 S	0 80 CALE IN FEET
JOB TITLE AND LOCATION: NIAGARA SANITATION / NASH ROAD LANDFILL SITE 7415 NASH ROAD TOWN OF WHEATFIELD, NIAGARA COUNTY, NEW YORK NYSDEC SITE NUMBER 932054	LIRO JOB NO.: 17-013-0289 SHEET OF
DRAWING TITLE: DEPTH TO THE GLACIAL TILL CONTOUR MAP	FIGURE NO. 4-14



RAWING TITLE:	FIGURE NO.
DEPTH TO TOP OF BEDROCK CONTOUR MAP	4-

4-	1	5
4-	1	5



DRAWING TITLE:		FIGURE NO.
	BEDROCK SURFACE ELEVATION CONTOUR MAP	4-16



© 2024 New York State Department of Environmental Conservation

rawing Name: 01 Sites - Active/Niggara Sanitation/2023 Sampling/AutoCAD/Niagara Sanitation - 2023 Sampling Report dw Deceder Name: Glann M. Mey, Disc Date: Sectember 17, 2024



Figure 5-2. Hydrograph for the Fill/Upper Sand Wells at the Niagara Sanitation Landfill Site.



Figure 5-3. Hydrograph for the Fill/Upper Sand Wells at the Niagara Sanitation Landfill Site.



Figure 5-4. Hydrograph for the Fill/Upper Sand Wells at the Niagara Sanitation Landfill Site.



Figure 5-5. Hydrograph for Upper Sand Well-Staff Gauge Couplets at the Niagara Sanitation Landfill Site.




































Figure 5-23. Hydrograph for the Upper Clay Aquitard Well at the Niagara Sanitation Landfill Site.



Figure 5-24. Hydrograph for Select Wells and Staff Gauges at the Niagara Sanitation Landfill Site. Solid lines denote the upper sand wells, dotted lines denote the staff gauges; and the dashed line denotes the upper clay aquitard well. Upper sand wells and staff guages with the same color are in close proximity to each other.



Figure 5-25. Hydrograph for the Lower Sand Wells at the Niagara Sanitation Landfill Site.



Figure 5-26. Hydrograph for the Glacial Till Wells at the Niagara Sanitation Landfill Site.









Figure 6-1. The three components of the Piper plot. At bottom left is a ternary plot of the cations (magnesium, calcium, and sodium plus potassium), while at bottom right is a ternary plot of the anions (chloride, sulfate, and carbonate plus bicarbonate). At the top is a diamond plot of the projection from the two ternary plots. Image downloaded from the Golden Software website on November 7, 2022.



Figure 6-2. Interpretation of the diamond plot. Samples in the top quadrant are calcium sulfate waters, which are typical of gypsum groundwater. Samples in the left quadrant are calcium bicarbonate waters, which are typical of shallow fresh groundwater. Samples in the right quadrant are sodium chloride waters, which are typical of marine and deep ancient ground water. Samples in the bottom quadrant are sodium bicarbonate waters, which are typical of deep ground water influenced by ion exchange. Image downloaded from the Golden Software website on November 7, 2022.



Figure 6-3A. Plot of the Major Cations for the Various Hydrogeologic Zones Underlying the Niagara Sanitation Landfill. Results Shown are the Arithmetic Means (in Percent) of Each Cation.



Figure 6-3B. Plot of the Major Anions for the Various Hydrogeologic Zones Underlying the Niagara Sanitation Landfill. Results Shown are the Arithmetic Means (in Percent) of Each Anion.



Figure 6-4. Piper plot of surface water at the Niagara Sanitation Landfill.



Figure 6-5. Piper plot of fill wells at the Niagara Sanitation Landfill.



Figure 6-6. Piper plot of upper sand deposit wells at the Niagara Sanitation Landfill.



Figure 6-7. Piper plot of the upper clay aquitard well at the Niagara Sanitation Landfill. This plot also shows two nearby upper sand wells.



Figure 6-8. Piper plot of lower sand deposit wells at the Niagara Sanitation Landfill.



Figure 6-9. Piper plot of glacial till deposit wells at the Niagara Sanitation Landfill.



Figure 6-10. Piper plot of upper Camillus Shale bedrock wells in the Tonawanda Area.



Figure 6-11. Piper plot of Lockport Dolostone bedrock wells in the Niagara Falls Area.



Figure 7-1. Hydrograph for Representative Wells from All Hydrogeologic Zones at the Niagara Sanitation Landfill Site. Solid lines denote the fill/upper sand wells, the dotted line denotes the upper clay aquitard well; the gray open symbols with a solid line denote the lower sand well; and the dashed lines denote the glacial till wells.



# **TABLES**



Department of Environmental Conservation

# Table 3-1Average Monthly Precipitation and Evapotranspiration DataNYSDEC Hydrogeologic Evaluation ReportNiagara Sanitation Site, Site No. 932054Wheatfield, New York

Month	Average Monthly Precipitation 1985-2015 (inches)	Average Monthly Precipitation 2016-2022 (inches)	Monthly Precipitation 2017 (inches)	Monthly Precipitation 2019 (inches)	Monthly Precipitation 2020 (inches)	Monthly Precipitation 2021 (inches)	Potential Evapotranspiration (Staubitz and Miller, 1987)
January	3.14	3.19	2.92	5.71	2.72	1.85	0.46
February	2.57	3.11	2.26	3.28	2.50	2.06	0.43
March	2.84	2.89	4.36	2.73	3.20	1.92	0.89
April	3.20	3.49	6.38	3.07	3.54	2.77	1.69
May	3.43	3.19	6.35	3.53	3.87	1.63	3.13
June	3.64	2.73	2.21	4.60	3.55	1.77	4.26
July	3.22	3.38	4.65	1.83	3.42	7.49	5.31
August	3.21	3.31	3.15	3.62	2.10	3.68	4.32
September	3.94	4.22	3.17	6.28	3.40	5.28	2.55
October	3.96	4.87	5.01	5.83	3.60	6.14	1.51
November	3.70	3.57	5.09	1.97	2.81	3.28	0.71
December	3.77	3.86	2.93	5.37	4.96	2.46	0.48
Totals	40.62	41.81	48.48	47.82	39.67	40.33	25.74

#### Notes:

From monthly precipitation data measured at the National Weather Service Station at the Buffalo Niagara International Airport.



Department of Environmental Conservation

# Table 4-1 Stratigraphic Sequence of Western New York Compiled from Buehler and Tesmer (1963) and Brett et al. (1995). NYSDEC Hydrogeologic Evaluation Report Niagara Sanitation Site, Site No. 932054 Wheatfield, New York

Epoch	Group	Formation	Member
		Moscow Shale	Windom Shale Kashong Shale
	Hamilton	Ludlowville Formation	Tichenor Limestone Wanakah Shale Ledyard Shale Centerfield Limestone
Middle Devonian		Skaneateles Formation	Levanna Shale Stafford Limestone
		Marcellus Shale	Oatka Creek Shale
		Onondaga Limestone	Seneca Limestone Morehouse Limestone Nedrow Limestone Clarence Limestone Edgecliff Limestone
		Akron Dolostone	
Late Silurian	Salina	Bertie Dolostone	Williamsville Dolostone Scajaquada Dolostone Falkirk Dolostone Oatka Dolostone
		Camillus Shale Syracuse Formation Vernon Shale	
		Guelph Dolostone Eramosa Dolostone	
	Lockport	Goat Island Dolostone	Vinemount Dolostone Ancaster Dolostone Niagara Falls Dolostone
		Gasport Limestone	Pekin Dolostone Gothic Hill Limestone
Middle Silurian		Decew Dolostone	
		Rochester Shale	Burleigh Hill Shale Lewiston Shale
	Clinton	Irondequoit Limestone Rockway Dolostone Williamson Shale Merritton Limestone	
		Reynales Limestone	Hickory Corners Limestone
Early Silurian	Medina	Neahga Shale Kodak Sandstone Cambria Shale Thorold Sandstone Grimsby Formation Devils Hole Shale Power Glen Shale Whirlpool Sandstone	
Late Ordovician	Richmond	Queenston Shale Oswego Sandstone	



Boring	Coordi	nates *	Total	Ground ● Surface		Fill Materia Reworked S	l & Soil	Brown Silt & Clay Deposit		/ Deposit	U	pper Sand D	eposit
Number	Latitude	Longitude	Depth	Elevation (ft. amsl)	Depth	Surface Elevation	Thickness	Depth	Surface Elevation	Thickness	Depth	Surface Elevation	Thickness
					1985 P	hase II Inves	tigation						
OW-1	43.069455	-78.854876	10.0	577.31				Same strat	tigraphic log	as well OW-1B			
OW-1B	43.069447	-78.854900	68.6	577.41				0.0	577.41	3.0			
OW-2	43.069495	-78.855536	14.0	576.37				0.0	576.37	2.0	2.0	574.37	3.0
OW-3	43.068537	-78.854823	68.7	577.28	0.0	577.28	5.0						
OW-4	43.069497	-78.858149	70.3	577.04	0.0	577.04	3.0	3.0	574.04	3.0	6.0	571.04	2.0
OW-5	43.068641	-78.859017	70.0	578.37							0.0	578.37	8.0
OW-6	43.068793	-78.860548	66.0	579.69	0.0	579.69	3.0				3.0	576.69	6.0
				198	9 Supplem	ental Phase	II Investigatio	n					
OW-11	43.069089	-78.855270	12.0	576.24	0.0	576.24	> 12.0						
OW-12	43.068924	-78.855244	34.0	576.94	0.0	576.94	5.0				5.0	571.94	1.5
OW-13	43.068961	-78.855806	6.0	575.52							1.5	574.02	3.5
OW-14A	43.069420	-78.855733	40.0	576.73							0.0	576.73	7.0
OW-14B	43.069330	-78.855709	10.0	576.91									
OW-15	43.069471	-78.858174	45.0	577.14				0.0	577.14	3.0	3.0	574.14	3.0
OW-16	43.068802	-78.860514	10.0	579.23	0.0	579.23	8.0						
					2013 S	ite Characte	rization						
SB-A/OW-24	43.068690	-78.855240	20.0	578.06	0.0	578.06	**						
SB-B/OW-25	43.068995	-78.855197	20.0	577.50	0.0	577.50	10.0				10.0	567.50	1.0
SB-C/OW-22	43.068882	-78.854962	12.0	577.45	0.0	577.45							
SB-D/OW-21	43.069158	-78.854797	12.0	577.71				0.0	577.71	1.0	1.0	576.71	6.0
SB-E	43.069356	-78.854903	12.0	577.20	0.0	577.20	4.0				4.0	573.20	4.0
SB-F/OW-23	43.068793	-78.855565	8.0	577.16				0.0	577.16	1.0	1.0	576.16	5.0
SB-G	43.068947	-78.856527	8.0	577.40	0.0	577.40	4.0				4.0	573.40	3.0
SB-H	43.069049	-78.855222	10.0	576.75	0.0	576.75	> 10.0						
SB-I	43.068917	-78.855105	8.0	578.20	0.0	578.20	2.0				2.0	576.20	5.0
SB-J	43.069044	-78.855312	16.0	577.00	0.0	577.00	2.5				2.5	574.50	7.5
SB-K	43.068768	-78.855234	8.0	579.00	0.0	579.00	2.0				2.0	577.00	4.0
SB-L	43.068846	-78.855227	8.0	578.50				0.0	578.50	4.0	4.0	574.50	2.0
SB-M	43.069045	-78.855149	12.0	576.90	0.0	576.90	8.0						



Boring	Gray-B	rown Silty C	lay Deposit	Red-Gr	ay Layered C	lay Deposit	Lo	ower Sand Do	eposit	Glacial Till			Dolostor	ne Bedrock
Number	Depth	Surface Elevation	Thickness	Depth	Surface Elevation	Thickness	Depth	Surface Elevation	Thickness	Depth	Surface Elevation	Thickness	Depth	Surface Elevation
						1985 Phase	II Investig	ation						
OW-1						Same s	tratigraphi	c log as well	OW-1B					
OW-1B	3.0	574.41	7.0	10.0	567.41	28.0				38.0	539.41	30.6	68.6	508.81
OW-2	5.0	571.37	7.0	12.0	564.37	> 2.0								
OW-3	5.0	572.28	3.0	8.0	569.28	18.5	26.3	550.98	0.2	26.5	550.78	42.2	68.7	508.58
OW-4	8.0	569.04	6.0	14.0	563.04	26.0	40.0	537.04	5.0	45.0	532.04	25.3	70.3	506.74
OW-5	8.0	570.37	5.0	13.0	565.37	29.0	42.0	536.37	3.0	45.0	533.37	24.8	69.8	508.57
OW-6	9.0	570.69	2.0	11.0	568.69	33.0				44.0	535.69	22.0	66.0	513.69
					1989	9 Supplementa	I Phase II I	nvestigation	l					
OW-11														
OW-12	6.5	570.44	4.2	10.7	566.24	19.3	30.0	546.94	> 4.0					
OW-13	5.0	570.52	> 1.0											
OW-14A	7.0	569.73	4.0	11.0	565.73	22.0	33.0	543.73	3.0	36.0	540.73	> 4.0		
OW-14B														
OW-15	6.0	571.14	4.0	10.0	567.14	29.0	39.0	538.14	4.5	43.5	533.64	> 1.5		
OW-16	8.0	571.23	> 2.0											
						2013 Site C	haracteriz	ation						
SB-A/OW-24														
SB-B/0W-25	11.0	566.50	> 9.0											
SB-C/OW-22	8.0	569.45	> 4.0											
SB-D/OW-21	7.0	570.71	> 5.0											
SB-E	8.0	569.20	> 4.0											
SB-F/OW-23	6.0	571.16	> 2.0											
SB-G	7.0	570.40	> 1.0											
SB-H														
SB-I	7.0	571.20	> 1.0											
SB-J	10.0	567.00	2.0	12.0	565.00	> 4.0								
SB-K	6.0	573.00	> 2.0											
SB-L	6.0	572.50	> 2.0											
SB-M	8.0	568.90	> 4.0											



Boring	Coord	linates	Total	Ground		Fill Materia Reworked S	l & Soil	Brown Silt & Clay Deposit		/ Deposit	U	pper Sand D	eposit
Number	Latitude	Longitude	Depth	Elevation	Depth	Surface Elevation	Thickness	Depth	Surface Elevation	Thickness	Depth	Surface Elevation	Thickness
				201	L4 Supplem	nental Site C	haracterizatior	ı					
SB-N	43.068473	-78.856715	8.0	577.25				0.0	577.25	2.0	2.0	575.25	4.0
SB-O	43.068676	-78.856112	8.0	577.25				0.0	577.25	3.0	3.0	574.25	3.0
SB-P	43.069003	-78.856958	8.0	577.00	0.0	577.00	2.0	2.0	575.00	2.0	4.0	573.00	2.0
SB-Q	43.069370	-78.857714	12.0	577.50	0.0	577.50	2.0	2.0	575.50	2.0	4.0	573.50	4.0
SB-R	43.068368	-78.855732	8.0	577.50				0.0	577.50	4.0	4.0	573.50	1.0
SB-S/OW-31	43.068356	-78.854756	8.0	577.71				0.0	577.71	1.0	1.0	576.71	5.0
SB-T/OW-32	43.068678	-78.858920	12.0	578.56	0.0	578.56	3.0				3.0	575.56	8.0
SB-U	43.068756	-78.858189	12.0	578.10	0.0	578.10	4.0				4.0	574.10	6.0
SB-V	43.068862	-78.858074	12.0	577.75	0.0	577.75	5.0				5.0	572.75	5.0
SB-W/OW-33	43.069025	-78.857664	12.0	579.83	0.0	579.83	4.0				4.0	575.83	7.0
SB-X	43.068359	-78.858326	12.0	575.75	0.0	575.75	3.5				3.5	572.25	7.5
SB-Y/OW-34	43.068330	-78.859949	16.0	579.00				0.0	579.00	4.0	4.0	575.00	11.0
SB-Z	43.068313	-78.860732	12.0	578.00	0.0	578.00	3.5				3.5	574.50	4.5
SB-AA	43.068316	-78.861153	12.0	586.00	0.0	586.00	> 12.0						
SB-BB/OW-35	43.069245	-78.859788	12.0	578.80				0.0	578.80	4.0	4.0	574.80	5.0
SB-CC	43.069426	-78.860316	6.0	578.75	0.0	578.75	> 6.0						
SB-DD/OW-36	43.069399	-78.860326	12.0	578.81	0.0	578.81	6.0				6.0	572.81	2.0
SB-EE	43.069335	-78.860222	8.0	578.00	0.0	578.00	4.0	4.0	574.00	2.5	6.5	571.50	0.5
SB-FF	43.068814	-78.860090	12.0	578.00	0.0	578.00	1.0				1.0	577.00	10.0
SB-GG	43.068861	-78.860443	12.0	580.10	0.0	580.10	6.0				6.0	574.10	4.0
SB-HH	43.069029	-78.860448	12.0	578.50	0.0	578.50	6.0				6.0	572.50	4.0
SB-II/OW-37	43.069458	-78.858134	8.0	577.32	0.0	577.32	4.0				4.0	573.32	2.0
SB-JJ	43.069020	-78.858865	12.0	578.10	0.0	578.10	0.5	0.5	577.60	3.5	4.0	574.10	6.0
SB-KK	43.069127	-78.859141	8.0	578.50	0.0	578.50	4.0				4.0	574.50	3.5
					2017 Re	emedial Inve	stigation						
OW-14BR	43.069546	-78.855775	8.0	577.18				0.0	577.18	1.0	1.0	576.18	6.0
LSB-01			6.0	576.50				0.0	576.50	1.5	1.5	575.00	3.8
LSB-02			12.0	577.60	0.0	577.60	9.5						
LSB-03			6.0	577.00							0.0	577.00	4.0
LPZ-01S	43.069535	-78.856600	7.0	577.25				0.0	577.25	1.0	1.0	576.25	4.9
LPZ-02S	43.069009	-78.856784	6.0	577.66				0.0	577.66	1.5	1.5	576.16	4.3
LPZ-03S	43.068198	-78.860660	18.0	577.86				0.0	577.86	1.0	1.0	576.86	7.0



Boring	Gray-B	rown Silty C	lay Deposit	Red-Gra	ay Layered C	lay Deposit	Lo	ower Sand D	eposit	Glacial Till			Dolostor	e Bedrock
Number	Depth	Surface Elevation	Thickness	Depth	Surface Elevation	Thickness	Depth	Surface Elevation	Thickness	Depth	Surface Elevation	Thickness	Depth	Surface Elevation
					201	4 Supplementa	al Site Chai	racterization						
SB-N	6.0	571.25	> 2.0											
SB-O	6.0	571.25	> 2.0											
SB-P	6.0	571.00	> 2.0											
SB-Q	8.0	569.50	> 4.0											
SB-R	5.0	572.50	> 3.0											
SB-S/OW-31	6.0	571.71	> 2.0											
SB-T/OW-32	11.0	567.56	> 1.0											
SB-U	10.0	568.10	> 2.0											
SB-V	10.0	567.75	> 2.0											
SB-W/OW-33	11.0	568.83	> 1.0											
SB-X	11.0	564.75	> 1.0											
SB-Y/OW-34	15.0	564.00	> 1.0											
SB-Z	8.0	570.00	> 4.0											
SB-AA														
SB-BB/OW-35	9.0	569.80	> 3.0											
SB-CC														
SB-DD/OW-36	8.0	570.81	> 4.0											
SB-EE	7.0	571.00	> 1.0											
SB-FF	11.0	567.00	> 1.0											
SB-GG	10.0	570.10	> 2.0											
SB-HH	10.0	568.50	> 2.0											
SB-II/OW-37	6.0	571.32	> 2.0											
SB-JJ	10.0	568.10	> 2.0											
SB-KK	7.5	571.00	> 0.5											
						2017 Remea	lial Investi	gation						
OW-14BR	7.0	570.18												
LSB-01	5.3	571.20												
LSB-02	9.5	568.10												
LSB-03	4.0	573.00												
LPZ-01S	5.9	571.35												
LPZ-02S	5.75	571.91												
LPZ-03S	8.0	569.86	8.0	16.0	561.86	> 2.0								



Boring	Coord	linates	Total	Ground		Fill Materia Reworked	ıl & Soil	Brov	vn Silt & Clay	/ Deposit	U	pper Sand D	eposit
Number	Latitude	Longitude	Depth	Elevation	Depth	Surface Elevation	Thickness	Depth	Surface Elevation	Thickness	Depth	Surface Elevation	Thickness
				20:	17 Remedia	al Investigati	ion (continued	)					
LPZ-04S	43.068220	-78.859642	6.0	576.87				0.0	576.87	1.0	1.0	575.87	> 5.0
LPZ-05S	43.068193	-78.858399	8.0	577.33				0.0	577.33	0.5	0.5	576.83	5.5
LPZ-06S	43.068187	-78.857203	18.0	578.03				0.0	578.03	1.0	1.0	577.03	7.0
LPZ-07S	43.068139	-78.856388	8.0	577.43				0.0	577.43	0.5	0.5	576.93	6.0
LPZ-08S	43.068842	-78.855921	6.0	575.95	0.0	575.95	3.0				3.0	572.95	1.0
LPZ-09S	43.069109	-78.858825	10.0	578.12	0.0	578.12	4.0				4.0	574.12	4.0
LPZ-10S	43.068511	-78.855143	8.0	577.41	0.0	577.41	4.4				4.4	573.01	0.4
LPZ-11S	43.069523	-78.857335	8.0	577.65	0.0	577.65	2.0				2.0	575.65	5.0
LPZ-12S	43.069538	-78.859457	8.0	577.09	0.0	577.09	5.0				5.0	572.09	1.0
LPZ-13S	43.068658	-78.857154	8.0	578.75	0.0	578.75	3.0				3.0	575.75	4.4
LDP-01	43.067974	-78.856667	5.3	576.92				0.0	576.92	1.6	1.6	575.32	> 3.7
LDP-02	43.067965	-78.855737	5.3	577.46				0.0	577.46	1.6	1.6	575.86	> 3.7
LDP-03	43.067970	-78.854756	5.1	577.25				0.0	577.25	1.0	1.0	576.25	3.9
LDP-04	43.069556	-78.860639	5.3	578.15	0.0	578.15	2.3	2.3	575.85	0.8	3.1	575.05	> 2.2
				202:	1 Suppleme	ental Remed	ial Investigatio	on					
LPZ-14S			12.0		0.0	0.00	4.0				4.0	-4.00	4.0
LPZ-15S			12.0		0.0	0.00	3.0				3.0	-3.00	4.5
LPZ-16S						0.00	0.0		0.00	0.0		0.00	0.0
LPZ-17S						0.00	0.0		0.00	0.0		0.00	0.0
LPZ-18S						0.00	0.0		0.00	0.0		0.00	0.0

Notes:

\* = Coordinates are from the LiRo surveyed completed during the 2017 Remedial Investigation.

• = Ground surface elevations for the monitoring wells are from Table 4-1 of the LiRo RI Report dated February 2019.

Depths in feet below ground surface.

---- = Indicates that the deposit was not encountered or identifed in the stated soil boring log.

Blue Shaded Boring: Located within the limits of the 2014/2015 IRM excavation.

Green Shaded Elevation: Estimated by adding the average elevation difference between the Engineering-Science & LiRo Surveys to the Engineering-Science elevation. This well was destroyed during the OCC IRM.

Orange Shaded Coordinate: From the GES Site Characterization Report dated November 2013.

Yellow Shaded Coordinate: From the GES Site Characterization Report dated June 2014.

Yellow Shaded Elevation: Estimated on November 1 & 2, 2022 from LiRo's Ground Surface Topography Map (Figure 2-3 of the RI Report) with the well layers turned on.

Gray Shaded Depth: The silt & clay deposit was described as gray instead of brown.



Boring	Gray-B	rown Silty C	lay Deposit	Red-Gr	ay Layered C	lay Deposit	Lo	ower Sand D	eposit	Glacial Till			Dolostor	ne Bedrock
Number	Depth	Surface Elevation	Thickness	Depth	Surface Elevation	Thickness	Depth	Surface Elevation	Thickness	Depth	Surface Elevation	Thickness	Depth	Surface Elevation
					201	7 Remedial Inv	vestigation	(continued)						
LPZ-04S														
LPZ-05S	6.0	571.33	> 2.0											
LPZ-06S	8.0	570.03	> 2.0											
LPZ-07S	6.5	570.93	> 4.0											
LPZ-08S	4.0	571.95	> 3.0											
LPZ-09S	8.0	570.12	> 2.0											
LPZ-10S	4.8	572.61	> 1.0											
LPZ-11S	7.0	570.65	> 2.0											
LPZ-12S	6.0	571.09	> 2.0											
LPZ-13S	7.4	571.35	> 1.0											
LDP-01														
LDP-02														
LDP-03	4.9	572.35	> 4.0											
LDP-04														
					2021	Supplementa	l Remedial	Investigatio	n					
LPZ-14S	8.0	-8.00	> 2.0											
LPZ-15S	7.5	-7.50	> 2.0											
LPZ-16S		0.00	> 2.0											
LPZ-17S		0.00	> 4.0											
LPZ-18S														



Notes (continued):

Orange Shaded Depth: Laminated gray-red clay is identified above fill material. This is likely reworked soil from the excavation of the disposal pit.

\*\* = Poor to no recovery from 4.0' to 20' depth.

**=** = No recovery from 4' to 8' depth so it is not certain if the upper sand deposit is present at this location.

Boring SB-L was completed in an area of the IRM excavation that went to 30 feet depth. Since this boring was only completed to 8 feet depth, and since records indicate that 12 feet of soil was placed over the top of the LaSalle Expressway wastes, this boring likely only encountered reworked soils. The boring log, however, does show layered deposits.

NEW YORK STATE Conservation

# Table 4-3 Summary of Grain Size Analyses NYSDEC Hydrogeologic Report Niagara Sanitation Site, Site No. 932054 Wheatfield, New York



Department of Environmental Conservation

Boring Number	Depth (ft)	Gravel (%)	Sand (%)	Silt (%)	Clay (%)	Unified Soil Classification	Stratigraphic Unit
<u></u>	•			Rework	ed Soil		
OW-11	2.0 - 4.0	14.8	20.8	66.8	4.6	ML	red-gray clay (reworked)
OW-16	2.0 - 4.0	0.1	66.9	26.2	6.8	SM	brown clay (reworked)
OW-16	6.0 - 8.0	26.9	26.6	25.3	21.2	GM	gray-brown silt (reworked)
Arit	thmetic Mean:	13.93	38.10	39.43	10.87		
Geo	ometric Mean:	3.41	33.33	35.38	8.72		
			Bro	own Silt & (	Clay Deposi	it	
OW-1	2.0 - 4.0	0.0	18.0	59.0	23.0	ML	brown silt & clay
				Upper San	d Deposit		
OW-5	5.0 - 7.0	0.0	84.0	16.	.0 *	SW	upper sand lens
OW-13	2.0 - 4.0	0.3	87.6	12.	1 *	SM	upper sand lens
OW-14B	4.0 - 6.0	0.0	74.4	23.2	2.4	SM	upper sand lens
Arit	thmetic Mean:	0.10	82.00	23.20	2.40		
Geo	ometric Mean:	N/A	81.81	23.20	2.40		
	-		Gray	Brown Silt	y Clay Dep	osit	
OW-4	12.0 - 13.0	0.0	0.0	14.0	86.0	CL	gray-brown silty clay
OW-12	5.0 - 7.0	0.3	6.7	69.8	23.2	ML	gray-brown silty clay
OW-13	4.0 - 6.0	0.1	4.8	95.	.1 *	ML	gray-brown silty clay
Arit	thmetic Mean:	0.13	3.83	41.90	54.60		
Geo	ometric Mean:	N/A	N/A	31.26	44.67		
			Red-G	aray Layere	d Clay Dep	osit	
OW-4	30.0 - 32.0	0.0	0.0	24.0	76.0	CL	red-gray layered clay
OW-12	20.0 - 22.0	0.0	0.9	15.1	84.0	CL	red-gray layered clay
OW-14A	25.0 - 27.0	0.0	0.3	13.7	86.0	CL	red-gray layered clay
OW-15	15.0 - 17.0	0.0	0.6	16.4	83.0	CL	red-gray layered clay
Arit	hmetic Mean:	0.00	0.45	17.30	82.25		
Geo	ometric Mean:	N/A	N/A	16.89	82.16		
				Lower San	d Deposit		
OW-4	44.6 - 45.0	0.0	65.0	35.	.0 *	SP	lower sand lens
OW-12	30.0 - 32.0	10.2	32.5	57.	.3 *	ML	lower sand lens
OW-15	42.0 - 44.0	18.3	30.4	39.2	12.1	ML	lower sand lens
Arit	thmetic Mean:	9.50	42.63	39.20	12.10		
Geo	ometric Mean:	N/A	40.05	39.20	12.10		
	1			Glacial Till	Deposit		
OW-1B	50.0 - 51.5	10.0	30.0	60.	.0 *	ML	glacial till
OW-6	60.0 - 60.5	15.0	19.0	66.	.0 *	ML	glacial till
OW-14A	36.0 - 38.0	15.3	34.7	11.4	39.1	CL	glacial till
Arit	hmetic Mean:	13.43	27.90	11.40	39.10		
Geo	ometric Mean:	13.19	27.04	11.40	39.10		

## Table 4-3 Summary of Grain Size Analyses NYSDEC Hydrogeologic Report Niagara Sanitation Site, Site No. 932054 Wheatfield, New York



Department of Environmental Conservation

#### Notes:

- \* = Percentage of clay and silt combined.
- Green shaded stratigraphic unit was originally described as brown/gray silty clay. A review of the boring log indicates that this is the deposit that overlies the upper sand deposit.
- Gray shaded stratigraphic unit was originally described as fill. A review of the boring log indicates that this deposit is reworked red-gray clay.
- Blue shaded stratigraphic unit was originally described as glacial till. A review of the boring log suggests that this deposit is the lower sand.
- Yellow shaded stratigraphic unit was originally described as brown/gray silty clay. This sample is above the one where trash was present so it must be reworked.
- Orange shaded stratigraphic unit was originally described as the upper sand lens. At that depth, the log indicates that trash was present.

# Table 5-1 Construction Summary of Existing and Decommissioned Wells at the Niagara Sanitation Landfill NYSDEC Hydrogeologic Report Niagara Sanitation Site, Site No. 932054 Wheatfield, New York



Department of Environmental Conservation

Well Number	Ground ● Surface Elevation	Top of ● Riser Elevation	Total Boring Depth	Sandpack Interval (ft. BGS)	Sandpack Interval (ft. amsl)	Well Screen Interval (ft. BGS)	Well Screen Interval (ft. amsl)	Screened Water-Bearing Zone
	(ft. amsl)	(ft. amsl)	(ft. BGS)					
					Upper Sand Deposit			
OW-1	577.31	578.30	10.0	4.0 to 10.0	573.31 to 567.31	4.0 to 9.0	573.31 to 568.31	Silty Clay with Sand Seams
<del>0W-11</del>	<del>576.40</del>	<del>579.04</del>	<del>12.0</del>	<del>5.0</del> to 9.0	<del>571.40</del> to 567.40	<del>7.0</del> to 9.0	<del>569.40</del> to 567.40	Fill/Reworked Soil
OW-13	575.52	579.33	6.0	2.5 to 5.0	573.02 to 570.52	3.0 to 5.0	572.52 to 570.52	Upper Sand
OW-14B	576.91	579.92	10.0	2.5 to 7.0	574.41 to 569.91	3.0 to 7.0	573.91 to 569.91	Upper Sand
OW-14BR	577.18	580.03	8.0	4.0 to 7.0	573.18 to 570.18	5.0 to 7.0	572.18 to 570.18	Upper Sand
OW-16	579.23	581.88	10.0	4.0 to 10.0	575.23 to 569.23	5.0 to 10.0	574.23 to 569.23	Fill/Silty Clay
OW-21	577.71	580.00	12.0	2.5 to 8.0	575.21 to 569.71	3.0 to 8.0	574.71 to 569.71	Upper Sand/Silty Clay
OW-22	577.45	579.46	12.0	2.5 to 8.0	574.95 to 569.45	3.0 to 8.0	574.45 to 569.45	Fill/Upper Sand?
OW-23	577.16	579.26	8.0	2.5 to 8.0	574.66 to 569.16	3.0 to 8.0	574.16 to 569.16	Upper Sand/Silty Clay
<del>0W-24</del>	<del>577.92</del>	<del>581.00</del>	<del>20.0</del>	4.0 to 10.0	<del>573.92</del> to 567.92	<del>5.0</del> to 10.0	572.92 to 567.92	Fill
<del>0W-25</del>	<del>577.36</del>	<del>579.91</del>	<del>20.0</del>	<del>5.0</del> to 12.0	<del>572.36</del> to 565.36	<del>7.0</del> to 12.0	570.36 to 565.36	Upper Sand/Silty Clay
OW-31	577.71	580.64	8.0	1.0 to 6.0	576.71 to 571.71	1.0 to 6.0	576.71 to 571.71	Upper Sand
OW-32	578.56	581.44	12.0	4.0 to 10.0	574.56 to 568.56	5.0 to 10.0	573.56 to 568.56	Upper Sand
OW-33	579.83	582.43	12.0	3.0 to 9.0	576.83 to 570.83	4.0 to 9.0	575.83 to 570.83	Fill/Upper Sand
OW-34	579.00	581.10	16.0	5.0 to 12.0	574.00 to 567.00	7.0 to 12.0	572.00 to 567.00	Upper Sand
OW-35	578.80	581.57	12.0	3.0 to 9.0	575.80 to 569.80	4.0 to 9.0	574.80 to 569.80	Fill/Upper Sand
OW-36	578.81	580.95	12.0	2.0 to 8.0	576.81 to 570.81	3.0 to 8.0	575.81 to 570.81	Fill/Upper Sand
OW-37	577.32	580.15	8.0	1.0 to 6.0	576.32 to 571.32	1.0 to 6.0	576.32 to 571.32	Fill/Upper Sand
LPZ-01S	577.25	580.31	7.0	4.0 to 7.0	573.25 to 570.25	5.0 to 7.0	572.25 to 570.25	Upper Sand/Silty Clay
LPZ-02S	577.66	581.03	6.0	2.0 to 6.0	575.66 to 571.66	3.0 to 6.0	574.66 to 571.66	Upper Sand/Silty Clay
LPZ-03S	577.86	581.16	18.0	2.0 to 8.0	575.86 to 569.86	3.0 to 8.0	574.86 to 569.86	Upper Sand/Silty Clay
LPZ-04S	576.87	579.68	6.0	2.0 to 6.0	574.87 to 570.87	3.0 to 6.0	573.87 to 570.87	Upper Sand/Silty Clay
LPZ-05S	577.33	580.41	8.0	2.0 to 6.0	575.33 to 571.33	3.0 to 6.0	574.33 to 571.33	Upper Sand/Silty Clay
LPZ-06S	578.03	581.00	18.0	2.0 to 8.0	576.03 to 570.03	3.0 to 8.0	575.03 to 570.03	Upper Sand/Silty Clay

# Table 5-1 Construction Summary of Existing and Decommissioned Wells at the Niagara Sanitation Landfill NYSDEC Hydrogeologic Report Niagara Sanitation Site, Site No. 932054 Wheatfield, New York



Department of Environmental Conservation

Well Number	Ground • Surface Elevation (ft_amsl)	Top of ● Riser Elevation (ft_amsl)	Total Boring Depth (ft BGS)	Sandpack Interval (ft. BGS)	Sandpack Interval (ft. amsl)	Well Screen Interval (ft. BGS)	Well Screen Interval (ft. amsl)	Screened Water-Bearing Zone
	(10. 01131)	(11. 01131)	(11. 003)	linne	r Sand Denosit (Continu	l		
LPZ-07S	577.43	580.56	8.0	2.0 to 7.0	575.43 to 570.43	3.0 to 7.0	574.43 to 570.43	Upper Sand/Silty Clay
LPZ-08S	575.95	579.47	6.0	2.0 to 4.0	573.95 to 571.95	2.5 to 4.0	573.45 to 571.95	Upper Sand
LPZ-09S	578.12	581.51	10.0	3.0 to 8.0	575.12 to 570.12	4.0 to 8.0	574.12 to 570.12	Upper Sand
LPZ-10S	577.41	580.38	8.0	3.0 to 6.0	574.41 to 571.41	4.0 to 6.0	573.41 to 571.41	Upper Sand
LPZ-11S	577.65	579.96	8.0	3.0 to 7.0	574.65 to 570.65	4.0 to 7.0	573.65 to 570.65	Upper Sand
LPZ-12S	577.09	580.03	8.0	3.0 to 7.0	574.09 to 570.09	3.0 to 7.0	574.09 to 570.09	Fill/Upper Sand
LPZ-13S	578.75	581.66	8.0	4.0 to 7.5	574.75 to 571.25	5.0 to 7.5	573.75 to 571.25	Upper Sand
LPZ-14S	579.68	582.13	12.0	3.0 to 12.0	576.68 to 567.68	4.0 to 9.0	575.68 to 570.68	Upper Sand
LPZ-15S	579.02	581.43	12.0	2.5 to 12.0	576.52 to 567.02	3.0 to 8.0	576.02 to 571.02	Upper Sand
LPZ-16S	577.76	580.13	16.0	3.0 to 16.0	574.76 to 561.76	5.0 to 15.0	572.76 to 562.76	Upper Sand/Silty Clay
LPZ-17S	576.69	579.45	18.0	3.0 to 18.0	573.69 to 558.69	5.0 to 15.0	571.69 to 561.69	Upper Sand/Silty Clay
LPZ-18S	578.66	581.90	16.0	3.0 to 16.0	575.66 to 562.66	5.0 to 15.0	573.66 to 563.66	Upper Sand/Silty Clay
LDP-01	576.92	580.34	5.3	3.3 to 5.3	573.62 to 571.62	4.3 to 5.3	572.62 to 571.62	Upper Sand
LDP-02R ♦	<del>577.46</del>	<del>581.03</del>	<del>5.3</del>	<del>3.3</del> to 5.3	<del>574.16</del> to 572.16	4.3 to 5.3	<del>573.16</del> to 572.16	Upper Sand/Silty Clay
LDP-03	577.25	580.73	5.1	2.4 to 5.1	574.85 to 572.15	4.1 to 5.1	573.15 to 572.15	Upper Sand/Silty Clay
LDP-04	578.15	581.42	5.3	3.3 to 5.3	574.85 to 572.85	4.3 to 5.3	573.85 to 572.85	Upper Sand
				Silty Cl	ay & Red-Gray Clay Aqu	uitard		
OW-2	576.37	577.26	14.0	5.0 to 14.0	571.37 to 562.37	9.0 to 14.0	567.37 to 562.37	Silty Clay/Red-Gray Clay
					Lower Sand Deposit			
<del>0W-12</del>	<del>577.10</del>	<del>579.74</del>	<del>34.0</del>	27.5 to 32.5	549.60 to 544.60	<del>29.5</del> to 32.5	547.60 to 544.60	Lower Sand
OW-14A	576.73	580.05	40.0	32.5 to 36.5	544.23 to 540.23	33.5 to 36.5	543.23 to 540.23	Lower Sand
OW-15	577.14	579.56	45.0	38.0 to 45.0	539.14 to 532.14	40.0 to 45.0	537.14 to 532.14	Lower Sand

### Table 5-1 Construction Summary of Existing and Decommissioned Wells at the Niagara Sanitation Landfill NYSDEC Hydrogeologic Report Niagara Sanitation Site, Site No. 932054 Wheatfield, New York



Department of Environmental Conservation

Well Number	Ground ● Surface Elevation (ft. amsl)	Top of ● Riser Elevation (ft. amsl)	Total Boring Depth (ft. BGS)	Sandpack Interval (ft. BGS)	Sandpack Interval (ft. amsl)	Well Screen Interval (ft. BGS)	Well Screen Interval (ft. amsl)	Screened Water-Bearing Zone
					Glacial Till Deposit			
OW-1B	577.41	579.14	68.6	55.0 to 68.6	522.41 to 508.81	58.6 to 68.6	518.81 to 508.81	Glacial Till
OW-3	577.28	579.56	68.7	43.0 to 55.0	534.28 to 522.28	45.0 to 55.0	532.28 to 522.28	Glacial Till
OW-4	577.04	579.45	70.3	56.0 to 69.0	521.04 to 508.04	59.0 to 69.0	518.04 to 508.04	Glacial Till
OW-5	578.37	579.75	70.0	56.0 to 70.0	522.37 to 508.37	60.0 to 70.0	518.37 to 508.37	Glacial Till
OW-6	579.69	582.36	66.0	55.0 to 66.0	524.69 to 513.69	56.0 to 66.0	523.69 to 513.69	Glacial Till
					Staff Gauges			
SG-1	573.53			to	to	to	to	Northern Boundary Ditch
SG-2	574.11			to	to	to	to	Site Pond (NE Corner)

Notes:

• = Elevations are from the 2019 LiRo Remedial Investigation Report.

ft. amsl = feet above mean sea level.

ft. bgs = Feet below ground surface.

Image: Second damaged in 2019 and was replaced during the 2019/2020 sampling event. Well LDP-02R was found damaged during the 2021 sampling event and was not replaced.

Orange shaded elevations were calculated from available information as the original survey of these wells used as assumed datum. These wells were decommissioned prior to the 2017 LiRo Remedial Investigation.
### Table 5-2A



Department of Environmental Conservation

# Summary of Water Level Measurements: February 8, 1988 To May 20, 2014 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York

Location ID	Measuring Point Elevation <sup>1</sup> (ft amsl <sup>2</sup> )	Measurement Date	Depth to Water (ft)	Water Elevation <sup>1</sup> (feet amsl)	Note			
			Fill/U	Upper Sand We	lls			
OW-11	NA	2/10/1988	8.30	NA	Destroyed prior to October 2017 Survey.			
OW-14B	579.92	2/10/1988	3.20	576.72				
Lower Sand Wells								
OW-15	579.56	2/10/1988	10.80	568.76				

Location ID	Measuring Point Elevation <sup>1</sup> (ft amsl <sup>2</sup> )	Measurement Date	Depth to Water (ft)	Water Elevation <sup>1</sup> (feet amsl)	Note					
	Fill/Upper Sand Wells									
OW-11	NA	2/18/1988	8.50	NA	Destroyed prior to October 2017 Survey.					
OW-13	579.33	2/18/1988	2.80	576.53						
OW-14B	579.92	2/18/1988	3.20	576.72						
OW-16	581.88	2/18/1988	4.80	577.08						
	Lower Sand Wells									
OW-12	NA	2/18/1988	16.90	NA	Destroyed prior to October 2017 Survey.					
OW-14A	580.05	2/18/1988	15.50	564.55						
OW-15	579.56	2/18/1988	10.80	568.76						

Location ID	Measuring Point Elevation <sup>1</sup> (ft amsl <sup>2</sup> )	Measurement Date	Depth to Water (ft)	Water Elevation <sup>1</sup> (feet amsl)	Note				
			Fill/U	Upper Sand We	lls				
OW-01	578.30	6/20/1988	5.30	573.00					
OW-11	NA	6/20/1988	4.60	NA	Destroyed prior to October 2017 Survey.				
OW-14B	579.92	6/20/1988	4.20	575.72					
OW-16	581.88	6/20/1988	6.30	575.58					
	Silty Clay & Red-Gray Clay Aquitard Wells								
OW-02	577.26	6/20/1988	3.90	573.36					
			Lo	wer Sand Wells					
OW-12	NA	6/20/1988	11.50	NA	Destroyed prior to October 2017 Survey.				
OW-14A	580.05	6/20/1988	11.30	568.75					
OW-15	579.56	6/20/1988	11.40	568.16					
	Glacial Till Wells								
OW-03	579.56	6/20/1988	15.00	564.56					
OW-04	579.45	6/20/1988	14.50	564.95					
OW-05	579.75	6/20/1988	15.10	564.65					
OW-06	582.36	6/20/1988	17.30	565.06					
OW-1B	579.14	6/20/1988	14.10	565.04					

### Table 5-2A



Department of Environmental Conservation

# Summary of Water Level Measurements: February 8, 1988 To May 20, 2014 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York

Location ID	Measuring Point Elevation <sup>1</sup> (ft amsl <sup>2</sup> )	Measurement Date	Depth to Water (ft)	Water Elevation <sup>1</sup> (feet amsl)	Note				
			Fill/	Upper Sand We	lls				
OW-11	NA	10/12/1988	4.50	NA	Destroyed prior to October 2017 Survey.				
OW-16	581.88	10/12/1988	8.70	573.18					
			Lo	wer Sand Wells					
OW-14A	580.05	10/12/1988	11.70	568.35					
OW-15	579.56	10/12/1988	11.80	567.76					
	Glacial Till Wells								
OW-03	579.56	10/12/1988	14.40	565.16					
OW-05	579.75	10/12/1988	15.10	564.65					
OW-06	582.36	10/12/1988	17.70	564.66					

Location ID	Measuring Point Elevation <sup>1</sup> (ft amsl <sup>2</sup> )	Measurement Date	Depth to Water (ft)	Water Elevation <sup>1</sup> (feet amsl)	Note				
			Fill/U	Upper Sand We	lls				
OW-01	578.30	8/2/2013	3.09	575.21					
OW-11	NA	8/2/2013	4.29	NA	Destroyed prior to October 2017 Survey.				
OW-13	579.33	8/2/2013	3.06	576.27					
OW-14B	579.92	8/2/2013	3.23	576.69					
OW-16	581.88	8/2/2013	6.18	575.70					
OW-21	580.00	8/2/2013	4.66	575.34					
OW-22	579.46	8/2/2013	3.96	575.50					
OW-23	579.26	8/2/2013	3.68	575.58					
OW-24	NA	8/2/2013	5.20	NA	Destroyed prior to October 2017 Survey				
OW-25	NA	8/2/2013	4.24	NA	Destroyed prior to October 2017 Survey				
	Silty Clay & Red-Gray Clay Aquitard Wells								
OW-02	577.26	8/2/2013	2.17	575.09					

Location ID	Measuring Point Elevation <sup>1</sup> (ft amsl <sup>2</sup> )	Measurement Date	Depth to Water (ft)	Water Elevation <sup>1</sup> (feet amsl)	Note
			Fill/U	Jpper Sand Wel	ls
OW-16	581.88	5/19/2014	4.66	577.22	
OW-31	580.64	5/20/2014	3.80	576.84	
OW-32	581.44	5/19/2014	4.59	576.85	
OW-33	582.43	5/20/2014	6.03	576.40	
OW-34	581.10	5/19/2014	4.00	577.10	
OW-35	581.57	5/19/2014	4.66	576.91	
OW-36	580.95	5/19/2014	3.99	576.96	
OW-37	580.15	5/20/2014	3.50	576.65	

Notes:

1 = Elevations are referenced to North American Vertical Datum of 1988 (NAVD 88).

2 = Above Mean Sea Level.

Green shaded dates are different than those shown in the RI table and were obtained from the original reports.

### Table 5-2B



Department of Environmental Conservation

# Summary of Water Level Measurements: August 2, 2017 To August 15, 2017 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York

Location ID	Measuring Point Elevation <sup>1</sup> (ft amsl <sup>2</sup> )	Measurement Date	Depth to Water (ft)	Water Elevation <sup>1</sup> (feet amsl)	Note
			Fill/	Upper Sand We	lls
OW-01	578.30	8/2/2017	3.98	574.32	
OW-14B	579.92	8/2/2017	11.42	568.50	Outer casing has heaved.
OW-16	581.88	8/2/2017	6.60	575.28	
OW-21	580.00	8/2/2017	5.73	574.27	
OW-31	580.64	8/2/2017	6.74	573.90	
OW-32	581.44	8/2/2017	6.61	574.83	
OW-33	582.43	8/2/2017	7.31	575.12	
OW-34	581.10	8/2/2017	6.51	574.59	
OW-35	581.57	8/2/2017	6.59	574.98	
OW-37	580.15	8/2/2017	5.12	575.03	
			Silty Clay & Re	d-Gray Clay Aq	uitard Wells
OW-02	577.26	8/2/2017	2.62	574.64	
			Lo	wer Sand Wells	
OW-14A	580.05	8/2/2017	14.66	565.39	Depth to water originally listed as 4.66 feet.
			G	lacial Till Wells	
OW-1B	579.14	8/2/2017	13.46	565.68	
OW-03	579.56	8/2/2017	13.94	565.62	
OW-04	579.45	8/2/2017	13.83	565.62	
OW-05	579.75	8/2/2017	14.33	565.42	
OW-06	582.36	8/2/2017	16.89	565.47	Casing tab for lock corroded.

Location ID	Measuring Point Elevation <sup>1</sup> (ft amsl <sup>2</sup> )	Measurement Date	Depth to Water (ft)	Water Elevation <sup>1</sup> (feet amsl)	Note			
			Fill/	Upper Sand We	lls			
OW-01	578.30	8/3/2017	4.20	574.10				
OW-14B	579.92	8/4/2017	4.64	575.28	Outer casing has heaved.			
OW-21	580.00	8/3/2017	5.92	574.08				
OW-31	580.64	8/3/2017	6.99	573.65				
OW-32	581.44	8/3/2017	6.61	574.83				
OW-33	582.43	8/4/2017	6.64	575.79				
OW-35	581.57	8/4/2017	6.74	574.83				
			Silty Clay & Re	d-Gray Clay Aq	uitard Wells			
OW-02	577.26	8/3/2017	2.62	574.64				
	Glacial Till Wells							
OW-04	579.45	8/3/2017	13.83	565.62				
OW-05	579.75	8/3/2017	14.33	565.42				

### Table 5-2B



Department of Environmental Conservation

# Summary of Water Level Measurements: August 2, 2017 To August 15, 2017 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York

Location ID	Measuring Point Elevation <sup>1</sup> (ft amsl <sup>2</sup> )	Measurement Date	Depth to Water (ft)	Water Elevation <sup>1</sup> (feet amsl)	Note
			Fill/U	Upper Sand We	lls
OW-16	581.88	8/7/2017	6.93	574.95	
OW-33	582.43	8/9/2017	7.54	574.89	
OW-34	581.10	8/7/2017	6.12	574.98	See note 1.
OW-37	580.15	8/8/2017	5.18	574.97	
LPZ-02S	581.03	8/8/2017	5.90	575.13	
LPZ-02S	581.03	8/9/2017	5.92	575.11	
LPZ-03S	581.16	8/7/2017	5.70	575.46	
LPZ-04S	579.68	8/7/2017	4.79	574.89	
LPZ-05S	580.41	8/7/2017	5.86	574.55	
LPZ-06S	581.00	8/7/2017	6.23	574.77	
			Silty Clay & Re	d-Gray Clay Aq	uitard Wells
OW-02	577.26	8/8/2017	3.20	574.06	
			Lo	wer Sand Wells	
OW-14A	580.05	8/9/2017	14.87	565.18	See note 2.
OW-15	579.56	8/8/2017	11.79	567.77	Casing tab for lock corroded. May be well OW-14A.
			G	lacial Till Wells	
OW-1B	579.14	8/9/2017	13.45	565.69	
OW-04	579.45	8/8/2017	13.84	565.61	
OW-05	579.75	8/10/2017	14.34	565.41	
OW-06	582.36	8/7/2017	16.84	565.52	Casing tab for lock corroded.

Location ID	Measuring Point Elevation <sup>1</sup> (ft amsl <sup>2</sup> )	Measurement Date	Depth to Water (ft)	Water Elevation <sup>1</sup> (feet amsl)	Note					
	Fill/Upper Sand Wells									
OW-13	579.33	8/15/2017	4.22	575.11	Casing tab for lock corroded & outer casing heaved.					
OW-22	579.46	8/15/2017	5.31	574.15						
OW-23	579.26	8/15/2017	4.35	574.91						
OW-31	580.64	8/15/2017	7.27	573.37						
	Glacial Till Wells									
OW-03	579.56	8/15/2017	13.91	565.65						

Notes:

1 = Elevations are referenced to North American Vertical Datum of 1988 (NAVD 88).

2 = Above Mean Sea Level.

Green shaded dates are different than those shown in the RI table and were obtained from the original reports. Yellow shaded depth to water is far lower that other water levels for this well. This is likely an incorrect reading.

Note 1: This well was originally listed as well OW-33. A review of the water level data indicates that depth to water at well OW-33 is always deeper than in well OW-34. This suggests that this Depth to Water is likely for well OW-34.

Note 2: This well was originally listed as well OW-15. The hydrographs for the lower sand wells suggest that this is well OW-14A.

### Table 5-2C



Department of Environmental Conservation

# Summary of Water Level Measurements: August 21, 2017 To August 22, 2017 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York

Location ID	Measuring Point Elevation <sup>1</sup> (ft amsl <sup>2</sup> )	Measurement Date	Depth to Water (ft)	Water Elevation <sup>1</sup> (feet amsl)	Note			
			Fill/	Upper Sand Wel	ls			
LPZ-03S	581.16	8/21/2017	5.42	575.74				
LPZ-04S	579.68	8/21/2017	5.34	574.34				
LPZ-05S	580.41	8/21/2017	5.25	575.16				
LPZ-06S	581.00	8/21/2017	5.47	575.53				
LPZ-07S	580.56	8/21/2017	5.92	574.64				
			G	lacial Till Wells				
OW-05	579.75	8/21/2017	14.34	565.41				
	Staff Gauges							
SG-01	579.33	8/21/2017	4.20	575.13				
SG-02	579.57	8/21/2017	4.27	575.30				

Location ID	Measuring Point Elevation <sup>1</sup> (ft amsl <sup>2</sup> )	Measurement Date	Depth to Water (ft)	Water Elevation <sup>1</sup> (feet amsl)	Note						
	Fill/Upper Sand Wells										
OW-01	578.30	8/22/2017	3.67	574.63							
OW-13	579.33	8/22/2017	4.06	575.27	Casing tab for lock corroded & outer casing heaved.						
OW-14B	579.92	8/22/2017	4.64	575.28	Outer casing has heaved.						
OW-14BR	580.03	8/22/2017	4.90	575.13							
OW-16	581.88	8/22/2017	6.65	575.23							
OW-21	580.00	8/22/2017	5.48	574.52							
OW-22	579.46	8/22/2017	4.85	574.61							
OW-23	579.26	8/22/2017	4.03	575.23							
OW-31	580.64	8/22/2017	6.33	574.31							
OW-32	581.44	8/22/2017	6.45	574.99							
OW-33	582.43	8/22/2017	7.49	574.94							
OW-34	581.10	8/22/2017	6.47	574.63							
OW-35	581.57	8/22/2017	6.54	575.03							
OW-36	580.95	8/22/2017	5.93	575.02							
OW-37	580.15	8/22/2017	5.06	575.09							
LPZ-01S	580.31	8/22/2017	5.22	575.09							
LPZ-02S	581.03	8/22/2017	5.80	575.23							
LPZ-03S	581.16	8/22/2017	5.42	575.74							
LPZ-04S	579.68	8/22/2017	5.44	574.24	Corrected field recorded DTW from 4.44 to 5.44.						
LPZ-05S	580.41	8/22/2017	5.41	575.00							
LPZ-06S	581.00	8/22/2017	5.55	575.45							
LPZ-07S	580.56	8/22/2017	5.95	574.61							
LPZ-08S	579.47	8/22/2017	4.33	575.14							
	Silty Clay & Red-Gray Clay Aquitard Wells										
OW-02	577.26	8/22/2017	2.11	575.15							
	Lower Sand Wells										
OW-14A	580.05	8/22/2017	20.69	559.36							
OW-15	579.56	8/22/2017	11.72	567.84	Casing tab for lock corroded.						

### Table 5-2C



Department of Environmental Conservation

# Summary of Water Level Measurements: August 21, 2017 To August 22, 2017 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York

Location ID	Measuring Point Elevation <sup>1</sup> (ft amsl <sup>2</sup> )	Measurement Date	Depth to Water (ft)	Water Elevation <sup>1</sup> (feet amsl)	Note			
Glacial Till Wells								
OW-01B	579.14	8/22/2017	14.19	564.95				
OW-03	579.56	8/22/2017	13.81	565.75				
OW-04	579.45	8/22/2017	13.79	565.66				
OW-05	579.75	8/22/2017	14.20	565.55				
OW-06	582.36	8/22/2017	16.80	565.56	Casing tab for lock corroded.			
	Staff Gauges							
SG-01	579.33	8/22/2017	4.15	575.18				
SG-02	579.57	8/22/2017	4.30	575.27				

Notes:

1 = Elevations are referenced to North American Vertical Datum of 1988 (NAVD 88).

## Table 5-2D Summary of Water Level Measurements: August 30, 2017 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York



Department of Environmental Conservation

	Measuring			Water				
Location	Point	Measurement	Depth to	Flevation <sup>1</sup>	Note			
ID	Elevation <sup>1</sup>	Date	Water (ft)	(feet amsl)	note			
	(ft amsl <sup>2</sup> )			(reet anisi)				
Fill/Upper Sand Wells								
OW-01	578.30	8/30/2017	4.19	574.11				
OW-13	579.33	8/30/2017	4.39	574.94	Casing tab for lock corroded & outer casing heaved.			
OW-14B	579.92	8/30/2017	4.97	574.95	Outer casing has heaved.			
OW-14BR	580.03	8/30/2017	5.36	574.67				
OW-16	581.88	8/30/2017	7.25	574.63				
OW-21	580.00	8/30/2017	6.11	573.89				
OW-22	579.46	8/30/2017	5.30	574.16				
OW-23	579.26	8/30/2017	4.56	574.70				
0W-31	580.04	8/30/2017	7.23	573.41				
011-32	582.44	8/30/2017	7.82	574.55				
OW-33	581 10	8/30/2017	6.86	574.01				
OW-35	581.57	8/30/2017	6,90	574.67				
OW-36	580.95	8/30/2017	6.25	574.70				
OW-37	580.15	8/30/2017	5.45	574.70				
LDP-01	580.34	8/30/2017	6.64	573.70	TD = 8.36 (TOIC), BTM Elev = 571.98			
LDP-02	581.03	8/30/2017	6.65	574.38				
LDP-03	580.73	8/30/2017	6.60	574.13				
LDP-04	581.42	8/30/2017	7.20	574.22				
LPZ-01S	580.31	8/30/2017	5.38	574.93				
LPZ-02S	581.03	8/30/2017	6.18	574.85				
LPZ-03S	581.16	8/30/2017	7.06	574.10				
LPZ-04S	579.68	8/30/2017	5.65	574.03				
LPZ-05S	580.41	8/30/2017	6.36	574.05				
LPZ-06S	581.00	8/30/2017	6.62	574.38				
LPZ-07S	580.56	8/30/2017	6.73	5/3.83				
LPZ-08S	579.47	8/30/2017	4.68	5/4./9	5 - 1 - 1 - 1			
		- /	Slity Clay & Re		ultard wells			
OW-02	577.26	8/30/2017	2.52	5/4./4				
			Lo	wer Sand Wells				
OW-14A	580.05	8/30/2017	17.85	562.20				
OW-15	579.56	8/30/2017	11.85	567.71	Casing tab for lock corroded.			
			G	lacial Till Wells				
OW-01B	579.14	8/30/2017	13.97	565.17				
OW-03	579.56	8/30/2017	13.92	565.64				
OW-04	579.45	8/30/2017	13.88	565.57				
OW-05	579.75	8/30/2017	14.28	565.47				
OW-06	582.36	8/30/2017	16.92	565.44	Lasing tab for lock corroded.			
				Staff Gauges				
SG-01	579.33	8/30/2017	4.49	574.84				
SG-02	579.57	8/30/2017	4.70	574.87				

Notes:

1 = Elevations are referenced to North American Vertical Datum of 1988 (NAVD 88).

# Table 5-2ESummary of Water Level Measurements: September 12, 2017NYSDEC Hydrogeologic ReportNiagara Sanitation Landfill, Site No. 932054Wheatfield, New York



Department of Environmental Conservation

	Measuring			Mator					
Location	Point	Measurement	Depth to	vvaler	Note				
ID	Elevation <sup>1</sup>	Date	Water (ft)	Elevation	Note				
	(ft amsl <sup>2</sup> )			(leet allisi)					
Fill/Upper Sand Wells									
OW-01	578.30	9/12/2017	4.52	573.78					
OW-13	579.33	9/12/2017	4.64	574.69	Casing tab for lock corroded & outer casing heaved.				
OW-14B	579.92	9/12/2017	5.20	574.72	Outer casing has heaved.				
OW-14BR	580.03	9/12/2017	5.74	574.29					
OW-16	581.88	9/12/2017	7.75	574.13					
OW-21	580.00	9/12/2017	6.52	573.48					
OW-22	579.46	9/12/2017	5.85	573.61					
OW-23	579.26	9/12/2017	4.74	574.52					
0W-31	580.64	9/12/2017	7.75	572.89					
01/ 22	582.44	9/12/2017	7.20	574.24					
010-33	502.43 581 10	9/12/2017	0.29 7.40	573.70					
011-34	581.10	9/12/2017	7.40	57/ 33					
OW-36	580.95	9/12/2017	6 58	574.35					
OW-37	580.15	9/12/2017	5.85	574.30					
LDP-01	580.34	9/12/2017	7.24	573.10	TD = 8.36 (TOIC). BTM Elev = 571.98				
LDP-02	581.03	9/12/2017	6.89	574.14					
LDP-03	580.73	9/12/2017	6.97	573.76					
LDP-04	581.42	9/12/2017	7.79	573.63					
LPZ-01S	580.31	9/12/2017	5.90	574.41					
LPZ-02S	581.03	9/12/2017	6.38	574.65					
LPZ-03S	581.16	9/12/2017	7.59	573.57					
LPZ-04S	579.68	9/12/2017	6.26	573.42					
LPZ-05S	580.41	9/12/2017	6.86	573.55					
LPZ-06S	581.00	9/12/2017	7.15	573.85					
LPZ-07S	580.56	9/12/2017	7.23	573.33					
LPZ-08S	579.47	9/12/2017	4.89	574.58	5 Jun 11				
			Silty Clay & Re	d-Gray Clay Aq	uitard Wells				
OW-02	577.26	9/12/2017	2.70	574.56					
			Lo	wer Sand Wells					
OW-14A	580.05	9/12/2017	17.40	562.65					
OW-15	579.56	9/12/2017	11.83	567.73	Casing tab for lock corroded.				
			G	lacial Till Wells					
OW-01B	579.14	9/12/2017	13.68	565.46					
OW-03	579.56	9/12/2017	14.03	565.53					
OW-04	579.45	9/12/2017	13.96	565.49					
OW-05	579.75	9/12/2017	14.35	565.40					
OW-06	582.36	9/12/2017	17.05	565.31	Casing tab for lock corroded.				
				Staff Gauges					
SG-01	579.33	9/12/2017	4.83	574.50					
SG-02	579.57	9/12/2017	4.94	574.63					

Notes:

1 = Elevations are referenced to North American Vertical Datum of 1988 (NAVD 88).

## Table 5-2F Summary of Water Level Measurements: September 25, 2017 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York



	Measuring			Matar					
Location	Point	Measurement	Depth to		Note				
ID	<b>Elevation</b> <sup>1</sup>	Date	Water (ft)	Elevation	Note				
	(ft amsl <sup>2</sup> )			(feet amsl)					
Fill/Upper Sand Wells									
OW-01	578.30	9/25/2017	5.23	573.07					
OW-13	579.33	9/25/2017	5.79	573.54	Casing tab for lock corroded & outer casing heaved.				
OW-14B	579.92	9/25/2017	5.68	574.24	Outer casing has heaved.				
OW-14BR	580.03	9/25/2017	6.36	573.67					
OW-16	581.88	9/25/2017	8.54	573.34					
OW-21	580.00	9/25/2017	7.23	572.77					
OW-22	579.46	9/25/2017	6.47	572.99					
OW-23	579.26	9/25/2017	5.30	573.96					
OW-31	580.64	9/25/2017	8.15	572.49					
OW-32	581.44	9/25/2017	7.77	573.67					
OW-33	582.43	9/25/2017	9.14	573.29					
OW-34	581.10	9/25/2017	8.46	572.64					
OW-35	581.57	9/25/2017	7.66	573.91					
OW-36	580.95	9/25/2017	6.93	574.02					
OW-37	580.15	9/25/2017	6.44	573.71					
LDP-01	580.34	9/25/2017	Dry	NA	TD = 8.36 (TOIC), BTM Elev = 571.98				
LDP-02	581.03	9/25/2017	8.39	572.64					
LDP-03	580.73	9/25/2017	8.13	572.60					
LDP-04	581.42	9/25/2017	8.61	572.81					
LPZ-01S	580.31	9/25/2017	6.55	573.76					
LPZ-02S	581.03	9/25/2017	7.01	574.02					
LPZ-03S	581.16	9/25/2017	8.80	572.36					
LPZ-04S	579.68	9/25/2017	7.23	572.45					
LPZ-05S	580.41	9/25/2017	7.59	572.82					
LPZ-06S	581.00	9/25/2017	8.24	572.76					
LPZ-07S	580.56	9/25/2017	8.19	572.37					
LPZ-08S	579.47	9/25/2017	5.33	574.14					
LPZ-09S	581.51	9/25/2017	7.74	573.77					
LPZ-10S	580.38	9/25/2017	7.12	573.26					
LPZ-11S	579.96	9/25/2017	6.43	573.53					
LPZ-12S	580.03	9/25/2017	6.69	573.34					
LPZ-13S	581.66	9/25/2017	8.64	573.02					
			Silty Clay & Re	d-Gray Clay Aq	uitard Wells				
OW-02	577.26	9/25/2017	3.52	573.74					
	-		Lo	wer Sand Wells					
OW-14A	580.05	9/25/2017	21.09	558.96					
OW-15	579.56	9/25/2017	11.98	567.58	Casing tab for lock corroded.				
			G	lacial Till Wells					
OW-01B	579.14	9/25/2017	13.85	565.29					
OW-03	579.56	9/25/2017	14.10	565.46					
OW-04	579.45	9/25/2017	14.09	565.36					
OW-05	579.75	9/25/2017	14.50	565.25					
OW-06	582.36	9/25/2017	17.20	565.16	Casing tab for lock corroded.				
				Staff Gauges					
SG-01	579.33	9/25/2017	Dry	NA	Ground Elevation = 574.12.				
SG-02	579.57	9/25/2017	Dry	NA	Ground Elevation = 573.53.				

Table 5-2F Summary of Water Level Measurements: September 25, 2017 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York



Department of Environmental Conservation

Notes:

1 = Elevations are referenced to North American Vertical Datum of 1988 (NAVD 88).

## Table 5-2G Summary of Water Level Measurements: October 17, 2017 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York



	Measuring								
Location	Point	Measurement	Depth to	Water					
ID	<b>Elevation</b> <sup>1</sup>	Date	Water (ft)	Elevation	Note				
	(ft amsl <sup>2</sup> )			(feet amsl)					
Fill/Upper Sand Wells									
OW-01	578.30	10/17/2017	3.98	574.32					
OW-13	579.33	10/17/2017	4.19	575.14	Casing tab for lock corroded & outer casing heaved.				
OW-14B	579.92	10/17/2017	5.02	574.90	Outer casing has heaved.				
OW-14BR	580.03	10/17/2017	5.08	574.95					
OW-16	581.88	10/17/2017	8.01	573.87					
OW-21	580.00	10/17/2017	6.03	573.97					
OW-22	579.46	10/17/2017	5.47	573.99					
OW-23	579.26	10/17/2017	4.36	574.90					
OW-31	580.64	10/17/2017	7.44	573.20					
OW-32	581.44	10/17/2017	7.31	574.13					
OW-33	582.43	10/17/2017	8.40	574.03					
OW-34	581.10	10/17/2017	6.46	574.64					
OW-35	581.57	10/17/2017	7.28	574.29					
OW-36	580.95	10/17/2017	6.68	574.27					
OW-37	580.15	10/17/2017	5.78	574.37					
LDP-01	580.34	10/17/2017	5.58	574.76	TD = 8.36 (TOIC), BTM Elev = 571.98				
LDP-02	581.03	10/17/2017	5.34	575.69					
LDP-03	580.73	10/17/2017	5.69	575.04					
LDP-04	581.42	10/17/2017	7.35	574.07					
LPZ-01S	580.31	10/17/2017	5.39	574.92					
LPZ-02S	581.03	10/17/2017	6.35	574.68					
LPZ-03S	581.16	10/17/2017	5.95	575.21					
LPZ-04S	579.68	10/17/2017	4.79	574.89					
LPZ-05S	580.41	10/17/2017	6.06	574.35					
LPZ-06S	581.00	10/17/2017	6.09	574.91					
LPZ-07S	580.56	10/17/2017	6.65	573.91					
LPZ-08S	579.47	10/17/2017	4.72	574.75					
LPZ-09S	581.51	10/17/2017	7.50	574.01					
LPZ-10S	580.38	10/17/2017	5.98	574.40					
LPZ-11S	579.96	10/17/2017	5.16	574.80					
LPZ-12S	580.03	10/17/2017	5.29	574.74					
LPZ-13S	581.66	10/1//201/	7.74	5/3.92					
	Silty Clay & Red-Gray Clay Aquitard Wells								
OW-02	577.26	10/17/2017	2.29	574.97					
			LO	wer Sand Wells					
OW-14A	580.05	10/1//201/	11.73	568.32					
OW-15	579.56	10/17/2017	11.66	567.90	Casing tab for lock corroded.				
		1	G	iaciai I ili Wells					
OW-01B	579.14	10/17/2017	13.69	565.45					
OW-03	579.56	10/17/2017	14.05	565.51					
OW-04	579.45	10/17/2017	14.14	565.31					
OW-05	579.75	10/17/2017	14.53	565.22					
OW-06	582.36	10/17/2017	17.24	565.12	Casing tab for lock corroded.				
				Staff Gauges					
SG-01	579.33	10/17/2017	4.35	574.98					
SG-02	579.57	10/17/2017	4.81	574.76					

Table 5-2G Summary of Water Level Measurements: October 17, 2017 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York



Department of Environmental Conservation

Notes:

1 = Elevations are referenced to North American Vertical Datum of 1988 (NAVD 88).

## Table 5-2H Summary of Water Level Measurements: October 20, 2017 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York



Location ID     Point (H:amsi <sup>1</sup> )     Measurement Date     Depth of Water (H)     Evention (Feet amsi)     INME       0W-01     578.30     10/20/2017     572.80     4.911 from TOC (0.89' above TOIC)       0W-13     579.92     10/20/2017     5.58     4.911 from TOC (0.89' above TOIC)       0W-148     580.93     10/20/2017     5.08     577.480     Casing tab for lock corroded & outer casing has heaved.       0W-148     580.03     10/20/2017     5.08     577.366        0W-121     581.08     10/20/2017     5.45     577.401        0W-32     579.46     10/20/2017     7.32     573.361        0W-32     579.46     10/20/2017     7.34     574.451        0W-33     581.44     10/20/2017     7.38     574.450        0W-34     580.55     10/20/2017     7.59     574.36        0W-35     580.35     10/20/2017     5.89     574.36        1DP-01     580.31     10/20/2017     5.89     574.36 <tr< th=""><th></th><th>Measuring</th><th></th><th></th><th>Wator</th><th colspan="3"></th></tr<>		Measuring			Wator					
ID     Elevation*     Date     Water (H)     Elevation*     Note       0W-01     578.30     10/20/2017     5.72     574.80     Casima table     Casima table       0W-01     578.30     10/20/2017     5.82     5.73.88     4.91 from TOC (0.89' above TOIC)       0W-148     579.92     10/20/2017     5.08     574.84     Outer casing has heaved.       0W-148     580.03     10/20/2017     7.92     573.85     Outer casing has heaved.       0W-148     580.03     10/20/2017     7.92     573.95     Outer casing has heaved.       0W-24     581.88     10/20/2017     7.82     574.401     Outer casing has heaved.       0W-32     580.64     10/20/2017     7.38     574.01     Outer casing has heaved.       0W-33     581.51     10/20/2017     7.38     574.04     International table index control table index cont	Location	Point	Measurement	Depth to		Nata				
(ft ams1 <sup>2</sup> )     (fteet ams1)       Fill/Upper Sand Wells       OW-01     578.30     10/20/2017     5.72     S72.58     4.91' from TOC (0.89' above TOIC)       OW-13     579.32     10/20/2017     5.83     574.80     Outer casing has heaved.       OW-148     580.03     10/20/2017     5.08     573.80     Unter casing has heaved.       OW-148     580.03     10/20/2017     6.03     573.97        OW-21     579.46     10/20/2017     7.92     573.97         OW-22     579.46     10/20/2017     7.31     573.97         OW-33     581.44     10/20/2017     7.33     574.06         OW-34     580.43     10/20/2017     7.38     574.06         OW-35     581.57     10/20/2017     7.38     574.30         OW-36     580.95     10/20/2017     5.94     574.39         OW-37     580.15     10/20/2017     5.94	ID	<b>Elevation</b> <sup>1</sup>	Date	Water (ft)	Elevation	Note				
Fill/Upper Sand Wells       OW-01     578.30     10/20/2017     5.72     572.88     4.91 'from TOC (0.89' above TOIC)       OW-148     579.33     10/20/2017     5.08     574.80     Casing tab for lock corroded & outer casing heaved.       OW-148     580.03     10/20/2017     5.08     574.80     Outer casing has heaved.       OW-146     581.88     10/20/2017     5.18     574.85     Outer casing has heaved.       OW-22     573.46     10/20/2017     5.45     574.41     Outer casing has heaved.       OW-31     580.64     10/20/2017     7.38     573.26     10/20/2017       OW-32     5573.45     10/20/2017     7.38     574.06        OW-33     581.57     10/20/2017     7.30     574.27        OW-35     580.51     10/20/2017     5.95     574.33        OW-36     580.31     10/20/2017     5.95     574.33        DP-01     580.31     10/20/2017     5.95     574.34        DP-02     581.03 <t< th=""><th></th><th>(ft amsl<sup>2</sup>)</th><th></th><th></th><th>(feet amsl)</th><th></th></t<>		(ft amsl <sup>2</sup> )			(feet amsl)					
OW-01     578.30     10/20/2017     5.72     572.88     4.91 f forn TOC (0.89" shower TOC)       OW-148     579.92     10/20/2017     5.08     574.80     Casing tab for lock corroded & outer casing heaved.       OW-148R     580.03     10/20/2017     5.08     574.84     Outer casing has heaved.       OW-14     581.88     10/20/2017     5.08     573.96        OW-2     579.46     10/20/2017     7.92     573.96        OW-31     580.04     10/20/2017     7.45     574.04        OW-32     578.46     10/20/2017     7.38     574.06        OW-33     582.44     10/20/2017     7.38     574.06         OW-34     580.55     10/20/2017     7.38     574.30          OW-35     580.55     10/20/2017     5.95     574.39     TD = 8.36 (TOIC), BTM Elev = 571.98        LDP-01     580.41     10/20/2017     5.99     575.14         LDP-02     581.03	Fill/Upper Sand Wells									
OW-13     579.32     10/20/2017     4.53     574.80     Casing tab for lock corroded & outer casing heaved.       OW-148     580.03     10/20/2017     5.08     574.85     Outer casing heaved.       OW-148     580.03     10/20/2017     5.98     574.85     Outer casing heaved.       OW-14     580.03     10/20/2017     5.92     573.96     Outer casing heaved.       OW-21     579.46     10/20/2017     6.53     574.37     Outer casing heaved.       OW-22     579.46     10/20/2017     4.51     574.75     Outer casing heaved.       OW-31     580.64     10/20/2017     7.37     573.27     Outer casing heaved.       OW-32     581.43     10/20/2017     7.30     574.27     Outer casing heaved.       OW-35     581.57     10/20/2017     5.99     574.36     Dea.36 (TOIC), BTM Elev = 571.98       IDP-01     580.34     10/20/2017     5.99     574.43     Dea.36 (TOIC), BTM Elev = 571.98       IDP-03     580.13     10/20/2017     5.49     574.43     Dea.36 (TOIC), BTM Elev = 571.98	OW-01	578.30	10/20/2017	5.72	572.58	4.91' from TOC (0.89' above TOIC)				
OW-14B     579.92     10/20/2017     5.08     574.84     Outer casing has heaved.       OW-14BR     580.03     10/20/2017     5.18     574.85       OW-14     580.00     10/20/2017     6.03     573.97       OW-21     580.00     10/20/2017     5.45     574.01       OW-23     579.46     10/20/2017     4.51     574.75       OW-31     580.64     10/20/2017     7.37     573.27       OW-33     581.44     10/20/2017     7.38     574.06       OW-33     582.43     10/20/2017     7.30     573.97       OW-34     580.51     10/20/2017     7.39     574.30       OW-35     580.35     10/20/2017     5.95     574.31       OW-36     580.35     10/20/2017     5.95     574.34       DP-01     580.31     10/20/2017     5.95     574.43       DP-02     580.31     10/20/2017     6.99     575.14       LDP-03     581.31     10/20/2017     6.43     574.73       LP2-045	OW-13	579.33	10/20/2017	4.53	574.80	Casing tab for lock corroded & outer casing heaved.				
OW-148R     580.03     10/20/2017     5.18     574.85       OW-16     581.88     10/20/2017     7.92     573.96       OW-21     580.00     10/20/2017     6.03     573.97       OW-22     579.46     10/20/2017     4.51     574.01       OW-23     579.26     10/20/2017     7.37     573.27       OW-31     580.64     10/20/2017     7.38     574.06       OW-33     582.43     10/20/2017     7.38     574.06       OW-33     581.44     10/20/2017     7.30     574.27       OW-35     581.57     10/20/2017     5.79     574.33       OW-36     580.95     10/20/2017     5.79     574.36       DP-01     580.43     10/20/2017     5.89     575.14       LDP-02     581.03     10/20/2017     5.49     574.82       LP2-035     580.11     10/20/2017     5.49     574.82       LP2-045     580.81     10/20/2017     6.34     574.55       LP2-045     580.41     10/20/2	OW-14B	579.92	10/20/2017	5.08	574.84	Outer casing has heaved.				
OW-16     S81.88     10/20/2017     7.92     573.96       OW-21     S80.00     10/20/2017     6.03     573.97       OW-22     579.46     10/20/2017     5.45     574.01       OW-23     579.26     10/20/2017     7.37     573.27       OW-31     580.64     10/20/2017     7.38     574.06       OW-32     581.44     10/20/2017     7.30     574.27       OW-33     582.43     10/20/2017     7.30     574.27       OW-36     580.95     10/20/2017     7.30     574.427       OW-36     580.95     10/20/2017     5.95     574.33       IDP-01     580.34     10/20/2017     5.89     575.14       IDP-02     581.03     10/20/2017     5.89     574.44       IDP-03     581.16     10/20/2017     5.89     574.464       IDP-04     581.42     10/20/2017     5.43     574.56       IP2-055     581.01     10/20/2017     6.43     574.66       IP2-055     581.01     10/20/	OW-14BR	580.03	10/20/2017	5.18	574.85					
OW-21     580.00     10/20/2017     6.03     573.97       OW-22     579.46     10/20/2017     5.45     574.01       OW-31     580.64     10/20/2017     7.37     573.27       OW-33     580.64     10/20/2017     7.38     574.06       OW-33     582.43     10/20/2017     7.38     574.06       OW-33     581.44     10/20/2017     7.30     574.27       OW-36     580.95     10/20/2017     6.64     574.31       OW-36     581.57     10/20/2017     6.64     574.31       OW-36     580.51     10/20/2017     5.89     575.14       LDP-01     580.34     10/20/2017     5.89     575.14       LDP-03     580.31     10/20/2017     6.38     574.64       LP2-015     580.31     10/20/2017     6.34     574.64       LP2-025     581.03     10/20/2017     6.34     574.65       LP2-035     581.61     10/20/2017     6.34     574.66       LP2-045     579.46     10/20/	OW-16	581.88	10/20/2017	7.92	573.96					
OW-22     579.46     10/20/2017     5.45     574.01       OW-23     579.26     10/20/2017     7.37     573.27       OW-31     580.64     10/20/2017     7.38     574.06       OW-32     581.44     10/20/2017     7.38     574.06       OW-33     581.57     10/20/2017     7.30     574.27       OW-36     580.95     10/20/2017     5.79     574.36       OW-36     580.95     10/20/2017     5.79     574.36       DP-01     580.31     10/20/2017     5.95     574.34       DP-02     580.33     10/20/2017     5.89     575.14       LDP-03     580.73     10/20/2017     5.89     574.44       LDP-04     581.42     10/20/2017     6.39     574.64       LP2-025     581.03     10/20/2017     6.31     574.62       LP2-035     581.16     10/20/2017     6.31     574.55       LP2-045     579.68     10/20/2017     6.34     574.66       LP2-055     581.04     10/20/	OW-21	580.00	10/20/2017	6.03	573.97					
OW-33     579.26     10/20/2017     4.51     574.75       OW-31     580.64     10/20/2017     7.38     574.06       OW-33     582.43     10/20/2017     7.38     574.06       OW-33     582.43     10/20/2017     7.38     574.06       OW-36     580.95     10/20/2017     6.64     574.31       OW-37     580.15     10/20/2017     5.79     574.39       DP-01     580.34     10/20/2017     5.79     574.34       DP-02     581.03     10/20/2017     5.89     575.14       DP-03     580.73     10/20/2017     5.89     574.64       LDP-04     581.42     10/20/2017     5.48     574.64       LP-2015     580.31     10/20/2017     6.43     574.73       LP2-035     581.16     10/20/2017     6.37     574.66       LP2-035     580.41     10/20/2017     6.34     574.73       LP2-045     580.56     10/20/2017     6.74     574.66       LP2-055     581.41     10/20	OW-22	579.46	10/20/2017	5.45	574.01					
OW-31     580.64     10/20/2017     7.37     573.27       OW-32     581.44     10/20/2017     7.38     574.06       OW-33     582.43     10/20/2017     8.46     573.97       OW-35     581.57     10/20/2017     6.64     574.31       OW-36     580.95     10/20/2017     5.79     574.36       DP-01     580.34     10/20/2017     5.59     574.39     D = 8.36 (TOIC), BTM Elev = 571.98       DP-02     581.03     10/20/2017     5.89     575.14        LDP-03     580.73     10/20/2017     6.99     574.64        LDP-04     581.42     10/20/2017     6.37     574.66         LP2-055     581.03     10/20/2017     6.37     574.66          LP2-055     581.01     10/20/2017     6.32     574.43          LP2-055     580.41     10/20/2017     6.32     574.43          LP2-055     580.41	OW-23	579.26	10/20/2017	4.51	574.75					
OW-32     581.44     10/20/2017     7.38     574.06       OW-33     582.43     10/20/2017     7.30     574.27       OW-36     580.95     10/20/2017     5.70     574.27       OW-36     580.95     10/20/2017     5.73     574.36       OW-37     580.15     10/20/2017     5.95     574.39     TD = 8.36 (TOIC), BTM Elev = 571.98       LDP-01     580.34     10/20/2017     5.89     575.14        LDP-03     580.73     10/20/2017     5.89     575.14        LDP-04     581.42     10/20/2017     5.49     574.64        LP2-015     580.31     10/20/2017     6.43     574.73        LP2-025     581.16     10/20/2017     6.43     574.73        LP2-045     579.68     10/20/2017     6.34     574.73        LP2-055     580.41     10/20/2017     6.43     574.73        LP2-055     580.51     10/20/2017     6.70     573.86 </td <td>OW-31</td> <td>580.64</td> <td>10/20/2017</td> <td>7.37</td> <td>573.27</td> <td></td>	OW-31	580.64	10/20/2017	7.37	573.27					
OW-33     582.43     10/20/2017     8.46     573.97       OW-35     581.57     10/20/2017     7.30     574.27       OW-36     580.95     10/20/2017     5.79     574.36       OW-37     580.15     10/20/2017     5.79     574.36       LDP-01     580.34     10/20/2017     5.89     575.14       LDP-03     580.33     10/20/2017     5.89     574.64       LDP-04     581.42     10/20/2017     5.49     574.64       LP2-05     580.31     10/20/2017     5.49     574.64       LP2-04     581.46     10/20/2017     5.43     574.66       LP2-05     581.03     10/20/2017     6.33     574.55       LP2-055     580.41     10/20/2017     6.34     574.66       LP2-055     580.41     10/20/2017     6.32     574.46       LP2-055     580.41     10/20/2017     6.74     2       LP2-055     580.38     10/20/2017     7.48     574.03       LP2-055     580.38     10/20	OW-32	581.44	10/20/2017	7.38	574.06					
OW-35     581.57     10/20/2017     7.30     574.27       OW-36     580.95     10/20/2017     6.64     574.31       OW-37     580.15     10/20/2017     5.79     574.36       LDP-01     580.34     10/20/2017     5.95     574.33     TD = 8.36 (TOIC), BTM Elev = 571.98       LDP-02     581.03     10/20/2017     5.89     575.14        LDP-03     580.73     10/20/2017     5.49     574.64        LDP-04     581.42     10/20/2017     5.49     574.64         LP2-015     580.31     10/20/2017     5.43     574.73         LP2-025     581.03     10/20/2017     5.13     574.73         LP2-035     581.16     10/20/2017     5.13     574.66         LP2-045     580.41     10/20/2017     6.74     574.66         LP2-055     580.11     10/20/2017     7.48     574.03         LP2-05	OW-33	582.43	10/20/2017	8.46	573.97					
OW-36     580.95     10/20/2017     6.64     574.31       OW-37     580.15     10/20/2017     5.79     574.36       LDP-01     580.34     10/20/2017     5.95     5774.39     TD = 8.36 (TOIC), BTM Elev = 571.98       LDP-02     581.03     10/20/2017     6.09     574.64       LDP-03     580.73     10/20/2017     6.49     574.64       LDP-04     581.42     10/20/2017     6.39     574.64       LP2-015     580.31     10/20/2017     6.37     574.66       LP2-025     581.03     10/20/2017     6.37     574.73       LP2-035     581.16     10/20/2017     6.34     574.66       LP2-045     581.00     10/20/2017     6.22     574.19       LP2-055     580.41     10/20/2017     6.70     573.86       LP2-055     580.51     10/20/2017     7.48     574.68       LP2-055     580.31     10/20/2017     5.28     574.68       LP2-055     580.33     10/20/2017     5.28     574.68	OW-35	581.57	10/20/2017	7.30	574.27					
0W-37     580.15     10/20/2017     5.79     574.36       LDP-01     580.34     10/20/2017     5.89     575.14       LDP-03     580.73     10/20/2017     5.89     575.14       LDP-04     581.42     10/20/2017     7.38     574.04       LP2-015     580.31     10/20/2017     7.38     574.04       LP2-04     581.42     10/20/2017     6.39     574.82       LP2-035     581.16     10/20/2017     6.37     574.66       LP2-035     581.16     10/20/2017     6.34     574.55       LP2-035     580.41     10/20/2017     6.34     574.55       LP2-035     580.41     10/20/2017     6.34     574.66       LP2-035     580.41     10/20/2017     6.34     574.68       LP2-045     581.00     10/20/2017     6.34     574.68       LP2-055     580.31     10/20/2017     7.48     574.68       LP2-055     580.33     10/20/2017     5.28     574.68       LP2-055     580.33	OW-36	580.95	10/20/2017	6.64	574.31					
LDP-01     580.34     10/20/2017     5.95     574.39     TD = 8.36 (TOIC), BTM Elev = 571.98       LDP-02     581.03     10/20/2017     5.89     575.14       LDP-04     580.73     10/20/2017     6.09     574.64       LDP-04     581.42     10/20/2017     7.38     574.04       LP2-015     580.31     10/20/2017     6.37     574.66       LP2-025     581.06     10/20/2017     6.43     574.73       LP2-045     579.68     10/20/2017     6.22     574.19       LP2-045     579.68     10/20/2017     6.34     574.55       LP2-055     580.01     10/20/2017     6.70     573.86       LP2-055     580.56     10/20/2017     6.70     573.86       LP2-055     580.56     10/20/2017     7.48     574.68       LP2-055     580.03     10/20/2017     5.28     574.68       LP2-055     580.03     10/20/2017     5.28     574.68       LP2-155     580.03     10/20/2017     5.28     574.68 <tr< td=""><td>OW-37</td><td>580.15</td><td>10/20/2017</td><td>5.79</td><td>574.36</td><td></td></tr<>	OW-37	580.15	10/20/2017	5.79	574.36					
LDP-02     S81.03     10/20/2017     5.89     S75.14       LDP-03     S80.73     10/20/2017     6.09     S74.64       LDP-04     S81.42     10/20/2017     7.38     S74.04       LDP-03     S80.73     10/20/2017     5.49     S74.82       LP2-015     S80.31     10/20/2017     6.43     S74.73       LP2-035     S81.16     10/20/2017     6.43     S74.73       LP2-045     S97.68     10/20/2017     6.22     S74.19       LP2-045     S80.41     10/20/2017     6.22     S74.66       LP2-045     S80.56     10/20/2017     6.70     S73.86       LP2-045     S81.51     10/20/2017     6.70     S73.86       LP2-045     S80.56     10/20/2017     7.48     S74.03       LP2-045     S80.38     10/20/2017     5.28     S74.64       LP2-045     S80.38     10/20/2017     5.28     S74.64       LP2-045     S80.38     10/20/2017     5.28     S74.65       LP2-045     S80.30	LDP-01	580.34	10/20/2017	5.95	574.39	TD = 8.36 (TOIC), BTM Elev = 571.98				
LDP-03     S80.73     10/20/2017     6.09     S74.64       LDP-04     S81.42     10/20/2017     7.38     S74.04       LP2-015     S80.31     10/20/2017     5.49     S74.82       LP2-025     S81.03     10/20/2017     6.37     S74.66       LP2-035     S81.16     10/20/2017     6.43     S74.73       LP2-045     S79.68     10/20/2017     6.13     S74.55       LP2-055     S80.41     10/20/2017     6.34     S74.66       LP2-055     S80.56     10/20/2017     6.34     S74.66       LP2-055     S80.50     10/20/2017     6.34     S74.66       LP2-055     S81.51     10/20/2017     6.74.82        LP2-055     S80.51     10/20/2017     7.48     S74.03       LP2-055     S80.38     10/20/2017     5.28     S74.65       LP2-105     S80.38     10/20/2017     5.28     S74.65       LP2-115     S79.96     10/20/2017     5.38     S74.65       UP2-125     S80.03	LDP-02	581.03	10/20/2017	5.89	575.14					
LDP-04     581.42     10/20/2017     7.38     574.04       LPZ-015     580.31     10/20/2017     5.49     574.82       LPZ-025     581.03     10/20/2017     6.37     574.66       LPZ-025     581.04     10/20/2017     6.33     574.65       LPZ-035     581.16     10/20/2017     6.33     574.55       LPZ-045     579.68     10/20/2017     6.22     574.19       LPZ-055     580.41     10/20/2017     6.34     574.66       LPZ-055     580.56     10/20/2017     6.70     573.86       LPZ-055     580.56     10/20/2017     4.79     574.68       LPZ-085     579.47     10/20/2017     7.48     574.03       LPZ-105     580.38     10/20/2017     5.28     574.68       LPZ-115     579.96     10/20/2017     5.28     574.68       LPZ-125     580.03     10/20/2017     5.78     574.76       OW-02     577.26     10/20/2017     2.47     574.79     Orginal depth to water was 4.27. See note 1. <td>LDP-03</td> <td>580.73</td> <td>10/20/2017</td> <td>6.09</td> <td>574.64</td> <td colspan="2"></td>	LDP-03	580.73	10/20/2017	6.09	574.64					
LPZ-01S     S80.31     10/20/2017     S.49     S74.82       LPZ-02S     S81.03     10/20/2017     G.37     S74.66       LPZ-02S     S81.16     10/20/2017     G.43     S74.55       LPZ-04S     S79.68     10/20/2017     G.33     S74.55       LPZ-04S     S80.41     10/20/2017     G.34     S74.66       LPZ-05S     S80.41     10/20/2017     G.34     S74.66       LPZ-06S     S81.00     10/20/2017     G.34     S74.66       LPZ-05S     S80.56     10/20/2017     G.73.86        LPZ-05S     S81.51     10/20/2017     G.74.82        LPZ-05S     S81.51     10/20/2017     G.66     S74.32       LPZ-10S     S80.38     10/20/2017     S.28     S74.68       LPZ-11S     S79.96     10/20/2017     S.28     S74.68       LPZ-10S     S80.30     10/20/2017     S.28     S74.68       LPZ-11S     S79.96     10/20/2017     S.47     S74.90       OW-02     S77.26	LDP-04	581.42	10/20/2017	7.38	574.04					
LP2-02S     581.03     10/20/2017     6.37     574.66       LP2-03S     581.16     10/20/2017     6.43     574.73       LP2-04S     579.68     10/20/2017     6.22     574.19       LP2-05S     580.41     10/20/2017     6.34     574.66       LP2-05S     580.41     10/20/2017     6.34     574.66       LP2-07S     580.56     10/20/2017     6.70     573.86       LP2-08S     579.47     10/20/2017     6.70     573.86       LP2-09S     581.51     10/20/2017     7.48     574.03       LP2-09S     580.38     10/20/2017     5.28     574.68       LP2-10S     580.38     10/20/2017     5.28     574.68       LP2-11S     579.96     10/20/2017     5.28     574.68       LP2-12S     580.03     10/20/2017     2.47     574.68       OW-02     577.26     10/20/2017     11.60     568.45     Casing tab for lock corroded.       OW-14A     580.05     10/20/2017     11.68     567.88     Casing t	LPZ-01S	580.31	10/20/2017	5.49	574.82					
LP2-03S     581.16     10/20/2017     6.43     574.73       LP2-04S     579.68     10/20/2017     5.13     574.55       LP2-05S     580.41     10/20/2017     6.22     574.19       LP2-05S     580.01     10/20/2017     6.34     574.66       LP2-07S     580.56     10/20/2017     6.73.86       LP2-08S     579.47     10/20/2017     7.48     574.68       LP2-09S     581.51     10/20/2017     7.48     574.68       LP2-10S     580.38     10/20/2017     5.28     574.68       LP2-11S     579.96     10/20/2017     5.28     574.68       LP2-12S     580.03     10/20/2017     5.38     574.65       Sitty Clay & Red-Gray Clay Aquitard Wells       OW-02     577.26     10/20/2017     1.47     574.79     Original depth to water was 4.27. See note 1.       Cower Sand Wells       OW-14A     580.05     10/20/2017     11.60     568.45     Casing tab for lock corroded.       OW-15     579.56     10/20/2017     13	LPZ-02S	581.03	10/20/2017	6.37	574.66					
LPZ-04S     579.68     10/20/2017     5.13     574.55       LPZ-05S     580.41     10/20/2017     6.22     574.19       LPZ-06S     581.00     10/20/2017     6.34     574.66       LPZ-07S     580.56     10/20/2017     6.70     573.86       LPZ-07S     580.56     10/20/2017     4.79     574.68       LPZ-09S     581.51     10/20/2017     7.48     574.03       LPZ-10S     580.38     10/20/2017     6.66     574.32       LPZ-11S     579.96     10/20/2017     5.28     574.68       LPZ-12S     580.03     10/20/2017     5.38     574.65       Sitly Clay & Red-Gray Clay Aquitard Wells       OW-02     577.26     10/20/2017     2.47     574.79     Original depth to water was 4.27. See note 1.       OW-02     577.26     10/20/2017     11.60     568.45     Casing tab for lock corroded.       OW-14A     580.05     10/20/2017     11.68     567.88     Casing tab for lock corroded.       OW-03     579.56     10/20/2017	LPZ-03S	581.16	10/20/2017	6.43	574.73					
LPZ-05S     580.41     10/20/2017     6.22     574.19       LPZ-06S     581.00     10/20/2017     6.34     574.66       LPZ-07S     580.56     10/20/2017     6.70     573.86       LPZ-07S     580.56     10/20/2017     6.70     573.86       LPZ-07S     580.56     10/20/2017     6.70     573.86       LPZ-08S     579.47     10/20/2017     7.48     574.03       LPZ-09S     581.51     10/20/2017     5.28     574.68       LPZ-10S     580.38     10/20/2017     5.28     574.68       LPZ-11S     579.96     10/20/2017     5.38     574.68       UPZ-12S     580.03     10/20/2017     5.38     574.68       UPZ-12S     580.03     10/20/2017     5.38     574.68       UPZ-12S     580.03     10/20/2017     5.48     Casing tab for lock corroded.       OW-02     577.26     10/20/2017     11.60     568.45     Casing tab for lock corroded.       OW-15     579.56     10/20/2017     13.62     565.52 <td>LPZ-04S</td> <td>579.68</td> <td>10/20/2017</td> <td>5.13</td> <td>574.55</td> <td></td>	LPZ-04S	579.68	10/20/2017	5.13	574.55					
LPZ-06S     581.00     10/20/2017     6.34     574.66       LPZ-07S     580.56     10/20/2017     6.70     573.86       LPZ-08S     579.47     10/20/2017     4.79     574.68       LPZ-09S     581.51     10/20/2017     7.48     574.08       LPZ-10S     580.38     10/20/2017     5.28     574.68       LPZ-11S     579.96     10/20/2017     5.28     574.68       LPZ-11S     579.96     10/20/2017     5.28     574.68       LPZ-12S     580.03     10/20/2017     5.28     574.68       OW-02     577.26     10/20/2017     5.28     574.68       OW-02     577.26     10/20/2017     2.47     574.79     Original depth to water was 4.27. See note 1.       OW-02     577.26     10/20/2017     11.60     568.45     Casing tab for lock corroded.       OW-14A     580.05     10/20/2017     11.68     567.88     Casing tab for lock corroded.       OW-03     579.56     10/20/2017     13.82     565.52        OW-04 </td <td>LPZ-05S</td> <td>580.41</td> <td>10/20/2017</td> <td>6.22</td> <td>574.19</td> <td></td>	LPZ-05S	580.41	10/20/2017	6.22	574.19					
LPZ-07S     580.56     10/20/2017     6.70     573.86       LPZ-08S     579.47     10/20/2017     4.79     574.68       LPZ-09S     581.51     10/20/2017     7.48     574.03       LPZ-09S     580.38     10/20/2017     6.06     574.32       LPZ-10S     580.38     10/20/2017     5.28     574.65       LPZ-11S     579.96     10/20/2017     5.38     574.65       OW-02     577.26     10/20/2017     2.47     574.79     Original depth to water was 4.27. See note 1.       OW-02     577.26     10/20/2017     2.47     574.79     Original depth to water was 4.27. See note 1.       OW-02     577.26     10/20/2017     11.60     568.45     Casing tab for lock corroded.       OW-14A     580.05     10/20/2017     11.68     567.88     Casing tab for lock corroded.       OW-15     579.56     10/20/2017     13.62     565.52        OW-04     579.45     10/20/2017     14.10     565.35        OW-05     579.75 <td< td=""><td>LPZ-06S</td><td>581.00</td><td>10/20/2017</td><td>6.34</td><td>574.66</td><td></td></td<>	LPZ-06S	581.00	10/20/2017	6.34	574.66					
LPZ-08S     579.47     10/20/2017     4.79     574.68       LPZ-09S     581.51     10/20/2017     7.48     574.03       LPZ-10S     580.38     10/20/2017     6.06     574.32       LPZ-11S     579.96     10/20/2017     5.28     574.68       LPZ-12S     580.03     10/20/2017     5.38     574.65 <b>CIVE Clay &amp; Rev Fary Clay Aquitard Wells CIVE Clay &amp; Rev Fary Clay Aquitard Wells OW</b> -02     577.26     10/20/2017     2.47     574.79     Original depth to water was 4.27. See note 1. <b>OW</b> -02     577.26     10/20/2017     11.60     568.45     Casing tab for lock corroded. <b>OW</b> -14A     580.05     10/20/2017     11.60     568.45     Casing tab for lock corroded. <b>OW</b> -14A     580.05     10/20/2017     11.60     568.45     Casing tab for lock corroded. <b>OW</b> -14A     579.16     10/20/2017     13.62     565.52     Colspan="3"> <b>OW</b> -01B       579.15     10/20/2017     14.10     565.55     IV/20/2017 <td>LPZ-07S</td> <td>580.56</td> <td>10/20/2017</td> <td>6.70</td> <td>573.86</td> <td></td>	LPZ-07S	580.56	10/20/2017	6.70	573.86					
LPZ-095     581.51     10/20/2017     7.48     574.03     International Content of Conte	LPZ-08S	579.47	10/20/2017	4.79	574.68					
LPZ-10S     580.38     10/20/2017     6.06     574.32       LPZ-11S     579.96     10/20/2017     5.28     574.68       LPZ-12S     580.03     10/20/2017     5.38     574.68       OW-02     577.26     10/20/2017     2.47     574.79     Original depth to water was 4.27. See note 1.       OW-02     577.26     10/20/2017     2.47     574.79     Original depth to water was 4.27. See note 1.       OW-02     577.26     10/20/2017     11.60     568.45     Casing tab for lock corroded.       OW-14A     580.05     10/20/2017     11.68     567.88     Casing tab for lock corroded.       OW-015     579.56     10/20/2017     13.62     565.52        OW-018     579.4     10/20/2017     13.98     565.58     14.50' from TOC (0.52' above TOIC).       OW-04     579.56     10/20/2017     14.10     565.35        OW-05     579.75     10/20/2017     14.50     565.17     Casing tab for lock corroded.       OW-06     582.36     10/20/2017     17.19     565.17	LPZ-09S	581.51	10/20/2017	7.48	574.03					
LPZ-11S     579.96     10/20/2017     5.28     574.68       LPZ-12S     580.03     10/20/2017     5.38     574.65       OW-02     577.26     10/20/2017     2.47     574.79     Original depth to water was 4.27. See note 1.       OW-02     577.26     10/20/2017     2.47     574.79     Original depth to water was 4.27. See note 1.       OW-04     580.05     10/20/2017     11.60     568.45     Casing tab for lock corroded.       OW-15     579.56     10/20/2017     11.68     567.88     Casing tab for lock corroded.       OW-018     579.14     10/20/2017     13.62     565.52        OW-03     579.56     10/20/2017     13.98     565.58     14.50' from TOC (0.52' above TOIC).       OW-04     579.45     10/20/2017     14.10     565.35        OW-05     579.75     10/20/2017     14.50     565.25        OW-06     582.36     10/20/2017     17.19     565.17     Casing tab for lock corroded.       OW-05     579.75     10/20/2017     17.19 <td< td=""><td>LPZ-10S</td><td>580.38</td><td>10/20/2017</td><td>6.06</td><td>574.32</td><td></td></td<>	LPZ-10S	580.38	10/20/2017	6.06	574.32					
LPZ-12S     580.03     10/20/2017     5.38     574.65       Sity Clay & Re-Gray Clay Autor Wells       OW-02     577.26     10/20/2017     2.47     574.79     Original depth to water was 4.27. See note 1.       OW-02     577.26     10/20/2017     2.47     574.79     Original depth to water was 4.27. See note 1.       OW-02     577.26     10/20/2017     11.60     568.45     Casing tab for lock corroded.       OW-14A     580.05     10/20/2017     11.60     568.45     Casing tab for lock corroded.       OW-015     579.56     10/20/2017     11.68     567.88     Casing tab for lock corroded.       OW-01B     579.14     10/20/2017     13.62     565.52        OW-03     579.56     10/20/2017     13.98     565.58     14.50' from TOC (0.52' above TOIC).       OW-04     579.45     10/20/2017     14.10     565.25       OW-05     579.75     10/20/2017     14.50     565.25       OW-06     582.36     10/20/2017     14.50	LPZ-11S	579.96	10/20/2017	5.28	574.68					
Silty Clay & Red-Gray Clay Aquitard Wells       OW-02     577.26     10/20/2017     2.47     574.79     Original depth to water was 4.27. See note 1.       OW-02     577.26     10/20/2017     2.47     574.79     Original depth to water was 4.27. See note 1.       OW-14A     580.05     10/20/2017     11.60     568.45     Casing tab for lock corroded.       OW-15     579.56     10/20/2017     11.68     567.88     Casing tab for lock corroded.       OW-01B     579.14     10/20/2017     13.62     565.52     Intervalue       OW-03     579.56     10/20/2017     13.88     565.58     14.50' from TOC (0.52' above TOIC).       OW-04     579.45     10/20/2017     14.10     565.35     Intervalue       OW-05     579.75     10/20/2017     14.50     565.25     Intervalue       OW-06     582.36     10/20/2017     17.19     565.17     Casing tab for lock corroded.       OW-06     582.36     10/20/2017     4.25     575.08     Intervalue       SG-01     579.57     10/20/2017     4.25	LPZ-12S	580.03	10/20/2017	5.38	574.65					
OW-02     577.26     10/20/2017     2.47     574.79     Original depth to water was 4.27. See note 1.       OW-14A     580.05     10/20/2017     11.60     568.45     Casing tab for lock corroded.       OW-15     579.56     10/20/2017     11.68     567.88     Casing tab for lock corroded.       OW-015     579.56     10/20/2017     11.68     567.88     Casing tab for lock corroded.       OW-016     579.14     10/20/2017     13.62     565.52     Image: Corroded corrode corrod corrode corrode corrod corrode corrode corrod corr				Silty Clay & Re	d-Gray Clay Aq	uitard Wells				
Lower Sand Wells       OW-14A     580.05     10/20/2017     11.60     568.45     Casing tab for lock corroded.       OW-15     579.56     10/20/2017     11.68     567.88     Casing tab for lock corroded.       OW-015     579.56     10/20/2017     11.68     567.88     Casing tab for lock corroded.       OW-018     579.14     10/20/2017     13.62     565.52       OW-03     579.56     10/20/2017     13.98     565.58     14.50' from TOC (0.52' above TOIC).       OW-04     579.45     10/20/2017     14.10     565.35     14.50' from TOC (0.52' above TOIC).       OW-05     579.75     10/20/2017     14.50     565.25     14.50' from TOC (0.52' above TOIC).       OW-06     582.36     10/20/2017     14.50     565.17     Casing tab for lock corroded.       Staff Gauges       SG-01     579.33     10/20/2017     4.25     575.08       SG-02     579.57     10/20/2017     4.75     574.82	OW-02	577.26	10/20/2017	2.47	574.79	Original depth to water was 4.27. See note 1.				
OW-14A     580.05     10/20/2017     11.60     568.45     Casing tab for lock corroded.       OW-15     579.56     10/20/2017     11.68     567.88     Casing tab for lock corroded.       Glacial Till Wells       OW-01B     579.14     10/20/2017     13.62     565.52       OW-03     579.56     10/20/2017     13.98     565.58     14.50' from TOC (0.52' above TOIC).       OW-04     579.45     10/20/2017     14.10     565.35     14.50' from TOC (0.52' above TOIC).       OW-05     579.75     10/20/2017     14.50     565.25     10/20/2017       OW-06     582.36     10/20/2017     14.50     565.25     10/20/2017       OW-06     582.36     10/20/2017     17.19     565.17     Casing tab for lock corroded.       OW-06     582.36     10/20/2017     4.25     575.08     10/20/2017       SG-02     579.57     10/20/2017     4.75     574.82     10/20/2017			-	Lo	wer Sand Wells	5				
OW-15     579.56     10/20/2017     11.68     567.88     Casing tab for lock corroded.       OW-01B     579.14     10/20/2017     13.62     565.52        OW-03     579.56     10/20/2017     13.98     565.58     14.50' from TOC (0.52' above TOIC).       OW-04     579.45     10/20/2017     14.10     565.35         OW-05     579.75     10/20/2017     14.10     565.35          OW-06     582.36     10/20/2017     14.50     565.25          OW-05     579.75     10/20/2017     14.50     565.25          OW-06     582.36     10/20/2017     14.50     565.17     Casing tab for lock corroded.       OW-06     582.36     10/20/2017     4.25     575.08         SG-01     579.57     10/20/2017     4.75     574.82	OW-14A	580.05	10/20/2017	11.60	568.45	Casing tab for lock corroded.				
Glacial Till Wells       OW-01B     579.14     10/20/2017     13.62     565.52       OW-03     579.56     10/20/2017     13.98     565.58     14.50' from TOC (0.52' above TOIC).       OW-04     579.45     10/20/2017     14.10     565.35     10/20/2017       OW-05     579.75     10/20/2017     14.50     565.25     10/20/2017       OW-06     582.36     10/20/2017     17.19     565.17     Casing tab for lock corroded.       Staff Gauges       SG-01     579.33     10/20/2017     4.25     575.08       SG-02     579.57     10/20/2017     4.75     574.82	OW-15	579.56	10/20/2017	11.68	567.88	Casing tab for lock corroded.				
OW-01B     579.14     10/20/2017     13.62     565.52       OW-03     579.56     10/20/2017     13.98     565.58     14.50' from TOC (0.52' above TOIC).       OW-04     579.45     10/20/2017     14.10     565.35        OW-05     579.75     10/20/2017     14.50     565.25        OW-06     582.36     10/20/2017     17.19     565.17     Casing tab for lock corroded.       Staff Gauges       SG-01     579.33     10/20/2017     4.25     575.08       SG-02     579.57     10/20/2017     4.75     574.82				G	lacial Till Wells					
OW-03     579.56     10/20/2017     13.98     565.58     14.50' from TOC (0.52' above TOIC).       OW-04     579.45     10/20/2017     14.10     565.35        OW-05     579.75     10/20/2017     14.50     565.25        OW-06     582.36     10/20/2017     17.19     565.17     Casing tab for lock corroded.       Staff Gauges       SG-01     579.33     10/20/2017     4.25     575.08       SG-02     579.57     10/20/2017     4.75     574.82	OW-01B	579.14	10/20/2017	13.62	565.52					
OW-04     579.45     10/20/2017     14.10     565.35       OW-05     579.75     10/20/2017     14.50     565.25       OW-06     582.36     10/20/2017     17.19     565.17     Casing tab for lock corroded.       Staff Gauges       SG-01     579.53     10/20/2017     4.25     575.08       SG-02     579.57     10/20/2017     4.75     574.82	OW-03	579.56	10/20/2017	13.98	565.58	14.50' from TOC (0.52' above TOIC).				
OW-05     579.75     10/20/2017     14.50     565.25       OW-06     582.36     10/20/2017     17.19     565.17     Casing tab for lock corroded.       Staff Gauges       SG-01     579.33     10/20/2017     4.25     575.08       SG-02     579.57     10/20/2017     4.75     574.82	OW-04	579.45	10/20/2017	14.10	565.35					
OW-06     582.36     10/20/2017     17.19     565.17     Casing tab for lock corroded.       Staff Gauges       SG-01     579.33     10/20/2017     4.25     575.08        SG-02     579.57     10/20/2017     4.75     574.82	OW-05	579.75	10/20/2017	14.50	565.25					
Staff Gauges       SG-01     579.33     10/20/2017     4.25     575.08       SG-02     579.57     10/20/2017     4.75     574.82	OW-06	582.36	10/20/2017	17.19	565.17	Casing tab for lock corroded.				
SG-01     579.33     10/20/2017     4.25     575.08       SG-02     579.57     10/20/2017     4.75     574.82					Staff Gauges					
SG-02 579.57 10/20/2017 4.75 574.82	SG-01	579.33	10/20/2017	4.25	575.08					
	SG-02	579.57	10/20/2017	4.75	574.82					

Table 5-2H Summary of Water Level Measurements: October 20, 2017 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York



Department of Environmental Conservation

#### Notes:

1 = Elevations are referenced to North American Vertical Datum of 1988 (NAVD 88).

2 = Above Mean Sea Level.

Hydrographs suggest that the yellow shaded depth to water is likely an incorrect reading. Note 1: Historic water level data suggests that 2 numbers were transposed.

## Table 5-21 Summary of Water Level Measurements: October 27, 2017 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York



Location ID     Point Elevation <sup>1</sup> (ft amsl <sup>2</sup> )     Measurement Date     Depth to Water (ft)     Water Elevation <sup>1</sup> (feet amsl)     Note       0W-01     578.30     10/27/2017     3.91     574.39     Original depth to water was 5.54. See note 1.       0W-13     579.33     10/27/2017     4.54     574.79     Original depth to water was 5.54. See note 1.       0W-14B     579.92     10/27/2017     5.09     574.83     Heaved       0W-14B     580.03     10/27/2017     5.25     574.78     Original depth to water was 5.54. See note 1.       0W-16     581.88     10/27/2017     5.91     574.09     Owned to water was 5.54. See note 1.       0W-21     580.00     10/27/2017     5.91     574.09     Owned to water was 5.54. See note 1.       0W-22     579.46     10/27/2017     5.42     574.04     Owned to water was 5.54. See note 1.       0W-31     580.64     10/27/2017     7.10     573.54     Owned to water wate
ID     Elevation1 (ft amsi <sup>2</sup> )     Date     Water (ft)     Elevation1 (feet amsi)     Note       0W-01     578.30     10/27/2017     3.91     574.39     Original depth to water was 5.54. See note 1.       0W-13     579.33     10/27/2017     4.54     574.79     Original depth to water was 5.54. See note 1.       0W-14B     579.92     10/27/2017     5.09     574.83     Heaved       0W-14B     580.03     10/27/2017     5.25     574.78     Owned       0W-16     581.88     10/27/2017     5.25     574.78     Owned       0W-21     580.00     10/27/2017     5.42     574.09     Owned       0W-21     580.00     10/27/2017     5.42     574.04     Owned       0W-22     579.46     10/27/2017     5.42     574.04     Owned     Owned       0W-31     580.64     10/27/2017     7.10     573.54     Owned     Owned     Owned     Owned     S74.03     Owned     Owned     S81.57     10/27/2017     7.35     574.09     Owned     S81.57
(ft amsl <sup>2</sup> )     (feet amsl)       Fill/Upper Sand Wells       OW-01     578.30     10/27/2017     3.91     574.39       OW-13     579.33     10/27/2017     4.54     574.79     Original depth to water was 5.54. See note 1.       OW-14B     579.92     10/27/2017     5.09     574.83     Heaved       OW-14BR     580.03     10/27/2017     5.25     574.78        OW-16     581.88     10/27/2017     7.91     573.97        OW-21     580.00     10/27/2017     5.91     574.09        OW-22     579.46     10/27/2017     5.42     574.04        OW-31     580.64     10/27/2017     7.10     573.54        OW-32     581.44     10/27/2017     7.35     574.09        OW-33     582.43     10/27/2017     7.35     574.03        OW-34     581.10     10/27/2017     6.55     574.55        OW-35     581.57     10/27/2017     6.55     574.
Fill/Upper Sand Wells       OW-01     578.30     10/27/2017     3.91     574.39       OW-13     579.33     10/27/2017     4.54     574.79     Original depth to water was 5.54. See note 1.       OW-14B     579.92     10/27/2017     5.09     574.83     Heaved       OW-14BR     580.03     10/27/2017     5.25     574.78       OW-16     581.88     10/27/2017     7.91     573.97       OW-21     580.00     10/27/2017     5.42     574.09       OW-22     579.46     10/27/2017     5.42     574.71       OW-31     580.64     10/27/2017     7.10     573.54       OW-32     579.26     10/27/2017     7.35     574.09       OW-31     580.64     10/27/2017     7.35     574.09       OW-32     581.44     10/27/2017     7.35     574.09       OW-33     582.43     10/27/2017     6.55     574.55       OW-34     581.10     10/27/2017     6.55     574.55       OW-35     581.57
OW-01     578.30     10/27/2017     3.91     574.39       OW-13     579.33     10/27/2017     4.54     574.79     Original depth to water was 5.54. See note 1.       OW-14B     579.92     10/27/2017     5.09     574.83     Heaved       OW-14BR     580.03     10/27/2017     5.25     574.78        OW-16     581.88     10/27/2017     7.91     573.97        OW-21     580.00     10/27/2017     5.91     574.09        OW-22     579.46     10/27/2017     5.42     574.04        OW-23     579.26     10/27/2017     4.55     574.71        OW-31     580.64     10/27/2017     7.10     573.54        OW-32     581.44     10/27/2017     7.35     574.09         OW-33     582.43     10/27/2017     7.35     574.09         OW-34     581.10     10/27/2017     6.55     574.55          OW-35
OW-13     579.33     10/27/2017     4.54     574.79     Original depth to water was 5.54. See note 1.       OW-14B     579.92     10/27/2017     5.09     574.83     Heaved       OW-14BR     580.03     10/27/2017     5.25     574.78       OW-16     581.88     10/27/2017     5.25     574.78       OW-21     580.00     10/27/2017     5.91     574.09       OW-22     579.46     10/27/2017     5.42     574.04       OW-33     580.64     10/27/2017     7.10     573.54       OW-32     581.44     10/27/2017     7.35     574.09       OW-33     582.43     10/27/2017     7.35     574.09       OW-34     581.10     10/27/2017     7.35     574.09       OW-33     582.43     10/27/2017     7.31     574.26       OW-34     581.57     10/27/2017     6.55     574.55       OW-35     581.57     10/27/2017     7.31     574.26       OW-36     580.95     10/27/2017     5.81     574.34
OW-14B     579.92     10/27/2017     5.09     574.83     Heaved       OW-14BR     580.03     10/27/2017     5.25     574.78        OW-16     581.88     10/27/2017     7.91     573.97        OW-21     580.00     10/27/2017     5.91     574.09        OW-22     579.46     10/27/2017     5.42     574.04        OW-33     580.64     10/27/2017     7.10     573.54        OW-32     581.44     10/27/2017     7.35     574.09        OW-33     582.43     10/27/2017     7.35     574.09        OW-34     581.10     10/27/2017     7.35     574.09        OW-34     581.10     10/27/2017     7.35     574.03        OW-35     581.57     10/27/2017     6.55     574.55        OW-36     580.95     10/27/2017     7.31     574.26        OW-37     580.15     10/27/2017     5.81     574.34     <
OW-14BR     580.03     10/27/2017     5.25     574.78       OW-16     581.88     10/27/2017     7.91     573.97       OW-21     580.00     10/27/2017     5.91     574.09       OW-22     579.46     10/27/2017     5.42     574.04       OW-23     579.26     10/27/2017     4.55     574.71       OW-31     580.64     10/27/2017     7.10     573.54       OW-32     581.44     10/27/2017     7.35     574.09       OW-33     582.43     10/27/2017     8.40     574.03       OW-34     581.10     10/27/2017     6.55     574.55       OW-35     581.57     10/27/2017     7.31     574.26       OW-36     580.95     10/27/2017     5.81     574.34       OW-37     580.15     10/27/2017     5.81     574.34       OW-37     580.15     10/27/2017     5.81     574.34       OW-37     580.34     10/27/2017     5.81     574.34
OW-16     581.88     10/27/2017     7.91     573.97       OW-21     580.00     10/27/2017     5.91     574.09       OW-22     579.46     10/27/2017     5.42     574.04       OW-23     579.26     10/27/2017     4.55     574.71       OW-31     580.64     10/27/2017     7.10     573.54       OW-32     581.44     10/27/2017     7.35     574.09       OW-33     582.43     10/27/2017     7.35     574.09       OW-34     581.10     10/27/2017     8.40     574.03       OW-35     581.57     10/27/2017     6.55     574.55       OW-36     580.95     10/27/2017     7.31     574.26       OW-37     580.15     10/27/2017     6.61     574.34       OW-37     580.15     10/27/2017     5.81     574.34       OW-37     580.15     10/27/2017     5.81     574.34       OW-37     580.34     10/27/2017     5.81     574.34
OW-21     580.00     10/27/2017     5.91     574.09       OW-22     579.46     10/27/2017     5.42     574.04       OW-23     579.26     10/27/2017     4.55     574.71       OW-31     580.64     10/27/2017     7.10     573.54       OW-32     581.44     10/27/2017     7.35     574.09       OW-33     582.43     10/27/2017     7.35     574.09       OW-34     581.10     10/27/2017     8.40     574.03       OW-34     581.10     10/27/2017     6.55     574.55       OW-35     581.57     10/27/2017     7.31     574.26       OW-36     580.95     10/27/2017     6.61     574.34       OW-37     580.15     10/27/2017     5.81     574.34       DW-37     580.34     10/27/2017     5.81     574.34       LDP-01     580.34     10/27/2017     6.33     574.01     TD = 8.36 (TOIC). BTM Elev = 571.98
OW-22     579.46     10/27/2017     5.42     574.04       OW-23     579.26     10/27/2017     4.55     574.71       OW-31     580.64     10/27/2017     7.10     573.54       OW-32     581.44     10/27/2017     7.35     574.09       OW-33     582.43     10/27/2017     8.40     574.03       OW-34     581.10     10/27/2017     6.55     574.55       OW-35     581.57     10/27/2017     7.31     574.26       OW-36     580.95     10/27/2017     6.61     574.34       OW-37     580.15     10/27/2017     5.81     574.34       OW-37     580.34     10/27/2017     5.81     574.34       LDP-01     580.34     10/27/2017     6.33     574.01     TD = 8.36 (TOIC). BTM Elev = 571.98
OW-23     579.26     10/27/2017     4.55     574.71       OW-31     580.64     10/27/2017     7.10     573.54       OW-32     581.44     10/27/2017     7.35     574.09       OW-33     582.43     10/27/2017     8.40     574.03       OW-34     581.10     10/27/2017     6.55     574.55       OW-35     581.57     10/27/2017     7.31     574.26       OW-36     580.95     10/27/2017     6.61     574.34       OW-37     580.15     10/27/2017     5.81     574.34       DW-37     580.15     10/27/2017     5.81     574.34       DW-37     580.34     10/27/2017     5.81     574.34
OW-31     580.64     10/27/2017     7.10     573.54       OW-32     581.44     10/27/2017     7.35     574.09       OW-33     582.43     10/27/2017     8.40     574.03       OW-34     581.10     10/27/2017     6.55     574.55       OW-35     581.57     10/27/2017     7.31     574.26       OW-36     580.95     10/27/2017     6.61     574.34       OW-37     580.15     10/27/2017     5.81     574.34       LDP-01     580.34     10/27/2017     6.33     574.01     TD = 8.36 (TOIC). BTM Elev = 571.98
OW-32     581.44     10/27/2017     7.35     574.09       OW-33     582.43     10/27/2017     8.40     574.03       OW-34     581.10     10/27/2017     6.55     574.55       OW-35     581.57     10/27/2017     7.31     574.26       OW-36     580.95     10/27/2017     6.61     574.34       OW-37     580.15     10/27/2017     5.81     574.34       LDP-01     580.34     10/27/2017     6.33     574.01     TD = 8.36 (TOIC). BTM Elev = 571.98
OW-33     582.43     10/27/2017     8.40     574.03       OW-34     581.10     10/27/2017     6.55     574.55       OW-35     581.57     10/27/2017     7.31     574.26       OW-36     580.95     10/27/2017     6.61     574.34       OW-37     580.15     10/27/2017     5.81     574.34       LDP-01     580.34     10/27/2017     6.33     574.01     TD = 8.36 (TOIC). BTM Elev = 571.98
OW-34     581.10     10/27/2017     6.55     574.55       OW-35     581.57     10/27/2017     7.31     574.26       OW-36     580.95     10/27/2017     6.61     574.34       OW-37     580.15     10/27/2017     5.81     574.34       LDP-01     580.34     10/27/2017     6.33     574.01     TD = 8.36 (TOIC). BTM Elev = 571.98
OW-35     581.57     10/27/2017     7.31     574.26       OW-36     580.95     10/27/2017     6.61     574.34       OW-37     580.15     10/27/2017     5.81     574.34       LDP-01     580.34     10/27/2017     6.33     574.01     TD = 8.36 (TOIC). BTM Elev = 571.98
OW-36     580.95     10/27/2017     6.61     574.34       OW-37     580.15     10/27/2017     5.81     574.34       LDP-01     580.34     10/27/2017     6.33     574.01     TD = 8.36 (TOIC). BTM Elev = 571.98
OW-37     580.15     10/27/2017     5.81     574.34       LDP-01     580.34     10/27/2017     6.33     574.01     TD = 8.36 (TOIC). BTM Elev = 571.98
LDP-01 580.34 10/27/2017 6.33 574.01 TD = 8.36 (TOIC). BTM Elev = 571.98
LDP-02 581.03 10/27/2017 6.47 574.56
LDP-03 580.73 10/27/2017 6.39 574.34
LDP-04 581.42 10/27/2017 7.29 574.13
LPZ-01S 580.31 10/27/2017 5.54 574.77
LPZ-02S 581.03 10/27/2017 6.37 574.66
LPZ-03S 581.16 10/27/2017 6.58 574.58
LPZ-04S 579.68 10/27/2017 5.15 574.53
LPZ-05S 580.41 10/27/2017 6.13 574.28
LPZ-06S 581.00 10/27/2017 6.42 574.58
LPZ-07S 580.56 10/27/2017 6.60 573.96
LPZ-08S 579.47 10/27/2017 4.78 574.69
LPZ-09S 581.51 10/27/2017 7.44 574.07
LPZ-10S 580.38 10/27/2017 6.14 574.24
LPZ-11S 579.96 10/27/2017 5.23 574.73
LPZ-12S 580.03 10/27/2017 5.39 574.64
LPZ-13S 581.66 10/27/2017 7.55 574.11
Silty Clay & Red-Gray Clay Aquitard Wells
OW-02 577.26 10/27/2017 2.42 574.84 3.35' from TOC (0.92' above TOIC)
Lower Sand Wells
OW-14A 580.05 10/27/2017 11.39 568.66 Casing tab for lock corroded.
OW-15 579.56 10/27/2017 11.62 567.94 Casing tab for lock corroded.
Glacial Till Wells
OW-01B 579.14 10/27/2017 13.62 565.52
OW-03 579.56 10/27/2017 13.97 565.59 14.50' from TOC (0.52' above TOIC)
OW-04 579.45 10/27/2017 13.85 565.60
OW-05 579.75 10/27/2017 14.45 565.30
OW-06 582.36 10/27/2017 17.32 565.04 Casing tab for lock corroded.
Staff Gauges
SG-01 579.33 10/27/2017 4.36 574.97
SG-02 579.57 10/27/2017 4.93 574.64

Table 5-21 Summary of Water Level Measurements: October 27, 2017 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York



Department of Environmental Conservation

### Notes:

1 = Elevations are referenced to North American Vertical Datum of 1988 (NAVD 88).

2 = Above Mean Sea Level.

Note 1: Hydrographs suggest that the original depth to water is 1 foot too high.

## Table 5-2J Summary of Water Level Measurements: November 7 & 8, 2017 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York



	Measuring									
Location	Point	Measurement	Depth to	water						
ID	Elevation <sup>1</sup>	Date	Water (ft)	Elevation	Note					
	(ft amsl <sup>2</sup> )			(feet amsl)						
Fill/Upper Sand Wells										
OW-01	578.30	11/7/2017	2.51	575.79						
OW-13	579.33	11/7/2017	4.01	575.32	Casing tab for lock corroded & outer casing heaved					
OW-14B	579.92	11/7/2017	4.52	575.40	Outer casing has heaved.					
OW-14BR	580.03	11/7/2017	4.72	575.31						
OW-16	581.88	11/7/2017	7.00	574.88						
OW-21	580.00	11/7/2017	4.06	575.94						
OW-22	579.46	11/7/2017	3.75	575.71						
OW-23	579.26	11/7/2017	3.76	575.50						
OW-31	580.64	11/7/2017	4.77	575.87						
OW-32	581.44	11/7/2017	6.56	574.88						
OW-33	582.43	11/7/2017	7.41	575.02						
OW-34	581.10	11/7/2017	5.10	576.00						
OW-35	581.57	11/7/2017	6.64	574.93						
OW-36	580.95	11/7/2017	5.65	575.30						
OW-37	580.15	11/7/2017	5.19	574.96						
LDP-01	580.34	11/7/2017	3.97	576.37	TD = 8.36 (TOIC), BTM Elev = 571.98					
LDP-02	581.03	11/7/2017	4.55	576.48						
LDP-03	580.73	11/7/2017	4.25	576.48						
LDP-04	581.42	11/7/2017	6.09	575.33						
LPZ-01S	580.31	11/7/2017	5.04	575.27						
LPZ-02S	581.03	11/7/2017	5.75	575.28						
LPZ-03S	581.16	11/7/2017	4.81	576.35						
LPZ-04S	579.68	11/7/2017	5.02	574.66						
LPZ-05S	580.41	11/7/2017	3.85	576.56						
LPZ-06S	581.00	11/7/2017	4.32	576.68						
LPZ-07S	580.56	11/7/2017	4.90	575.66						
LPZ-08S	579.47	11/7/2017	4.23	575.24						
LPZ-09S	581.51	11/7/2017	6.61	574.90						
LPZ-10S	580.38	11/7/2017	4.73	575.65						
LPZ-11S	579.96	11/8/2017	4.55	575.41						
LPZ-12S	580.03	11/7/2017	4.67	575.36						
LPZ-13S	581.66	11/7/2017	6.37	575.29						
			Silty Clay & Re	d-Gray Clay Aq	uitard Wells					
OW-02	577.26	11/7/2017	1.82	575.44	3.35' from TOC (0.92' above TOIC)					
			Lo	wer Sand Wells						
OW-14A	580.05	11/7/2017	11.19	568.86	Casing tab for lock corroded.					
OW-15	579.56	11/7/2017	11.45	568.11	Casing tab for lock corroded.					
			G	lacial Till Wells						
OW-01B	579.14	11/7/2017	13.71	565.43						
OW-03	579.56	11/7/2017	14.06	565.50	14.50' from TOC (0.52' above TOIC)					
OW-04	579.45	11/7/2017	14,19	565.26						
OW-05	579.75	11/7/2017	14,61	565.14						
OW-06	582.36	11/7/2017	17,28	565.08	Casing tab for lock corroded.					
0.700	002.00	,.,.01,	2.120	Staff Gauges						
SG 01	570.22	11/7/2017	4.00	575 22						
30-01	573.33	11/7/2017	4.00	5/5.33						
<u>3G-02</u>	5/9.5/	11///201/	4.22	575.35						

Table 5-2J Summary of Water Level Measurements: November 7 & 8, 2017 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York



Department of Environmental Conservation

Notes:

1 = Elevations are referenced to North American Vertical Datum of 1988 (NAVD 88).

## Table 5-2K Summary of Water Level Measurements: November 21, 2019 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York



	Measuring									
Location	Point	Measurement	Depth to	Water						
ID	<b>Elevation</b> <sup>1</sup>	Date	Water (ft)	Elevation	Note					
	(ft amsl <sup>2</sup> )			(feet amsl)						
	Fill/Upper Sand Wells									
OW-01	578.30	11/21/2019	3.72	574.58						
OW-13	579.33	11/21/2019	4.63	574.70						
OW-14B	579.92	11/21/2019	5.14	574.78						
OW-14BR	580.03	11/21/2019	4.93	575.10						
OW-16	581.88	11/21/2019	8.25	573.63						
OW-21	580.00	11/21/2019	5.94	574.06						
OW-22	579.46	11/21/2019	5.45	574.01						
OW-23	579.26	11/21/2019	4.48	574.78						
OW-31	580.64	11/21/2019	NM	NA						
OW-32	581.44	11/21/2019	7.80	573.64						
OW-33	582.43	11/21/2019	8.58	573.85						
OW-34	581.10	11/21/2019	5.90	575.20						
OW-35	581.57	11/21/2019	7.41	574.16						
OW-36	580.95	11/21/2019	6.64	574.31						
OW-37	580.15	11/21/2019	5.47	574.68						
LDP-01	580.34	11/21/2019	3.83	576.51						
LDP-02	581.03	11/21/2019	4.58	576.45						
LDP-03	580.73	11/21/2019	4.40	576.33						
LDP-04	581.42	11/21/2019	7.40	574.02						
LPZ-01S	580.31	11/21/2019	5.30	575.01						
LPZ-02S	581.03	11/21/2019	6.80	574.23						
LPZ-03S	581.16	11/21/2019	5.36	575.80						
LPZ-04S	579.68	11/21/2019	3.63	576.05						
LPZ-05S	580.41	11/21/2019	4.76	575.65						
LPZ-06S	581.00	11/21/2019	5.31	575.69						
LPZ-07S	580.56	11/21/2019	6.59	573.97						
LPZ-08S	579.47	11/21/2019	4.88	574.59						
LPZ-09S	581.51	11/21/2019	7.79	573.72						
LPZ-10S	580.38	11/21/2019	6.03	574.35						
LPZ-11S	579.96	11/21/2019	4.75	575.21						
LPZ-12S	580.03	11/21/2019	5.08	574.95						
LPZ-13S	581.66	11/21/2019	8.43	573.23						
			Silty Clay & Re	d-Gray Clay Aqu	uitard Wells					
OW-02 577.26 11/21/2019 NM NA										
	Lower Sand Wells									
OW-14A	580.05	11/21/2019	NM	NA						
OW-15	579.56	11/21/2019	NM	NA						
			G	lacial Till Wells						
OW-01B	579.14	11/21/2019	NM	NA						
OW-03	579.56	11/21/2019	NM	NA						
OW-04	579.45	11/21/2019	NM	NA						
OW-05	579.75	11/21/2019	NM	NA						
OW-06	582.36	11/21/2019	NM	NA						
				Staff Gauges						
SG-01	579.33	11/21/2019	NM	NA						
SG-02	579.57	11/21/2019	NM	NA						

Table 5-2K Summary of Water Level Measurements: November 21, 2019 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York



Department of Environmental Conservation

Notes:

1 = Elevations are referenced to North American Vertical Datum of 1988 (NAVD 88).

2 = Above Mean Sea Level.

NA = Not applicable.

NM = Not measured.

## Table 5-2L Summary of Water Level Measurements: April 3, 2020 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York



	Measuring			Matar					
Location	Point	Measurement	Depth to	water	Nete				
ID	<b>Elevation</b> <sup>1</sup>	Date	Water (ft)	Elevation	Νοτε				
	(ft amsl <sup>2</sup> )			(feet amsl)					
Fill/Upper Sand Wells									
OW-01	578.30	4/3/2020	1.72	576.58					
OW-13	579.33	4/3/2020	3.21	576.12					
OW-14B	579.92	4/3/2020	3.72	576.20					
OW-14BR	580.03	4/3/2020	4.41	575.62					
OW-16	581.88	4/3/2020	4.90	576.98					
OW-21	580.00	4/3/2020	2.99	577.01					
OW-22	579.46	4/3/2020	2.49	576.97					
OW-23	579.26	4/3/2020	3.09	576.17					
OW-31	580.64	4/3/2020	3.51	577.13					
OW-32	581.44	4/3/2020	4.76	576.68					
OW-33	582.43	4/3/2020	6.08	576.35					
OW-34	581.10	4/3/2020	4.15	576.95					
OW-35	581.57	4/3/2020	4.85	576.72					
OW-36	580.95	4/3/2020	4.23	576.72					
OW-37	580.15	4/3/2020	3.60	576.55					
LDP-01	580.34	4/3/2020	3.56	576.78					
LDP-02	581.03	4/3/2020	4.12	576.91					
LDP-03	580.73	4/3/2020	4.34	576.39					
LDP-04	581.42	4/3/2020	4.66	576.76					
LPZ-01S	580.31	4/3/2020	4.55	575.76					
LPZ-02S	581.03	4/3/2020	4.80	576.23					
LPZ-03S	581.16	4/3/2020	4.41	576.75					
LPZ-04S	579.68	4/3/2020	2.96	576.72					
LPZ-05S	580.41	4/3/2020	3.28	577.13					
LPZ-06S	581.00	4/3/2020	3.97	577.03					
LPZ-07S	580.56	4/3/2020	3.60	576.96					
LPZ-08S	579.47	4/3/2020	3.48	575.99					
LPZ-09S	581.51	4/3/2020	4.79	576.72					
LPZ-10S	580.38	4/3/2020	3.43	576.95					
LPZ-11S	579.96	4/3/2020	3.76	576.20					
LPZ-12S	580.03	4/3/2020	3.30	576.73					
LPZ-13S	581.66	4/3/2020	5.44	576.22					
			Silty Clay & Re	d-Gray Clay Aqu	uitard Wells				
OW-02 577.26 4/3/2020 NM NA									
			Lo	wer Sand Wells					
OW-14A	580.05	4/3/2020	NM	NA					
OW-15	579.56	4/3/2020	NM	NA					
			G	lacial Till Wells					
OW-018	579 14	4/3/2020	NM	NΔ					
0\\/_03	579 56	4/3/2020	NM	ΝΔ					
OW-04	579.30	4/3/2020	NM	NΔ					
OW-05	579 75	4/3/2020	NM	NΔ					
0W-06	582.36	4/3/2020	NM	NΔ					
010-00	562.50	7/3/2020							
SC 01	E70.22	4/2/2020	NIN 4						
56-01	579.33	4/3/2020		NA NA					
SG-02	579.57	4/3/2020	NM	NA					

Table 5-2L Summary of Water Level Measurements: April 3, 2020 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York



Department of Environmental Conservation

Notes:

1 = Elevations are referenced to North American Vertical Datum of 1988 (NAVD 88).

2 = Above Mean Sea Level.

NA = Not applicable.

NM = Not measured.

## Table 5-2M Summary of Water Level Measurements: November 23, 2021 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York



	Measuring			Matan					
Location	Point	Measurement	Depth to	water					
ID	<b>Elevation</b> <sup>1</sup>	Date	Water (ft)	Elevation	Note				
	(ft amsl <sup>2</sup> )			(feet amsl)					
Fill/Upper Sand Wells									
OW-01	578.30	11/23/2021	2.21	576.09					
OW-13	579.33	11/23/2021	3.81	575.52					
OW-14B	579.92	11/23/2021	4.35	575.57					
OW-14BR	580.03	11/23/2021	4.63	575.40					
OW-16	581.88	11/23/2021	6.00	575.88					
OW-21	580.00	11/23/2021	3.58	576.42					
OW-22	579.46	11/23/2021	3.11	576.35					
OW-23	579.26	11/23/2021	3.71	575.55					
OW-31	580.64	11/23/2021	3.95	576.69					
OW-32	581.44	11/23/2021	6.15	575.29					
OW-33	582.43	11/23/2021	7.14	575.29					
OW-34	581.10	11/23/2021	4.92	576.18					
OW-35	581.57	11/23/2021	6.21	575.36					
OW-36	580.95	11/23/2021	5.20	575.75					
OW-37	580.15	11/23/2021	4.91	575.24					
LDP-01	580.34	11/23/2021	3.64	576.70					
LDP-02	581.03	11/23/2021	NM	NA					
LDP-03	580.73	11/23/2021	4.13	576.60					
LDP-04	581.42	11/23/2021	5.64	575.78					
LPZ-01S	580.31	11/23/2021	4.92	575.39					
LPZ-02S	581.03	11/23/2021	5.62	575.41					
LPZ-03S	581.16	11/23/2021	4.78	576.38					
LPZ-04S	579.68	11/23/2021	3.20	576.48					
LPZ-05S	580.41	11/23/2021	4.09	576.32					
LPZ-06S	581.00	11/23/2021	3.38	577.62					
LPZ-07S	580.56	11/23/2021	NM	NA					
LPZ-08S	579.47	11/23/2021	4.06	575.41					
LPZ-09S	581.51	11/23/2021	6.14	575.37					
LPZ-10S	580.38	11/23/2021	4.00	576.38					
LPZ-11S	579.96	11/23/2021	4.43	575.53					
LPZ-12S	580.03	11/23/2021	4.29	575.74					
LPZ-13S	581.66	11/23/2021	NM	NA					
			Silty Clay & Re	d-Gray Clay Aqu	uitard Wells				
OW-02	577.26	11/23/2021	NM	NA					
Lower Sand Wells									
OW-14A	580.05	11/23/2021	NM	NA					
OW-15	579.56	11/23/2021	NM	NA					
			G	lacial Till Wells					
OW-01B	579.14	11/23/2021	NM	NA					
OW-03	579.56	11/23/2021	NM	NA					
OW-04	579.45	11/23/2021	NM	NA					
OW-05	579.75	11/23/2021	NM	NA					
OW-06	582.36	11/23/2021	NM	NA					
		, -,		Staff Gauges					
SG-01	570.33	11/23/2021	NIN/	N/A					
SC 02	570 57	11/23/2021		NA					
30-02	519.51	11/23/2021	INIVI	INA					

Table 5-2M Summary of Water Level Measurements: November 23, 2021 NYSDEC Hydrogeologic Report Niagara Sanitation Landfill, Site No. 932054 Wheatfield, New York



Department of Environmental Conservation

Notes:

1 = Elevations are referenced to North American Vertical Datum of 1988 (NAVD 88).

2 = Above Mean Sea Level.

NA = Not applicable.

NM = Not measured.

### Table 5-3 Summary of Hydraulic Conductivity Testing Results NYSDEC Hydrogeologic Report Niagara Sanitation Site, Site No. 932054 Wheatfield, New York



Department of Environmental Conservation

Well Number	Screened * Interval (ft. bgs)	Test Type	Transmissivity (ft <sup>2</sup> /day)	Hydraulic Conductivity (cm/sec)	Description * of Screened Material				
Upper Sand Deposit									
OW-1	4.0 - 9.0	Falling Head	N/A	4.37E-04	Upper Sand/Silty Clay				
A	Arithmetic Mean:	N/A	N/A	4.37E-04					
	Geometric Mean:	N/A	N/A	4.37E-04					
Silty Clay & Red-Gray Clay Aquitard									
OW-2	9.0 - 14.0	Falling Head	N/A	6.75E-04	Silty Clay/Red-Gray Clay				
P	Arithmetic Mean:	N/A	N/A	6.75E-04					
	Geometric Mean:	N/A	N/A	6.75E-04					
	Glacial Till Deposit								
OW-1B	58.6 - 68.6	Falling Head	N/A	8.43E-07	Glacial Till				
OW-3	45.0 - 55.0	Falling Head	N/A	1.43E-06	Wet Zone in Till				
OW-4	59.0 - 69.0	Falling Head	N/A	7.88E-07	Glacial Till				
A	Arithmetic Mean:	N/A	N/A	1.02E-06					
	Geometric Mean:	N/A	N/A	9.83E-07					
		Gla	cial Till Deposit						
OW-5	60.0 - 70.0	Falling Head	N/A	7.50E-04	Glacial Till				
OW-6	56.0 - 66.0	Falling Head	N/A	6.80E-04	Glacial Till				
A	Arithmetic Mean:	N/A	N/A	7.15E-04					
	Geometric Mean:	N/A	N/A	7.14E-04					

Notes:

\* = Information from Table 4-1.

ft. bgs = Feet below ground surface.

N/A = Not Available.

Hydraulic conductivities for the Niagara Sanitation Landfill are summarized in Table IV.1 of the Phase II Report dated July 1985.