

**FINAL SUBSURFACE INVESTIGATION  
REPORT  
AAFE MIXED-USE BUILDING  
FLUSHING, NEW YORK**

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**January 13, 2017**

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January 13, 2017

JCJ Architecture  
404 Fifth Avenue, 3<sup>rd</sup> Floor  
New York, NY 10018

Attn: George Chin

Re: Final Subsurface Investigation  
AAFE Mixed-Use Building  
Flushing, Queens, New York  
MRCE File 12629

Dear Mr. Chin,

In accordance with our revised proposal, dated January 14, 2016, we have completed our final subsurface investigation for the referenced project comprising construction of a new, mixed-use building in Flushing, Queens, New York. This report summarizes the results of our final boring program, including additional observations and interpretation of subsurface conditions, and notes any revisions to recommendations provided for foundation design and construction in our October 2016 Preliminary Geotechnical Report.

**EXHIBITS**

The following exhibits are attached:

Drawing No. S-1	Site Location Plan
Drawing No. B-1	Boring Location Plan
Drawing No. GS-1	Geologic Section A-A
Drawing No. GS-2	Geologic Section B-B
Drawing No. GS-R	Geotechnical Reference Standards
Appendix A	MRCE Final Boring Logs
Appendix B	Adjacent Building Records

**PROJECT DATUM**

Elevations herein are referenced to the North American Vertical Datum (NAVD 1988) where El. 0.0 is 1.625 feet below the Queens Borough Datum.

**EXISTING SITE CONDITIONS**

The project site is located at 133-04 39<sup>th</sup> Avenue in Flushing, Queens, New York, at the southeast corner of College Point Boulevard and 39<sup>th</sup> Avenue as shown on Drawing No. S-1. The site comprises Block 4973, Lot 6 with a total area of about 13,388 square feet (sq. ft.). The formerly existing structures were demolished to grade and the parking lot surface removed in November 2016.

The site is generally level at around El. +45. A concrete retaining wall supports a

drop of about 6 to 7 feet between the site lot and the gas station lot to the south. The west sidewalk also slopes down from north to south to accommodate this grade change with a retaining wall constructed along the west property line to maintain fairly level site grades.

## **SITE GEOLOGY**

Bedrock was not encountered in any of the borings at the site. According to published data, bedrock lies about 200 feet below ground surface. The oldest and lowest sediments overlying bedrock are of Cretaceous age followed by Pleistocene age glacial deposits.

The site is at the edge of a deep valley carved into the Cretaceous Raritan clay. During the Pleistocene, a series of glaciers flowed across the region. The glaciers scoured the valley deeper, reworked the clay, and redeposited it as glacial sediments. With each advance and retreat, the ice typically deposited in and along the valley layers of till that may contain large slabs of Raritan clay, outwash sand and glacial lake silt and clay derived in part from the Raritan. In the process, the ice glacially sheared and loaded the older sediments below, densifying them, before depositing less dense soil above. Surficial fills placed by man to level and develop the site and surrounding area overlie the natural soil formations.

## **SUBSURFACE INVESTIGATION**

MRCE proposed a phased investigation consisting of six borings made in two phases (preliminary and final phase) to expedite the start of foundation design and satisfy NYC Building Code requirements for subsurface exploration. The preliminary investigation was intended to consist of five borings made in accessible areas (parking lot and sidewalk) and provide sufficient subsurface data to initiate foundation design. Subsurface data available from prior site investigations allowed reduction in the number of preliminary borings from five to three and addition of three Cone Penetration Test (CPT) soundings to assist in the preliminary investigation. CPT soundings provide a continuous record of soil strength and stiffness with depth and were added to facilitate a better evaluation of foundation performance during building design. We refer to our October 2016 Preliminary Subsurface Investigation Report for details of the previous investigations and findings.

The final subsurface investigation was performed following demolition of existing buildings in November 2016 and included two additional borings. A test pit was also planned as part of the final investigation to investigate the depth and character of foundations supporting the adjacent building along the east side of the site. However, the test pit was deleted from the final investigation following a records search in the Department of Buildings (Queens) which produced foundation design drawings for the adjacent building (See Appendix B).

### ***MRCE Final Phase Investigation***

Two additional borings (Borings MR-4P and MR-5U) were made in the southeast quarter of the site where former structures previously prevented access for drilling. The borings were drilled by Craig Test Boring, Inc. of Mays Landing, New Jersey on December 15<sup>th</sup>, 2016 under the continuous inspection of our Engineer, Mr. Eric Poon. As-built locations of the borings were determined by our Engineer by measuring distances from property features and are shown on Drawing No. B-1.

Borings were advanced with a truck-mounted CME 75 drill rig using wash-rotary methods with casing and biodegradable drilling mud to stabilize the borehole. Soil samples in MR-4P were collected continuously from ground surface to a depth to 12 feet and at five foot intervals thereafter. Soil samples in MR-5U were collected at five foot intervals from ground surface to end of boring. Soil samples were obtained by performing Standard Penetration Tests (SPT), where a standard, 2-inch O.D. split-spoon sampler is driven through four 6-inch intervals with a 140-pound hammer, free-falling 30 inches. The SPT resistance, also termed N-value and expressed in blows per foot (bpf), is an indication of the relative density of the

material sampled and is calculated by summing the blows from the second and third 6-inch intervals. In some instances, where the sampler was unable to penetrate the full 24 inches due to the presence of dense soils, large gravel, cobbles, boulders, or other obstructions, the sampler was driven until refusal (i.e. 50 to 100 blows were administered) and the actual penetration of the sampler was measured and recorded. Recovered soil samples were classified in the field in accordance with the Unified Soil Classification System (USCS) and placed in jars for preservation and transport to our laboratory.

One undisturbed sample was taken of the Stratum C clay encountered in Boring MR-5U by mechanically pushing a 3-inch diameter tube using a Shelby tube sampler. The length of push and recovery of the tube sample is recorded in the boring log for MR-5U in Appendix A. Upon recovery, the tube sample was sealed with hot wax and plastic end caps for sample preservation and transported to our laboratory. The recovered sample was classified in the field in accordance with the Unified Soil Classification System (USCS) and transported to our laboratory.

A deep well-point piezometer was installed in MR-4P at completion to monitor water levels. The piezometer consisted of two inch I.D. PVC standpipe installed to a depth of 75 feet. The bottom ten feet of the standpipe is slotted and surrounded by filter sand to allow free water movement into the piezometer without movement of soil particles. A falling head test was performed by filling the standpipe with water and measuring the drop in water level with time to ensure proper operation of the well. Logs of the completed borings are provided in Appendix A.

## LABORATORY TESTING PROGRAM

All soil samples were delivered to our soil mechanics laboratory in Manhattan. Samples were reviewed and field descriptions were revised as necessary for conformance with MRCE's Geotechnical Reference Standards, described on Drawing No. GS-R. Individual sample descriptions are provided on the final, typed boring logs in Appendix A.

**Index Testing:** Natural water contents were determined on all fine-grained soil (silt and clay) samples. The results of the water content determinations are included on the boring logs in Appendix A. Water contents are expressed as a percentage of the sample dry weight.

## SUBSURFACE CONDITIONS

We have updated soil strata descriptions from our October 2016 Preliminary Geotechnical Report to incorporate the results of the final borings. General descriptions of each of the strata, including material classification (Class) in accordance with the New York City Building Code (2014), are summarized below in order of their occurrence with depth. We refer to Geologic Sections A-A and B-B on Drawing Nos. GS-1 and GS-2 for a graphical representation of the variation in soil strata across the site.

**Stratum F – Fill (NYC Class 7):** The site is covered with fill comprised of natural soils reworked or transported by man. The fill ranges from loose to medium compact, brown fine to coarse sand, some to trace silt, trace to some gravel, trace brick to soft brown clayey silt, some to trace coarse to fine sand. The fill thickness is expected to vary across the site as it ranged between 8 and 13.5 feet in the MRCE borings. N-values range from 6 to refusal with an average of 13 bpf. The erratic sampling resistance indicates uncontrolled fill placement with the higher N-values typically the result of large gravel, cobbles, boulders or other obstructions within the fill. Remnant foundations and local concentrations of construction debris are also expected within the fill from prior site construction and the completed demolition of site structures.

**Stratum S – Sand (NYC Class 3b):** Sand underlies the fill in all borings and is interlayered with the underlying Stratum C clay (described below) in Borings MR-1 and MR-3U. Stratum S consists of loose to medium compact, brown fine to medium to fine to coarse sand, trace to some silt, and trace gravel. The

thickness of the sand ranges from 35 feet in MR-2U to between 2.5 and 15 feet where the sand is interlayered with Stratum C clay in MR-1 and MR-3U. N-values range from 4 to 36 bpf and average 17 bpf.

**Stratum C – Silty Clay (NYC Class 4b):** Stiff to hard clay exists below and is typically interlayered with the sand in all borings except Boring MR-4P made in the southeast corner of the site. Stratum C consists of stiff to hard brown, red-brown and gray silty clay, sometimes interlayered or varved with clayey silt, silt or fine to medium sand seams. In MR-2U, Stratum C underlies the Stratum S sand and is ten feet thick. In borings MR-1 and MR-3U, Stratum C is interlayered with Stratum S and ranges in thickness from five to 17.5 feet. The top of Stratum C varies from 23.5 feet (El. +15) in MR-3U to 48.5 feet (El. -4) in MR-2U. N-values range from 14 to 53 bpf with an average of 26 bpf. Natural water contents range from 25 to 40 percent, with an average value of 31 percent.

Slickensides are evident in many Stratum C samples. Slickensides in a soil are secondary structures that result from prior friction along a fault plane and are found in cohesive material that was disturbed or locally reworked after deposition. These slickensides then become irregular planes of weakness which affect the clay strength. Compression tests on undisturbed samples of Stratum C indicate a range in clay shear strength between 1.9 and 2.1 kips per square foot (ksf).

The consolidation tests indicate that the clay stratum is moderately to heavily over-consolidated with an over-consolidation ratio (OCR) greater than 4. The OCR is the ratio of the pre-consolidation pressure as determined from consolidation testing to the estimated existing overburden pressure at the sample depth.

**Stratum T – Till (NYC Class 3a):** Glacial till underlies the clay deposits. Stratum T consists of medium compact to very compact, brown to gray fine to coarse sand, trace to some silt with layers and pockets of clayey sand and trace gravel, lignite. The top of the till ranges in depth from 43.5 feet (El. +1) in MR-4P to 58.5 feet (El. -14) in MR-2U. N-values vary between 24 and 107 bpf with an average of 58 bpf. Three fine-grained till samples encountered in Borings MR-1 and MR-3 show an average water content of 21 percent.

**Groundwater:** Groundwater levels were typically measured during borehole advance and are shown on the boring logs and geologic sections. Borehole levels may not represent stabilized water levels and therefore may not be indicative of the groundwater regime.

Groundwater levels measured in January 2017 in the deep piezometer MR-4 range from a depth of 47.9 to 49.7 feet below the standpipe rim, or between El. -2.0 and El. -3.8. In comparison, ground water levels measured in the shallower environmental monitoring wells installed by Roux Associates, Inc. in June 2016 range from a depth of 35 to 36.5 feet below ground surface, or between about El. +8.3 and El. +9.7.

The deeper water levels measured in January 2017 are attributed to on-going dewatering for a deep excavation in progress across the street from the AAFE project site at the northeast corner of the intersection of 39<sup>th</sup> Avenue and College Point Boulevard. We understand that the adjacent excavation requires groundwater lowering of about twenty (20) feet, or to about El. -10. It is likely, given the granular deposits and discontinuous nature of the clay strata at the AAFE site, that this work has affected the groundwater levels at the Project site. However, water perched at the top of the Stratum C clay is still anticipated even with on-going dewatering and may result in groundwater encountered at higher elevation in excavations at the Project site.

Groundwater levels are expected to vary seasonally throughout the year depending on precipitation levels and surface water infiltration. As such, the groundwater level at the time of construction may be different from levels observed during our field investigations.

## FOUNDATION DESIGN AND CONSTRUCTION RECOMMENDATIONS

The results of the final subsurface investigation are generally consistent with the findings of our preliminary investigation. Foundation recommendations in our October 2016 Preliminary Report therefore remain applicable. Recommendations below are intended to enhance or supplement our prior recommendations:

1. **Soil Profile:** The additional borings (MR-4P and MR-5U) further demonstrate the variability of the natural soils within the proposed depth of excavation. The Stratum C clay is interlayered with the Stratum S sand and locally missing in some areas. However, soils at mat subgrade are expected to consist of predominantly of the stiff to hard clays of Stratum C. These sensitive soils are susceptible to softening and disturbance by construction operations, particularly in the presence of water or freezing weather.

Proper performance of the mat foundation requires support on undisturbed soil subgrade. Final subgrade exposure must be made using a smooth edged excavating tool, such as a backhoe or bucket with the teeth shielded, and operating by reach of equipment and working on mats or at least two feet above subgrade. All water must be diverted away from and not allowed to pond in excavations. Mat construction should either proceed immediately after subgrade approval or subgrade promptly covered with a lean concrete mud to protect subgrade materials from subsequent deterioration from weather, surface water infiltration and construction traffic in the interim period until foundation construction

2. **Groundwater:** The deep piezometer MR-4P installed in the final investigation indicates that the adjacent construction at the site across 39<sup>th</sup> Avenue has lowered groundwater levels significantly at the site. However, the duration of this on-going work is unknown and such lowered site water levels should not be counted on during construction of the proposed AAFE project. In any event, even with on-going dewatering at the adjacent site, perched water at the top of the Stratum C clay is still anticipated and may result in groundwater encountered at higher elevation in excavations at the Project site. Dewatering considerations in our October 2016 Preliminary Report therefore remain applicable.
3. **Mat Foundation Settlements:** Incorporating the results of the final investigation in our settlement models confirms our prior recommendation that the design of the foundation mat should accommodate a differential settlement of one (1) inch between the center and corner of the mat.
4. **Underpinning and Protection of Adjacent Structures:** The adjacent building abutting the east property line has a single cellar level estimated at a depth of about 14 feet. From documentation found at the Department of Buildings (Queens), the adjacent building is supported on a narrow strip footing at a depth of approximately 15 feet (El. 30) below current site grades. In comparison, excavation for new building construction will require excavation to a depth of about 30 feet to general subgrade (El. 13.5) and locally deeper to 36 feet (El. 7.5) for elevator construction along the east property line. Underpinning of the adjacent foundations is therefore necessary. Underpinning will require obtaining permission from adjacent property owners which must be negotiated in advance of construction.
5. **Permeation Grouting:** The adjacent property along the east building line consists of a series of narrow buildings (13 to 14 feet wide) supported on shallow foundations bearing near the top of the Stratum S sands. The narrow width of the building places the footings supporting the common wall between the adjacent and neighboring building within the influence zone of the deep AAFE excavation. Permeation grouting of the Stratum S sand beneath the building is therefore recommended prior to underpinning to stabilize the sands, avoid ground loss and thereby mitigate movement of the adjacent buildings during underpinning and subsequent

excavation for foundation construction. Permeation grouting using sodium silicate grout is recommended due to the variable character of the Stratum S sands.

## **GEOTECHNICAL REVIEW OF FOUNDATION DESIGN & CONSTRUCTION**

The borings disclose a complex subsurface profile with interlayered sands and clays expected at and below foundation subgrade. This variable profile may result in foundations bearing on soil of different character and thickness. Interaction between the geotechnical and structural engineer is therefore essential as foundation design progresses to optimize building foundations and provide adequate building performance under the range in service loading conditions. Geotechnical review and assistance in preparation of foundation plans and specifications for below grade work is also recommended so that foundation and construction recommendations provided herein are properly interpreted and implemented in the design.

Recommendations for foundation design and construction in this report are based on the information obtained from the borings and associated field and laboratory testing. However, conditions on the site may vary between discrete boring locations and observed at the time of our subsurface exploration. The nature and extent of variations between borings may not become evident until exposed in construction. Geotechnical observation of foundation construction and testing is recommended to provide an opportunity to observe soil conditions and behavior as exposed during construction, evaluate the applicability of the recommendations provided in this report to the soil conditions encountered, and recommend appropriate changes in design or construction procedures if conditions differ from those described herein. We recommend that all foundation construction be observed by a qualified geotechnical engineer in accordance with the requirements of the NYC Building Code.

## **CLOSURE**

This report presents the results of our investigations and our recommendations for foundation design and construction for the proposed project. We will be pleased to answer questions regarding this report and further assist in design and construction of the project as you may request.

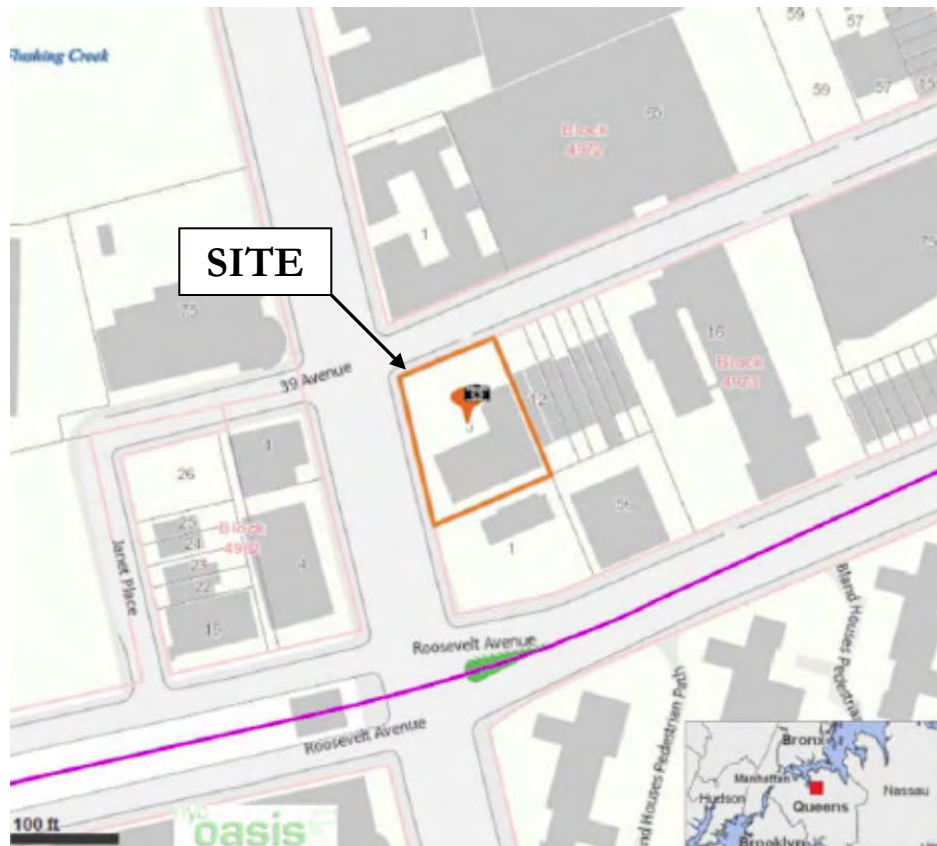
Very truly yours,

**MUESER RUTLEDGE CONSULTING ENGINEERS**

By: Walter E. Kaeck  
Walter E. Kaeck

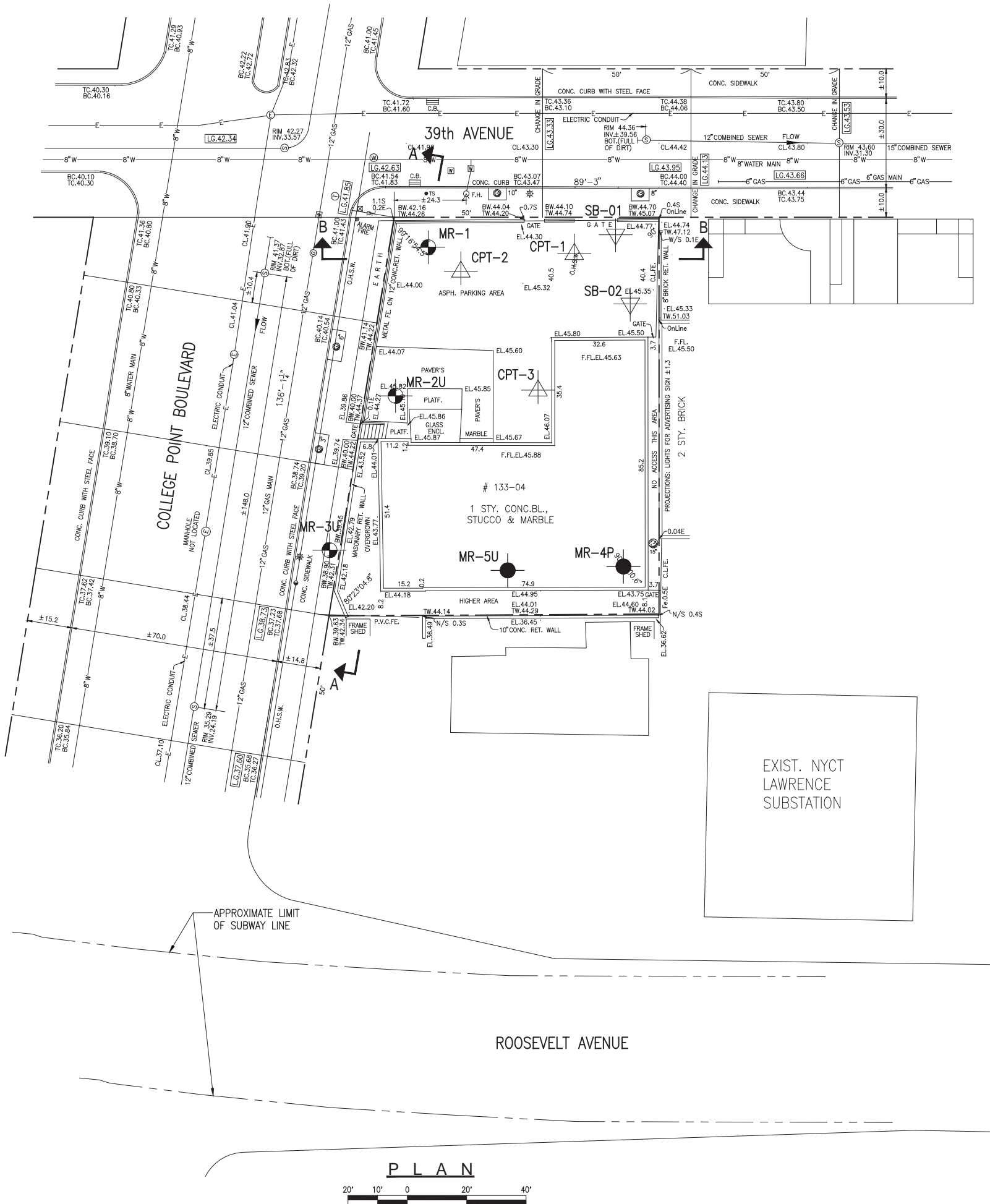
## **EXHIBITS**





NOTE: Map from the Open Accessible Space Information System (OASIS) website, [www.oasisnyc.net](http://www.oasisnyc.net), retrieved on 6/30/2016

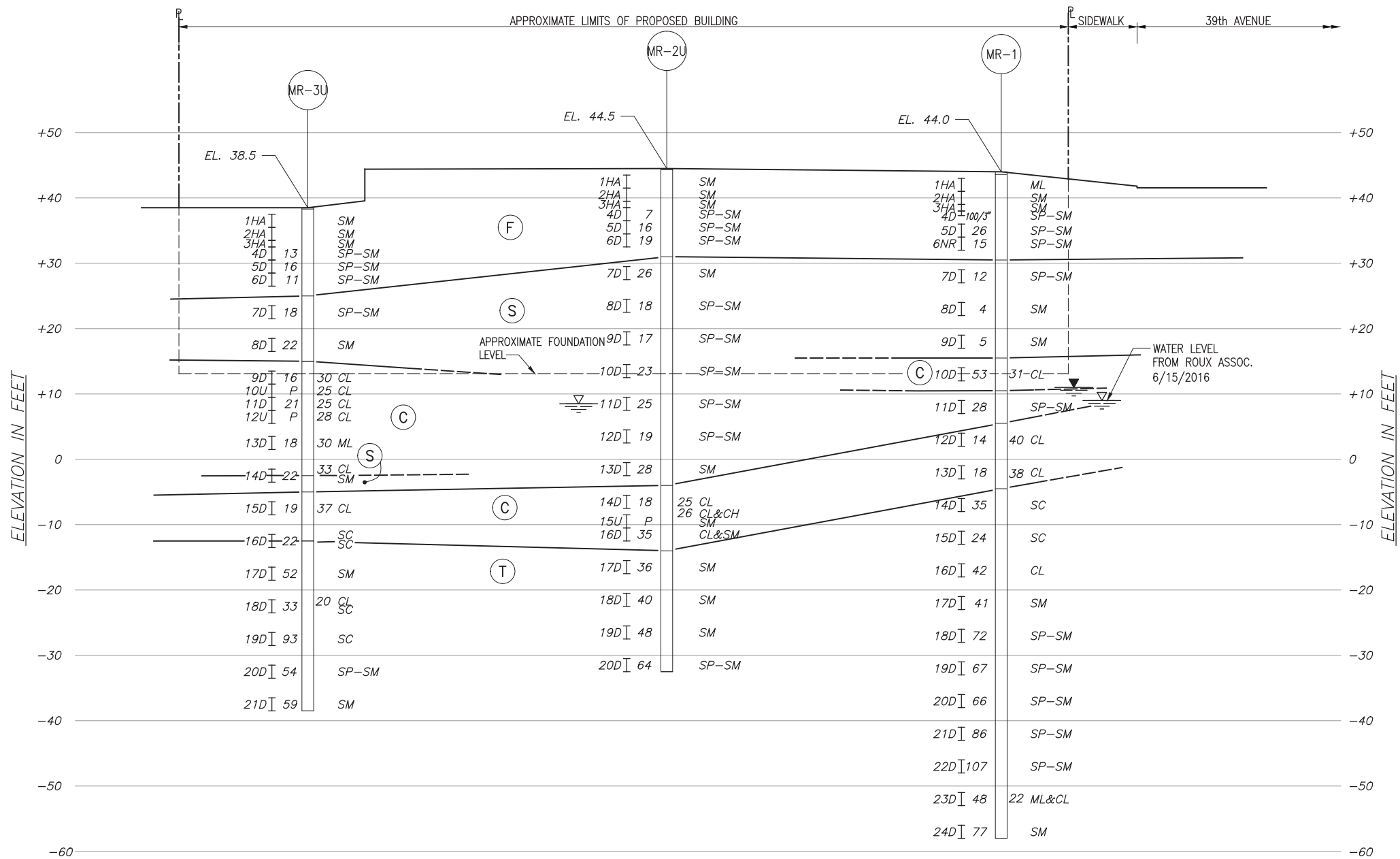
AAFE Mixed-Use Building, Queens, New York	
Mueser Rutledge Consulting Engineers 225 West 34 <sup>th</sup> Street • New York, NY 10122	06/30/16
Site Location Plan	MRCE 12629



- NOTES:**
1. THE BASE PLAN FOR THE PROJECT SITE IS FROM THE ARCHITECTURAL SITE SURVEY, DRAWING REFERENCE NO. Q4973-002, PREPARED BY JOSEPH NICOLETTI ASSOCIATES, 499 JERICHO TURNPIKE, SUITE 201, MINEOLA, NEW YORK, 11501, DATED MARCH 1, 2016.
  2. THE OUTLINES OF ADJACENT BUILDINGS WERE TAKEN FROM THE NEW YORK CITY DEPARTMENT OF CITY PLANNING ZONING MAP.
  3. THE LOCATION OF THE NYCT SUBWAY TUNNEL UNDER ROOSEVELT AVE WAS TAKEN FROM NYCT DRAWING ROUTE NO. 52 - SECTION NO.3, STA. 0 + 00 TO STA. 8 + 30, STRUCTURAL PLAN DWG NO. 28, DATED 4-02-1923.
  4. THE LOCATION OF THE NYCT SUBWAY SUBSTATION WAS TAKEN FROM NYCT DRAWING ROUTE NO. 52 - SECTION NO. 3, LAWRENCE SUBSTATION STRUCTURAL PLANS, FIRST FLOOR PLAN. DWG NO. 306, DATED 9-19-1951.
  5. THE NYCT STRUCTURES WERE LOCATED BY SCANNING THE REFERENCED DRAWINGS AND SCALING THEM TO FIT ON THE BASE PLAN. ALL LOCATIONS ARE APPROXIMATE.
  6. BORINGS MR-1, MR-2U, MR-3U AND CPTS WERE MADE BY CRAIG DRILLING, INC., OF MAYS LANDING, NEW JERSEY, BETWEEN MAY 2, THROUGH MAY 10, 2016, UNDER THE CONTINUOUS INSPECTION OF MUESER RUTLEDGE CONSULTING ENGINEERS (MRCE).
  7. BORINGS MR-4P & MR-5U WERE MADE BY CRAIG DRILLING OF MAYS LANDING, NY, ON DECEMBER 15, 2016, UNDER THE CONTINUOUS INSPECTION OF MUESER RUTLEDGE CONSULTING ENGINEERS.
  8. BORINGS TWP-01/SB-01 AND TWP-02/SB-02 WERE MADE BY AQUIFER DRILLING AND TESTING, BETWEEN NOVEMBER 4 & 5, 2006, UNDER THE INSPECTION OF LOUIS BERGER AND ASSOCIATES, P.C.
  9. ELEVATIONS AT THE BORING LOCATIONS WERE ESTIMATED IN REFERENCE TO NAVD88 BASED ON AVAILABLE SITE SURVEY INFORMATION.
  10. BORING LOCATIONS WERE MEASURED IN THE FIELD OFF OF EXISTING STRUCTURAL FEATURES.
  11. GEOLOGIC SECTION A-A IS SHOWN ON DRAWING GS-1 AND GEOLOGIC SECTION B-B IS SHOWN ON DWG. GS-2.

- LEGEND:**
- MR-3U
    - PRELIMINARY PHASE BORING
    - "U" UNDISTURBED SAMPLE
  - MR-4P
    - FINAL PHASE BORING
    - "P" PIEZOMETER
  - CPT-1
    - CPT BY CRAIG TEST
  - SB-01
    - EXISTING BORING MADE BY AQUIFER DRILLING AND TESTING

1	01-12-17	S.O.H.J.	FINAL PHASE
REV.	DATE	BY	DESCRIPTION
AAFE MIXED USE BUILDING			
QUEENS		NEW YORK	
ASIAN AMERICANS FOR EQUALITY			
NEW YORK		NEW YORK	
MUESER RUTLEDGE CONSULTING ENGINEERS			
14 PENN PLAZA — 225 W. 34TH STREET, NY, NY 10122			
SCALE	MADE BY: E.C.	DATE: 06-07-2016	FILE NUMBER
GRAPHIC	CH'KD BY: S.O.H.J.	DATE: 06-07-2016	12629
BORING LOCATION PLAN			DRAWING NUMBER
			B-1



**GEOLOGIC SECTION A-A**

**GENERAL STRATA DESCRIPTIONS:**

- (F) **FILL** – LOOSE TO MEDIUM COMPACT, BROWN FINE TO COARSE SAND, SOME TO TRACE SILT, TRACE TO SOME GRAVEL.
- (S) **SAND** – LOOSE TO MEDIUM COMPACT, BROWN FINE TO COARSE SAND, TRACE TO SOME SILT, TRACE GRAVEL.
- (C) **SILTY CLAY** – STIFF TO HARD BROWN, RED-BROWN AND GRAY SILTY CLAY, SOMETIMES INTERLAYERED OR VARVED WITH CLAYEY SILT, SILT OR FINE TO MEDIUM SAND SEAMS.
- (T) **TILL** – MEDIUM COMPACT TO VERY COMPACT, BROWN TO GRAY FINE TO COARSE SAND, TRACE TO SOME SILT WITH LAYERS AND POCKETS OF CLAYEY SAND, TRACE GRAVEL, LIGNITE.

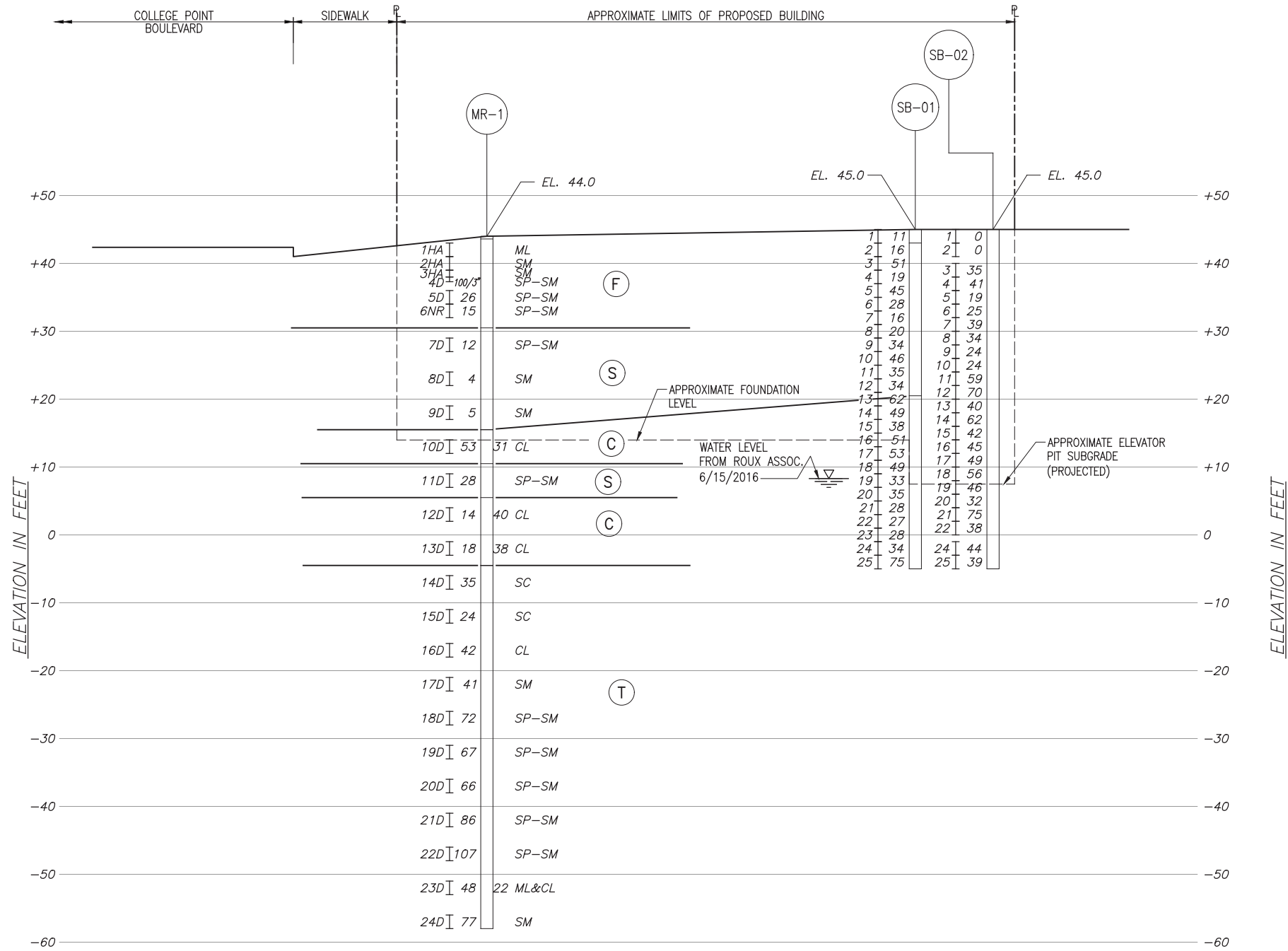
**GEOLOGIC SECTION NOTES:**

- FOR GENERAL NOTES AND LOCATIONS OF BORINGS AND GEOLOGIC SECTIONS, SEE BORING LOCATION PLAN, DRAWING NO. B-1.
- FOR BORING LEGEND AND SOIL CLASSIFICATION SYSTEM, SEE GEOTECHNICAL REFERENCE STANDARDS, DRAWING NO. GS-R.
- BORINGS ILLUSTRATED ON GEOLOGIC SECTIONS ARE IN SOME CASES PROJECTED TO THE SECTION OR OFFSET FOR CLARITY. STRATIFICATIONS SHOWN ON GEOLOGIC SECTIONS ARE NECESSARY INTERPOLATIONS BETWEEN AND BEYOND BORINGS AND MAY NOT REPRESENT ACTUAL SUBSURFACE CONDITIONS.
- WATER LEVELS SHOWN ARE PRELIMINARY WATER LEVELS PROVIDED BY ROUX ASSOCIATES, INC. FROM THEIR ENVIRONMENTAL INVESTIGATION, JUNE, 2016.



1	01-12-17	S.O.H.J.	FINAL PHASE
REV.	DATE	BY	DESCRIPTION
AAFE MIXED USE BUILDING			
QUEENS		NEW YORK	
ASIAN AMERICANS FOR EQUALITY			
NEW YORK		NEW YORK	
MUESER RUTLEDGE CONSULTING ENGINEERS			
14 PENN PLAZA — 225 W. 34TH STREET, NY, NY 10122			
SCALE GRAPHIC	MADE BY: E.C. CHK'D BY: S.O.H.J.	DATE: 06-07-2016 DATE: 06-07-2016	FILE NUMBER 12629
GEOLOGIC SECTION A-A			DRAWING NUMBER GS-1

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**GEOLOGIC SECTION B-B**

**GENERAL STRATA DESCRIPTIONS:**

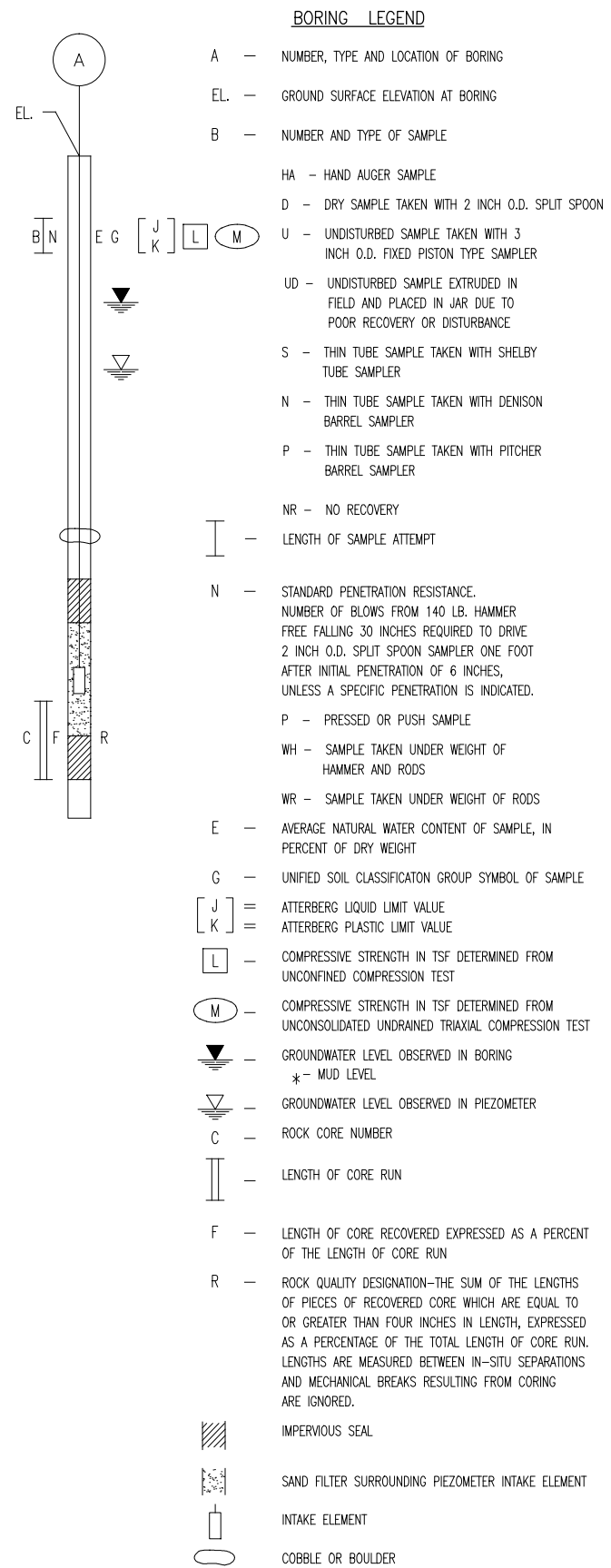
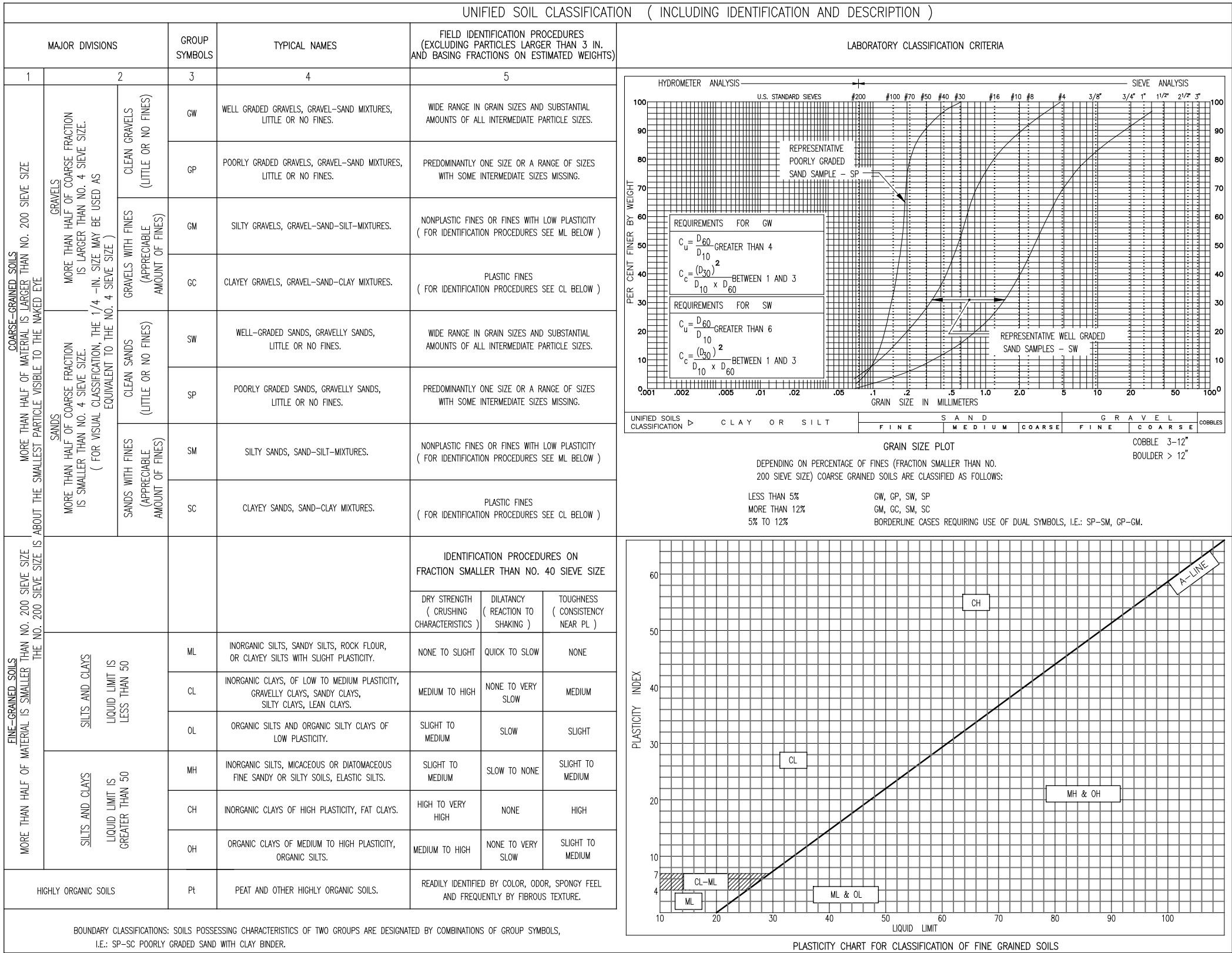
- (F) **FILL** - LOOSE TO MEDIUM COMPACT, BROWN FINE TO COARSE SAND, SOME TO TRACE SILT, TRACE TO SOME GRAVEL.
- (S) **SAND** - LOOSE TO MEDIUM COMPACT, BROWN FINE TO COARSE SAND, TRACE TO SOME SILT, TRACE GRAVEL.
- (C) **SILTY CLAY** - STIFF TO HARD BROWN, RED-BROWN AND GRAY SILTY CLAY, SOMETIMES INTERLAYERED OR VARVED WITH CLAYEY SILT, SILT OR FINE TO MEDIUM SAND SEAMS.
- (T) **TILL** - MEDIUM COMPACT TO VERY COMPACT, BROWN TO GRAY FINE TO COARSE SAND, TRACE TO SOME SILT WITH LAYERS AND POCKETS OF CLAYEY SAND, TRACE GRAVEL, LIGNITE.

**NOTES:**

FOR NOTES, SEE DRAWING NO. GS-1.



1	01-12-17	S.O.H.J.	FINAL PHASE
REV.	DATE	BY	DESCRIPTION
AAFE MIXED USE BUILDING			
QUEENS			NEW YORK
ASIAN AMERICANS FOR EQUALITY			
NEW YORK			NEW YORK
MUESER RUTLEDGE CONSULTING ENGINEERS			
14 PENN PLAZA - 225 W. 34TH STREET, NY, NY 10122			
SCALE GRAPHIC	MADE BY: E.C. CH'KD BY: S.O.H.J.	DATE: 06-07-2016 DATE: 06-07-2016	FILE NUMBER 12629
GEOLOGIC SECTION B-B			DRAWING NUMBER GS-2



REVISED 10-25-2012

**MUESER RUTLEDGE CONSULTING ENGINEERS**  
225 WEST 34th STREET — 14 PENN PLAZA  
NEW YORK, NY 10122

GEOTECHNICAL REFERENCE STANDARDS **GS-R**

DRAWING NO.

TERMINOLOGY USED IN MRCE SOIL DESCRIPTIONS

DEGREE OF COMPACTION FOR NON-PLASTIC SOIL		CONSISTENCY OF CLAY AND CLAYEY SILT <sup>+</sup>			DESCRIPTION OF CONSTITUENT PERCENTAGES AS USED IN SOIL SAMPLE CLASSIFICATIONS
DEGREE OF COMPACTION	BLOWS* PER FOOT	CONSISTENCY	UNCONFINED COMPRESSIVE STRENGTH (TSF)	IDENTIFICATION CHARACTERISTICS	
LOOSE	0 TO 10	SOFT	LESS THAN 0.5	EASILY REMOLDED WITH SLIGHT FINGER PRESSURE	1% TO 12% — "TRACE" 13% TO 30% — "SOME" 31% TO 49% — ADJECTIVE FORM OF SOIL GROUP (EG. SANDY) EQUAL AMOUNT — "AND" (EG. SAND AND GRAVEL)
MEDIUM COMPACT	11 TO 29	MEDIUM	0.5 TO 1.0	REQUIRES SUBSTANTIAL PRESSURE FOR REMOLDING	
COMPACT	30 TO 50	STIFF	1.0 TO 4.0	DIFFICULT TO REMOLD WITH FINGERS	
VERY COMPACT	GREATER THAN 50	HARD	GREATER THAN 4.0	CANNOT BE REMOLDED WITH FINGERS	
* STANDARD PENETRATION RESISTANCE USING 140 LB. HAMMER FREE FALLING 30 INCHES TO DRIVE A 2 INCH O.D. SPLIT-SPOON SAMPLER.		+ NONPLASTIC SILTS ARE DESCRIBED USING DEGREE OF COMPACTION AS PRESENTED FOR NON-PLASTIC SOIL.			

## **APPENDIX A**

MRCE Final Boring Drawings

# MUESER RUTLEDGE CONSULTING ENGINEERS

## BORING LOG

PROJECT: AAFE MIXED USE BUILDING  
LOCATION: FLUSHING, QUEENS

BORING NO. MR-4P  
SHEET 1 OF 4  
FILE NO. 12629  
SURFACE ELEV. 44.5±  
RES. ENGR. ERIC POON

DAILY PROGRESS	SAMPLE			SAMPLE DESCRIPTION	STRATA	DEPTH	CASING	REMARKS
	NO.	DEPTH	BLOWS/6"				BLOWS	
07:00	1D	0.0	7-6	Brown silty fine to medium sand, trace coarse	F		DRILLED	REC=6"
12-15-16		2.0	7-9	sand, gravel (Fill) (SM)			AHEAD	
Thursday	2D	2.0	8-7	Do 1D, trace brick (Fill) (SM)			4"	
Overcast		4.0	8-8					
23°F	3D	4.0	6-4	Brown silty fine to medium sand, trace gravel		5		
		6.0	2-5	(Fill) (SM)				
	4D	6.0	6-6	Brown fine to coarse sand, some silt, trace				
		8.0	5-9	gravel (Fill) (SM)		8		
	5D	8.0	15-18	Brown fine to coarse sand, some gravel, silt	S			
		10.0	15-10	(Fill) (SM)		10		
	6D	10.0	16-16	Brown fine to coarse sand, some gravel, trace				
		12.0	12-17	silt (SP-SM)				
						15		
	7D	15.0	11-9	Brown fine to coarse sand, some gravel, trace				
		17.0	8-8	silt (SP-SM)				
						20		
	8D	20.0	10-13	Brown fine to medium sand, trace silt, coarse	T			
		22.0	10-12	sand, gravel (SP-SM)				
						25		
	9D	25.0	12-17	Do 8D (SP-SM)				
		27.0	19-18					
						28.5		
						30		
	10D	30.0	18-19	Brown fine to medium sand, some silt (SM)				
		32.0	19-15					
						35		
	11D	35.0	15-18	Brown fine to coarse sand, trace silt, gravel	T			
		37.0	19-15	(SP-SM)				
						40		
	12D	40.0	17-20	Gray fine sand, some silt, trace coarse sand (SM)				
		42.0	22-22					
						43.5		
						45		
	13D	45.0	16-20	Gray fine to coarse sand, trace silt, gravel				
		47.0	23-17	(SP-SM)				
						50		
	14D	50.0	20-18	Brown fine to coarse sand, some silt, gravel				
		52.0	20-17	(SP-SM)				

## BORING LOG

BORING NO.	MR-4P
SHEET 2 OF	4
FILE NO.	12629
SURFACE ELEV.	44.5±
RES. ENGR.	ERIC POON

[illegible]



**Mueser Rutledge Consulting Engineers**

14 Penn Plaza - 225 West 34th Street

New York, NY 10122

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www.mrce.com

**PIEZOMETER RECORD**PIEZOMETER OR BORING NO. MR-4PSHEET 3 OF 4FILE NO. 12629INSTALLATION DATE 12-15-2016RES ENGR. ERIC POONPROJECT: AAFE MIXED USE BUILDINGLOCATION: FLUSHING, QUEENSPIEZOMETER LOCATION: SEE BLP☐ SEE SKETCH ON BACK

STRATA	PIEZOMETER INSTALLATION DETAILS	DEPTH (FT)	PIEZOMETER TYPE <u>PVC SLOTTED PIPE</u>																																																							
GROUND SURFACE ELEV. <u>±44.5</u> (F)		0	<b>INTAKE POINT</b> depth to bottom, ft = <u>75</u> depth to top, ft = <u>65</u> length, ft = <u>10</u> = L diameter, in = <u>2.375</u> ID, ft = <u>0.17</u> = 2R																																																							
		8	<b>STANDPIPE/RISER</b> elevation of rim, ft = <u>± 45.9</u> diameter, in = <u>2.063</u> ID, ft = <u>0.17</u> = 2R																																																							
(S)		43.5	<table border="1"> <thead> <tr> <th colspan="2">READING TIME</th> <th rowspan="2">DEPTH - RIM TO WATER</th> <th rowspan="2">ELEVATION OF WATER</th> <th rowspan="2">REMARKS</th> </tr> <tr> <th>DATE</th> <th>CLOCK</th> </tr> </thead> <tbody> <tr> <td>12-15-2016</td> <td>14:00</td> <td>8.3</td> <td>37.6</td> <td>UPON COMPLETION</td> </tr> <tr> <td>1-4-2017</td> <td>16:00</td> <td>47.9</td> <td>-2.0</td> <td>SCHEDULED READING</td> </tr> <tr> <td>1-9-2017</td> <td>07:30</td> <td>49.7</td> <td>-3.8</td> <td>SCHEDULED READING</td> </tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> </tbody> </table>				READING TIME		DEPTH - RIM TO WATER	ELEVATION OF WATER	REMARKS	DATE	CLOCK	12-15-2016	14:00	8.3	37.6	UPON COMPLETION	1-4-2017	16:00	47.9	-2.0	SCHEDULED READING	1-9-2017	07:30	49.7	-3.8	SCHEDULED READING																														
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 SAND  
 GRAVEL

 BENTONITE  
 GROUT
GROUND SURFACE ELEV. 44.5 (±)PIEZOMETER NO. MR-4P

# MUESER RUTLEDGE CONSULTING ENGINEERS

	BORING NO. <u>MR-4P</u>
	SHEET <u>4</u> OF <u>4</u>
PROJECT <u>AAFE MIXED USE BUILDING</u>	FILE NO. <u>12629</u>
LOCATION <u>FLUSHING, QUEENS</u>	SURFACE ELEV. <u>44.5±</u>
BORING LOCATION <u>SEE BORING LOCATION PLAN</u>	DATUM <u>NAVD 88</u>

## BORING EQUIPMENT AND METHODS OF STABILIZING BOREHOLE

TYPE OF BORING RIG	TYPE OF FEED	CASING USED	<input checked="" type="checkbox"/> YES	<input type="checkbox"/> NO	
TRUCK <u>CME-75</u>	DURING CORING	DIA., IN. <u>4</u>			DEPTH, FT. FROM <u>0</u> TO <u>8</u>
SKID	MECHANICAL	DIA., IN.			DEPTH, FT. FROM <u>    </u> TO <u>    </u>
BARGE	HYDRAULIC <u>X</u>	DIA., IN.			DEPTH, FT. FROM <u>    </u> TO <u>    </u>
OTHER	OTHER	DIA., IN.			DEPTH, FT. FROM <u>    </u> TO <u>    </u>

TYPE AND SIZE OF:	DRILLING MUD USED
D-SAMPLER <u>2" O. D. SPLIT SPOON</u>	<input checked="" type="checkbox"/> YES <input type="checkbox"/> NO
U-SAMPLER <u>    </u>	DIAMETER OF ROTARY BIT, IN. <u>3-7/8</u>
S-SAMPLER <u>    </u>	TYPE OF DRILLING MUD <u>BIO-BORE</u>
CORE BARREL <u>    </u>	
CORE BIT <u>    </u>	AUGER USED <input type="checkbox"/> YES <input checked="" type="checkbox"/> NO
DRILL RODS <u>NWJ</u>	TYPE AND DIAMETER, IN. <u>    </u>
	*CASING HAMMER, LBS. <u>300</u> AVERAGE FALL, IN. <u>24</u>
	*SAMPLER HAMMER, LBS. <u>140</u> AVERAGE FALL, IN. <u>30</u>
	*USED AUTOMATIC HAMMER.

## WATER LEVEL OBSERVATIONS IN BOREHOLE

DATE	TIME	DEPTH OF HOLE	DEPTH OF CASING	DEPTH TO WATER	CONDITIONS OF OBSERVATION
					SEE PIEZOMETER RECORD SHEET.

PIEZOMETER INSTALLED	<input checked="" type="checkbox"/> YES	<input type="checkbox"/> NO	SKETCH SHOWN ON <u>SEE SHEET NO. 3</u>
----------------------	---	-----------------------------	--

STANDPIPE:	TYPE	PVC	ID, IN.	1-3/4	LENGTH, FT.	65	TOP ELEV.	45.9
INTAKE ELEMENT:	TYPE	SLOTTED PVC	OD, IN.	2	LENGTH, FT.	10	TIP ELEV.	-29.1
FILTER:	MATERIAL	SAND	OD, IN.	4	LENGTH, FT.	12	BOT. ELEV.	-32.5

## PAY QUANTITIES

3.5" DIA. DRY SAMPLE BORING	LIN. FT.	77	NO. OF 3" SHELBY TUBE SAMPLES	
3.5" DIA. U-SAMPLE BORING	LIN. FT.		NO. OF 3" UNDISTURBED SAMPLES	
CORE DRILLING IN ROCK	LIN. FT.		OTHER:	

BORING CONTRACTOR	CRAIG GEOTECHNICAL DRILLING
DRILLER	JOHN MILLINGTON      HELPERS      JIMMY MARTINEZ
REMARKS	PIEZOMETER INSTALLED.
RESIDENT ENGINEER	ERIC POON      DATE      12-15-16
CLASSIFICATION CHECK:	CHERYL J. MOSS      TYPING CHECK:      SARAH JOHNSON
	BORING NO. <u>MR-4P</u>

# MUESER RUTLEDGE CONSULTING ENGINEERS

## BORING LOG

PROJECT: AAFE MIXED USE BUILDING  
LOCATION: FLUSHING, QUEENS

BORING NO. MR-5U  
SHEET 1 OF 2  
FILE NO. 12629  
SURFACE ELEV. +44 (±)  
RES. ENGR. ERIC POON

DAILY PROGRESS	SAMPLE			SAMPLE DESCRIPTION	STRATA	CASING		REMARKS				
	NO.	DEPTH	BLOWS/6"			DEPTH	BLOWS					
12:40	1D	0.0	11-6	Brown fine to coarse sand, trace silt, gravel (Fill) (SM)	F		DRILLED	REC=1"				
12-15-16		2.0	3-4				AHEAD					
Thursday							4"					
Sunny						3.5						
23°F				5								
	2D	5.0	WR/12"	Brown clayey silt, some fine to medium sand (ML)		F			WC=21			
		7.0	1-2									
								10	↓			
	3D	10.0	6-2	Do 2D, trace coarse sand (ML)			F			WC=22		
		12.0	2-2									
								13.5				
								15				
	4D	15.0	6-5	Brown clayey fine to coarse sand, trace gravel (SC)	S							
		17.0	8-13									
									20			
	5D	20.0	6-10	Brown fine to medium sand, some silt, trace coarse sand, gravel (SM)		S						
		22.0	9-7									
								23.5				
								25				
	6D	25.0	4-6	Stiff red brown silty clay, trace fine to coarse sand (CL)			C			WC=27, pp=2.0		
		27.0	9-8									
	7U	28.0	PUSH=24"	Stiff red brown silty clay (CL)	C					WC=33, pp=3.0, slickensided.		
		30.0	REC=19"								30	
	8D	30.0	7-8									
		32.0	11-12									
				Stiff red brown silty clay (CH)		C				WC=28, pp=2.0, slickensided.		
	9D	35.0	5-9									
		37.0	14-14									
				Do 9D (CH)			C			WC=25, pp=2.5, slickensided.		
					C					WC=29, pp=3.0, slickensided.		
											40	
14:15	10D	40.0	9-10	Do 9D (CH)		C				WC=29, pp=3.0, slickensided.		
		42.0	19-18								42	
							C			End of Boring at 42'.		
											45	
					C					WC=Water Content in percent of dry weight.		
						C				pp=Pocket Penetrometer		
											50	
							C			Unconfined Compressive Strength in tsf.		

# MUESER RUTLEDGE CONSULTING ENGINEERS

	BORING NO. <u>MR-5U</u>
	SHEET <u>2</u> OF <u>2</u>
PROJECT <u>AAFE MIXED USE BUILDING</u>	FILE NO. <u>12629</u>
LOCATION <u>FLUSHING, QUEENS</u>	SURFACE ELEV. <u>+44 (±)</u>
BORING LOCATION <u>SEE BORING LOCATION PLAN</u>	DATUM <u>NAVD 88</u>

## BORING EQUIPMENT AND METHODS OF STABILIZING BOREHOLE

TYPE OF BORING RIG	TYPE OF FEED	CASING USED	<input checked="" type="checkbox"/> YES	<input type="checkbox"/> NO	
TRUCK <u>CME-75</u>	DURING CORING	DIA., IN. <u>4</u>			DEPTH, FT. FROM <u>0</u> TO <u>10</u>
SKID	MECHANICAL	DIA., IN.			DEPTH, FT. FROM <u>    </u> TO <u>    </u>
BARGE	HYDRAULIC <u>X</u>	DIA., IN.			DEPTH, FT. FROM <u>    </u> TO <u>    </u>
OTHER	OTHER	DIA., IN.			DEPTH, FT. FROM <u>    </u> TO <u>    </u>

TYPE AND SIZE OF:	DRILLING MUD USED <input checked="" type="checkbox"/> YES <input type="checkbox"/> NO
D-SAMPLER <u>2" O. D. SPLIT SPOON</u>	DIAMETER OF ROTARY BIT, IN. <u>3-3/4</u>
U-SAMPLER <u>THIN WALL</u>	TYPE OF DRILLING MUD <u>BIO-BORE</u>
S-SAMPLER	
CORE BARREL	AUGER USED <input type="checkbox"/> YES <input checked="" type="checkbox"/> NO
CORE BIT	TYPE AND DIAMETER, IN. <u>    </u>
DRILL RODS <u>NWJ</u>	
	*CASING HAMMER, LBS. <u>300</u> AVERAGE FALL, IN. <u>24</u>
	*SAMPLER HAMMER, LBS. <u>140</u> AVERAGE FALL, IN. <u>30</u>
	*USED AUTOMATIC HAMMER.

## WATER LEVEL OBSERVATIONS IN BOREHOLE

DATE	TIME	DEPTH OF HOLE	DEPTH OF CASING	DEPTH TO WATER	CONDITIONS OF OBSERVATION
					NO WATER OBSERVATIONS MADE.

PIEZOMETER INSTALLED ☐ YES ☒ NO SKETCH SHOWN ON     

STANDPIPE:	TYPE <u>    </u>	ID, IN. <u>    </u>	LENGTH, FT. <u>    </u>	TOP ELEV. <u>    </u>
INTAKE ELEMENT:	TYPE <u>    </u>	OD, IN. <u>    </u>	LENGTH, FT. <u>    </u>	TIP ELEV. <u>    </u>
FILTER:	MATERIAL <u>    </u>	OD, IN. <u>    </u>	LENGTH, FT. <u>    </u>	BOT. ELEV. <u>    </u>

## PAY QUANTITIES

3.5" DIA. DRY SAMPLE BORING	LIN. FT. <u>42</u>	NO. OF 3" SHELBY TUBE SAMPLES <u>1</u>	
3.5" DIA. U-SAMPLE BORING	LIN. FT. <u>    </u>	NO. OF 3" UNDISTURBED SAMPLES <u>    </u>	
CORE DRILLING IN ROCK	LIN. FT. <u>    </u>	OTHER: <u>    </u>	

BORING CONTRACTOR <u>CRAIG GEOTECHNICAL DRILLING</u>	
DRILLER <u>JOHN MILLINGTON</u>	HELPERS <u>JIMMY MARTINEZ</u>
REMARKS <u>BOREHOLE BACKFILLED WITH CUTTINGS UPON COMPLETION.</u>	
RESIDENT ENGINEER <u>ERIC POON</u>	DATE <u>12-15-16</u>
CLASSIFICATION CHECK: <u>CHERYL J. MOSS</u>	TYPING CHECK: <u>SARAH JOHNSON</u>
	BORING NO. <u>MR-5U</u>

## **APPENDIX B**

### Adjacent Building Information







**EXHIBIT LOG SHEET**

1. TYPICAL FLOOR AND ROOF SYSTEM SHALL BE 8" PRECAST ROLLER CONE SLABS WITH PRETENSIONED REINFORCEMENT.
2. ALL PRECAST SLABS SHALL CONFORM TO ALL REQUIREMENTS OF A.C.I. 318 AND NEW YORK CITY BUILDING CODES.
3. REINFORCEMENT SHALL CONSIST OF MULTIPLE WIRE STRESS RELIEVED HIGH TENSILE STRAND PRETENSIONED IN ACCORDANCE WITH THE STATED DESIGN PARAMETERS.
4. CONCRETE MATERIALS SHALL CONFORM WITH THE PREVIOUSLY STATED REQUIREMENTS. MINIMUM COMPRESSIVE STRENGTH AT 28 DAYS SHALL BE 6,000 P.S.I.
5. PROVIDE ANCHORAGE OF STRUCTURE AS SHOWN ON DRAWINGS AND AS PER MANUFACTURER'S SUGGESTED DETAILS.
6. ALL PRECAST SLABS SHALL BE 2' UNFACED AND SHALL HAVE 8'S A NUMBER.
7. WELL LATES, WHERE INDICATED ON DRAWINGS, SHALL BE INCORPORATED INTO SLABS AT TIME OF PLACEMENT OF CONCRETE.
8. CONTRACTOR SHALL FURNISH SHOP DRAWINGS FOR APPROVAL PRIOR TO FABRICATION. CONTRACTOR SHALL ASSUME FULL RESPONSIBILITY FOR DIMENSIONAL CORRECTNESS. CONTRACTOR SHALL REFER TO MECHANICAL AND ELECTRICAL DRAWINGS FOR LOCATION OF OPENINGS, RECESSES ETC.
9. ALL OPENINGS LARGER THAN 14" PERPENDICULAR TO SP. OF PRECAST SLAB SHALL RECEIVE A STEEL CASTER FOR THE SUPPORT OF THE CUT SLAB.
10. PRECAST SLAB CONTRACTOR SHALL GROUT ALL JOINTS BETWEEN UNITS, AND ALL SPACES WHERE SLABS MEET SUPPORTING MEMBERS. ALL JOINTS SHALL BE CLEANED PRIOR TO PLACEMENT OF GROUT. GROUT SHALL BE WASH "TIGHT".

**STANDARD STEEL INDUSTRY**

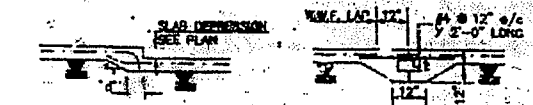
1. FABRICATION AND ERECTION OF ALL STRUCTURAL STEEL WORK SHALL CONFORM TO THE A.I.S.C. SPECIFICATION FOR DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BUILDINGS - LATEST EDITION AND SUPPLEMENT 1003 OF THE N.Y. CITY BUILDING CODE. AN AFFIDAVIT WILL BE REQUIRED FROM THE PRODUCER OF THE STEEL CERTIFYING THAT ALL STEEL MEETS THE REQUIREMENTS AS DEFINED IN SECTIONS C2A-1005.6 TO C2A-1405.3 INCLUSIVE; OF THE N.Y. CITY BUILDING CODE.
2. ALL STEEL SHALL CONFORM TO ASTM DESIGNATION A-36.
3. CONTRACTOR SHALL FILE AN AFFIDAVIT FROM THE PRODUCER OF THE STRUCTURAL STEEL CERTIFYING THAT THE STEEL MEETS THE REQUIREMENTS OF ASTM DESIGNATION A-36.
4. CONTRACTOR SHALL PROVIDE ALL NECESSARY TEMPORARY BRACING AND SHORING REQUIRED TO ERECT AND HOLD THE JOIST FRAME IN ALIGNMENT AND COLUMNS PLUMB, UNTIL DECK AND WALKING IS IN PLACE.
5. ALL CONNECTIONS TO BE ADEQUATE TO CARRY THE REACTIONS DUE TO MAXIMUM UNIFORMLY-DISTRIBUTED LOAD THAT THE BEAM IS CAPABLE OF SUPPORTING FOR ITS SPAN UNDER THE A.I.S.C. SAFE LOAD TABLES. ALL CONNECTIONS TO BE TO MEET STANDARD SHEAR CONNECTIONS WHERE POSSIBLE.
6. ALL HIGH STRENGTH BOLTS TO BE FRICTION TYPE, A-325, 3/4" DIA. MINIMUM.
7. ALL SHOP CONNECTIONS TO BE WELDED OR HIGH STRENGTH BOLTED.
8. FIELD CONNECTIONS MAY BE MADE WITH A-307, 3/4" DIA. COMMON BOLTS EXCEPT AS FOLLOWS:
  - A. FOR JOIST-TO-FRAME JOINTS COLUMNS OR WITHIN 24" OF COLUMNS, USE HIGH STRENGTH BOLTS.
  - B. WHERE HIGH STRENGTH BOLTS OR WELDS ARE CALLED FOR ON DRAWINGS.
9. BEARING SLOES OF COLUMNS SHALL BE MILLED TO COMPLETE TRUE BEARING.
10. PROVIDE HANGING ANCHORS AS REQUIRED AND AS SHOWN ON DRAWINGS.
11. ALL STEEL TO RECEIVE ONE SHOP COAT OF PAINT.
12. SUBMIT SHOP DRAWINGS FOR APPROVAL BEFORE FABRICATION.

### UNDERLYING NOTES

- WHERE UNDERPINNING OF EXISTING FOOTINGS IS REQUIRED THE CONTRACTOR SHALL TAKE ADEQUATE PRECAUTIONS TO PREVENT SETTLEMENT OR MOVEMENT OF EXISTING ADJACENT CONSTRUCTION. THE CONTRACTOR SHALL SUBMIT SHOP DRAWINGS PREPARED, SIGNED AND SEALED BY A LICENSED PROFESSIONAL ENGINEER RELIANT BY THE CONTRACTOR TO THE ARCHITECT SHOWING PROPOSED DETAILS OF UPPINING. THE CONTRACTOR SHALL NOT BEGIN UNDERPINNING WORK UNTIL THE ARCHITECT APPROVES THE SHOP DRAWINGS SUBMITTED BY THE CONTRACTOR. APPROVAL OF THESE SHOP DRAWINGS SHALL NOT RENDER THE ARCHITECT RESPONSIBLE FOR ANY ERRORS OR OMISSIONS RESULTING FROM THE PROPOSED UNDERPINNING SYSTEM OF UNDERPINNING, METHODS, PROCEDURES, CONSTRUCTION ETC., ALL OF WHICH IS THE SOLE RESPONSIBILITY OF THE CONTRACTOR.
- A SEPARATE AGREEMENT FOR THE UNDERPINNING SHALL BE FILED WITH THE DEPARTMENT OF BUILDINGS AS REQUIRED BY LAW.
- THIS OFFICE DOES NOT RETAIN TO PREPARE ANY DOCUMENTS RELATING TO UNDERPINNING NOR TO SUPERVISE ANY PART OF THE UNDERPINNING PROCEDURES.

1993, 1994, 1995, 1996, 1997, 1998, 1999, 2000, 2001, 2002, 2003, 2004, 2005, 2006, 2007, 2008, 2009, 2010, 2011, 2012, 2013, 2014, 2015, 2016, 2017, 2018, 2019, 2020, 2021, 2022, 2023, 2024, 2025, 2026, 2027, 2028, 2029, 2030, 2031, 2032, 2033, 2034, 2035, 2036, 2037, 2038, 2039, 2040, 2041, 2042, 2043, 2044, 2045, 2046, 2047, 2048, 2049, 2050, 2051, 2052, 2053, 2054, 2055, 2056, 2057, 2058, 2059, 2060, 2061, 2062, 2063, 2064, 2065, 2066, 2067, 2068, 2069, 2070, 2071, 2072, 2073, 2074, 2075, 2076, 2077, 2078, 2079, 2080, 2081, 2082, 2083, 2084, 2085, 2086, 2087, 2088, 2089, 2090, 2091, 2092, 2093, 2094, 2095, 2096, 2097, 2098, 2099, 2100, 2101, 2102, 2103, 2104, 2105, 2106, 2107, 2108, 2109, 2110, 2111, 2112, 2113, 2114, 2115, 2116, 2117, 2118, 2119, 2120, 2121, 2122, 2123, 2124, 2125, 2126, 2127, 2128, 2129, 2130, 2131, 2132, 2133, 2134, 2135, 2136, 2137, 2138, 2139, 2140, 2141, 2142, 2143, 2144, 2145, 2146, 2147, 2148, 2149, 2150, 2151, 2152, 2153, 2154, 2155, 2156, 2157, 2158, 2159, 2160, 2161, 2162, 2163, 2164, 2165, 2166, 2167, 2168, 2169, 2170, 2171, 2172, 2173, 2174, 2175, 2176, 2177, 2178, 2179, 2180, 2181, 2182, 2183, 2184, 2185, 2186, 2187, 2188, 2189, 2190, 2191, 2192, 2193, 2194, 2195, 2196, 2197, 2198, 2199, 2200, 2201, 2202, 2203, 2204, 2205, 2206, 2207, 2208, 2209, 2210, 2211, 2212, 2213, 2214, 2215, 2216, 2217, 2218, 2219, 2220, 2221, 2222, 2223, 2224, 2225, 2226, 2227, 2228, 2229, 2230, 2231, 2232, 2233, 2234, 2235, 2236, 2237, 2238, 2239, 2240, 2241, 2242, 2243, 2244, 2245, 2246, 2247, 2248, 2249, 2250, 2251, 2252, 2253, 2254, 2255, 2256, 2257, 2258, 2259, 2260, 2261, 2262, 2263, 2264, 2265, 2266, 2267, 2268, 2269, 2270, 2271, 2272, 2273, 2274, 2275, 2276, 2277, 2278, 2279, 2280, 2281, 2282, 2283, 2284, 2285, 2286, 2287, 2288, 2289, 2290, 2291, 2292, 2293, 2294, 2295, 2296, 2297, 2298, 2299, 2300, 2301, 2302, 2303, 2304, 2305, 2306, 2307, 2308, 2309, 2310, 2311, 2312, 2313, 2314, 2315, 2316, 2317, 2318, 2319, 2320, 2321, 2322, 2323, 2324, 2325, 2326, 2327, 2328, 2329, 2330, 2331, 2332, 2333, 2334, 2335, 2336, 2337, 2338, 2339, 2340, 2341, 2342, 2343, 2344, 2345, 2346, 2347, 2348, 2349, 2350, 2351, 2352, 2353, 2354, 2355, 2356, 2357, 2358, 2359, 2360, 2361, 2362, 2363, 2364, 2365, 2366, 2367, 2368, 2369, 2370, 2371, 2372, 2373, 2374, 2375, 2376, 2377, 2378, 2379, 2380, 2381, 2382, 2383, 2384, 2385, 2386, 2387, 2388, 2389, 2390, 2391, 2392, 2393, 2394, 2395, 2396, 2397, 2398, 2399, 2400, 2401, 2402, 2403, 2404, 2405, 2406, 2407, 2408, 2409, 2410, 2411, 2412, 2413, 2414, 2415, 2416, 2417, 2418, 2419, 2420, 2421, 2422, 2423, 2424, 2425, 2426, 2427, 2428, 2429, 2430, 2431, 2432, 2433, 2434, 2435, 2436, 2437, 2438, 2439, 2440, 2441, 2442, 2443, 2444, 2445, 2446, 2447, 2448, 2449, 2450, 2451, 2452, 2453, 2454, 2455, 2456, 2457, 2458, 2459, 2460, 2461, 2462, 2463, 2464, 2465, 2466, 2467, 2468, 2469, 2470, 2471, 2472, 2473, 2474, 2475, 2476, 2477, 2478, 2479, 2480, 2481, 2482, 2483, 2484, 2485, 2486, 2487, 2488, 2489, 2490, 2491, 2492, 2493, 2494, 2495, 2496, 2497, 2498, 2499, 2500, 2501, 2502, 2503, 2504, 2505, 2506, 2507, 2508, 2509, 2510, 2511, 2512, 2513, 2514, 2515, 2516, 2517, 2518, 2519, 2520, 2521, 2522, 2523, 2524, 2525, 2526, 2527, 2528, 2529, 2530, 2531, 2532, 2533, 2534, 2535, 2536, 2537, 2538, 2539, 2540, 2541, 2542, 2543, 2544, 2545, 2546, 2547, 2548, 2549, 2550, 2551, 2552, 2553, 2554, 2555, 2556, 2557, 2558, 2559, 2560, 2561, 2562, 2563, 2564, 2565, 2566, 2567, 2568, 2569, 2570, 2571, 2572, 2573, 2574, 2575, 2576, 2577, 2578, 2579, 2580, 2581, 2582, 2583, 2584, 2585, 2586, 2587, 2588, 2589, 2590, 2591, 2592, 2593, 2594, 2595, 2596, 2597, 2598, 2599, 2600, 2601, 2602, 2603, 2604, 2605, 2606, 2607, 2608, 2609, 2610, 2611, 2612, 2613, 2614, 2615, 2616, 2617, 2618, 2619, 2620, 2621, 2622, 2623, 2624, 2625, 2626, 2627, 2628, 2629, 2630, 2631, 2632, 2633, 2634, 2635, 2636, 2637, 2638, 2639, 2640, 2641, 2642, 2643, 2644, 2645, 2646, 2647, 2648, 2649, 2650, 2651, 2652, 2653, 2654, 2655, 2656, 2657, 2658, 2659, 2660, 2661, 2662, 2663, 2664, 2665, 2666, 2667, 2668, 2669, 2670, 2671, 2672, 2673, 2674, 26

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AT DEPRESSION      AT CONSTRUCTION JOINT  
TYPICAL SLAB ON GRADE DETAILS



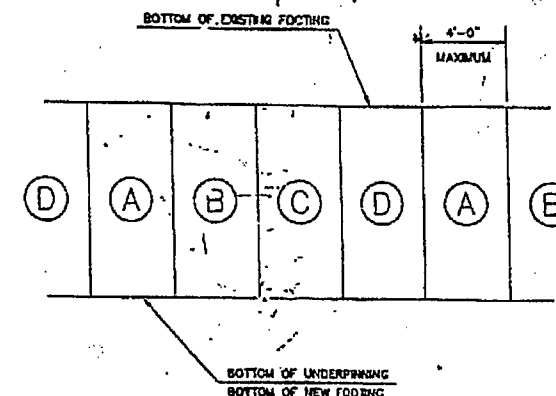
NOTE: ALL SPURCE BARS TO BE THE SAME SIZE AND SPACING AS WALL REINFORCEMENT.

TYPICAL REINFORCEMENT DETAILS  
AT CORNERS OF CONCRETE WALLS

NOTE: MINIMUM SIZE OF INTERSECTING REINFORCEMENT BAR AREA AT EACH END OF OPENING.

REINFORCEMENT AT  
WALL OPENINGS

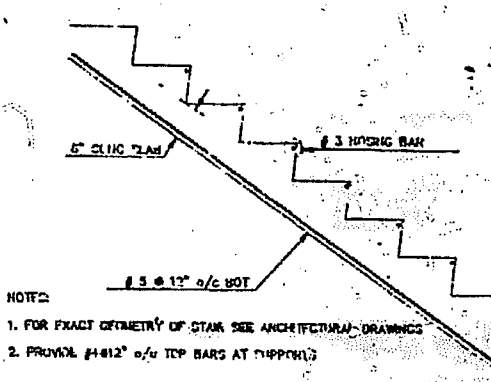
TYPICAL REINFORCEMENT DETAILS  
AT CORNERS OF CONCRETE WALLS



## NOTES

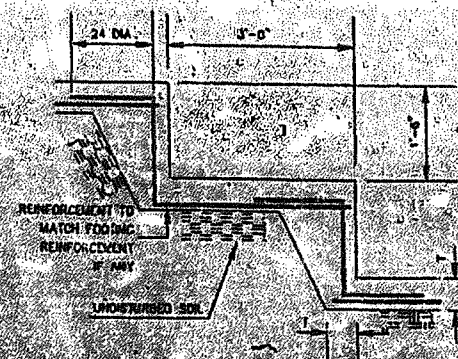
1. FOR EXACT GEOMETRY OF STAIR SEE ARCHITECTURAL DRAWING.
2. PROVIDE #4@12" o/c TOP BARS AT SUPPORTS.

TYPICAL CONCRETE STAIR DETAIL

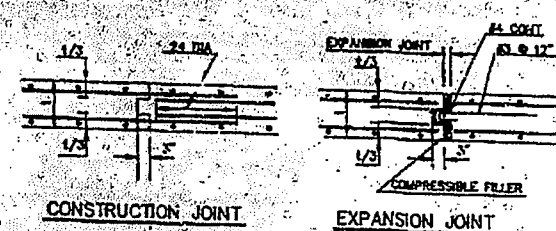


TYPICAL ELEVATION OF UNDERPINNING

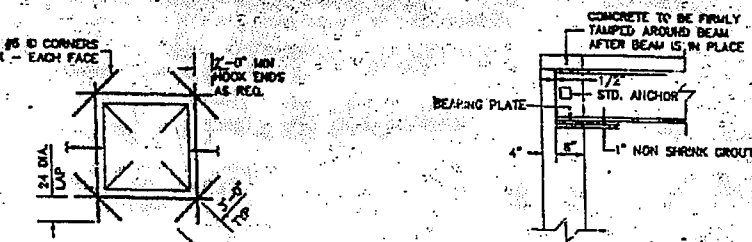
UNDERPINNING SHALL BE DONE IN SECTIONS. MAXIMUM CUT SHALL BE 4'-0" WIDE. SUCCESSIVE OR SIMULTANEOUS CUTS SHALL HAVE AT LEAST 12'-0" OF CLEAR DISTANCE BETWEEN THEM. EXCAVATE AND PLACE PANELS "A" FIRST, "B" SECOND "C" THIRD AND "D" LAST.



TYPICAL DETAIL  
AT STEPPED FOOTING

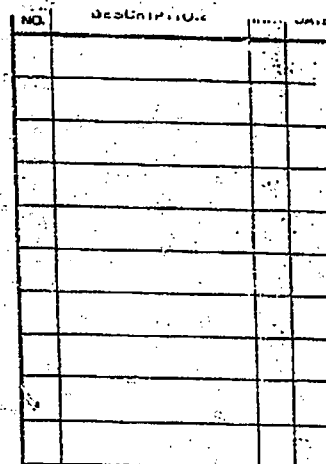


### VERTICAL JOINT DETAILS IN CONCRETE WALLS



REINFORCEMENT AT  
WALL OPENINGS

TYPICAL SECTION AT BEAM POCKETS



133-10 TO 133-22 39TH AVE.  
FLUSHING NY

**RAYMON**

**C H A**

ARCHITECT

DEPARTMENT OF  
PLANNING  
BOROUGH QUEENS  
111 124504/87

APPROVED  
DATE 8/20/95

100-40 1000 AVE. PHARMACY NY 10

FD-302a (Rev. 11-27-70) Page 210-200-1

PROJECT MANAGER SHEET NO.

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JOHN HUNTER

1995

DRAWN BY

2.1.

DATE 11/10/77



