## Geotechnical Report

# Allstate Ventures, LLC New Mixed-Use Building

64 Centre Avenue New Rochelle, New York

July 13, 2018

Prepared for:

Allstate Venture, LLC 13 Hayes Court – Unit 112 Monroe, NY 10950

Prepared by:

**SKYLANDS ENGINEERING, LLC** 124 Milton Road Sparta, NJ 07871

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Eugene J. Schwarzrock, Professional Engineer New York License No. 077007-1 Date

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#### INTRODUCTION

This project involves the design and construction of a new mixed-use building at 64 Centre Avenue, New Rochelle, Westchester County, New York. The property consists of two adjoining tax lots, Lot 8 to the left (northwest), and Lot 6 to the right (southeast). Both lots are  $\pm 50$  ft. wide, and the left lot is  $\pm 100$  ft. deep and the right lot is 155 ft. deep. Current plans indicate the building will be 14 to 16 sty tall, with two (2) levels of below ground parking and storage. The below ground levels will be constructed out to the lot lines encompassing a footprint of  $\pm 12,540$  SF, and beginning at the  $3^{rd}$  floor the left side of the building will end  $\pm 15$  ft. in from the rear lot line. The ground floor elevation will match the adjacent sidewalk.

The site currently contains mostly asphalt pavement, however a 50 ft. wide x 57 ft. deep one story stucco garage is situated in the rear of the left lot, and a 47.5 ft. wide x 22 ft. deep covered car wash area is situated in the rear of the right lot. Site elevations are unknown at this time, but the site is generally flat.

This report presents the findings of a subsurface investigation conducted specifically for this project, as well as recommendations for foundation design and construction of the proposed improvements.

#### **GEOLOGY**

Based on our review of topographic maps and published geologic data for this area of New Rochelle, including the *Surficial Geologic Map of New York - Lower Hudson Sheet*, 1989, by the New York State Geological Survey, this site is expected to be underlain by glacial till consisting of a mixture of grain sizes ranging from clay and silt, to sand, cobbles and boulders. Underlying bedrock is expected to consist of schists, based on the (*Bedrock*) *Geologic Map of New York - Lower Hudson Sheet*, 1970, by the New York State Museum and Science Service.

#### SUBSURFACE INVESTIGATION

Soiltesting, Inc. performed five (5) borings to identify the subsurface conditions present beneath the project site, including borings B-1, B-2, B-3, and B-4 which were drilled on March 22, 2018, and borings B-2A, B-3A, and B-5 which were drilled between June 19 and 20, 2018. Borings B-1, B-2/B-2A and B-3/B-3A were located in the right lot, rear to front, respectively, and Borings B-4, and B-5 were located in the left lot, front to rear, respectively, with boring B-5 drilled inside the existing garage. All borings were sampled continuously to a depth of  $\pm 6$  ft. to  $\pm 17$ , then at 5 ft. intervals to the completion of each boring. Borings B-2, B-3 and B-5 were terminated on auger refusal at depths of 12.5 ft., 11 ft., and 18 ft., respectively, while 5 ft. of bedrock was cored at the bottom of borings B-1, B-2A, B-3A and B-4, with the first three (3) borings terminated at a depth of 25 ft., and boring B-4 terminated at a depth of 17 ft.

All borings were drilled using a truck-mounted nominal 4-¼ in. hollow stem auger to advance and maintain the hole. Sampling was performed using a 2 in. O.D. split spoon sampler driven by a 140 lb. safety hammer with a 30 in. drop and the number of blows for each 6 in. increment was recorded, in accordance with procedures outlined in ASTM D1586 - Standard Test Method for Standard Penetration Test (SPT) and Split-Barrel Sampling of Soils. Bedrock was sampled using a double-tube core barrel in accordance with procedures outlined in ASTM D2113 - Standard Practice for Rock Core Drilling and Sampling.

Soil samples were classified by an experienced geologist in general accordance with D.M. Burmister's "Suggested Test Methods for Identification of Soils" (ASTM, 1958) and bedrock samples were classified according to their rock type, and measured percentage recovery and rock quality designation (RQD).

Groundwater was recorded in the field when it was first encountered in the borings and also from two (2) groundwater measurement wells installed in borings B-2 and B-3 in March. These wells were read after 24 hr. in March, and again in June during the subsequent drilling program

A Boring Location Plan and the boring logs are presented in the Appendix.

#### SUBSURFACE CONDITIONS

The subsurface conditions encountered beneath this site are generally consistent with the published geologic literature. Beneath the pavements, which contained 2 in. to 6 in. of asphalt over 0 in. to 10 in. of concrete, in situ conditions generally contained 3 ft. to 8 ft. of very loose to mostly medium dense granular fill. The majority of the fill was classified as silt with minor amounts of medium to fine sand, however the fill at boring B-4 was predominantly well-graded sand with silt and gravel. Wood and other organic material was also present in the fill from 6 ft. to 8 ft. deep at boring B-4. Beneath this fill, decomposed bedrock was present at boring B-4, while 2 ft. to 5 ft. of medium dense and dense silt or sand was present above weathered bedrock at borings B-1, B-2/2A, and B-3/3A. No fill was encountered at boring B-5 within the garage, and this boring contained well-graded sand with silt and fine gravel from beneath the concrete slab to the top of weathered bedrock at a depth of 11 ft.

Weathered bedrock was encountered in all five (5) borings at depths varying from 7 ft. to 11 ft. This softer bedrock was augered into for a distance of 3 ft. to 13 ft. before either terminating each boring on auger refusal, and/or beginning to core sample the lower, more competent bedrock. Based on the rock cores recovered from borings B-1, B-2A, B-3A, and B-4, underlying bedrock consists of schist.

SPT N-values in the upper fill layer ranged from 4 to 17 blows per foot (bpf). N-values in the underlying virgin soils ranged from 19 bpf to 70 bpf, with an average N-value of 45.

The four (4) bedrock cores had fair to excellent recoveries and RQDs, with recoveries ranging from 72.5% to 100% with an average of 89%, and RQDs ranging from 30% to 90% with an average of 56%.

Water was encountered in most borings at or just below the top of decomposed bedrock during drilling. Readings 24 hr. after installation of the two (2) wells at borings B-2 and B-3 indicated water to present at depths of 5.5 ft. at B-2 near the middle of the site, and 9.5 ft. at B-3 near the front of the site. The June readings from these wells indicated groundwater had stabilized at depths of 7.75 ft. and 7.25 ft., respectively. Given the underlying soil conditions, flat topography of the project site and surrounding area, and the fact that the borings were drilled without the introduction of water, we believe the readings obtained are not a temporary or perched condition and the depth to groundwater varies from 5 ft. to 7 ft. as a function of season.

#### **DESIGN RECOMMENDATIONS**

Based on the findings of the above-described subsurface investigation program, it is recommended that conventional spread footings are suitable for support of the proposed building. The recommended frost depth for this area of New York is 42 in. below exterior grade therefore all footings will be well below



this depth. With the planned construction of two (2) underground levels, footings will be ±20 ft. below grade, which means they will likely be supported on the more competent bedrock present below the weathered bedrock. Based on the results of this investigation, an allowable bearing capacity of 10 tons per square foot (tsf) is recommended for footings constructed on weathered bedrock and a higher allowable bearing capacity of 20 tsf may be used for footings founded on unweathered bedrock. Both these values are higher than the presumptive load-bearing values presented in Table 1806.2 of the New York 2015 Building Code; however, we believe these value are still somewhat conservative and therefore reasonable. The recommended coefficient of friction between cast in place concrete footings and the weathered bedrock is 0.60, which is also higher than that shown in Table 1806.2, but we feel is reasonable.

Following the above recommendations, it is estimated that post construction settlements will be no more than ¼ in., with no more than ¼ in. differential settlement between adjacent columns. These values are within generally accepted tolerance limits for this type of structure and use. Settlement will be elastic (instantaneous), and essentially complete at the end of construction.

It is expected that construction of the lowest level floor will require backfilling and leveling with granular fill in order to fill areas of excavation. A minimum of 3 in. of granular fill is recommended for placement beneath this slab(s) in order to avoid hard points of contact with the underlying bedrock. Additional granular fill may be preferred so that sub-slab drainage piping can be installed to handle long term dewatering. A modulus of subgrade reaction equal to 250 pci is recommended for a slab-on-grade constructed in this manner. Since groundwater is expected to be  $\pm 13$  ft. above the lower level slab, waterproofing or dampproofing with groundwater control is required per section 1805 of the Code.

In accordance with the provisions of Section 1613.3.2 of Code, and ASCE 7 Chapter 20, a seismic site class of B, rock, is recommended for design of the new addition, based on the conditions encountered during the investigation. Based on the project location, in conjunction with the above site class, the following seismic parameters follow from the Code:

$S_s =$	0.275	$S_1 =$	0.072
$F_a =$	1.0	$F_v =$	1.0
S <sub>MS</sub> =	0.275	S <sub>M1</sub> =	0.072
S <sub>DS</sub> =	0.184	$S_{D1} =$	0.048

Seismic Design Category Based on Short Period Response Accelerations = B\*
Seismic Design Category Based on 1-sec Period Response Accelerations = A\*
\* based on assumed Risk Category II

Liquefaction is not a concern since this building will be founded on bedrock.

#### CONSTRUCTION RECOMMENDATIONS

Footings shall not be constructed on frozen or overly wet subgrade materials. All frozen or saturated subgrade soil should be removed and replaced with compacted structural fill, or clean crushed stone, as required. Bedrock surfaces should be protected from ponding or freezing water since these conditions may weaken the in situ rock during construction. Foundation concrete should be placed as quickly as possible, and within a few days of completing each footing excavation, so that precipitation or freezing temperatures do not adversely affect the bearing rock.

The wood and organic soils encountered in boring B-4 will be removed completely during basement construction therefore these materials should be removed off site and not used as site or structural backfill. Other organic soils were not encountered within the other borings; however, if other organic soils are encountered they should be removed off site and not be used as backfill.

Cobbles and boulders were encountered sporadically in most borings. Any cobbles or boulders encountered during construction should be removed so that no part protrudes into the bottom or sides of foundation excavations.

Based on the reported recoveries and RQD's of the bedrock samples we believe the weathered bedrock may be removed and shaped to the required elevations using conventional hydraulic equipment such as large excavators and rock hammers. The lower, more competent bedrock may need to be drilled and hydraulically split in order to be removed. Blasting is not recommended due to the proximity of the adjacent buildings.

Dewatering is expected to be required during foundation construction since groundwater was observed to be as high as 5.5 ft. below grade, or ±8 ft. above the anticipated bottom of footing excavations. Depending on the type of support of excavation chosen (see next paragraph), if interlocking steel sheeting is installed around the perimeter of the foundation and that the sheets are toed into the weathered bedrock, it is anticipated that most of the water will be prevented from entering the excavation once the initial volume is removed. Therefore on-going dewatering operations may be accomplished using conventional sump pumps. Should soldier piles and lagging be used, then inflows of groundwater will be higher.

Due to the proximity of adjacent buildings, they will either need to be underpinned down to weathered bedrock, or the support of excavation will need to be designed to handle these additional loads, if it can be so designed. The surrounding buildings are 1 and 2 story brick and 1 story stucco finish so while the loads are not significant, the façades will be susceptible to cracking at very little settlement.

Compacted structural fill should consist of predominately well-graded, coarse to fine sand and/or gravel with a maximum 10% non-plastic fines (material passing a No. 200 sieve) and be free of organics and other deleterious materials. Aggregate size should be limited to no bigger than 1 in. in the largest dimension. It is estimated that none of the in situ materials will be suitable for use as structural fill due to the high silt content. Representative samples of any proposed fill material should be tested for gradation and moisture-density relationship prior to use to confirm its suitability.

Structural fill material should be placed in maximum 12 in. loose lifts and compacted to 95% of its maximum dry density at optimum moisture content as determined by the Modified Proctor Density Test (ASTM D1557). These operations should be performed under full-time geotechnical inspection and testing by either the Sand Cone Method (ASTM D1556), Nuclear Density Gauge (ASTM D2922 and D3012), or other moisture/density test methods. These density tests should be performed by an experienced geotechnical inspector at sufficient frequency and spacing to ensure proper compaction, with the following criteria suggested as guidelines:

Location	Frequency of Testing
Structural fill beneath foundations, adjacent to structures & beneath slabs-on-grade	1 test every 2,500 SF min. 1 test per lift
Utility trenches	1 test every 50-100 LF per lift min. 3 tests per day
General site fill (beyond building limits)	1 test every 5,000 SF per lift min. 1 test per lift

The soils present on site are not considered moisture sensitive, however proper grading and compaction techniques are still required to prevent soils from softening and/or pumping.

For excavations that extend deeper than 5 ft., sheeting, shoring, sloping, or benching of the excavation sidewalls is required per OSHA standards. Considering the proximity of adjacent properties, buildings, and sidewalks, it is expected that sheeting or shoring will be required. For the design of temporary sheeting or shoring, the following soil parameters may be used:

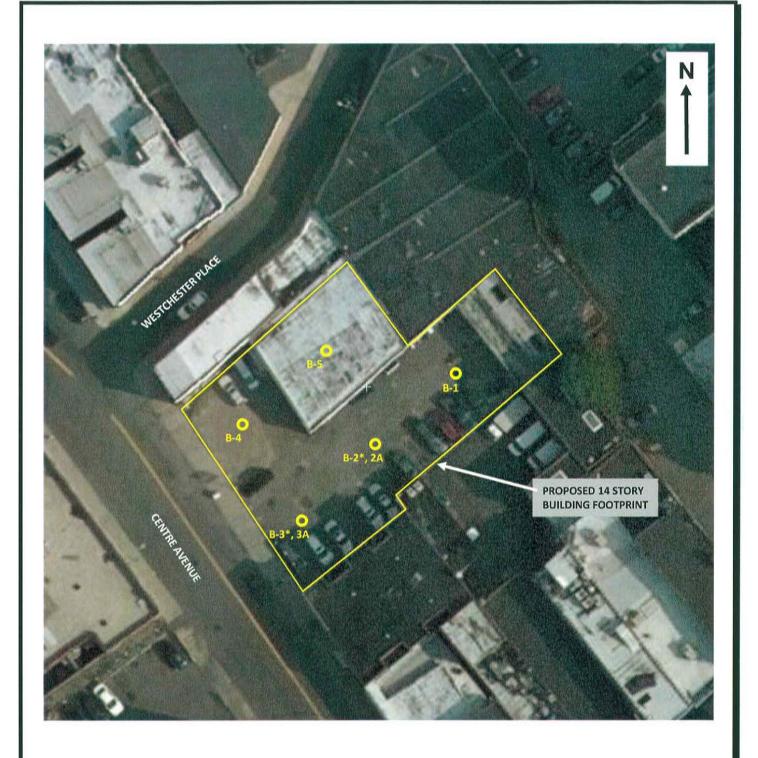
Fill (0 - ±8 ft.)	
Moist unit weight of soil,	$\gamma_t = 115 \text{ pcf}$
Angle of internal friction,	$\phi = 28^{\circ}$
Silty sand (±8 - 11 ft. top of we	eathered bedrock)

 $\begin{array}{ll} \mbox{Moist unit weight of soil,} & \gamma_t = 120 \mbox{ pcf} \\ \mbox{Angle of internal friction,} & \varphi = 36^{\circ} \end{array}$ 

All sheeting, shoring and bracing shall be designed by a professional engineer licensed in the State of New York. Shorter, unbraced excavations will experience localized instability (i.e., sloughing) if left open for more than a few days due to the gradation of the material and lack of moisture. To reduce the severity of this sloughing, such excavations should be covered with plastic sheeting for protection from rainfall and moisture changes.

It is recommended that all foundation and slab-on-grade subgrade preparation procedures be inspected by a qualified geotechnical engineer experienced with this type of construction.

### **APPENDIX**



**LEGEND** 

O BOR

BORING

TEMP. GW MEASURING WELL

#### NOTES:

1. BASE IMAGERY @ ZOOM.EARTH, 7-12-2018

SCALE N.T.S.

### **BORING LOCATION PLAN**

ALLSTATE VENTURES, LLC 64 CENTRE AVENUE NEW ROCHELLE, NEW YORK

#### SKYLANDS ENGINEERING, LLC

124 MILTON ROAD SPARTA, NJ 07871 CERTIFICATE OF AUTHORIZATION NO. 0013524

DATE: 7-13-2018

# **Boring Logs**

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		2					1 / 12"				v soft		Brn SILT	100 E - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -
		SS	24"	18"	4'0"	2	4			moist/wet	2161	Brn SILT, sm F	FM sand ( fill )	
5		3	SS	24"	17"	6'0"	9	15 7			stiff moist/wet	3'6"	Brn SII T & FM	1 SAND, lit C gravel, cobbles
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		7	SS	1"	0"	15'1"	50/1"				hard			
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IINC	BPECTOR							TYPE			HSA	SS	NQ2	DATE START	6/19/18
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PR	OPORTIO	NS II	SED:	TRAC	E = C	- 10%	ITTLE	= 10 -	20% 5	OME =	20 - 35% A	ND =35 - 5	0%	F = FINE	

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		DO								044	0046 40			HOLE NO. B-3			
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		Γ (20 Υ (91					PROJE	ECT NA	ME	64 C	entre Ave	nue		BORING LOCATIONS per Plan			
FO	REMAN -			10-10	,,,,		LOCAT	TION			Rochelle			perman			
M 080	DJD/jk									STATUS		1094 B					
INS	PECTOR							1877 TO 5 UK			CASING	SAMPLER	CORE BAR	OFFSET			
								TYPE			HSA	SS		DATE START	3/22/18		
0.000	OUND WA					3		SIZE I		_	3¾"	1 3/8"	DIT	DATE FINISH	3/22/18		
1000	none_FT 9'6"_FT		100000000000000000000000000000000000000		JKS				IER WI IER FA			140# 30"	BIT	SURFACE ELEV. GROUND WATER ELEV.			
	7'3"_FT							TIPAVIIV	ILKIA	to be		- 00		OKOOND WATER CEEV.			
		Г		SAMI	PIF					Г	T	1					
		-		7/1011							DENSITY	STRATA	FIELD ID	ENTIFICATION OF SOI	L REMARKS		
표	CASING						PERSONAL PROPERTY.	VS PEI SAMP		CORE	OR	CHANGE	INCL. COL	OR, LOSS OF WASH W	ATER, SEAMS		
DEPTH	BLOWS PER	NO	Туре	PEN	REC	DEPTH	(FOR	CE ON	TUBE)	PER	CONSIST	DEPTH		IN ROCK, ETC.			
	FOOT					@ BOT	0 - 6	6 - 12	12- 18	FT (MIN)	MOIST	ELEV					
		1	SS	24"	6"	2'0"	4	4			moist			SPHALT / 8" CONCRETE			
		2		24"	18"	4'0"	6	3	_		stiff	3'0"		FM sand, tr clay, F gravel			
		2	SS	24	10	40	13	17			moist compact	30	SAME ( fill ) Brn FM SAND & SILT, lit C sand, tr F gravel				
5		3	SS	24"	20"	6'0"	16	21			moist			& C SAND, SILT, sm F grave			
*****							17	19			dense						
		4	SS	24"	20"	8'0"	13 12	17 25	_		moist	8'0"	Brn Gry FMC	SAND & F GRAVEL, sm silt, tr	cobbles, boulders		
		5	SS	6"	5"	8'6"	100/6"	20			compact v dense	00	partially decon	nposed BEDROCK			
10												STANCE PROPERTY.					
		6	SS	1"	1"	10'1"	50/1"				v dense	11'0"	SAME		UGER REFUSAL		
										-				E.O.B, 11'0"			
15														ed 1" SCH 40 PVC observ	Olev.		
								_			-			with 10' screen to 11' dep Set curb box at surface			
			_	-							1			Set curb box at surface	•		
1																	
20					_												
			_		_						-						
											1						
											1						
25					_						-						
			_					_	_								
			-														
2222																	
30			-	_	_					-	-						
								_			1						
35			_						_		-						
											1						
40																	
40 NC	TE: Su	heoi	cor	ditio	ne -	eveale	d by t	hie in	veeti	ration	represen	+					
INC						c locat											
-	cor	ditio	ons a	at oth	her l	ocation	s or t		7 ·	1.51			OILLO ===	er IIIALETTA	8.0		
	DUND SU AUGER						SED	T = TH	IINWAL	CASING	G THEN_ V = VANE		SING TO	FT. HOLE NO	). B-3		
wo	R = WEIG	HT O	F ROI	DS		WOH =		T OF H	АММЕ	R & RO		n vavecă ii		C = COARSE			
	= SPLIT T					H.S.A. =					20 - 35% A	ND =35 - 50	0/_	M = MEDIUM F = FINE			

	SOI					<b>:</b> .	CLIEN	T:	Allst	ate Ve	ntures, L	SHEET_1_OF_1			
			NOV											HOLE NO.	B-3A
			D, C				-	ECT NO	-	G115	-1034-18				
			3) 26				PROJE	ECT NA	ME	CAC	mtus Aves			BORING LOCATIONS	
EO	REMAN -		4) 94	10-40	550		LOCA	TION			entre Aver Rochelle,			per Plan	
ľ	DJD/m						LOOM				,				
INS	PECTOR										CASING	SAMPLER	CORE BAR	OFFSET	
			-					TYPE			HSA	SS	NQ2	DATE START	6/19/18
	OUND W					3	l	SIZE I			4 1/4"	1 3/8"	2"	DATE FINISH	6/20/18
10000	<u>_7'</u> _FT <i>A</i> FT AF				S				1ER W 1ER FA		-	140# 30"	BIT dia	SURFACE ELEV. GROUND WATER ELEV.	
Α1,		I LIV			DI E			HAIVIIV	IER FA	I		30	T CIA	OROGRA WATER ELEV.	
		_		SAMI I	LE		200000000			Name (Contract)	DENSITY	STRATA	FIELD ID	ENTIFICATION OF SOIL	REMARKS
DEPTH	CASING BLOWS PER	NO	Туре	PEN	REC	DEPTH	ON (FOR	WS PEI SAMP CE ON	LER TUBE)	CORE TIME PER FT	OR CONSIST	CHANGE DEPTH		OR, LOSS OF WASH WA IN ROCK, ETC.	
I ETR	FOOT					@ BOT	0 - 6	6 - 12	12- 18	(MIN)	MOIST	ELEV			
													A CONTRACTOR OF STREET, SAN AND STREET, SAN AN	10" CONCRETE	
													( See B-3 )		
5															
												7'0"			
											moist/wet	70	partially decon	posed BEDROCK	
25700													Entropy of the Part of the Control o	orden processor and consistence of the consistence	
10				_	_					-					
											]				
40															
15		_								-					
20												20'0"	AUGER REFU	SAL	
-		1	С	60"	60"	25'0"	RQD =	90%		2		200		chist / Gniess )	
							Rec =	100%		2.05					
		_			_					2.15					
25										2.2		25'0"			
														E.O.B. 25'0"	
					-										
											1				
30															
											-				
											1				
35	_	_	_			_		_							
											1				
40															
40 NC		heol	Lcon	ditio	ne -	evesle	d by f	hie in	vestic	ation	represent	<u> </u>			
NOTE: Subsoil conditions revealed by this investigation represent conditions at specific locations and may not represent conditions at other locations or times.															
	OUND SU AUGER						SEDCASING THENCASING TO _					ASING TO	FT. HOLE NO.	. B-3A	
	R = WEI				VDED		= WEIGHT OF HAMMER & RODS							C = COARSE	
	= SPLIT					H.S.A. =					00 0504	AND -25 5	000/	M = MEDIUM	
PR	OPORTIO	NS U	SED:	IRA	JE = (	J - 10%	LITTLE	= 10 -	20%	SOME =	20 - 35%	4MD =35 - 5	0070	F = FINE	

	SOI					<b>.</b>	CLIEN	T:	Allst	ate Ve	ntures, L	SHEET_1_OF_1					
			NOV							0.11	00.40.40			HOLE NO.	B-4		
			RD, C				PROJE			G41-	0946-18			50500010010010000			
			3) 26 4) 94				PROJE	CINA	ME	64 Ce	entre Ave	nue		BORING LOCATIONS per Plan			
FO	REMAN -	DRILL	ER				LOCAT	TION			Rochelle,			por r terr			
	DJD/jk		50T														
INS	SPECTOR							TVDE			CASING	SAMPLER	CORE BAR	OFFSET	3/22/18		
GP	OUND W	TED	OBSI	ED\/A	TIONS	2		TYPE SIZE I	D		HSA 3¾"	1 3/8"	NQ 2"	DATE START DATE FINISH	3/22/18		
	none FT					,			.D. IER W	г.	3/4	140#	BIT	SURFACE ELEV.	3/22/10		
AT.	FTAF	TER_	_но	URS					IER FA		<u> </u>	30"	dia	GROUND WATER ELEV.			
			5	SAM	PLE					Г							
DEPTH	CASING BLOWS PER FOOT	NO	Туре	PEN	REC	DEPTH	ON (FOR	VS PEI SAMP CE ON 6 - 12	LER TUBE)	CORE TIME PER FT	DENSITY OR CONSIST MOIST	STRATA CHANGE DEPTH		ENTIFICATION OF SOIL DR, LOSS OF WASH WA IN ROCK, ETC.			
-	FOOT	1	SS	24"	6"	@ BOT 2'0"	12	9	I	(MIN)	dry	ELEV	2" ASPHALT				
							7	6			compact		Brn FM SAND	FM SAND & SILT, C SAND, F GRAVEL			
		2	SS	24"	9"	4'0"	5 7	6 8			dry compact		SAME				
5		3	SS	24"	10"	6'0"	25	72			wet		Brn FMC SANI				
~				0.411		01011	39	3			v dense						
		4	SS	24"	6"	8'0"	2	4			v loose	8'0"	SAME; tr wood	, organics ( fill )			
		5	SS	5"	5"	8'5"	100/5"				dry	- 00	partially weath	ered BEDROCK			
10		6		4"	4"	10'4"	50/4"				v dense v dense						
		0	SS	4	4	104	50/4	i.			v dense	12'0"	AUGER REFU	SAL			
	1 c 60" 60" 17						RQD =			2			BEDROCK (S	The state of the s			
15							Rec =	100%		3	-						
10										3							
										2		17'0"		F O D 47/01			
					-									E.O.B. 17'0"			
20																	
										-							
												1					
25					_												
30				_							1						
											1						
			_		_												
											1						
35																	
					-					-							
40																	
40 NC		bsoil	Lcon	ditio	ns r	eveale	d by th	nis in	vestic	ation	represent						
	COL	nditio	ons a	at sp	ecifi	c locat	ions a	ınd m	ay no	t repr	esent	1					
GP	COI OUND SU					ocation	ns or t	imes.		CASIN	G THEN	C	ASING TO	FT.  HOLE NO.	B-4		
A =	AUGER	UP =	UND	ISTUR	RBED	PISTON	0000010446		INWAI	Ī.	V = VANE			37 807	<del>-</del>		
11,5077	OR = WEIG = SPLIT 1					WOH = H.S.A. =					DS			C = COARSE M = MEDIUM			
											20 - 35%	0%	F = FINE				

Г	SOILTESTING, INC. 90 DONOVAN RD.					<b>.</b>	CLIEN	T:	Allst	ate Ve	ntures, L	SHEET_1_OF_1					
												HOLE NO. B-5					
				T 06			PROJE	-		G41-	0946-18			The state of the s			
				62-93 46-48			PROJE	CT NA	ME	64 C	entre Ave	nue.		BORING LOCATIONS per Plan			
FO	REMAN -	_	_	10 10	,,,,		LOCAT	ION			Rochelle,			porrian			
	DJD/m		16.5473.675														
INS	PECTOR										CASING	SAMPLER	CORE BAR	OFFSET	0110110		
CD.	OLINID W	ATED	ODG	=D\/A	TION			TYPE	_		HSA 2 ½"	SS 1 3/8"		DATE START DATE FINISH	6/19/18 6/20/18		
	OUND WA					5	l	SIZE I	.b. 1ER W	Т	2 /2	140#	BIT	SURFACE ELEV.	6/20/18		
	FT AF								IER FA			30"		GROUND WATER ELEV.			
				SAM	PLE					T			1				
DEPTH	CASING BLOWS PER FOOT		REC	DEPTH	ON (FOR	VS PEI SAMP CE ON 6 - 12	LER TUBE)	FT	DENSITY OR CONSIST	STRATA CHANGE DEPTH		ENTIFICATION OF SOIL OR, LOSS OF WASH WA IN ROCK, ETC.	1994 Y (				
	F001	1	SS	18"	18"	@ BOT 2'0"	2	2		(MIN)	MOIST dry	ELEV	10" CONCRET	E			
							7				loose		Brn FMC SANI	AND, sm clay, lit F gravel, tr silt			
		2	SS	15"	15"	3'3"	15 50/3"	26			dry v dense		Brn FMC SANI	FMC SAND, lit F gravel, tr silt			
5		SS	17"	7"	5'5"	47	62			dry		Brn Gry FMC SAND & SILT, sm F gravel, tr cobbles					
A000							100/5"				v dense		ANYONA MINE ARONA	10 8 10 15 15 15 15 15 15 15 15 15 15 15 15 15			
		4	SS	2"	2"	6'2"	50/2"				v dense		Brn Gry FMC S	SAND & SILT, sm F gravel			
10		5	SS	0.41	4770	4.01011	0.0	0.7			2007	4.41011					
		24"	17"	12'0"	32	37 34		-	v dense	11'0"	SAME partially decom	posed BEDROCK					
				33 34													
15		6		0"	0"	15'0"	50/0"			-	. u donce		No Possyon				
15		0	SS	U	0	150	50/0				v dense		No Recovery				
												10.01.00 Page 20	A CATCH DRIVING HIS CONTROL OF				
		_	_									18'0"	AUGER REFU	E.O.B. 18'0"			
20														L.O.D. 100			
)		_			_					-							
25		_		_													
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30										<del>                                     </del>	1						
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72 SA											]						
40				1100	Grand II	2000											
NC	COL	nditi	ons a	at sp	ecifi	eveale ic locat ocation	ions a	nd m	ay no		represent esent						
	OUND SU	IRFAC	E TO		F	T. U	SED_			CASIN		The state of the s	ASING TO	FT. HOLE NO.	B-5		
1975 and Inc.	AUGER R = WEIG				RBED	PISTON WOH =			INWAI IAMME	555.	V = VANE :	TEST		C = COARSE			
SS	= SPLIT 1	TUBE	SAME	PLER		H.S.A. =	HOLL	ow st	EM AL	JGER				M = MEDIUM			
PR	OPORTIO	NS II	SED:	TRAC	CF = (	1 - 10%	LITTLE	= 10 -	20% 5	SOME =	20 - 35%	ND = 35 - 5	0%	F = FINE			