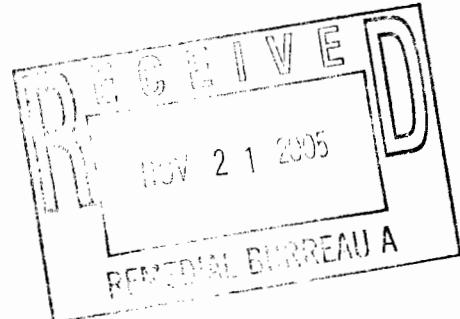


This Investigation Beneath the 140 Building (Survey Unit 06 and Survey Unit 07) Report has been reviewed by URS Corporation – New York, and I am in agreement with the conclusions.

URS Corporation – New York



Robert D. Brathovde, P.E.
Engineer of Record



This Investigation Beneath the 140 Building (Survey Unit 06 and Survey Unit 07) Report has been reviewed by Professional Radiation Consulting, Inc. (PRCI), and I am in agreement with the conclusions.

Professional Radiation Consulting, Inc.

A handwritten signature of "Shane Brightwell" in black ink.

Shane Brightwell, CHP
President

This Investigation Beneath the 140 Building (Survey Unit 06 and Survey Unit 07) Report has been reviewed by Envirocon, Inc. and I am in agreement with the conclusions.

Envirocon, Inc.

A handwritten signature of "Richard Hafner" in black ink.

Richard Hafner
Radiation Safety Officer

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Appendix B: Correspondence regarding the Systematic Subsurface Soil Sampling and Analysis Plan, Beneath the 140 Building, November 2004
Appendix C: Boring Logs (Boring Logs are included as Appendix C on the enclosed CD. The enclosed CD includes a complete electronic copy of this report.)
Appendix D: MARSSIM and COMPASS Software Evaluations

1.0 INTRODUCTION

This report provides the results, data assessments and conclusions made with respect to the characterization of surface and subsurface soils pursuant to the *Systematic Subsurface Soil Sampling and Analysis Plan, Beneath the 140 Building* (SSSA Plan), dated November 2004 (**Appendix A**) at the Former Sylvania Electric Products Incorporated (Sylvania) facility located at 140, 100 and 70 Cantiague Rock Road, Hicksville, New York (the Site). The New York State Department of Environmental Conservation (NYSDEC) provided comments on the SSSA Plan in a letter dated December 20, 2004. GTE Operations Support Incorporated (GTEOSI) responded to the NYSDEC comments in a letter dated January 20, 2005. The SSSA Plan was approved by NYSDEC in a letter dated January 31, 2005. These letters are included in **Appendix B**.

The areas investigated were designated as Survey Units (SUs) as defined in NUREG 1575, *Multi-Agency Radiation Survey and Site Investigation Manual* (the MARSSIM). The areas designated as SU06 and SU07 are located respectively under the eastern and western portions of the 140 Building (**Figure 1**). This investigation commenced on February 22, 2005 and sampling was completed on April 14, 2005.

Included in this report are sample analytical results, data assessments and conclusions regarding radiological, volatile organic compounds (VOCs) and nickel (Ni) data. Also reported herein are the analytical results for beryllium (Be).

2.0 SCREENING AND SAMPLING

A systematic triangular sampling pattern was used to provide uniform lateral coverage of the SUs. Soil borings were advanced and soil samples were collected continuously, beginning at ground surface (just below the bottom of the concrete slab) to 30 feet below ground surface (bgs). The sampling pattern grid, rows and boring locations are shown in **Figure 1**.

A 2-foot (ft) long split spoon sampling device was advanced for soil retrieval. The recovered soils were screened using a photoionization detector (PID) for VOCs and a 3-inch sodium iodide (NaI) detector for radioactivity prior to sample collection.

The samples designated as sample point (SP) samples were collected at intervals that were vertically staggered by 1 meter (m) (approximately 3 ft). SP samples were collected in 2-ft increments to maximize sample volume. This additional volume of soil was needed to perform both on-Site and off-Site analyses. Row 1 borings had SP samples at 1 ft, 11 ft and 21 ft; Row 2 borings had SP samples at 4 ft, 14 ft and 24 ft; and Row 3 borings had SP samples at 7 ft, 17 ft and 27 ft. In addition, each boring had an SP sample at 30 ft (**Figure 2**).

Samples designated as delineation (DL) samples were collected in 1-ft increments between the staggered SP sample intervals.

Samples were analyzed both on Site for timely response to guide investigation and off Site at Severn Trent Laboratories, Inc. (STL) of Earth City, Missouri for final verification. The sample analytical results were compared to the Site cleanup levels specified in the approved *Comprehensive Soil Remediation Program Work Plan, Former Sylvania Electric Products*

Facility, January 18, 2002 (Revision 5: June 2003) (Work Plan). Intervals, increments and analyses for each row type are summarized on **Figure 2**.

A field geologist classified the soils in general accordance with the Unified Soil Classification System (USCS). Sample descriptions included soil type, color, moisture, and visual observations. Boring Logs are provided in **Appendix C**.

2.1 RADIONUCLIDES

DL samples were homogenized and analyzed on Site by gamma spectroscopy for thorium (Th-232) and uranium (U-238).

SP samples were homogenized and split. One portion was analyzed on Site by gamma spectroscopy and the other portion was sent off Site to STL for alpha spectroscopy analysis. STL performed isotopic thorium analysis using National Academy of Science (NAS)/Department of Energy (DOE) 3004/RP-725 and isotopic uranium analysis using NAS/DOE 3050/RP-725 (which includes U-234).

2.2 VOLATILE ORGANIC COMPOUNDS

DL samples were collected and analyzed for VOCs if PID readings were greater than 25 parts per million (ppm) or if visual observations (e.g., staining) warranted. DL samples to be analyzed on Site by Stone Environmental Inc. (SEI) for trichloroethene (TCE) and tetrachloroethene (PCE) using solid phase microextraction and capillary gas chromatography. Based on field screening results as noted in the boring logs (**Appendix C**), no DL samples were identified for analysis on Site.

Two samples were collected at each SP interval for VOC analysis. One sample was analyzed on Site by SEI. The other sample was sent off Site to STL for VOC analysis using United States Environmental Protection Agency (USEPA) Method 8260B.

2.3 METALS

DL samples were collected for Ni analysis at alternating 1-ft intervals between SP samples. If sample recovery was insufficient, analysis could not be performed. In such an event, a sample for Ni was collected at the next available interval and at alternate intervals thereafter. Ni DL samples were analyzed on Site using x-ray fluorescence spectroscopy (XRF) by SEI.

Two samples were collected at each SP interval for metals analysis. One sample was analyzed on Site by SEI for Ni. The other sample was sent off Site to STL for analysis of Ni and Be using USEPA Method 6010B.

2.4 SAMPLING SUMMARY

The SSSA Plan was designed to allow flexibility to respond to field conditions (e.g., boring relocation and insufficient sample recovery). Nineteen soil borings had to be moved from their proposed locations due to limited access (e.g., utilities and obstructions). The relocations were

within the limits specified in the SSSA Plan. These obstructions, each designated as an "interference area" in **Figure 1**, consisted of areas inaccessible to large equipment. Each soil boring location was surveyed using the laser positioning system (LPS).

In SU06 a total of 15 soil borings were advanced resulting in the recovery of 60 SP samples, 312 radionuclide DL samples, and 173 Ni DL samples. In SU07 a total of 22 soil borings were advanced resulting in the recovery of 88 SP samples, 478 radionuclide DL samples, and 260 Ni DL samples.

3.0 ANALYTICAL RESULTS/ASSESSMENTS

The results of the DL and SP sample analyses from SU06 and SU07 are summarized in **Table 1**. The results of the SP sample analyses from SU06 and SU07 are summarized in **Table 2**. Statistical assessments of radiological off-Site SP data were performed with applicable methods specified in the MARSSIM and analytical results were also compared to Site cleanup levels. VOC and Ni results were compared to the Site cleanup levels. Be results were compared to the NYSDEC Technical and Administrative Guidance Memorandum (TAGM) #4046 values and other published literature sources for New York State soils. These assessments are described herein.

3.1 RADIOLOGICAL

A statistical assessment of radiological SP data (with the exception of samples from the final depth) was performed using the MARSSIM methods. SP samples at the final depth (30 ft) were compared to the Site cleanup levels in the Work Plan (**Table 2**).

3.1.1 Survey Unit Assessment

Each SU was characterized vertically at 3-m (10-ft) staggered depths. Since the MARSSIM provides characterization and final verification guidance primarily on surface soils, each 3-m (10-ft) SU interval was evaluated independently as if that SU interval were representative of an undulating soil surface. For the purposes of the assessment, the 0- to 3-m (0- to 10-ft) SU interval was labeled SU Interval 1, the 3- to 6-m (11- to 20-ft) was SU Interval 2, and the 6- to 9-m (21- to 30-ft) was SU Interval 3. Thus, for the 15 borings advanced in SU06, 45 samples were used in the MARSSIM assessment of the three SU intervals. For the 22 borings advanced in SU07, 66 samples were used in the MARSSIM assessment of the three SU intervals.

The assessment of the SU interval data sets was performed using the *Compass Software*. The *Compass Software* allows the user to set up the analytical data for all radiological analytes in a readable input file format, and then evaluate the data set using the applicable MARSSIM methods. The *Compass Software* evaluations of each of the three SU intervals are in **Appendix D**.

The Work Plan specifies Site cleanup levels for three radionuclides (Th-232, U-234 and U-238). The MARSSIM addresses evaluation of multiple radionuclides by employing the Sum of Ratios (SOR) Method. First, for SP samples, the ratio of the concentration for each radionuclide to its corresponding Site cleanup level is calculated. The ratios for all three radionuclides are then

summed for a single sample. This results in a single unitless SOR value for each sample. The samples in a given SU interval are then evaluated using the statistical methods inherent in the *Compass Software*.

3.1.1.1 SU06 Assessment

Evaluation of the DL and SP samples in SU06 indicates that the concentrations are below the radionuclide Site cleanup levels. While most samples exhibited natural prevalence of uranium, samples at soil boring 007, at depths of 17, 27 and 30 ft bgs, indicated concentrations of U-234 greater than concentrations of U-238. SU06, soil boring 007 is in the same subcell (I06) as Historic Leach Pool (LPH) 21 (**Figure 3**). LPH21 is discussed in greater detail in Section 4.0 of this report.

3.1.1.2 SU07 Assessment

Evaluation of the DL and SP samples in SU07 indicates that the concentrations are below the radionuclide Site cleanup levels. There is an indication in three soil borings (014, 031 and 032) immediately below the bottom of the concrete slab that disturbed material (fill) contains U-238 (25 to 33 picoCuries per gram [pCi/g]). Borings 007, 017 and 035 indicated concentrations of U-234 greater than concentrations of U-238 just beneath the bottom of the concrete slab.

3.1.2 Decision Analysis

The decision analysis for the radiological analytical results was based on the default null hypothesis recommended in the MARSSIM, which states: "The residual radioactivity in the survey unit exceeds the release criterion." The MARSSIM "Sign Test" (assuming no contribution from background radionuclides) was used to reject the null hypothesis. When the null hypothesis is rejected, the SU passes and qualifies for release. If the null hypothesis cannot be rejected, further investigation or remedial action may be necessary.

As stated earlier, each of the three intervals was evaluated independently in each SU. Therefore, there were a total of six independent evaluations. The following table summarizes the results of the *Compass Software* evaluations.

| SU | SU Interval | Depth Range (ft) | # Samples (N) | | Sum of Ratios | | Null Hypothesis | SU Interval Status |
|----|-------------|------------------|---------------|--------|---------------|------|-----------------|--------------------|
| | | | Required | Actual | Avg | Max | | |
| 06 | 1 | 0-10 | 13 | 15 | 0.31 | 0.62 | Rejected | Passes |
| | 2 | 11-20 | 13 | 15 | 0.13 | 0.80 | Rejected | Passes |
| | 3 | 21-30 | 14 | 15 | 0.14 | 0.97 | Rejected | Passes |
| 07 | 1 | 0-10 | 15 | 22 | 0.40 | 1.22 | Rejected | Passes |
| | 2 | 11-20 | 13 | 22 | 0.10 | 0.29 | Rejected | Passes |
| | 3 | 21-30 | 13 | 22 | 0.07 | 0.13 | Rejected | Passes |

The evaluation of the SP analytical results for SU06 and SU07 using the *Compass Software* indicated that the average concentrations of Th-232, U-234, and U-238 in the soils beneath the 140 Building are below the Site cleanup levels.

3.2 VOLATILE ORGANIC COMPOUNDS

The VOC analytical results of TCE and PCE were compared to the Site cleanup levels of 0.7 milligrams per kilogram (mg/kg) and 1.82 mg/kg, respectively. The following table provides the highest concentrations of VOC sample analytical results from **Table 1**.

| SU | Depth Range (ft) | TCE (mg/kg) | PCE (mg/kg) |
|----|------------------|-------------|-------------|
| 06 | 0-10 | 0.0078 | 0.030 |
| | 11-20 | 0.0026 U | 0.0026 U |
| | 21-30 | 0.0026 U | 0.0026 U |
| 07 | 0-10 | 0.0016 J | 0.022 |
| | 11-20 | 0.0026 U | 0.0026 U |
| | 21-30 | 0.0026 U | 0.0026 U |

Notes: U – not detected J – estimated value

Based on a review of DL and SP analytical data, TCE and PCE were not detected above Site cleanup levels.

3.3 METALS

The Ni analytical results were compared to the Site cleanup level (560 mg/kg) while the Be results were compared to NYSDEC TAGM #4046 values (0.16 mg/kg or Site background) and other published literature sources for New York State soils. The following table provides the highest concentrations of Ni and Be from **Table 1**.

| SU | Depth Range (ft) | Ni (mg/kg) | Be (mg/kg) |
|----|------------------|------------|------------|
| 06 | 0-10 | 330 | 0.91 |
| | 11-20 | 3.1J | 0.21J |
| | 21-30 | 3.5J | 0.38J |
| 07 | 0-10 | 82.8J | 1.2J |
| | 11-20 | 42.3J | 0.63 |
| | 21-30 | 4.6 | 0.31J |

Based on a review of DL and SP analytical data, Ni was not detected above the Site cleanup level. Several samples had concentrations of Be above the TAGM value of 0.16 mg/kg. However, Be concentrations in New York soils are reported to range between 0 to 7 mg/kg^{1, 2}. The Be soil results are interpreted to be within the anticipated range in soils for New York State.

¹ Schacklette, H.T., and J.G. Boerngen. 1984. *Elemental Concentrations in Soils and Other Surficial Materials of the Conterminous United States*. US Geological Survey. Pub. 1270.

² Dragun, J. and A. Chiasson. 1991. *Elements in North American Soils*. Hazardous Materials Control Resources Institute. Greenbelt, Maryland.

4.0 ADDITIONAL INVESTIGATIONS

In addition to the systematic characterization of soils beneath the 140 Building, an investigation of the soils was implemented concurrently to identify and delineate contaminants associated with the LPHs. That investigation was implemented in accordance with the *Systematic Subsurface Soil Sampling and Analysis Plan Historic Leach Pools, September 2004, Revision 1: October 2004* (LPH Plan). The purpose of the LPH investigation was to identify and delineate contaminants, if any, associated with suspected LPHs.

There were 14 LPHs investigated under the LPH Plan, 3 of which were located beneath the 140 Building, 2 in SU06 (LPH20 and LPH21), and 1 in SU07 (LPH34). All three LPHs are shown on **Figure 3** and the soil boring sample results are in **Table 3**.

4.1 LPH20

LPH20, soil boring 04, had contaminants above the Site cleanup level for Ni at 1 ft bgs (1,105 J mg/kg). The samples at 1 to 2 ft bgs from three soil borings (01, 03 and 05) north of soil boring 04 in LPH20 indicated Ni concentrations below the Site cleanup level.

The Ni result above the Site cleanup level indicates the presence of contaminants in shallow soils (fill) beneath the concrete slab. The Ni result in the fill does not indicate the potential presence of contaminants to undisturbed subsurface soils from LPH20.

LPH20 did not have radiological and VOC contaminants above Site cleanup levels.

4.2 LPH21

LPH21, soil boring 01, had contaminants above the Site cleanup levels for Th-232, U-234, U-238, TCE and PCE from 16 to 19 ft bgs (estimated bottom of the LPH). There were no detected contaminants above the Site cleanup levels below 20 feet bgs. LPH21, soil boring 05, had contaminants above the Site cleanup levels for U-238 at 10 ft bgs. The isotopic ratios of U-234 to U-238 (soil boring 1 at 16 and 30 ft bgs and soil borings 3 and 4 at 30 ft bgs) indicate that the radiological contaminants associated with LPH21 are from enriched uranium.

LPH21 did not have Ni contaminants above Site cleanup levels.

4.3 LPH34

LPH34 did not have contaminants above the Site cleanup levels.

5.0 CONCLUSIONS

SU06, soil boring 007, at depths of 17, 27 and 30 ft bgs, indicated concentrations of U-234 greater than concentrations of U-238. Evaluation of the samples in SU07 indicated three soil

borings (014, 031 and 032) immediately below the bottom of the concrete slab with disturbed material (fill) containing U-238 (25 to 33 pCi/g). Evaluation of the samples in SU06 and SU07 indicates that the values are below the radionuclide Site cleanup levels.

Direct comparison of the analytical results from SU06 and SU07 for VOCs and Ni to Site cleanup levels indicates that there were no contaminants above the Site cleanup levels. Several locations had Be in excess of the TAGM values but are within the reported range in soils for New York State.

Sampling conducted during the LPH investigation indicated that residual contaminants above Site cleanup levels are present at LPH20 and LPH21. The Ni result in LPH20 indicates the potential for contaminants in shallow disturbed soils (fill) at other locations beneath the concrete slab. The sample results above the Site cleanup levels at LPH21 are an indication of contaminants to soils at 10 ft bgs. In addition, the isotopic ratios of U-234 to U-238 (soil boring 1 at 16 and 30 ft bgs and soil borings 3 and 4 at 30 ft bgs) indicate that radiological contaminants are characteristic of enriched uranium. The results of the LPH investigation are detailed in the *Systematic Subsurface Sampling and Analysis Report, Historic Leach Pools*.

Based on the MARSSIM evaluation for radionuclides and the comparison of analytical results for VOCs and Ni to Site cleanup levels, the soils within the boundaries of SU06 and SU07 meet the requirements to be released for unrestricted use with the exception of areas near LPH20 and LPH21.

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 06 | 001 | 28336 | 1.0 | 0.61 | | 10.54 J | | | <100 | |
| 06 | 001 | 28337 | 2.0 | 0.54 | | 3.48 J | | | | |
| 06 | 001 | 28338 | 3.0 | 0.22 J | | 1.69 | | | <100 | |
| 06 | 001 | 28342 | 4.0 | 0.38 | 1.08 | 0.77 | 0.0025 U | 0.0025 U | 2.1 J | 0.13 J |
| 06 | 001 | 28352 | 6.0 | 0.64 | | 0.96 J | | | | |
| 06 | 001 | 28353 | 7.0 | 0.49 J | | 2.96 | | | <100 | |
| 06 | 001 | 28354 | 9.0 | 0.39 | | 1.63 J | | | <100 | |
| 06 | 001 | 28355 | 10.0 | 0.35 | | 1.83 J | | | | |
| 06 | 001 | 28356 | 11.0 | 0.40 J | | 2.07 | | | <100 | |
| 06 | 001 | 28357 | 12.0 | 0.35 | | 1.43 J | | | | |
| 06 | 001 | 28358 | 13.0 | 0.34 | | 1.15 J | | | <100 | |
| 06 | 001 | 28359 | 14.0 | 0.191 | 0.187 | 0.223 | 0.0025 U | 0.0025 U | 2.8 J | 0.14 J |
| 06 | 001 | 28365 | 16.0 | 0.34 J | | 0.39 | | | | |
| 06 | 001 | 28366 | 17.0 | 0.07 | | 1.17 J | | | <100 | |
| 06 | 001 | 28367 | 19.0 | 0.17 | | 1.10 J | | | <100 | |
| 06 | 001 | 28368 | 20.0 | 0.18 J | | 1.73 | | | | |
| 06 | 001 | 28369 | 21.0 | 0.75 | | 1.99 J | | | <100 | |
| 06 | 001 | 28370 | 23.0 | 0.22 | | 0.85 J | | | <100 | |
| 06 | 001 | 28371 | 24.0 | 0.160 | 0.200 | 0.130 | 0.0025 U | 0.0025 U | 1.1 J | 0.098 J |
| 06 | 001 | 28376 | 26.0 | 0.25 J | | 0.88 J | | | | |
| 06 | 001 | 28377 | 27.0 | 0.17 | | 0.96 J | | | <100 | |
| 06 | 001 | 28378 | 28.0 | 0.29 | | 0.93 J | | | | |
| 06 | 001 | 28379 | 29.0 | 0.26 J | | 1.92 | | | <100 | |
| 06 | 001 | 28384 | 30.0 | 0.120 | 0.127 | 0.134 | 0.0026 U | 0.0026 U | 3.1 J | 0.15 J |
| 06 | 002 | 27973 | 0.0 | 1.36 | | 8.65 | | | 41.6 J | |
| 06 | 002 | 27977 | 1.0 | 0.474 | 2.44 | 1.19 | 0.0025 U | 0.0025 U | 3.7 J | 0.26 J |
| 06 | 002 | 27983 | 3.0 | 0.52 | | 1.86 J | | | | |
| 06 | 002 | 27984 | 4.0 | 0.64 | | 1.62 J | | | <100 | |
| 06 | 002 | 27985 | 5.0 | 0.46 | | 0.88 J | | | | |
| 06 | 002 | 27986 | 6.0 | 0.74 | | 2.17 | | | <100 | |
| 06 | 002 | 27993 | 7.0 | 0.52 | | 0.43 | | | | |
| 06 | 002 | 27994 | 8.0 | 0.34 | | 1.13 J | | | <100 | |
| 06 | 002 | 27995 | 10.0 | 0.26 | | 1.14 | | | <100 | |
| 06 | 002 | 28008 | 11.0 | 0.417 | 0.317 | 0.329 | 0.0025 U | 0.0025 U | 1.7 J | 0.18 J |
| 06 | 002 | 28009 | 13.0 | 0.22 | | 0.96 J | | | | |
| 06 | 002 | 28010 | 14.0 | 0.32 | | 1.32 J | | | <100 | |
| 06 | 002 | 28012 | 15.0 | 0.21 | | 1.43 | | | | |
| 06 | 002 | 28013 | 16.0 | 0.26 | | 1.21 | | | <100 | |
| 06 | 002 | 28014 | 17.0 | 0.20 | | 0.86 | | | | |
| 06 | 002 | 28015 | 18.0 | 0.30 | | 1.38 J | | | <100 | |
| 06 | 002 | 28016 | 20.0 | 0.05 | | 1.03 J | | | <100 | |
| 06 | 002 | 28017 | 21.0 | 0.141 | 0.184 | 0.206 | 0.0026 U | 0.0026 U | 1.3 J | 0.19 J |
| 06 | 002 | 28023 | 23.0 | 0.25 | | 0.53 J | | | | |
| 06 | 002 | 28026 | 24.0 | 0.19 | | 0.77 J | | | <100 | |
| 06 | 002 | 28027 | 25.0 | 0.25 | | 1.06 J | | | | |
| 06 | 002 | 28030 | 26.0 | 0.31 | | 1.04 | | | <100 | |
| 06 | 002 | 28031 | 27.0 | 0.21 | | 0.51 J | | | | |
| 06 | 002 | 28038 | 28.0 | NS | | NS | | | <100 | |
| 06 | 002 | 28039 | 29.0 | 0.23 | | 0.52 UJ | | | | |
| 06 | 002 | 28040 | 30.0 | 0.151 | 0.088 J | 0.167 | 0.0026 U | 0.0026 U | 2.3 J | 0.21 J |
| 06 | 003 | 27406 | 0.0 | NS | | NS | | | 326 | |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 06 | 003 | 27407 | 2.0 | 0.74 | | 1.23 UJ | | | <100 | |
| 06 | 003 | 27415 | 3.0 | 0.78 | | 1.66 J | | | | |
| 06 | 003 | 27416 | 4.0 | 0.53 | | 1.18 J | | | <100 | |
| 06 | 003 | 27417 | 5.0 | 0.54 | | 3.60 J | | | | |
| 06 | 003 | 27418 | 6.0 | 0.65 | | 1.53 J | | | <100 | |
| 06 | 003 | 27421 | 7.0 | 1.08 | 0.75 | 0.76 | 0.0030 U | 0.0030 U | 6.7 | 0.50 J |
| 06 | 003 | 27422 | 10.0 | 0.24 | | 0.45 J | | | <100 | |
| 06 | 003 | 27423 | 11.0 | 0.31 | | 0.87 J | | | | |
| 06 | 003 | 27424 | 12.0 | 0.28 J | | 0.60 J | | | <100 | |
| 06 | 003 | 27431 | 14.0 | 0.25 | | 1.37 | | | <100 | |
| 06 | 003 | 27432 | 15.0 | 0.23 | | 0.88 J | | | | |
| 06 | 003 | 27433 | 16.0 | 0.26 J | | 0.37 | | | <100 | |
| 06 | 003 | 27436 | 17.0 | 0.187 | 0.204 | 0.173 | 0.0025 U | 0.0025 U | 1.6 J | 0.13 J |
| 06 | 003 | 27440 | 20.0 | 0.29 | | 0.82 J | | | <100 | |
| 06 | 003 | 27441 | 21.0 | 0.03 | | 0.38 | | | | |
| 06 | 003 | 27442 | 22.0 | 0.24 J | | 1.55 | | | <100 | |
| 06 | 003 | 27450 | 24.0 | 0.24 | | 0.55 J | | | <100 | |
| 06 | 003 | 27451 | 26.0 | 0.06 | | 0.76 J | | | <100 | |
| 06 | 003 | 27453 | 27.0 | 0.257 | 0.266 | 0.180 | 0.0026 U | 0.0026 U | 2.9 J | 0.21 J |
| 06 | 003 | 27454 | 29.0 | 0.33 J | | 1.69 | | | | |
| 06 | 003 | 27457 | 30.0 | 0.198 | 0.140 | 0.197 | 0.0026 U | 0.0026 U | 3.5 J | 0.32 J |
| 06 | 004 | 27310 | 0.0 | 1.03 | | 2.48 J | | | | |
| 06 | 004 | 27311 | 1.0 | 1.45 | | 3.75 J | | | <100 | |
| 06 | 004 | 27312 | 2.0 | 0.63 | | 4.34 J | | | | |
| 06 | 004 | 27313 | 3.0 | 0.55 | | 0.50 UJ | | | <100 | |
| 06 | 004 | 27318 | 4.0 | 0.65 | 0.69 | 0.410 | 0.0025 U | 0.0025 U | 4.8 | 0.31 J |
| 06 | 004 | 27322 | 6.0 | 0.47 | | 1.27 J | | | | |
| 06 | 004 | 27323 | 7.0 | 0.43 | | 1.05 J | | | <100 | |
| 06 | 004 | 27324 | 9.0 | 0.05 | | 1.05 J | | | <100 | |
| 06 | 004 | 27330 | 11.0 | 0.12 | | 2.28 J | | | <100 | |
| 06 | 004 | 27333 | 12.0 | 0.30 | | 1.55 J | | | | |
| 06 | 004 | 27334 | 13.0 | 0.05 | | 2.49 J | | | <100 | |
| 06 | 004 | 27335 | 14.0 | 0.261 | 0.211 | 0.213 | 0.0025 U | 0.0025 U | 1.4 J | 0.19 J |
| 06 | 004 | 27339 | 16.0 | 0.23 | | 1.60 J | | | | |
| 06 | 004 | 27340 | 17.0 | 0.26 | | 1.64 J | | | <100 | |
| 06 | 004 | 27347 | 19.0 | 0.24 | | 3.04 J | | | <100 | |
| 06 | 004 | 27358 | 20.0 | 0.16 | | 0.69 J | | | | |
| 06 | 004 | 27359 | 21.0 | 0.30 | | 0.65 J | | | <100 | |
| 06 | 004 | 27360 | 23.0 | 0.37 | | 1.11 J | | | <100 | |
| 06 | 004 | 27365 | 24.0 | 0.187 | 0.185 | 0.177 | 0.0025 U | 0.0025 U | 3.3 J | 0.20 J |
| 06 | 004 | 27373 | 26.0 | 0.25 | | 1.82 J | | | | |
| 06 | 004 | 27374 | 27.0 | 0.26 | | 0.70 J | | | <100 | |
| 06 | 004 | 27375 | 28.0 | 0.31 | | 1.71 J | | | | |
| 06 | 004 | 27376 | 29.0 | 0.04 | | 1.33 J | | | <100 | |
| 06 | 004 | 27379 | 30.0 | 0.121 | 0.138 | 0.123 J | 0.0025 U | 0.0025 U | 2.9 J | 0.38 J |
| 06 | 005 | 26850 | 0.0 | 0.96 | | 13.10 | | | | |
| 06 | 005 | 26851 | 1.0 | 0.83 | 2.37 | 1.87 | 0.0027 U | 0.0024 J | 6.6 | 0.18 J |
| 06 | 005 | 26854 | 3.0 | 0.81 J | | 0.87 | | | | |
| 06 | 005 | 26855 | 4.0 | 0.62 | | 2.46 J | | | <100 | |
| 06 | 005 | 26865 | 5.0 | 0.78 | | 2.45 | | | | |
| 06 | 005 | 26866 | 6.0 | 1.00 J | | 1.64 J | | | <100 | |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 06 | 005 | 26867 | 7.0 | 0.34 | | 1.31 J | | | | |
| 06 | 005 | 26868 | 8.0 | 0.29 J | | 0.47 J | | | <100 | |
| 06 | 005 | 26869 | 9.0 | 0.24 | | 0.32 UJ | | | | |
| 06 | 005 | 26870 | 10.0 | 0.47 | | 1.09 J | | | <100 | |
| 06 | 005 | 26873 | 11.0 | 0.268 | 0.241 | 0.295 | 0.0025 U | 0.0025 U | 3.1 J | 0.20 J |
| 06 | 005 | 26874 | 13.0 | 0.37 J | | 1.46 | | | | |
| 06 | 005 | 26875 | 14.0 | 0.45 | | 1.11 J | | | <100 | |
| 06 | 005 | 26887 | 16.0 | 0.23 | | 0.53 J | | | <100 | |
| 06 | 005 | 26888 | 18.0 | 0.22 J | | 1.69 | | | <100 | |
| 06 | 005 | 26889 | 19.0 | 0.29 | | 0.77 J | | | <100 | |
| 06 | 005 | 26890 | 20.0 | 0.24 | | 0.80 J | | | <100 | |
| 06 | 005 | 26899 | 21.0 | 0.235 | 0.220 | 0.227 | 0.0025 U | 0.0025 U | 1.9 J | 0.17 J |
| 06 | 005 | 26900 | 23.0 | 0.32 | | 0.89 J | | | | |
| 06 | 005 | 26907 | 28.0 | 0.25 J | | 0.71 J | | | <100 | |
| 06 | 005 | 26908 | 29.0 | 0.25 | | 1.13 J | | | | |
| 06 | 005 | 26909 | 30.0 | 0.183 | 0.154 | 0.222 | 0.0025 U | 0.0025 U | 3.0 J | 0.25 J |
| 06 | 006 | 28396 | 0.0 | 0.68 | | 3.20 J | | | | |
| 06 | 006 | 28398 | 1.0 | 0.58 | 0.50 | 0.61 | 0.0025 U | 0.0025 U | 9.8 | 0.91 |
| 06 | 006 | 28403 | 3.0 | 0.42 | | 2.07 | | | | |
| 06 | 006 | 28404 | 4.0 | 0.83 | | 1.53 J | | | <100 | |
| 06 | 006 | 28407 | 5.0 | 0.47 | | 1.68 | | | | |
| 06 | 006 | 28408 | 6.0 | 0.16 | | 2.12 | | | <100 | |
| 06 | 006 | 28409 | 7.0 | 0.50 | | 3.45 J | | | | |
| 06 | 006 | 28410 | 8.0 | 0.36 | | 0.62 | | | <100 | |
| 06 | 006 | 28412 | 10.0 | 0.32 | | 2.50 J | | | <100 | |
| 06 | 006 | 28413 | 11.0 | 0.249 | 0.233 | 0.244 | 0.0025 U | 0.0025 U | 1.3 J | 0.10 J |
| 06 | 006 | 28414 | 13.0 | 0.37 | | 0.73 | | | | |
| 06 | 006 | 28415 | 14.0 | 0.29 | | 1.04 J | | | <100 | |
| 06 | 006 | 28416 | 15.0 | 0.19 | | 0.41 | | | | |
| 06 | 006 | 28417 | 16.0 | 0.05 | | 0.63 | | | <100 | |
| 06 | 006 | 28418 | 18.0 | 0.28 | | 0.88 J | | | <100 | |
| 06 | 006 | 28419 | 20.0 | 0.24 | | 0.42 | | | <100 | |
| 06 | 006 | 28420 | 21.0 | 0.223 | 0.180 | 0.170 | 0.0025 U | 0.0025 U | 1.5 J | 0.11 J |
| 06 | 006 | 28421 | 24.0 | 0.33 | | 1.18 | | | <100 | |
| 06 | 006 | 28422 | 25.0 | 0.03 | | 0.55 J | | | | |
| 06 | 006 | 28423 | 26.0 | 0.04 | | 2.02 | | | <100 | |
| 06 | 006 | 28424 | 27.0 | 0.21 | | 0.38 | | | | |
| 06 | 006 | 28425 | 28.0 | 0.30 | | 1.92 J | | | <100 | |
| 06 | 006 | 28426 | 29.0 | 0.04 | | 0.81 | | | | |
| 06 | 006 | 28427 | 30.0 | 0.17 U | 0.148 | 0.113 | 0.0025 U | 0.0025 U | 2.4 J | 0.17 J |
| 06 | 007 | 28086 | 0.0 | 0.54 | | 3.90 | | | <100 | |
| 06 | 007 | 28087 | 1.0 | 1.04 | | 6.25 | | | | |
| 06 | 007 | 28088 | 2.0 | 0.80 | | 2.26 J | | | <100 | |
| 06 | 007 | 28098 | 3.0 | 0.34 | | 1.00 J | | | | |
| 06 | 007 | 28097 | 4.0 | 0.39 | | 1.23 J | | | <100 | |
| 06 | 007 | 28103 | 5.0 | 0.67 | | 2.04 J | | | | |
| 06 | 007 | 28104 | 6.0 | 0.83 | | 1.84 | | | <100 | |
| 06 | 007 | 28107 | 7.0 | 0.42 | 0.42 | 0.380 | 0.00071 J | 0.0025 U | 1.7 J | 0.15 J |
| 06 | 007 | 28108 | 10.0 | 0.28 | | 0.70 J | | | <100 | |
| 06 | 007 | 28120 | 11.0 | 0.26 | | 1.03 J | | | | |
| 06 | 007 | 28121 | 12.0 | 0.32 | | 3.65 | | | <100 | |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Ber (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|--------------------|
| 06 | 007 | 28128 | 13.0 | 0.22 | | 8.20 | | | | |
| 06 | 007 | 28129 | 14.0 | 0.33 | | 13.56 | | | <100 | |
| 06 | 007 | 28130 | 15.0 | 0.33 | | 16.59 | | | | |
| 06 | 007 | 28131 | 16.0 | 0.39 | | 17.29 | | | <100 | |
| 06 | 007 | 28144 | 17.0 | 0.281 | 23.8 | 11.2 | 0.0025 U | 0.0025 U | 1.9 J | 0.11 J |
| 06 | 007 | 28143 | 19.0 | 0.39 | | 15.88 | | | | |
| 06 | 007 | 28145 | 20.0 | 0.50 | | 17.07 | | | <100 | |
| 06 | 007 | 28148 | 21.0 | 0.37 | | 12.72 | | | | |
| 06 | 007 | 28149 | 22.0 | 0.54 | | 9.51 | | | <100 | |
| 06 | 007 | 28157 | 23.0 | 0.30 | | 10.10 | | | | |
| 06 | 007 | 28158 | 24.0 | 0.26 | | 16.02 | | | <100 | |
| 06 | 007 | 28159 | 25.0 | 0.37 | | 16.53 | | | | |
| 06 | 007 | 28160 | 26.0 | 0.45 | | 30.19 | | | <100 | |
| 06 | 007 | 28171 | 27.0 | 0.239 | 29.0 | 15.0 | 0.0025 U | 0.0025 U | 2.8 J | 0.20 J |
| 06 | 007 | 28172 | 29.0 | 0.12 | | 14.68 | | | | |
| 06 | 007 | 28173 | 30.0 | 0.44 | 20.7 | 11.5 | 0.0025 U | 0.0025 U | 2.2 J | 0.15 J |
| 06 | 008 | 27868 | 1.0 | 0.64 | | 6.14 | | | <100 | |
| 06 | 008 | 27869 | 2.0 | 0.81 | | 5.50 | | | | |
| 06 | 008 | 27870 | 3.0 | 0.50 | | 2.18 | | | <100 | |
| 06 | 008 | 27882 | 4.0 | 0.356 | 1.91 | 0.83 | 0.0025 U | 0.00061 J | 2.8 J | 0.22 J |
| 06 | 008 | 27886 | 6.0 | 0.67 | | 1.74 J | | | | |
| 06 | 008 | 27887 | 7.0 | 0.42 | | 0.74 J | | | <100 | |
| 06 | 008 | 27888 | 9.0 | 0.27 | | 0.37 J | | | <100 | |
| 06 | 008 | 27897 | 10.0 | 0.28 | | 1.67 | | | | |
| 06 | 008 | 27898 | 11.0 | 0.40 | | 1.32 J | | | <100 | |
| 06 | 008 | 27899 | 12.0 | 0.30 J | | 0.96 | | | | |
| 06 | 008 | 27900 | 13.0 | 0.32 | | 0.39 J | | | <100 | |
| 06 | 008 | 27911 | 14.0 | 0.147 | 0.236 | 0.175 | 0.0025 U | 0.0025 U | 1.5 J | 0.17 J |
| 06 | 008 | 27915 | 16.0 | 0.26 | | 1.42 | | | | |
| 06 | 008 | 27916 | 17.0 | 0.25 | | 0.99 J | | | <100 | |
| 06 | 008 | 27917 | 19.0 | 0.25 | | 0.44 J | | | <100 | |
| 06 | 008 | 27918 | 21.0 | 0.06 | | 2.46 | | | <100 | |
| 06 | 008 | 27931 | 24.0 | 0.259 | 0.205 | 0.170 | 0.0026 U | 0.0026 U | 1.8 J | 0.19 J |
| 06 | 008 | 27934 | 26.0 | 0.23 | | 0.46 | | | | |
| 06 | 008 | 27935 | 27.0 | 0.26 | | 0.78 J | | | <100 | |
| 06 | 008 | 27936 | 28.0 | 0.21 | | 1.06 | | | | |
| 06 | 008 | 27937 | 29.0 | 0.29 | | 1.95 J | | | <100 | |
| 06 | 008 | 27938 | 30.0 | 0.139 | 0.108 | 0.183 | 0.0026 U | 0.0026 U | 1.5 J | 0.17 J |
| 06 | 009 | 27681 | 0.0 | 0.74 | | 17.67 | | | 92.4 J | |
| 06 | 009 | 27682 | 1.0 | 0.97 | 7.40 | 6.06 | 0.0028 U | 0.0071 | 330 | 0.41 J |
| 06 | 009 | 27683 | 3.0 | 0.33 | | 2.87 | | | | |
| 06 | 009 | 27684 | 4.0 | 0.44 | | 0.69 | | | <100 | |
| 06 | 009 | 27691 | 5.0 | 0.65 | | 3.00 | | | | |
| 06 | 009 | 27692 | 6.0 | 0.53 | | 1.89 | | | <100 | |
| 06 | 009 | 27693 | 7.0 | 0.91 | | 0.94 | | | | |
| 06 | 009 | 27694 | 8.0 | 0.27 | | 0.77 J | | | <100 | |
| 06 | 009 | 27704 | 10.0 | 0.25 | | 1.07 J | | | <100 | |
| 06 | 009 | 27705 | 11.0 | 0.269 | 0.311 | 0.245 | 0.0025 U | 0.0025 U | 1.8 J | 0.18 J |
| 06 | 009 | 27706 | 13.0 | 0.24 | | 0.64 J | | | | |
| 06 | 009 | 27707 | 14.0 | 0.26 | | 1.29 J | | | <100 | |
| 06 | 009 | 27708 | 15.0 | 0.28 | | 1.97 | | | | |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 06 | 009 | 27709 | 16.0 | 0.28 | | 0.64 | | | <100 | |
| 06 | 009 | 27710 | 17.0 | 0.23 | | 1.15 | | | | |
| 06 | 009 | 27711 | 18.0 | 0.29 | | 0.61 J | | | <100 | |
| 06 | 009 | 27712 | 19.0 | 0.23 | | 0.80 J | | | | |
| 06 | 009 | 27713 | 20.0 | 0.24 | | 1.02 J | | | <100 | |
| 06 | 009 | 27720 | 21.0 | 0.249 | 0.174 | 0.179 | 0.0026 U | 0.0026 U | 0.98 J | 0.13 J |
| 06 | 009 | 27721 | 23.0 | 0.25 | | 1.24 J | | | | |
| 06 | 009 | 27732 | 24.0 | 0.26 | | 1.24 | | | <100 | |
| 06 | 009 | 27733 | 25.0 | 0.34 | | 0.95 J | | | | |
| 06 | 009 | 27739 | 26.0 | 0.22 | | 0.95 J | | | <100 | |
| 06 | 009 | 27740 | 27.0 | 0.27 | | 1.98 | | | | |
| 06 | 009 | 27741 | 28.0 | NS | | NS | | | <100 | |
| 06 | 009 | 27742 | 29.0 | 0.22 | | 1.21 | | | | |
| 06 | 009 | 27743 | 30.0 | 0.149 | 0.149 | 0.128 | 0.0025 U | 0.0025 U | 1.7 J | 0.13 J |
| 06 | 010 | 27583 | 0.0 | 1.20 J | | 5.87 | | | <100 | |
| 06 | 010 | 27584 | 1.0 | 1.25 J | | 2.00 | | | | |
| 06 | 010 | 27585 | 2.0 | 0.81 J | | 2.04 | | | <100 | |
| 06 | 010 | 27586 | 3.0 | 0.60 J | | 0.65 | | | | |
| 06 | 010 | 27587 | 4.0 | 0.45 J | | 0.60 | | | <100 | |
| 06 | 010 | 27591 | 5.0 | 0.95 J | | 1.28 J | | | | |
| 06 | 010 | 27592 | 6.0 | 0.78 J | | 1.57 J | | | <100 | |
| 06 | 010 | 27593 | 7.0 | 0.220 | 0.294 | 0.272 | 0.0026 U | 0.0026 U | 1.4 J | 0.14 J |
| 06 | 010 | 27594 | 10.0 | 0.35 J | | 1.59 | | | <100 | |
| 06 | 010 | 27596 | 11.0 | 0.04 UJ | | 1.14 | | | | |
| 06 | 010 | 27597 | 12.0 | 0.38 J | | 0.82 J | | | <100 | |
| 06 | 010 | 27598 | 13.0 | 0.29 J | | 0.59 | | | | |
| 06 | 010 | 27599 | 14.0 | 0.36 J | | 1.18 J | | | <100 | |
| 06 | 010 | 27607 | 15.0 | 0.26 J | | 0.19 | | | | |
| 06 | 010 | 27608 | 16.0 | 0.20 J | | 0.40 | | | <100 | |
| 06 | 010 | 27609 | 17.0 | 0.105 | 0.134 | 0.133 | 0.0026 U | 0.0026 U | 0.89 J | 0.092 J |
| 06 | 010 | 27610 | 20.0 | 0.23 J | | 1.29 | | | <100 | |
| 06 | 010 | 27611 | 21.0 | 0.25 J | | 0.89 J | | | | |
| 06 | 010 | 27612 | 22.0 | 0.31 J | | 2.27 | | | <100 | |
| 06 | 010 | 27622 | 23.0 | 0.29 J | | 2.32 J | | | | |
| 06 | 010 | 27623 | 24.0 | 0.35 J | | 1.08 | | | <100 | |
| 06 | 010 | 27633 | 25.0 | 0.18 | | 0.77 J | | | | |
| 06 | 010 | 27634 | 26.0 | 0.26 | | 1.54 | | | <100 | |
| 06 | 010 | 27635 | 27.0 | 0.181 | 0.159 | 0.127 | 0.0026 U | 0.0026 UJ | 1.3 J | 0.16 J |
| 06 | 010 | 27636 | 29.0 | 0.05 | | 1.06 J | | | | |
| 06 | 010 | 27642 | 30.0 | 0.148 | 0.167 | 0.145 | 0.0026 U | 0.0026 UJ | 1.1 J | 0.17 J |
| 06 | 012 | 28202 | 0.0 | 0.95 | | 6.96 J | | | | |
| 06 | 012 | 28203 | 1.0 | 0.75 | | 2.49 J | | | <100 | |
| 06 | 012 | 28204 | 3.0 | 0.85 J | | 6.09 | | | <100 | |
| 06 | 012 | 28205 | 4.0 | 0.79 | 3.19 | 2.33 | 0.0078 | 0.024 | 5.6 | 0.20 J |
| 06 | 012 | 28206 | 6.0 | 0.63 | | 1.65 J | | | | |
| 06 | 012 | 28207 | 7.0 | 0.90 | | 2.35 J | | | <100 | |
| 06 | 012 | 28217 | 8.0 | 0.42 J | | 2.57 | | | | |
| 06 | 012 | 28218 | 9.0 | 0.23 | | 0.38 UJ | | | <100 | |
| 06 | 012 | 28219 | 10.0 | 0.38 J | | 2.89 | | | | |
| 06 | 012 | 28220 | 11.0 | 0.30 | | 1.31 J | | | <100 | |
| 06 | 012 | 28221 | 12.0 | 0.28 J | | 1.21 J | | | | |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 06 | 012 | 28222 | 13.0 | 0.26 | | 1.17 J | | | <100 | |
| 06 | 012 | 28223 | 14.0 | 0.172 | 0.208 | 0.164 | 0.0025 U | 0.0025 U | 1.8 J | 0.12 J |
| 06 | 012 | 28233 | 16.0 | 0.24 | | 1.38 J | | | | |
| 06 | 012 | 28234 | 17.0 | 0.23 | | 0.43 | | | <100 | |
| 06 | 012 | 28235 | 18.0 | 0.20 | | 1.38 | | | | |
| 06 | 012 | 28236 | 19.0 | 0.27 | | 0.48 | | | <100 | |
| 06 | 012 | 28237 | 20.0 | 0.35 | | 1.29 | | | | |
| 06 | 012 | 28238 | 21.0 | 0.09 | | 1.88 J | | | <100 | |
| 06 | 012 | 28256 | 23.0 | 0.18 | | 1.24 | | | <100 | |
| 06 | 012 | 28257 | 24.0 | 0.178 | 0.301 | 0.163 | 0.0025 U | 0.0025 U | 0.99 J | 0.058 J |
| 06 | 012 | 28264 | 26.0 | 0.33 | | 0.86 J | | | | |
| 06 | 012 | 28265 | 27.0 | 0.23 | | 1.84 | | | <100 | |
| 06 | 012 | 28271 | 28.0 | 0.28 | | 1.70 | | | | |
| 06 | 012 | 28272 | 29.0 | 0.18 | | 0.79 J | | | <100 | |
| 06 | 012 | 28273 | 30.0 | 0.089 J | 0.185 | 0.117 | 0.0025 U | 0.0025 U | 1.9 J | 0.12 J |
| 06 | 013 | 28277 | 0.0 | 0.65 | | 1.13 J | | | | |
| 06 | 013 | 28278 | 1.0 | 0.64 | 5.19 | 1.93 | 0.0077 | 0.030 | 7.6 J | 0.34 J |
| 06 | 013 | 28292 | 3.0 | 0.81 | | 2.81 J | | | | |
| 06 | 013 | 28293 | 4.0 | 0.59 | | 1.37 J | | | <100 | |
| 06 | 013 | 28294 | 5.0 | 0.55 | | 2.11 | | | | |
| 06 | 013 | 28295 | 6.0 | 0.61 | | 1.23 J | | | <100 | |
| 06 | 013 | 28296 | 7.0 | 0.48 | | 2.10 | | | | |
| 06 | 013 | 28297 | 8.0 | 0.31 | | 0.46 J | | | <100 | |
| 06 | 013 | 28298 | 10.0 | 0.35 | | 0.38 | | | <100 | |
| 06 | 013 | 28299 | 11.0 | 0.210 | 0.224 | 0.215 | 0.0025 U | 0.0025 U | 1.2 J | 0.071 J |
| 06 | 013 | 28301 | 13.0 | 0.27 | | 0.38 | | | | |
| 06 | 013 | 28302 | 14.0 | 0.31 | | 1.45 J | | | <100 | |
| 06 | 013 | 28303 | 15.0 | 0.33 | | 0.73 J | | | | |
| 06 | 013 | 28304 | 16.0 | 0.29 | | 0.96 J | | | <100 | |
| 06 | 013 | 28307 | 17.0 | 0.15 | | 0.60 | | | | |
| 06 | 013 | 28308 | 18.0 | 0.06 | | 2.18 | | | <100 | |
| 06 | 013 | 28309 | 20.0 | 0.31 | | 0.56 | | | <100 | |
| 06 | 013 | 28318 | 21.0 | 0.302 | 0.194 | 0.138 | 0.0025 U | 0.0025 U | 2.8 J | 0.086 J |
| 06 | 013 | 28319 | 23.0 | 0.34 | | 0.56 J | | | | |
| 06 | 013 | 28320 | 24.0 | 0.32 J | | 0.46 | | | <100 | |
| 06 | 013 | 28321 | 25.0 | 0.26 J | | 1.45 J | | | | |
| 06 | 013 | 28322 | 26.0 | 0.27 | | 2.40 J | | | <100 | |
| 06 | 013 | 28323 | 27.0 | 0.30 | | 1.58 J | | | | |
| 06 | 013 | 28324 | 28.0 | 0.23 J | | 0.73 J | | | <100 | |
| 06 | 013 | 28325 | 29.0 | 0.45 | | 1.84 J | | | | |
| 06 | 013 | 28326 | 30.0 | 0.240 | 0.175 | 0.166 | 0.0025 U | 0.0025 U | 3.2 J | 0.087 J |
| 06 | 014 | 27473 | 0.0 | 0.99 J | | 40.65 | | | 165 | |
| 06 | 014 | 27477 | 1.0 | 1.09 | | 3.27 | | | | |
| 06 | 014 | 27478 | 2.0 | 0.74 | | 0.78 | | | <100 | |
| 06 | 014 | 27488 | 3.0 | 0.44 J | | 1.68 | | | | |
| 06 | 014 | 27489 | 4.0 | 0.76 J | | 2.43 | | | <100 | |
| 06 | 014 | 27500 | 5.0 | 0.86 J | | 1.22 J | | | | |
| 06 | 014 | 27501 | 6.0 | 0.98 J | | 2.88 | | | <100 | |
| 06 | 014 | 27502 | 7.0 | 0.286 | 0.322 | 0.231 | 0.0025 U | 0.0025 U | 1.3 J | 0.14 J |
| 06 | 014 | 27503 | 10.0 | 0.32 J | | 1.39 J | | | <100 | |
| 06 | 014 | 27512 | 11.0 | 0.36 J | | 0.58 J | | | <100 | |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 06 | 014 | 27513 | 12.0 | 0.36 J | | 0.94 J | | | | |
| 06 | 014 | 27514 | 14.0 | 0.38 J | | 1.05 J | | | <100 | |
| 06 | 014 | 27521 | 15.0 | 0.40 J | | 0.69 | | | | |
| 06 | 014 | 27522 | 16.0 | 0.25 J | | 0.41 | | | <100 | |
| 06 | 014 | 27528 | 17.0 | 0.172 | 0.139 | 0.147 | 0.0025 U | 0.0025 U | 1.0 J | 0.11 J |
| 06 | 014 | 27529 | 19.0 | 0.17 J | | 0.42 J | | | | |
| 06 | 014 | 27530 | 20.0 | 0.24 J | | 1.32 | | | <100 | |
| 06 | 014 | 27531 | 21.0 | 0.29 J | | 1.23 | | | | |
| 06 | 014 | 27532 | 22.0 | 0.35 J | | 0.94 J | | | <100 | |
| 06 | 014 | 27543 | 23.0 | 0.24 J | | 1.06 | | | | |
| 06 | 014 | 27544 | 24.0 | 0.32 J | | 0.51 | | | <100 | |
| 06 | 014 | 27549 | 25.0 | 0.25 J | | 0.86 J | | | | |
| 06 | 014 | 27550 | 26.0 | 0.23 J | | 0.63 J | | | <100 | |
| 06 | 014 | 27555 | 27.0 | 0.168 | 0.156 | 0.167 | 0.0025 U | 0.0025 U | 1.9 J | 0.24 J |
| 06 | 014 | 27556 | 29.0 | 0.19 J | | 0.58 | | | | |
| 06 | 014 | 27561 | 30.0 | 0.262 | 0.122 | 0.141 | 0.0026 U | 0.0026 U | 1.4 J | 0.14 J |
| 06 | 015 | 27763 | 0.0 | 0.80 | | 15.24 | | | | |
| 06 | 015 | 27764 | 1.0 | 1.03 | | 13.74 | | | <100 | |
| 06 | 015 | 27765 | 3.0 | 0.95 | | 5.39 | | | <100 | |
| 06 | 015 | 27776 | 4.0 | 1.07 | 4.62 | 4.89 | 0.00054 J | 0.0018 J | 13.1 | 0.49 J |
| 06 | 015 | 27777 | 7.0 | 0.50 | | 0.78 | | | <100 | |
| 06 | 015 | 27778 | 9.0 | 0.28 | | 1.24 | | | <100 | |
| 06 | 015 | 27787 | 10.0 | 0.26 | | 1.22 J | | | | |
| 06 | 015 | 27788 | 11.0 | 0.25 | | 0.55 J | | | <100 | |
| 06 | 015 | 27789 | 12.0 | 0.42 | | 1.20 J | | | | |
| 06 | 015 | 27790 | 13.0 | 0.31 | | 0.87 J | | | <100 | |
| 06 | 015 | 27791 | 14.0 | 0.259 | 0.164 | 0.182 | 0.0025 U | 0.0025 U | 1.4 J | 0.11 J |
| 06 | 015 | 27798 | 16.0 | 0.34 | | 0.55 | | | | |
| 06 | 015 | 27799 | 17.0 | 0.10 | | 1.30 J | | | <100 | |
| 06 | 015 | 27800 | 18.0 | 0.16 | | 0.42 | | | | |
| 06 | 015 | 27801 | 19.0 | 0.23 | | 1.25 J | | | <100 | |
| 06 | 015 | 27802 | 20.0 | 0.25 | | 1.09 J | | | | |
| 06 | 015 | 27803 | 21.0 | 0.24 | | 1.12 | | | <100 | |
| 06 | 015 | 27814 | 22.0 | 0.34 | | 0.83 J | | | | |
| 06 | 015 | 27815 | 23.0 | 0.18 | | 1.01 J | | | <100 | |
| 06 | 015 | 27816 | 24.0 | 0.167 | 0.131 | 0.140 | 0.0026 U | 0.0026 U | 2.5 J | 0.19 J |
| 06 | 015 | 27826 | 26.0 | 0.32 | | 0.37 | | | | |
| 06 | 015 | 27827 | 27.0 | 0.04 | | 0.75 J | | | <100 | |
| 06 | 015 | 27828 | 28.0 | 0.21 | | 0.74 J | | | | |
| 06 | 015 | 27829 | 29.0 | 0.06 | | 0.65 J | | | <100 | |
| 06 | 015 | 27832 | 30.0 | 0.196 | 0.180 | 0.138 | 0.0025 U | 0.0025 U | 1.5 J | 0.12 J |
| 06 | 016 | 27059 | 0.0 | 0.55 | | 2.44 | | | | |
| 06 | 016 | 27060 | 1.0 | 0.72 | 5.76 | 5.42 | 0.0026 J | 0.018 J | 21.7 | 0.30 J |
| 06 | 016 | 27061 | 3.0 | 0.37 J | | 1.83 J | | | | |
| 06 | 016 | 27062 | 4.0 | 0.37 J | | 1.46 J | | | <100 | |
| 06 | 016 | 27063 | 5.0 | 0.31 J | | 1.44 J | | | | |
| 06 | 016 | 27064 | 6.0 | 0.86 | | 1.27 J | | | <100 | |
| 06 | 016 | 27065 | 7.0 | 0.41 | | 0.39 | | | | |
| 06 | 016 | 27066 | 8.0 | 0.30 | | 0.52 J | | | <100 | |
| 06 | 016 | 27067 | 9.0 | 0.47 | | 0.87 J | | | | |
| 06 | 016 | 27068 | 10.0 | 0.21 | | 1.80 | | | <100 | |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 06 | 016 | 27082 | 11.0 | 0.170 | 0.213 | 0.235 | 0.0025 U | 0.0025 U | 2.3 J | 0.21 J |
| 06 | 016 | 27083 | 13.0 | 0.34 | | 1.45 | | | | |
| 06 | 016 | 27084 | 14.0 | 0.29 | | 0.89 J | | | <100 | |
| 06 | 016 | 27085 | 15.0 | 0.27 | | 1.22 | | | | |
| 06 | 016 | 27086 | 16.0 | 0.33 | | 1.42 J | | | <100 | |
| 06 | 016 | 27087 | 17.0 | 0.23 J | | 0.53 J | | | | |
| 06 | 016 | 27088 | 18.0 | 0.33 | | 0.97 J | | | <100 | |
| 06 | 016 | 27092 | 19.0 | 0.04 | | 0.89 | | | | |
| 06 | 016 | 27093 | 20.0 | 0.23 | | 1.08 J | | | <100 | |
| 06 | 016 | 27094 | 21.0 | 0.328 | 0.322 | 0.329 | 0.0025 U | 0.0025 U | 0.92 J | 0.12 J |
| 06 | 016 | 27095 | 23.0 | 0.32 J | | 0.68 J | | | | |
| 06 | 016 | 27109 | 24.0 | 0.23 | | 0.33 | | | <100 | |
| 06 | 016 | 27110 | 25.0 | 0.31 | | 0.74 J | | | | |
| 06 | 016 | 27111 | 26.0 | 0.29 | | 0.76 J | | | <100 | |
| 06 | 016 | 27112 | 27.0 | 0.26 | | 0.68 | | | | |
| 06 | 016 | 27115 | 28.0 | 0.15 J | | 0.32 UJ | | | <100 | |
| 06 | 016 | 27116 | 29.0 | 0.19 J | | 0.41 J | | | | |
| 06 | 016 | 27117 | 30.0 | 0.225 | 0.128 | 0.145 | 0.0026 U | 0.0026 U | 1.8 J | 0.22 J |
| 07 | 004 | 29453 | 0.0 | 0.79 | | 5.00 | | | <100 | |
| 07 | 004 | 29454 | 1.0 | 0.386 | 0.53 | 0.47 | 0.0026 U | 0.0026 UJ | 13.6 | 0.47 J |
| 07 | 004 | 29455 | 3.0 | 0.42 | | 1.77 J | | | | |
| 07 | 004 | 29456 | 4.0 | 0.37 | | 1.43 | | | <100 | |
| 07 | 004 | 29457 | 5.0 | 0.42 | | 0.90 | | | | |
| 07 | 004 | 29458 | 6.0 | 1.32 | | 1.32 J | | | <100 | |
| 07 | 004 | 29459 | 7.0 | 0.54 | | 2.04 | | | | |
| 07 | 004 | 29460 | 8.0 | 0.91 | | 1.55 J | | | <100 | |
| 07 | 004 | 29461 | 9.0 | 1.32 | | 2.56 J | | | | |
| 07 | 004 | 29462 | 10.0 | 0.69 | | 1.77 J | | | <100 | |
| 07 | 004 | 29463 | 11.0 | 0.74 | 0.64 | 0.46 | 0.0026 U | 0.0026 UJ | 9.2 | 0.63 |
| 07 | 004 | 29466 | 13.0 | 0.23 | | 0.44 | | | | |
| 07 | 004 | 29467 | 14.0 | 0.32 | | 1.44 | | | <100 | |
| 07 | 004 | 29468 | 15.0 | 0.31 | | 1.85 | | | | |
| 07 | 004 | 29469 | 16.0 | 0.23 | | 0.86 J | | | <100 | |
| 07 | 004 | 29470 | 17.0 | 0.03 | | 1.35 J | | | | |
| 07 | 004 | 29471 | 18.0 | 0.20 | | 0.47 | | | <100 | |
| 07 | 004 | 29472 | 19.0 | 0.32 | | 0.53 J | | | | |
| 07 | 004 | 29473 | 20.0 | 0.31 | | 0.66 J | | | <100 | |
| 07 | 004 | 29474 | 21.0 | 0.207 J | 0.220 | 0.154 | 0.0026 U | 0.0026 UJ | 1.0 J | 0.13 J |
| 07 | 004 | 29475 | 23.0 | 0.21 | | 0.41 | | | | |
| 07 | 004 | 29476 | 24.0 | 0.29 | | 0.99 J | | | <100 | |
| 07 | 004 | 29477 | 25.0 | 0.20 | | 1.08 | | | | |
| 07 | 004 | 29478 | 26.0 | 0.24 | | 0.73 J | | | <100 | |
| 07 | 004 | 29479 | 27.0 | 0.19 | | 0.98 J | | | | |
| 07 | 004 | 29480 | 28.0 | 0.09 | | 1.21 | | | <100 | |
| 07 | 004 | 29481 | 29.0 | 0.22 | | 1.11 | | | | |
| 07 | 004 | 29482 | 30.0 | 0.125 | 0.111 | 0.120 | 0.0026 U | 0.0026 UJ | 2.2 J | 0.16 J |
| 07 | 005 | 29291 | 0.0 | 0.40 | | 0.40 | | | | |
| 07 | 005 | 29297 | 2.0 | 0.88 | | 13.89 | | | 82.8 J | |
| 07 | 005 | 29298 | 6.0 | 1.54 | | 1.76 J | | | <100 | |
| 07 | 005 | 29306 | 7.0 | 0.364 | 0.322 | 0.305 | 0.0025 U | 0.0025 U | 2.3 J | 0.16 J |
| 07 | 005 | 29307 | 9.0 | 0.47 | | 0.69 J | | | | |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 07 | 005 | 29308 | 10.0 | 0.48 | | 1.71 J | | | <100 | |
| 07 | 005 | 29309 | 11.0 | 0.29 | | 1.85 | | | | |
| 07 | 005 | 29310 | 12.0 | 0.27 | | 0.43 | | | <100 | |
| 07 | 005 | 29313 | 13.0 | 0.30 | | 0.54 J | | | | |
| 07 | 005 | 29314 | 14.0 | 0.33 | | 1.12 J | | | <100 | |
| 07 | 005 | 29317 | 15.0 | 0.53 J | | 1.73 | | | | |
| 07 | 005 | 29318 | 16.0 | 0.26 | | 0.54 J | | | <100 | |
| 07 | 005 | 29320 | 17.0 | 0.176 | 0.157 | 0.193 | 0.0026 U | 0.0026 U | 1.8 J | 0.048 J |
| 07 | 005 | 29321 | 19.0 | 0.36 J | | 0.78 J | | | | |
| 07 | 005 | 29322 | 20.0 | 0.36 J | | 1.65 | | | <100 | |
| 07 | 005 | 29327 | 21.0 | 0.38 J | | 0.96 J | | | | |
| 07 | 005 | 29328 | 22.0 | 0.25 J | | 2.01 | | | <100 | |
| 07 | 005 | 29329 | 24.0 | 0.05 | | 2.11 J | | | <100 | |
| 07 | 005 | 29332 | 25.0 | 0.16 | | 1.92 | | | | |
| 07 | 005 | 29333 | 26.0 | 0.24 J | | 0.30 | | | <100 | |
| 07 | 005 | 29334 | 27.0 | 0.201 | 0.162 | 0.178 | 0.0026 U | 0.0026 U | 1.1 J | 0.084 J |
| 07 | 005 | 29340 | 29.0 | 0.05 | | 1.78 | | | | |
| 07 | 005 | 29341 | 30.0 | 0.141 | 0.225 | 0.182 | 0.0026 U | 0.0026 U | 2.1 J | 0.23 J |
| 07 | 006 | 29250 | 0.0 | 0.66 | | 3.03 | | | | |
| 07 | 006 | 29251 | 1.0 | 0.48 | | 1.62 J | | | <100 | |
| 07 | 006 | 29254 | 2.0 | 1.03 | | 1.57 J | | | | |
| 07 | 006 | 29255 | 3.0 | 1.01 | | 1.94 J | | | <100 | |
| 07 | 006 | 29256 | 4.0 | 0.78 | 0.62 | 0.55 | 0.0025 U | 0.0025 U | 2.0 J | 0.12 J |
| 07 | 006 | 29257 | 6.0 | 0.39 | | 1.32 | | | | |
| 07 | 006 | 29258 | 7.0 | 0.62 | | 1.98 J | | | <100 | |
| 07 | 006 | 29259 | 8.0 | 0.33 | | 3.31 J | | | | |
| 07 | 006 | 29260 | 9.0 | 0.33 | | 1.16 J | | | <100 | |
| 07 | 006 | 29265 | 10.0 | 0.24 | | 0.68 J | | | | |
| 07 | 006 | 29266 | 11.0 | 0.22 | | 1.74 | | | <100 | |
| 07 | 006 | 29267 | 12.0 | 0.36 | | 2.09 J | | | | |
| 07 | 006 | 29268 | 13.0 | 0.44 | | 1.03 | | | <100 | |
| 07 | 006 | 29269 | 14.0 | 0.248 | 0.296 | 0.271 | 0.0026 U | 0.0026 U | 2.3 J | 0.084 J |
| 07 | 006 | 29270 | 16.0 | 0.23 | | 0.67 J | | | | |
| 07 | 006 | 29271 | 17.0 | 0.28 | | 0.44 J | | | <100 | |
| 07 | 006 | 29273 | 19.0 | 0.22 | | 1.43 | | | <100 | |
| 07 | 006 | 29279 | 20.0 | 0.39 | | 1.15 | | | | |
| 07 | 006 | 29280 | 21.0 | 0.02 | | 1.31 | | | <100 | |
| 07 | 006 | 29281 | 22.0 | 0.29 | | 0.88 J | | | | |
| 07 | 006 | 29282 | 23.0 | 0.27 | | 0.63 J | | | <100 | |
| 07 | 006 | 29283 | 24.0 | 0.207 | 0.318 | 0.311 | 0.0026 U | 0.0026 U | 1.1 J | 0.079 J |
| 07 | 006 | 29284 | 26.0 | 0.21 | | 0.78 J | | | | |
| 07 | 006 | 29285 | 27.0 | 0.24 | | 1.23 J | | | <100 | |
| 07 | 006 | 29286 | 28.0 | 0.22 | | 0.42 J | | | | |
| 07 | 006 | 29287 | 29.0 | 0.20 | | 1.38 | | | <100 | |
| 07 | 006 | 29288 | 30.0 | 0.125 | 0.133 | 0.131 | 0.0026 U | 0.0026 U | 1.7 J | 0.13 J |
| 07 | 007 | 29206 | 0.0 | 0.63 | | 1.74 J | | | <100 | |
| 07 | 007 | 29209 | 1.0 | 0.73 | 15.3 | 8.8 | 0.0028 U | 0.0028 U | 19.3 | 0.61 |
| 07 | 007 | 29210 | 3.0 | 0.51 | | 2.94 | | | | |
| 07 | 007 | 29211 | 4.0 | 0.57 | | 6.65 | | | <100 | |
| 07 | 007 | 29214 | 5.0 | 0.32 | | 2.60 | | | | |
| 07 | 007 | 29215 | 6.0 | 0.35 | | 5.94 | | | <100 | |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 07 | 007 | 29218 | 7.0 | 0.21 | | 1.16 | | | | |
| 07 | 007 | 29219 | 8.0 | 0.37 | | 0.90 J | | | <100 | |
| 07 | 007 | 29220 | 9.0 | 0.25 | | 1.33 J | | | | |
| 07 | 007 | 29221 | 10.0 | 0.41 | | 1.27 J | | | <100 | |
| 07 | 007 | 29222 | 11.0 | 0.222 | 0.320 | 0.299 | 0.0026 U | 0.0026 U | 3.2 J | 0.26 J |
| 07 | 007 | 29223 | 13.0 | 0.27 | | 0.52 | | | | |
| 07 | 007 | 29224 | 14.0 | 0.31 | | 1.21 J | | | <100 | |
| 07 | 007 | 29227 | 15.0 | 0.05 | | 1.29 J | | | | |
| 07 | 007 | 29228 | 16.0 | 0.25 | | 1.01 | | | <100 | |
| 07 | 007 | 29229 | 17.0 | 0.34 | | 1.04 | | | | |
| 07 | 007 | 29230 | 18.0 | NS | | NS | | | <100 | |
| 07 | 007 | 29231 | 19.0 | 0.29 | | 0.64 | | | | |
| 07 | 007 | 29232 | 20.0 | 0.33 | | 0.50 | | | <100 | |
| 07 | 007 | 29237 | 21.0 | 0.145 | 0.229 | 0.171 | 0.0026 U | 0.0026 U | 1.2 J | 0.074 J |
| 07 | 007 | 29238 | 23.0 | 0.28 | | 1.32 | | | | |
| 07 | 007 | 29241 | 24.0 | 0.25 | | 0.52 J | | | <100 | |
| 07 | 007 | 29242 | 25.0 | 0.19 | | 0.72 UJ | | | | |
| 07 | 007 | 29243 | 26.0 | 0.15 | | 0.38 | | | <100 | |
| 07 | 007 | 29244 | 27.0 | 0.28 | | 1.79 J | | | | |
| 07 | 007 | 29245 | 28.0 | 0.24 | | 1.68 | | | <100 | |
| 07 | 007 | 29246 | 29.0 | 0.34 | | 1.17 J | | | | |
| 07 | 007 | 29247 | 30.0 | 0.161 | 0.167 | 0.158 | 0.0026 U | 0.0026 U | 0.98 J | 0.081 J |
| 07 | 012 | 29784 | 0.0 | 0.52 | | 3.12 | | | <100 | |
| 07 | 012 | 29785 | 2.0 | 0.81 | | 6.04 | | | <100 | |
| 07 | 012 | 29786 | 3.0 | 0.30 | | 1.72 | | | | |
| 07 | 012 | 29787 | 4.0 | 0.50 | | 1.30 J | | | <100 | |
| 07 | 012 | 29789 | 5.0 | 0.54 | | 2.93 J | | | | |
| 07 | 012 | 29790 | 6.0 | 0.87 | | 1.21 J | | | <100 | |
| 07 | 012 | 29791 | 7.0 | 0.181 | 0.223 | 0.013 | 0.0025 U | 0.0025 UJ | 1.5 J | 0.14 J |
| 07 | 012 | 29794 | 9.0 | 0.43 | | 0.65 | | | | |
| 07 | 012 | 29795 | 10.0 | 0.76 | | 3.68 | | | <100 | |
| 07 | 012 | 29799 | 11.0 | 0.46 | | 0.88 J | | | | |
| 07 | 012 | 29800 | 12.0 | 1.12 | | 2.19 J | | | <100 | |
| 07 | 012 | 29801 | 13.0 | 0.34 | | 0.61 J | | | | |
| 07 | 012 | 29802 | 14.0 | 0.31 | | 0.51 | | | <100 | |
| 07 | 012 | 29803 | 15.0 | 0.24 | | 0.59 J | | | | |
| 07 | 012 | 29804 | 16.0 | 0.27 | | 1.30 | | | <100 | |
| 07 | 012 | 29814 | 17.0 | 0.121 | 0.153 | 0.107 | 0.0025 U | 0.0025 UJ | 1.1 J | 0.14 J |
| 07 | 012 | 29815 | 20.0 | 0.33 | | 0.51 | | | <100 | |
| 07 | 012 | 29818 | 21.0 | 0.32 | | 1.81 | | | | |
| 07 | 012 | 29819 | 22.0 | 0.39 | | 1.36 J | | | <100 | |
| 07 | 012 | 29820 | 23.0 | 0.33 | | 0.99 J | | | | |
| 07 | 012 | 29821 | 24.0 | 0.06 | | 0.48 | | | <100 | |
| 07 | 012 | 29822 | 25.0 | 0.33 | | 0.36 | | | | |
| 07 | 012 | 29823 | 26.0 | 0.20 | | 1.18 J | | | <100 | |
| 07 | 012 | 29833 | 27.0 | 0.179 | 0.155 | 0.176 | 0.0025 U | 0.0025 UJ | 1.2 J | 0.16 J |
| 07 | 012 | 29834 | 29.0 | 0.25 | | 1.70 J | | | | |
| 07 | 012 | 29835 | 30.0 | 0.246 | 0.158 | 0.145 | 0.0025 U | 0.0025 UJ | 4.6 | 0.31 J |
| 07 | 013 | 29710 | 0.0 | 0.66 | | 13.70 | | | | |
| 07 | 013 | 29711 | 1.0 | 0.73 | | 5.36 | | | <100 | |
| 07 | 013 | 29715 | 2.0 | 0.56 | | 6.38 | | | | |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 07 | 013 | 29716 | 3.0 | 0.57 | | 1.85 | | | <100 | |
| 07 | 013 | 29717 | 4.0 | 0.57 | 3.04 | 2.70 | 0.0025 U | 0.0025 UJ | 3.4 J | 0.21 J |
| 07 | 013 | 29724 | 6.0 | 0.66 | | 1.49 | | | | |
| 07 | 013 | 29725 | 7.0 | 1.32 | | 3.30 | | | <100 | |
| 07 | 013 | 29726 | 8.0 | 0.95 | | 2.64 | | | | |
| 07 | 013 | 29727 | 9.0 | 0.47 | | 1.25 J | | | <100 | |
| 07 | 013 | 29728 | 11.0 | 0.46 | | 1.78 J | | | <100 | |
| 07 | 013 | 29729 | 12.0 | 0.36 | | 1.90 | | | | |
| 07 | 013 | 29730 | 13.0 | 0.39 | | 0.50 | | | <100 | |
| 07 | 013 | 29732 | 14.0 | 0.221 | 0.271 | 0.288 | 0.0025 U | 0.0025 UJ | 2.1 J | 0.24 J |
| 07 | 013 | 29733 | 16.0 | 0.35 | | 2.06 | | | | |
| 07 | 013 | 29734 | 17.0 | 0.29 | | 1.16 | | | <100 | |
| 07 | 013 | 29738 | 18.0 | 0.24 | | 0.93 J | | | | |
| 07 | 013 | 29739 | 19.0 | 0.29 | | 0.74 J | | | <100 | |
| 07 | 013 | 29740 | 20.0 | 0.31 | | 0.70 J | | | | |
| 07 | 013 | 29741 | 21.0 | 0.27 | | 1.48 | | | <100 | |
| 07 | 013 | 29744 | 22.0 | 0.32 | | 0.93 J | | | | |
| 07 | 013 | 29745 | 23.0 | 0.34 | | 1.86 | | | <100 | |
| 07 | 013 | 29746 | 24.0 | 0.215 | 0.209 | 0.165 | 0.0025 U | 0.0025 UJ | 0.70 J | 0.10 J |
| 07 | 013 | 29750 | 26.0 | 0.19 | | 0.92 | | | | |
| 07 | 013 | 29751 | 27.0 | 0.25 | | 4.00 | | | <100 | |
| 07 | 013 | 29752 | 28.0 | 0.30 | | 1.43 | | | | |
| 07 | 013 | 29753 | 29.0 | 0.17 | | 0.56 J | | | <100 | |
| 07 | 013 | 29754 | 30.0 | 0.177 | 0.109 | 0.013 | 0.0025 U | 0.0025 UJ | 1.6 J | 0.16 J |
| 07 | 014 | 29345 | 0.0 | 0.36 | | 1.26 | | | <100 | |
| 07 | 014 | 29346 | 1.0 | 0.432 | 26.8 | 26.6 | 0.0025 U | 0.0025 UJ | 5.3 | 0.19 J |
| 07 | 014 | 29347 | 3.0 | 1.08 J | | 6.21 | | | | |
| 07 | 014 | 29348 | 4.0 | 0.44 | | 9.37 | | | <100 | |
| 07 | 014 | 29349 | 5.0 | 0.56 J | | 5.78 | | | | |
| 07 | 014 | 29350 | 6.0 | 0.50 | | 0.73 J | | | <100 | |
| 07 | 014 | 29351 | 7.0 | 0.34 J | | 1.57 | | | | |
| 07 | 014 | 29352 | 8.0 | 0.09 UJ | | 0.68 J | | | <100 | |
| 07 | 014 | 29353 | 9.0 | 0.08 UJ | | 0.44 | | | | |
| 07 | 014 | 29354 | 10.0 | 0.06 UJ | | 0.88 J | | | <100 | |
| 07 | 014 | 29355 | 11.0 | 0.153 | 0.340 | 0.300 | 0.0025 U | 0.0025 UJ | 2.3 J | 0.11 J |
| 07 | 014 | 29356 | 13.0 | 0.33 J | | 0.55 | | | | |
| 07 | 014 | 29357 | 14.0 | 0.34 J | | 1.78 | | | <100 | |
| 07 | 014 | 29358 | 15.0 | 0.23 J | | 0.91 J | | | | |
| 07 | 014 | 29359 | 16.0 | 0.22 J | | 0.57 | | | <100 | |
| 07 | 014 | 29360 | 17.0 | 0.27 | | 1.32 | | | | |
| 07 | 014 | 29361 | 18.0 | 0.23 J | | 0.88 J | | | <100 | |
| 07 | 014 | 29362 | 20.0 | 0.22 J | | 1.01 | | | <100 | |
| 07 | 014 | 29363 | 21.0 | 0.110 | 0.190 | 0.184 | 0.0025 U | 0.0025 UJ | 1.0 J | 0.51 U |
| 07 | 014 | 29364 | 23.0 | 0.38 J | | 0.57 | | | | |
| 07 | 014 | 29365 | 24.0 | 0.29 J | | 1.59 J | | | <100 | |
| 07 | 014 | 29366 | 25.0 | 0.25 J | | 2.46 J | | | | |
| 07 | 014 | 29373 | 26.0 | 0.26 | | 1.35 J | | | <100 | |
| 07 | 014 | 29374 | 27.0 | 0.14 | | 0.27 | | | | |
| 07 | 014 | 29378 | 28.0 | NS | | NS | | | <100 | |
| 07 | 014 | 29379 | 29.0 | 0.22 | | 1.18 J | | | | |
| 07 | 014 | 29380 | 30.0 | 0.165 | 0.155 | 0.139 | 0.0026 U | 0.0026 UJ | 2.4 J | 0.17 J |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 07 | 015 | 29111 | 0.0 | 0.49 | | 2.83 J | | | <100 | |
| 07 | 015 | 29115 | 1.0 | 1.13 | | 24.47 J | | | | |
| 07 | 015 | 29116 | 2.0 | 0.62 | | 5.11 J | | | 45.8 | |
| 07 | 015 | 29117 | 3.0 | 0.55 J | | 1.29 J | | | | |
| 07 | 015 | 29118 | 4.0 | 0.35 J | | 5.99 J | | | <100 | |
| 07 | 015 | 29121 | 5.0 | 0.39 | | 1.60 J | | | | |
| 07 | 015 | 29122 | 6.0 | 0.40 | | 3.09 J | | | <100 | |
| 07 | 015 | 29127 | 7.0 | 0.392 | 0.297 | 0.219 | 0.0025 U | 0.0025 U | 1.9 J | 0.13 J |
| 07 | 015 | 29130 | 9.0 | 0.28 J | | 1.13 J | | | | |
| 07 | 015 | 29131 | 10.0 | 0.02 | | 1.09 UJ | | | <100 | |
| 07 | 015 | 29133 | 11.0 | 0.31 | | 0.38 J | | | | |
| 07 | 015 | 29134 | 12.0 | 0.28 | | 1.46 J | | | <100 | |
| 07 | 015 | 29140 | 13.0 | 0.30 | | 0.64 J | | | | |
| 07 | 015 | 29141 | 14.0 | 0.25 | | 0.76 J | | | <100 | |
| 07 | 015 | 29142 | 15.0 | 0.23 | | 0.52 UJ | | | | |
| 07 | 015 | 29143 | 16.0 | 0.27 | | 0.94 J | | | <100 | |
| 07 | 015 | 29144 | 17.0 | 0.125 | 0.137 | 0.165 | 0.0025 U | 0.0025 U | 1.0 J | 0.075 J |
| 07 | 015 | 29150 | 19.0 | 0.25 | | 1.21 J | | | | |
| 07 | 015 | 29151 | 20.0 | 0.30 | | 1.68 J | | | 42.3 J | |
| 07 | 015 | 29152 | 21.0 | 0.21 | | 1.10 J | | | | |
| 07 | 015 | 29153 | 22.0 | 0.27 | | 0.69 J | | | <100 | |
| 07 | 015 | 29156 | 23.0 | 0.25 J | | 1.07 J | | | | |
| 07 | 015 | 29157 | 24.0 | 0.29 | | 0.79 J | | | <100 | |
| 07 | 015 | 29160 | 25.0 | 0.28 | | 2.43 J | | | | |
| 07 | 015 | 29161 | 26.0 | 0.26 J | | 1.59 J | | | <100 | |
| 07 | 015 | 29162 | 27.0 | 0.226 | 0.170 | 0.110 | 0.0026 U | 0.0026 U | 1.7 J | 0.11 J |
| 07 | 015 | 29163 | 29.0 | 0.03 | | 0.87 J | | | | |
| 07 | 015 | 29165 | 30.0 | 0.129 | 0.167 | 0.132 | 0.0026 U | 0.0026 U | <100 | |
| 07 | 016 | 29026 | 0.0 | 0.63 | | 8.31 J | | | | |
| 07 | 016 | 29027 | 1.0 | 1.10 | | 4.49 | | | 43.5 J | |
| 07 | 016 | 29028 | 2.0 | 0.86 | | 4.20 | | | | |
| 07 | 016 | 29029 | 3.0 | 0.52 | | 1.65 J | | | <100 | |
| 07 | 016 | 29030 | 4.0 | 0.368 | 0.427 | 0.412 | 0.0025 U | 0.0025 UJ | 1.7 J | 0.16 J |
| 07 | 016 | 29031 | 6.0 | 0.53 | | 0.39 UJ | | | | |
| 07 | 016 | 29032 | 7.0 | 0.44 | | 0.89 J | | | <100 | |
| 07 | 016 | 29033 | 8.0 | 0.52 | | 1.28 J | | | | |
| 07 | 016 | 29034 | 9.0 | 0.07 | | 1.18 J | | | <100 | |
| 07 | 016 | 29035 | 10.0 | 0.40 | | 2.31 J | | | | |
| 07 | 016 | 29036 | 11.0 | 0.24 | | 1.04 J | | | <100 | |
| 07 | 016 | 29037 | 12.0 | 0.85 | | 3.04 J | | | | |
| 07 | 016 | 29038 | 13.0 | 0.21 | | 0.65 J | | | <100 | |
| 07 | 016 | 29039 | 14.0 | 0.73 | 0.270 | 0.258 | 0.0026 U | 0.0026 UJ | 0.68 J | 0.12 J |
| 07 | 016 | 29040 | 16.0 | 0.28 | | 0.79 J | | | | |
| 07 | 016 | 29041 | 17.0 | 0.18 | | 1.14 J | | | <100 | |
| 07 | 016 | 29042 | 18.0 | 0.25 | | 1.89 | | | | |
| 07 | 016 | 29043 | 19.0 | 0.21 | | 1.74 | | | <100 | |
| 07 | 016 | 29044 | 21.0 | 0.19 | | 1.18 J | | | <100 | |
| 07 | 016 | 29045 | 22.0 | 0.35 | | 0.34 | | | | |
| 07 | 016 | 29046 | 23.0 | 0.29 | | 0.89 J | | | <100 | |
| 07 | 016 | 29047 | 24.0 | 0.112 | 0.173 | 0.111 | 0.0026 U | 0.0026 UJ | 0.65 J | 0.069 J |
| 07 | 016 | 29050 | 26.0 | 0.20 | | 1.16 | | | | |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 07 | 016 | 29051 | 27.0 | 0.26 | | 1.27 J | | | <100 | |
| 07 | 016 | 29055 | 28.0 | 0.27 | | 0.93 J | | | | |
| 07 | 016 | 29056 | 29.0 | 0.24 | | 1.68 | | | <100 | |
| 07 | 016 | 29057 | 30.0 | 0.145 | 0.096 J | 0.099 J | 0.0026 U | 0.0026 UJ | 1.1 J | 0.18 J |
| 07 | 017 | 28745 | 0.0 | 0.59 | | 11.31 J | | | | |
| 07 | 017 | 28746 | 1.0 | 0.76 | 24.1 | 11.6 | 0.0027 U | 0.0091 | 58.1 | 1.2 J |
| 07 | 017 | 28747 | 4.0 | 0.77 | | 14.33 J | | | <100 | |
| 07 | 017 | 28748 | 6.0 | 0.60 | | 4.45 J | | | <100 | |
| 07 | 017 | 28753 | 8.0 | 0.11 | | 0.77 UJ | | | <100 | |
| 07 | 017 | 28754 | 10.0 | 0.20 | | 0.58 J | | | <100 | |
| 07 | 017 | 28763 | 11.0 | 0.209 | 0.398 | 0.302 | 0.0025 U | 0.0025 U | 1.6 J | 0.20 J |
| 07 | 017 | 28764 | 14.0 | 0.40 J | | 1.48 | | | <100 | |
| 07 | 017 | 28765 | 15.0 | 0.33 | | 1.30 J | | | | |
| 07 | 017 | 28766 | 16.0 | 0.24 J | | 0.38 | | | <100 | |
| 07 | 017 | 28767 | 17.0 | 0.19 | | 1.77 | | | | |
| 07 | 017 | 28768 | 18.0 | 0.30 J | | 1.23 J | | | <100 | |
| 07 | 017 | 28771 | 20.0 | 0.28 | | 0.74 J | | | <100 | |
| 07 | 017 | 28772 | 21.0 | 0.233 | 0.152 J | 0.145 J | 0.0026 U | 0.0026 U | 1.6 J | 0.17 J |
| 07 | 017 | 28778 | 23.0 | 0.25 J | | 0.91 J | | | | |
| 07 | 017 | 28779 | 24.0 | 0.23 | | 0.53 J | | | <100 | |
| 07 | 017 | 28780 | 25.0 | 0.19 J | | 0.48 J | | | | |
| 07 | 017 | 28781 | 26.0 | NS | | NS | | | <100 | |
| 07 | 017 | 28782 | 27.0 | 0.23 | | 1.33 | | | | |
| 07 | 017 | 28787 | 28.0 | NS | | NS | | | <100 | |
| 07 | 017 | 28788 | 29.0 | 0.26 | | 0.57 J | | | | |
| 07 | 017 | 28793 | 30.0 | 0.129 | 0.119 | 0.099 J | 0.0026 U | 0.0026 U | 2.4 J | 0.17 J |
| 07 | 018 | 28447 | 0.0 | 0.88 | | 11.62 J | | | <100 | |
| 07 | 018 | 28448 | 2.0 | 0.51 | | 1.84 J | | | <100 | |
| 07 | 018 | 28450 | 3.0 | 0.70 | | 2.31 | | | | |
| 07 | 018 | 28451 | 4.0 | 0.37 | | 0.61 | | | <100 | |
| 07 | 018 | 28457 | 5.0 | 0.68 | | 1.33 J | | | | |
| 07 | 018 | 28458 | 6.0 | 0.76 | | 1.26 J | | | <100 | |
| 07 | 018 | 28456 | 7.0 | 0.297 | 0.288 | 0.293 | 0.0025 U | 0.0025 U | 1.8 J | 0.19 J |
| 07 | 018 | 28463 | 10.0 | 0.05 UJ | | 1.20 J | | | <100 | |
| 07 | 018 | 28469 | 11.0 | 0.32 | | 1.15 | | | | |
| 07 | 018 | 28470 | 12.0 | 0.07 UJ | | 1.71 J | | | <100 | |
| 07 | 018 | 28471 | 13.0 | 0.28 J | | 1.26 | | | | |
| 07 | 018 | 28472 | 14.0 | 0.30 | | 1.22 J | | | <100 | |
| 07 | 018 | 28473 | 15.0 | 0.02 UJ | | 1.71 J | | | | |
| 07 | 018 | 28474 | 16.0 | 0.30 J | | 0.33 | | | <100 | |
| 07 | 018 | 28475 | 17.0 | 0.219 | 0.169 | 0.230 | 0.0026 U | 0.0026 U | 4.1 J | 0.17 J |
| 07 | 018 | 28476 | 22.0 | 0.33 | | 0.70 J | | | <100 | |
| 07 | 018 | 28477 | 23.0 | 0.32 J | | 1.41 J | | | | |
| 07 | 018 | 28478 | 24.0 | 0.29 J | | 0.76 J | | | <100 | |
| 07 | 018 | 28479 | 25.0 | 0.06 UJ | | 1.32 J | | | | |
| 07 | 018 | 28480 | 26.0 | 0.22 J | | 0.52 J | | | <100 | |
| 07 | 018 | 28487 | 27.0 | 0.174 | 0.140 | 0.142 | 0.0025 U | 0.0025 U | 1.0 J | 0.076 J |
| 07 | 018 | 28488 | 29.0 | 0.22 | | 1.23 | | | | |
| 07 | 018 | 28489 | 30.0 | 0.223 | 0.201 | 0.182 | 0.0026 U | 0.0026 U | 1.3 J | 0.11 J |
| 07 | 022 | 29657 | 0.0 | NS | | NS | | | <100 | |
| 07 | 022 | 29656 | 1.0 | 0.56 | 9.5 | 9.3 | 0.0025 U | 0.0025 UJ | 9.9 | 0.42 J |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 07 | 022 | 29664 | 3.0 | 0.83 | | 1.49 J | | | | |
| 07 | 022 | 29665 | 4.0 | 1.04 | | 2.69 J | | | <100 | |
| 07 | 022 | 29666 | 5.0 | 0.39 | | 1.03 J | | | | |
| 07 | 022 | 29667 | 6.0 | 0.33 | | 1.40 J | | | <100 | |
| 07 | 022 | 29671 | 7.0 | 0.42 | | 0.89 J | | | | |
| 07 | 022 | 29672 | 8.0 | 0.71 | | 1.30 J | | | <100 | |
| 07 | 022 | 29673 | 10.0 | 0.25 | | 1.27 J | | | <100 | |
| 07 | 022 | 29677 | 11.0 | 0.206 | 0.245 | 0.246 | 0.0025 U | 0.0025 U | 1.3 J | 0.13 J |
| 07 | 022 | 29678 | 13.0 | 0.03 | | 0.70 | | | | |
| 07 | 022 | 29679 | 14.0 | 0.43 | | 0.98 J | | | <100 | |
| 07 | 022 | 29680 | 15.0 | 0.31 | | 1.50 | | | | |
| 07 | 022 | 29681 | 16.0 | 0.31 | | 0.61 | | | <100 | |
| 07 | 022 | 29687 | 17.0 | 0.26 | | 1.90 | | | | |
| 07 | 022 | 29688 | 18.0 | 0.38 | | 0.78 | | | <100 | |
| 07 | 022 | 29689 | 20.0 | 0.23 | | 0.47 | | | <100 | |
| 07 | 022 | 29692 | 21.0 | 0.169 | 0.345 | 0.262 | 0.0025 U | 0.0025 UJ | 1.5 J | 0.15 J |
| 07 | 022 | 29693 | 24.0 | 0.30 | | 0.43 | | | <100 | |
| 07 | 022 | 29694 | 25.0 | 0.22 | | 1.09 | | | | |
| 07 | 022 | 29698 | 26.0 | 0.22 | | 0.61 J | | | <100 | |
| 07 | 022 | 29699 | 27.0 | 0.31 | | 1.56 | | | | |
| 07 | 022 | 29700 | 28.0 | 0.21 | | 1.48 | | | <100 | |
| 07 | 022 | 29701 | 29.0 | 0.19 | | 0.78 J | | | | |
| 07 | 022 | 29702 | 30.0 | 0.132 | 0.206 | 0.173 | 0.0025 U | 0.0025 UJ | 1.7 J | 0.17 J |
| 07 | 023 | 29570 | 0.0 | 0.57 | | 2.14 | | | <100 | |
| 07 | 023 | 29571 | 1.0 | 0.57 | | 1.21 J | | | | |
| 07 | 023 | 29572 | 2.0 | 0.36 | | 1.73 | | | <100 | |
| 07 | 023 | 29573 | 3.0 | 0.36 | | 1.45 | | | | |
| 07 | 023 | 29574 | 4.0 | 0.42 | | 1.73 J | | | <100 | |
| 07 | 023 | 29575 | 5.0 | 0.77 | | 2.07 J | | | | |
| 07 | 023 | 29576 | 6.0 | 0.51 | | 1.29 J | | | <100 | |
| 07 | 023 | 29577 | 7.0 | 0.195 | 0.229 | 0.189 | 0.0025 U | 0.0025 UJ | 1.3 J | 0.12 J |
| 07 | 023 | 29578 | 9.0 | 0.42 | | 2.01 J | | | | |
| 07 | 023 | 29579 | 10.0 | 0.18 | | 0.99 | | | <100 | |
| 07 | 023 | 29580 | 11.0 | 0.33 | | 0.43 J | | | | |
| 07 | 023 | 29581 | 12.0 | 0.25 | | 1.17 J | | | <100 | |
| 07 | 023 | 29582 | 13.0 | 0.49 | | 1.55 | | | | |
| 07 | 023 | 29583 | 14.0 | 0.24 | | 0.32 | | | <100 | |
| 07 | 023 | 29584 | 15.0 | 0.19 | | 0.54 | | | | |
| 07 | 023 | 29585 | 16.0 | 0.31 | | 0.63 J | | | <100 | |
| 07 | 023 | 29586 | 17.0 | 0.153 | 0.217 | 0.131 | 0.0025 U | 0.0025 UJ | 0.97 J | 0.12 J |
| 07 | 023 | 29587 | 19.0 | 0.19 | | 0.61 J | | | | |
| 07 | 023 | 29588 | 20.0 | 0.42 | | 0.67 | | | <100 | |
| 07 | 023 | 29593 | 21.0 | 0.23 | | 1.33 J | | | | |
| 07 | 023 | 29594 | 22.0 | 0.27 | | 0.75 J | | | <100 | |
| 07 | 023 | 29595 | 23.0 | 0.51 | | 3.22 | | | | |
| 07 | 023 | 29596 | 24.0 | 0.24 | | 1.08 J | | | <100 | |
| 07 | 023 | 29597 | 25.0 | 0.25 | | 0.47 | | | | |
| 07 | 023 | 29598 | 26.0 | 0.22 | | 0.67 J | | | <100 | |
| 07 | 023 | 29599 | 27.0 | 0.226 | 0.206 | 0.179 | 0.0025 U | 0.0025 UJ | 2.0 J | 0.28 J |
| 07 | 023 | 29600 | 29.0 | 0.22 | | 0.97 | | | | |
| 07 | 023 | 29601 | 30.0 | 0.172 | 0.216 | 0.166 | 0.0026 U | 0.0026 UJ | 1.9 J | 0.18 J |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 07 | 024 | 29401 | 0.0 | 0.50 | | 9.08 | | | | |
| 07 | 024 | 29402 | 1.0 | 0.52 | | 1.09 J | | | <100 | |
| 07 | 024 | 29403 | 4.0 | 0.38 | 0.48 | 0.53 | 0.0025 U | 0.0025 UJ | 1.2 J | 0.18 J |
| 07 | 024 | 29404 | 6.0 | 0.31 | | 1.64 | | | | |
| 07 | 024 | 29405 | 7.0 | 0.46 | | 0.96 J | | | <100 | |
| 07 | 024 | 29406 | 9.0 | 0.35 | | 1.14 J | | | <100 | |
| 07 | 024 | 29407 | 10.0 | 0.23 | | 1.21 J | | | | |
| 07 | 024 | 29408 | 11.0 | 0.07 | | 1.25 J | | | <100 | |
| 07 | 024 | 29409 | 12.0 | 0.06 | | 0.77 J | | | | |
| 07 | 024 | 29410 | 13.0 | 0.08 | | 2.20 | | | <100 | |
| 07 | 024 | 29416 | 14.0 | 0.178 | 0.251 | 0.225 | 0.0025 U | 0.0025 UJ | 1.8 J | 0.19 J |
| 07 | 024 | 29421 | 16.0 | 0.06 | | 1.20 J | | | | |
| 07 | 024 | 29422 | 17.0 | 0.25 | | 1.40 | | | <100 | |
| 07 | 024 | 29423 | 19.0 | 0.26 | | 0.97 J | | | <100 | |
| 07 | 024 | 29424 | 20.0 | 0.18 | | 0.63 J | | | | |
| 07 | 024 | 29425 | 21.0 | 0.21 | | 0.53 J | | | <100 | |
| 07 | 024 | 29429 | 23.0 | 0.39 | | 1.96 | | | <100 | |
| 07 | 024 | 29430 | 24.0 | 0.164 | 0.202 | 0.168 | 0.0025 U | 0.0025 UJ | 1.3 J | 0.12 J |
| 07 | 024 | 29431 | 26.0 | 0.05 | | 1.10 J | | | | |
| 07 | 024 | 29432 | 27.0 | 0.19 | | 0.71 J | | | <100 | |
| 07 | 024 | 29440 | 28.0 | 0.25 | | 1.20 J | | | | |
| 07 | 024 | 29441 | 29.0 | 0.20 | | 0.56 J | | | <100 | |
| 07 | 024 | 29442 | 30.0 | 0.155 | 0.190 | 0.161 | 0.0025 U | 0.0025 UJ | 0.62 J | 0.10 J |
| 07 | 025 | 29066 | 0.0 | 0.68 | | 8.35 | | | <100 | |
| 07 | 025 | 29067 | 1.0 | 0.85 | 2.69 | 2.63 | 0.0025 U | 0.0025 U | 6.4 | 0.35 J |
| 07 | 025 | 29068 | 3.0 | 0.46 | | 0.49 J | | | | |
| 07 | 025 | 29069 | 4.0 | 0.47 | | 1.57 J | | | <100 | |
| 07 | 025 | 29076 | 5.0 | 0.58 | | 0.85 J | | | | |
| 07 | 025 | 29077 | 6.0 | 0.63 | | 0.62 | | | <100 | |
| 07 | 025 | 29079 | 7.0 | 0.53 | | 0.89 J | | | | |
| 07 | 025 | 29080 | 8.0 | 0.57 | | 1.56 J | | | <100 | |
| 07 | 025 | 29084 | 10.0 | 0.34 | | 0.47 | | | <100 | |
| 07 | 025 | 29085 | 11.0 | 0.373 | 0.390 | 0.322 | 0.0025 U | 0.0025 U | 0.60 J | 0.10 J |
| 07 | 025 | 29086 | 13.0 | 0.25 | | 0.56 J | | | | |
| 07 | 025 | 29087 | 14.0 | 0.34 | | 1.62 | | | <100 | |
| 07 | 025 | 29088 | 15.0 | 0.23 J | | 1.07 | | | | |
| 07 | 025 | 29089 | 16.0 | 0.32 | | 0.31 | | | <100 | |
| 07 | 025 | 29097 | 17.0 | 0.21 | | 1.71 | | | | |
| 07 | 025 | 29098 | 18.0 | 0.39 | | 0.49 J | | | <100 | |
| 07 | 025 | 29095 | 19.0 | 0.42 | | 0.41 J | | | | |
| 07 | 025 | 29096 | 20.0 | 0.27 | | 1.03 J | | | <100 | |
| 07 | 025 | 29099 | 21.0 | 0.185 | 0.216 | 0.179 | 0.0025 U | 0.0025 U | 1.6 J | 0.10 J |
| 07 | 025 | 29100 | 23.0 | 0.30 | | 1.50 | | | | |
| 07 | 025 | 29101 | 24.0 | 0.20 | | 0.38 | | | <100 | |
| 07 | 025 | 29102 | 25.0 | 0.26 | | 0.84 J | | | | |
| 07 | 025 | 29103 | 26.0 | 0.27 | | 1.05 J | | | <100 | |
| 07 | 025 | 29104 | 27.0 | 0.21 | | 0.43 | | | | |
| 07 | 025 | 29105 | 28.0 | 0.27 | | 2.81 | | | <100 | |
| 07 | 025 | 29106 | 29.0 | 0.23 | | 0.63 | | | | |
| 07 | 025 | 29107 | 30.0 | 0.120 J | 0.201 | 0.213 | 0.0026 U | 0.0026 U | 2.1 J | 0.16 J |
| 07 | 026 | 28830 | 0.0 | 0.95 | | 0.98 J | | | <100 | |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 07 | 026 | 28831 | 1.0 | 1.33 J | | 4.95 | | | | |
| 07 | 026 | 28832 | 2.0 | 1.27 | | 0.78 | | | <100 | |
| 07 | 026 | 28833 | 3.0 | 0.62 | | 3.05 | | | | |
| 07 | 026 | 28834 | 4.0 | 0.39 | | 0.77 J | | | <100 | |
| 07 | 026 | 28842 | 5.0 | 0.61 | | 2.35 | | | | |
| 07 | 026 | 28843 | 6.0 | 0.63 J | | 0.97 J | | | <100 | |
| 07 | 026 | 28844 | 7.0 | 0.365 | 0.236 | 0.256 | 0.0025 U | 0.0025 U | 0.91 J | 0.069 J |
| 07 | 026 | 28845 | 9.0 | 0.61 | | 0.47 J | | | | |
| 07 | 026 | 28846 | 10.0 | 0.03 UJ | | 1.16 J | | | <100 | |
| 07 | 026 | 28851 | 11.0 | 0.26 | | 1.35 J | | | | |
| 07 | 026 | 28852 | 12.0 | 0.44 | | 1.77 | | | <100 | |
| 07 | 026 | 28853 | 13.0 | 0.46 | | 1.44 J | | | | |
| 07 | 026 | 28854 | 14.0 | 0.33 J | | 1.33 | | | <100 | |
| 07 | 026 | 28857 | 16.0 | 0.29 | | 0.88 J | | | <100 | |
| 07 | 026 | 28858 | 17.0 | 0.104 | 0.114 | 0.125 | 0.0025 U | 0.0025 U | 1.0 J | 0.077 J |
| 07 | 026 | 28859 | 20.0 | 0.28 J | | 1.00 J | | | <100 | |
| 07 | 026 | 28864 | 21.0 | 0.31 | | 0.39 | | | | |
| 07 | 026 | 28865 | 22.0 | 0.25 J | | 0.57 J | | | <100 | |
| 07 | 026 | 28866 | 23.0 | 0.30 | | 1.25 J | | | | |
| 07 | 026 | 28867 | 24.0 | 0.26 | | 1.55 | | | <100 | |
| 07 | 026 | 28868 | 25.0 | 0.29 | | 1.43 | | | | |
| 07 | 026 | 28869 | 26.0 | 0.27 | | 0.42 | | | <100 | |
| 07 | 026 | 28875 | 27.0 | 0.131 | 0.114 | 0.092 J | 0.0025 U | 0.0025 U | 1.1 J | 0.14 J |
| 07 | 026 | 28876 | 29.0 | 0.23 | | 1.17 J | | | | |
| 07 | 026 | 28877 | 30.0 | 0.115 | 0.129 | 0.087 J | 0.0025 U | 0.0025 U | 1.7 J | 0.092 J |
| 07 | 027 | 28506 | 0.0 | 0.84 J | | 0.88 J | | | | |
| 07 | 027 | 28507 | 1.0 | 0.97 | | 3.57 | | | <100 | |
| 07 | 027 | 28514 | 2.0 | 0.48 J | | 0.88 J | | | | |
| 07 | 027 | 28515 | 3.0 | 0.62 | | 1.52 J | | | <100 | |
| 07 | 027 | 28517 | 4.0 | 0.52 | 0.97 | 0.294 | 0.0025 U | 0.0025 U | 1.7 J | 0.13 J |
| 07 | 027 | 28518 | 6.0 | 0.63 J | | 1.11 J | | | | |
| 07 | 027 | 28519 | 7.0 | 0.77 J | | 0.87 J | | | <100 | |
| 07 | 027 | 28520 | 9.0 | 0.05 | | 1.46 | | | <100 | |
| 07 | 027 | 28521 | 10.0 | 0.44 J | | 0.54 | | | | |
| 07 | 027 | 28522 | 11.0 | 0.07 UJ | | 1.45 | | | <100 | |
| 07 | 027 | 28523 | 12.0 | 0.37 | | 1.96 | | | | |
| 07 | 027 | 28524 | 13.0 | 0.36 J | | 1.35 J | | | <100 | |
| 07 | 027 | 28525 | 14.0 | 0.270 | 0.257 | 0.209 | 0.0025 U | 0.0025 U | 1.4 J | 0.15 J |
| 07 | 027 | 28526 | 16.0 | 0.07 UJ | | 0.59 J | | | | |
| 07 | 027 | 28527 | 17.0 | 0.06 | | 0.69 J | | | <100 | |
| 07 | 027 | 28528 | 18.0 | 0.28 J | | 3.53 | | | | |
| 07 | 027 | 28529 | 19.0 | 0.30 J | | 1.49 J | | | <100 | |
| 07 | 027 | 28530 | 20.0 | 0.33 | | 2.41 | | | | |
| 07 | 027 | 28531 | 21.0 | 0.25 J | | 0.86 J | | | <100 | |
| 07 | 027 | 28532 | 22.0 | 0.36 J | | 0.96 J | | | | |
| 07 | 027 | 28533 | 23.0 | 0.34 | | 0.32 | | | <100 | |
| 07 | 027 | 28538 | 24.0 | 0.227 | 0.124 | 0.170 | 0.0025 U | 0.0025 U | 0.79 J | 0.10 J |
| 07 | 027 | 28541 | 26.0 | 0.20 | | 0.45 | | | | |
| 07 | 027 | 28542 | 27.0 | 0.27 | | 1.82 J | | | <100 | |
| 07 | 027 | 28549 | 29.0 | 0.06 | | 0.82 J | | | <100 | |
| 07 | 027 | 28551 | 30.0 | 0.244 | 0.194 | 0.145 | 0.0025 U | 0.0025 U | 0.63 J | 0.14 J |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 07 | 031 | 29618 | 1.0 | 0.71 | | 33.77 | | | <100 | |
| 07 | 031 | 29619 | 3.0 | 0.39 | | 6.77 | | | <100 | |
| 07 | 031 | 29620 | 4.0 | 0.455 | 0.411 | 0.397 | 0.0025 U | 0.0025 UJ | 3.0 J | 0.15 J |
| 07 | 031 | 29628 | 6.0 | 0.63 | | 1.47 J | | | | |
| 07 | 031 | 29629 | 7.0 | 0.26 | | 1.47 J | | | <100 | |
| 07 | 031 | 29630 | 8.0 | 0.26 | | 0.89 J | | | | |
| 07 | 031 | 29631 | 9.0 | 0.35 | | 0.65 | | | <100 | |
| 07 | 031 | 29632 | 10.0 | 0.27 | | 0.59 | | | | |
| 07 | 031 | 29633 | 11.0 | 0.07 | | 2.58 J | | | <100 | |
| 07 | 031 | 29634 | 12.0 | 0.32 | | 1.56 J | | | | |
| 07 | 031 | 29635 | 13.0 | 0.42 | | 2.04 | | | <100 | |
| 07 | 031 | 29636 | 14.0 | 0.218 | 0.248 | 0.178 | 0.0025 U | 0.0025 UJ | 1.4 J | 0.20 J |
| 07 | 031 | 29638 | 16.0 | 0.31 | | 1.61 J | | | | |
| 07 | 031 | 29639 | 17.0 | 0.28 | | 0.54 | | | <100 | |
| 07 | 031 | 29637 | 19.0 | 0.27 | | 1.20 J | | | <100 | |
| 07 | 031 | 29640 | 20.0 | 0.20 | | 1.80 | | | | |
| 07 | 031 | 29641 | 21.0 | 0.26 | | 0.76 J | | | <100 | |
| 07 | 031 | 29642 | 23.0 | 0.48 | | 1.79 | | | <100 | |
| 07 | 031 | 29649 | 24.0 | 0.152 | 0.167 | 0.139 | 0.0025 U | 0.0025 UJ | 1.1 J | 0.16 J |
| 07 | 031 | 29650 | 26.0 | 0.18 | | 0.32 J | | | | |
| 07 | 031 | 29651 | 27.0 | 0.27 | | 0.34 | | | <100 | |
| 07 | 031 | 29652 | 28.0 | 0.29 | | 1.43 | | | | |
| 07 | 031 | 29653 | 29.0 | 0.22 | | 0.50 | | | <100 | |
| 07 | 031 | 29654 | 30.0 | 0.130 | 0.143 | 0.136 | 0.0025 U | 0.0025 UJ | 1.8 J | 0.19 J |
| 07 | 032 | 29544 | 0.0 | 0.74 | | 25.02 | | | <100 | |
| 07 | 032 | 29545 | 1.0 | 0.69 | 18.5 | 18.9 | 0.0027 U | 0.0027 UJ | 23.9 | 0.37 J |
| 07 | 032 | 29546 | 4.0 | 1.20 | | 2.20 J | | | <100 | |
| 07 | 032 | 29547 | 5.0 | 1.21 | | 1.81 J | | | | |
| 07 | 032 | 29548 | 6.0 | 0.92 | | 2.52 J | | | <100 | |
| 07 | 032 | 29549 | 7.0 | 0.55 | | 2.13 | | | | |
| 07 | 032 | 29550 | 8.0 | 0.31 | | 1.86 | | | <100 | |
| 07 | 032 | 29551 | 9.0 | 0.42 | | 1.05 J | | | | |
| 07 | 032 | 29552 | 10.0 | 0.31 | | 1.74 | | | <100 | |
| 07 | 032 | 29553 | 11.0 | 0.252 | 0.423 | 0.386 | 0.0026 U | 0.0026 UJ | 2.2 J | 0.15 J |
| 07 | 032 | 29554 | 13.0 | 0.41 | | 1.66 | | | | |
| 07 | 032 | 29555 | 14.0 | 0.27 | | 0.56 J | | | <100 | |
| 07 | 032 | 29556 | 15.0 | 0.29 | | 0.94 J | | | | |
| 07 | 032 | 29557 | 16.0 | 0.23 | | 2.03 | | | <100 | |
| 07 | 032 | 29558 | 18.0 | 0.06 | | 0.61 J | | | <100 | |
| 07 | 032 | 29559 | 19.0 | 0.29 | | 2.61 | | | | |
| 07 | 032 | 29560 | 20.0 | 0.40 | | 0.95 J | | | <100 | |
| 07 | 032 | 29561 | 21.0 | 0.167 | 0.201 | 0.178 | 0.0025 U | 0.0025 UJ | 1.3 J | 0.17 J |
| 07 | 032 | 29562 | 23.0 | 0.23 | | 2.20 | | | | |
| 07 | 032 | 29563 | 24.0 | 0.22 | | 1.00 | | | <100 | |
| 07 | 032 | 29564 | 25.0 | 0.25 | | 1.14 | | | | |
| 07 | 032 | 29565 | 26.0 | 0.25 | | 1.33 | | | <100 | |
| 07 | 032 | 29566 | 27.0 | 0.31 | | 0.73 J | | | | |
| 07 | 032 | 29567 | 28.0 | 0.28 | | 2.21 J | | | <100 | |
| 07 | 032 | 29568 | 29.0 | 0.26 | | 0.95 J | | | | |
| 07 | 032 | 29569 | 30.0 | 0.126 | 0.184 | 0.166 | 0.0025 U | 0.0025 UJ | 1.7 J | 0.18 J |
| 07 | 033 | 29483 | 0.0 | 0.51 | | 3.57 | | | <100 | |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 07 | 033 | 29485 | 1.0 | 0.74 | | 6.62 | | | | |
| 07 | 033 | 29486 | 2.0 | 1.31 | | 4.65 | | | <100 | |
| 07 | 033 | 29491 | 3.0 | 0.70 | | 2.19 | | | | |
| 07 | 033 | 29492 | 4.0 | 0.39 | | 0.86 J | | | <100 | |
| 07 | 033 | 29494 | 5.0 | 0.45 | | 1.19 J | | | | |
| 07 | 033 | 29493 | 6.0 | 0.51 | | 0.98 J | | | <100 | |
| 07 | 033 | 29500 | 7.0 | 0.52 | 0.38 | 0.282 | 0.0026 U | 0.0026 UJ | 1.2 J | 0.16 J |
| 07 | 033 | 29503 | 10.0 | 0.34 | | 1.35 | | | <100 | |
| 07 | 033 | 29506 | 11.0 | 0.29 | | 0.98 J | | | | |
| 07 | 033 | 29507 | 12.0 | 0.40 | | 1.55 J | | | <100 | |
| 07 | 033 | 29513 | 13.0 | 0.43 | | 0.57 | | | | |
| 07 | 033 | 29514 | 14.0 | 0.37 | | 1.48 J | | | <100 | |
| 07 | 033 | 29515 | 16.0 | 0.27 | | 1.53 J | | | <100 | |
| 07 | 033 | 29516 | 17.0 | 0.184 | 0.117 | 0.178 | 0.0025 U | 0.0025 UJ | 0.80 J | 0.15 J |
| 07 | 033 | 29517 | 19.0 | 0.29 | | 0.74 | | | | |
| 07 | 033 | 29518 | 20.0 | 0.35 | | 0.93 J | | | <100 | |
| 07 | 033 | 29519 | 21.0 | 0.24 | | 2.01 | | | | |
| 07 | 033 | 29520 | 22.0 | 0.30 | | 1.02 J | | | <100 | |
| 07 | 033 | 29524 | 23.0 | 0.23 | | 1.40 J | | | | |
| 07 | 033 | 29525 | 24.0 | 0.27 | | 0.74 J | | | <100 | |
| 07 | 033 | 29529 | 25.0 | 0.19 | | 1.74 | | | | |
| 07 | 033 | 29530 | 26.0 | 0.18 | | 0.78 J | | | <100 | |
| 07 | 033 | 29531 | 27.0 | 0.157 | 0.151 | 0.156 | 0.0025 U | 0.0025 UJ | 1.1 J | 0.13 J |
| 07 | 033 | 29532 | 29.0 | 0.19 | | 2.19 | | | | |
| 07 | 033 | 29533 | 30.0 | 0.097 J | 0.116 | 0.130 | 0.0025 U | 0.0025 UJ | 1.4 J | 0.17 J |
| 07 | 034 | 28961 | 0.0 | 1.00 | | 1.32 J | | | | |
| 07 | 034 | 28962 | 1.0 | 0.66 | | 0.63 J | | | <100 | |
| 07 | 034 | 28963 | 2.0 | 0.37 | | 0.58 J | | | | |
| 07 | 034 | 28964 | 3.0 | 0.64 | | 0.64 UJ | | | <100 | |
| 07 | 034 | 28969 | 4.0 | 0.57 | 0.386 | 0.322 | 0.0026 U | 0.0026 U | 2.1 J | 0.21 J |
| 07 | 034 | 28971 | 6.0 | 0.76 | | 1.07 J | | | | |
| 07 | 034 | 28972 | 7.0 | 0.44 | | 0.70 J | | | <100 | |
| 07 | 034 | 28973 | 8.0 | 0.22 | | 1.78 J | | | | |
| 07 | 034 | 28974 | 9.0 | 0.30 | | 1.46 J | | | <100 | |
| 07 | 034 | 28975 | 10.0 | 0.39 | | 2.38 J | | | | |
| 07 | 034 | 28976 | 11.0 | 0.38 | | 2.02 J | | | <100 | |
| 07 | 034 | 28977 | 12.0 | 0.37 | | 0.57 J | | | | |
| 07 | 034 | 28978 | 13.0 | 0.26 | | 0.60 J | | | <100 | |
| 07 | 034 | 28979 | 14.0 | 0.298 | 0.228 | 0.234 | 0.0025 U | 0.0025 UJ | 1.7 J | 0.13 J |
| 07 | 034 | 28983 | 16.0 | 0.20 | | 0.36 UJ | | | | |
| 07 | 034 | 28984 | 17.0 | 0.04 | | 0.54 J | | | <100 | |
| 07 | 034 | 28985 | 18.0 | 0.24 | | 0.51 UJ | | | | |
| 07 | 034 | 28986 | 19.0 | 0.24 | | 0.86 J | | | <100 | |
| 07 | 034 | 28991 | 20.0 | 0.25 | | 1.15 J | | | | |
| 07 | 034 | 28992 | 21.0 | 0.33 | | 0.69 UJ | | | <100 | |
| 07 | 034 | 28993 | 23.0 | 0.41 | | 0.73 J | | | <100 | |
| 07 | 034 | 28994 | 24.0 | 0.346 | 0.234 | 0.238 | 0.0026 U | 0.0026 UJ | 0.36 J | 0.082 J |
| 07 | 034 | 28995 | 26.0 | 0.22 | | 0.90 J | | | | |
| 07 | 034 | 28996 | 27.0 | 0.20 | | 1.07 J | | | <100 | |
| 07 | 034 | 28999 | 28.0 | 0.06 | | 2.38 J | | | | |
| 07 | 034 | 29000 | 29.0 | 0.25 | | 1.65 J | | | <100 | |

Table 1
SU06 and SU07 Soil Boring Sample Results

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 07 | 034 | 29004 | 30.0 | 0.220 | 0.165 | 0.160 | 0.0025 U | 0.0025 UJ | 1.4 J | 0.15 J |
| 07 | 035 | 28901 | 0.0 | 0.71 | | 6.13 | | | <100 | |
| 07 | 035 | 28902 | 1.0 | 0.93 | 32.4 | 10.3 | 0.0016 J | 0.022 | 15.1 | 0.37 J |
| 07 | 035 | 28903 | 4.0 | 0.77 | | 6.75 | | | <100 | |
| 07 | 035 | 28909 | 5.0 | 0.69 | | 4.64 | | | | |
| 07 | 035 | 28910 | 6.0 | 0.63 | | 3.41 | | | <100 | |
| 07 | 035 | 28911 | 7.0 | 0.87 | | 1.75 J | | | | |
| 07 | 035 | 28912 | 8.0 | 0.42 | | 1.81 | | | <100 | |
| 07 | 035 | 28914 | 9.0 | 0.49 | | 0.64 J | | | | |
| 07 | 035 | 28915 | 10.0 | 0.24 | | 1.22 J | | | <100 | |
| 07 | 035 | 28916 | 11.0 | 0.294 | 0.307 | 0.337 | 0.0025 U | 0.0025 U | 1.8 J | 0.096 J |
| 07 | 035 | 28917 | 13.0 | 0.35 | | 2.42 | | | | |
| 07 | 035 | 28918 | 14.0 | 0.34 | | 1.06 J | | | <100 | |
| 07 | 035 | 28919 | 15.0 | 0.29 | | 3.04 | | | | |
| 07 | 035 | 28920 | 16.0 | 0.04 | | 0.52 J | | | <100 | |
| 07 | 035 | 28921 | 17.0 | 0.14 | | 0.87 J | | | | |
| 07 | 035 | 28922 | 18.0 | 0.28 | | 1.25 J | | | <100 | |
| 07 | 035 | 28927 | 19.0 | 0.05 | | 2.76 | | | | |
| 07 | 035 | 28928 | 20.0 | 0.17 | | 0.35 J | | | <100 | |
| 07 | 035 | 28929 | 21.0 | 0.131 | 0.166 | 0.220 | 0.0026 U | 0.0026 U | 0.95 J | 0.11 J |
| 07 | 035 | 28930 | 23.0 | 0.31 | | 1.22 | | | | |
| 07 | 035 | 28933 | 24.0 | 0.25 | | 0.54 J | | | <100 | |
| 07 | 035 | 28934 | 25.0 | 0.33 | | 0.50 J | | | | |
| 07 | 035 | 28935 | 26.0 | 0.05 | | 0.52 | | | | |
| 07 | 035 | 28936 | 27.0 | 0.34 | | 1.24 | | | <100 | |
| 07 | 035 | 28942 | 28.0 | 0.17 | | 0.88 J | | | <100 | |
| 07 | 035 | 28943 | 29.0 | 0.19 | | 1.27 | | | | |
| 07 | 035 | 28944 | 30.0 | 0.282 | 0.206 | 0.262 | 0.0026 U | 0.0026 U | 1.3 J | 0.17 J |

Table 1
SU06 and SU07 Soil Boring Sample Results

Analytics:

| | |
|-----------------------|-------------------------|
| Th-232 - Thorium-232 | PCE - Tetrachloroethene |
| U-234 - Uranium-234 | Ni - Nickel |
| U-238 - Uranium-238 | Be - Beryllium |
| TCE - Trichloroethene | |

Units:

pCi/g - picoCurie/gram
mg/kg - milligram/kilogram

Qualifiers:

U - Validation qualifier used to indicate that the result was qualified as non-detect.
J - Validation qualifier used to indicate that the result is considered an estimate.
UJ - Validation qualifier used to indicate that the result was qualified as non-detect and the associated reporting limit is considered an estimate.

Notes:

See Figure 1 for boring locations.
DL sample is analyzed on Site for radionuclides (Th-232 and U-238) using the gamma spectroscopy system.
DL sample is analyzed on Site for Ni using x-ray fluorescence spectroscopy by Stone Environmental Inc. Ni result that is between the detection limit of 40 mg/kg and the reporting limit of 100 mg/kg is estimated. Ni result that is less than the detection limit of 40 mg/kg is reported as less than the reporting limit (<100 mg/kg).
SP sample result is bold and indicates that analysis was performed off Site by Severn Trent Laboratories, Inc.
NS - Not sampled due to insufficient recovery.
Due to an artifact in the laboratory data reporting program, the on-Site analytical data should be interpreted to two significant figures.
Blank cell indicates analysis was not performed.

Table 2
SU06 and SU07 Soil Boring Sample Results
Severn Trent Laboratories, Inc.

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | -234 (pCi/g) | -238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|---------------------|---------------------|--------------------|--------------------|-------------------|-------------------|
| 06 | 001 | 28342 | 4.0 | 0.38 | 1.08 | 0.77 | 0.0025 | 0.0025 | 2.1 J | 0.13 J |
| 06 | 001 | 28359 | 14.0 | 0.191 | 0.187 | 0.223 | 0.0025 | 0.0025 | 2.8 J | 0.14 J |
| 06 | 001 | 28371 | 24.0 | 0.160 | 0.200 | 0.130 | 0.0025 | 0.0025 | 1.1 J | 0.098 J |
| 06 | 001 | 28384 | 30.0 | 0.120 | 0.127 | 0.134 | 0.0026 | 0.0026 | 3.1 J | 0.15 J |
| 06 | 002 | 27977 | 1.0 | 0.474 | 2.44 | 1.19 | 0.0025 | 0.0025 | 3.7 J | 0.26 J |
| 06 | 002 | 28008 | 11.0 | 0.417 | 0.317 | 0.329 | 0.0025 | 0.0025 | 1.7 J | 0.18 J |
| 06 | 002 | 28017 | 21.0 | 0.141 | 0.184 | 0.206 | 0.0026 | 0.0026 | 1.3 J | 0.19 J |
| 06 | 002 | 28040 | 30.0 | 0.151 | 0.088 J | 0.167 | 0.0026 | 0.0026 | 2.3 J | 0.21 J |
| 06 | 003 | 27421 | 7.0 | 1.08 | 0.75 | 0.76 | 0.0030 | 0.0030 | 6.7 | 0.50 J |
| 06 | 003 | 27436 | 17.0 | 0.187 | 0.204 | 0.173 | 0.0025 | 0.0025 | 1.6 J | 0.13 J |
| 06 | 003 | 27453 | 27.0 | 0.257 | 0.266 | 0.180 | 0.0026 | 0.0026 | 2.9 J | 0.21 J |
| 06 | 003 | 27457 | 30.0 | 0.198 | 0.140 | 0.197 | 0.0026 | 0.0026 | 3.5 J | 0.32 J |
| 06 | 004 | 27318 | 4.0 | 0.65 | 0.69 | 0.410 | 0.0025 | 0.0025 | 4.8 | 0.31 J |
| 06 | 004 | 27335 | 14.0 | 0.261 | 0.211 | 0.213 | 0.0025 | 0.0025 | 1.4 J | 0.19 J |
| 06 | 004 | 27365 | 24.0 | 0.187 | 0.185 | 0.177 | 0.0025 | 0.0025 | 3.3 J | 0.20 J |
| 06 | 004 | 27379 | 30.0 | 0.121 | 0.138 | 0.123 J | 0.0025 | 0.0025 | 2.9 J | 0.38 J |
| 06 | 005 | 26851 | 1.0 | 0.83 | 2.37 | 1.87 | 0.0027 | 0.0024 J | 6.6 | 0.18 J |
| 06 | 005 | 26873 | 11.0 | 0.268 | 0.241 | 0.295 | 0.0025 | 0.0025 | 3.1 J | 0.20 J |
| 06 | 005 | 26899 | 21.0 | 0.235 | 0.220 | 0.227 | 0.0025 | 0.0025 | 1.9 J | 0.17 J |
| 06 | 005 | 26909 | 30.0 | 0.183 | 0.154 | 0.222 | 0.0025 | 0.0025 | 3.0 J | 0.25 J |
| 06 | 006 | 28398 | 1.0 | 0.58 | 0.50 | 0.61 | 0.0025 | 0.0025 | 9.8 | 0.91 |
| 06 | 006 | 28413 | 11.0 | 0.249 | 0.233 | 0.244 | 0.0025 | 0.0025 | 1.3 J | 0.10 J |
| 06 | 006 | 28420 | 21.0 | 0.223 | 0.180 | 0.170 | 0.0025 | 0.0025 | 1.5 J | 0.11 J |
| 06 | 006 | 28427 | 30.0 | 0 | 0.148 | 0.113 | 0.0025 | 0.0025 | 2.4 J | 0.17 J |
| 06 | 007 | 28107 | 7.0 | 0.42 | 0.42 | 0.380 | 0.00071 J | 0.0025 | 1.7 J | 0.15 J |
| 06 | 007 | 28144 | 17.0 | 0.281 | 23.8 | 11.2 | 0.0025 | 0.0025 | 1.9 J | 0.11 J |
| 06 | 007 | 28171 | 27.0 | 0.239 | 29.0 | 15.0 | 0.0025 | 0.0025 | 2.8 J | 0.20 J |
| 06 | 007 | 28173 | 30.0 | 0.44 | 20.7 | 11.5 | 0.0025 | 0.0025 | 2.2 J | 0.15 J |
| 06 | 008 | 27882 | 4.0 | 0.356 | 1.91 | 0.83 | 0.0025 | 0.00061 J | 2.8 J | 0.22 J |
| 06 | 008 | 27911 | 14.0 | 0.147 | 0.236 | 0.175 | 0.0025 | 0.0025 | 1.5 J | 0.17 J |
| 06 | 008 | 27931 | 24.0 | 0.259 | 0.205 | 0.170 | 0.0026 | 0.0026 | 1.8 J | 0.19 J |
| 06 | 008 | 27938 | 30.0 | 0.139 | 0.108 | 0.183 | 0.0026 | 0.0026 | 1.5 J | 0.17 J |
| 06 | 009 | 27682 | 1.0 | 0.97 | 7.40 | 6.06 | 0.0028 | 0.0071 | 330 | 0.41 J |
| 06 | 009 | 27705 | 11.0 | 0.269 | 0.311 | 0.245 | 0.0025 | 0.0025 | 1.8 J | 0.18 J |
| 06 | 009 | 27720 | 21.0 | 0.249 | 0.174 | 0.179 | 0.0026 | 0.0026 | 0.98 J | 0.13 J |
| 06 | 009 | 27743 | 30.0 | 0.149 | 0.149 | 0.128 | 0.0025 | 0.0025 | 1.7 J | 0.13 J |
| 06 | 010 | 27593 | 7.0 | 0.220 | 0.294 | 0.272 | 0.0026 | 0.0026 | 1.4 J | 0.14 J |
| 06 | 010 | 27609 | 17.0 | 0.105 | 0.134 | 0.133 | 0.0026 | 0.0026 | 0.89 J | 0.092 J |
| 06 | 010 | 27635 | 27.0 | 0.181 | 0.159 | 0.127 | 0.0026 | 0.0026 J | 1.3 J | 0.16 J |
| 06 | 010 | 27642 | 30.0 | 0.148 | 0.167 | 0.145 | 0.0026 | 0.0026 J | 1.1 J | 0.17 J |
| 06 | 012 | 28205 | 4.0 | 0.79 | 3.19 | 2.33 | 0.0078 | 0.024 | 5.6 | 0.20 J |
| 06 | 012 | 28223 | 14.0 | 0.172 | 0.208 | 0.164 | 0.0025 | 0.0025 | 1.8 J | 0.12 J |
| 06 | 012 | 28257 | 24.0 | 0.178 | 0.301 | 0.163 | 0.0025 | 0.0025 | 0.99 J | 0.058 J |
| 06 | 012 | 28273 | 30.0 | 0.089 J | 0.185 | 0.117 | 0.0025 | 0.0025 | 1.9 J | 0.12 J |
| 06 | 013 | 28278 | 1.0 | 0.64 | 5.19 | 1.93 | 0.0077 | 0.030 | 7.6 J | 0.34 J |
| 06 | 013 | 28299 | 11.0 | 0.210 | 0.224 | 0.215 | 0.0025 | 0.0025 | 1.2 J | 0.071 J |
| 06 | 013 | 28318 | 21.0 | 0.302 | 0.194 | 0.138 | 0.0025 | 0.0025 | 2.8 J | 0.086 J |
| 06 | 013 | 28326 | 30.0 | 0.240 | 0.175 | 0.166 | 0.0025 | 0.0025 | 3.2 J | 0.087 J |
| 06 | 014 | 27502 | 7.0 | 0.286 | 0.322 | 0.231 | 0.0025 | 0.0025 | 1.3 J | 0.14 J |
| 06 | 014 | 27528 | 17.0 | 0.172 | 0.139 | 0.147 | 0.0025 | 0.0025 | 1.0 J | 0.11 J |
| 06 | 014 | 27555 | 27.0 | 0.168 | 0.156 | 0.167 | 0.0025 | 0.0025 | 1.9 J | 0.24 J |
| 06 | 014 | 27561 | 30.0 | 0.262 | 0.122 | 0.141 | 0.0026 | 0.0026 | 1.4 J | 0.14 J |
| 06 | 015 | 27776 | 4.0 | 1.07 | 4.62 | 4.89 | 0.00054 J | 0.0018 J | 13.1 | 0.49 J |

Table 2
SU06 and SU07 Soil Boring Sample Results
Severn Trent Laboratories, Inc.

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| 06 | 015 | 27791 | 14.0 | 0.259 | 0.164 | 0.182 | 0.0025 | 0.0025 | 1.4 J | 0.11 J |
| 06 | 015 | 27816 | 24.0 | 0.167 | 0.131 | 0.140 | 0.0026 | 0.0026 | 2.5 J | 0.19 J |
| 06 | 015 | 27832 | 30.0 | 0.196 | 0.180 | 0.138 | 0.0025 | 0.0025 | 1.5 J | 0.12 J |
| 06 | 016 | 27060 | 1.0 | 0.72 | 5.76 | 5.42 | 0.0026 J | 0.018 J | 21.7 | 0.30 J |
| 06 | 016 | 27082 | 11.0 | 0.170 | 0.213 | 0.235 | 0.0025 | 0.0025 | 2.3 J | 0.21 J |
| 06 | 016 | 27094 | 21.0 | 0.328 | 0.322 | 0.329 | 0.0025 | 0.0025 | 0.92 J | 0.12 J |
| 06 | 016 | 27117 | 30.0 | 0.225 | 0.128 | 0.145 | 0.0026 | 0.0026 | 1.8 J | 0.22 J |
| 07 | 004 | 29454 | 1.0 | 0.386 | 0.53 | 0.47 | 0.0026 | 0.0026 J | 13.6 | 0.47 J |
| 07 | 004 | 29463 | 11.0 | 0.74 | 0.64 | 0.46 | 0.0026 | 0.0026 J | 9.2 | 0.63 |
| 07 | 004 | 29474 | 21.0 | 0.207 J | 0.220 | 0.154 | 0.0026 | 0.0026 J | 1.0 J | 0.13 J |
| 07 | 004 | 29482 | 30.0 | 0.125 | 0.111 | 0.120 | 0.0026 | 0.0026 J | 2.2 J | 0.16 J |
| 07 | 005 | 29306 | 7.0 | 0.364 | 0.322 | 0.305 | 0.0025 | 0.0025 | 2.3 J | 0.16 J |
| 07 | 005 | 29320 | 17.0 | 0.176 | 0.157 | 0.193 | 0.0026 | 0.0026 | 1.8 J | 0.048 J |
| 07 | 005 | 29334 | 27.0 | 0.201 | 0.162 | 0.178 | 0.0026 | 0.0026 | 1.1 J | 0.084 J |
| 07 | 005 | 29341 | 30.0 | 0.141 | 0.225 | 0.182 | 0.0026 | 0.0026 | 2.1 J | 0.23 J |
| 07 | 006 | 29256 | 4.0 | 0.78 | 0.62 | 0.55 | 0.0025 | 0.0025 | 2.0 J | 0.12 J |
| 07 | 006 | 29269 | 14.0 | 0.248 | 0.296 | 0.271 | 0.0026 | 0.0026 | 2.3 J | 0.084 J |
| 07 | 006 | 29283 | 24.0 | 0.207 | 0.318 | 0.311 | 0.0026 | 0.0026 | 1.1 J | 0.079 J |
| 07 | 006 | 29288 | 30.0 | 0.125 | 0.133 | 0.131 | 0.0026 | 0.0026 | 1.7 J | 0.13 J |
| 07 | 007 | 29209 | 1.0 | 0.73 | 15.3 | 8.8 | 0.0028 | 0.0028 | 19.3 | 0.61 |
| 07 | 007 | 29222 | 11.0 | 0.222 | 0.320 | 0.299 | 0.0026 | 0.0026 | 3.2 J | 0.26 J |
| 07 | 007 | 29237 | 21.0 | 0.145 | 0.229 | 0.171 | 0.0026 | 0.0026 | 1.2 J | 0.074 J |
| 07 | 007 | 29247 | 30.0 | 0.161 | 0.167 | 0.158 | 0.0026 | 0.0026 | 0.98 J | 0.081 J |
| 07 | 012 | 29791 | 7.0 | 0.181 | 0.223 | 0.013 | 0.0025 | 0.0025 J | 1.5 J | 0.14 J |
| 07 | 012 | 29814 | 17.0 | 0.121 | 0.153 | 0.107 | 0.0025 | 0.0025 J | 1.1 J | 0.14 J |
| 07 | 012 | 29833 | 27.0 | 0.179 | 0.155 | 0.176 | 0.0025 | 0.0025 J | 1.2 J | 0.16 J |
| 07 | 012 | 29835 | 30.0 | 0.246 | 0.158 | 0.145 | 0.0025 | 0.0025 J | 4.6 | 0.31 J |
| 07 | 013 | 29717 | 4.0 | 0.57 | 3.04 | 2.70 | 0.0025 | 0.0025 J | 3.4 J | 0.21 J |
| 07 | 013 | 29732 | 14.0 | 0.221 | 0.271 | 0.288 | 0.0025 | 0.0025 J | 2.1 J | 0.24 J |
| 07 | 013 | 29746 | 24.0 | 0.215 | 0.209 | 0.165 | 0.0025 | 0.0025 J | 0.70 J | 0.10 J |
| 07 | 013 | 29754 | 30.0 | 0.177 | 0.109 | 0.013 | 0.0025 | 0.0025 J | 1.6 J | 0.16 J |
| 07 | 014 | 29346 | 1.0 | 0.432 | 26.8 | 26.6 | 0.0025 | 0.0025 J | 5.3 | 0.19 J |
| 07 | 014 | 29355 | 11.0 | 0.153 | 0.340 | 0.300 | 0.0025 | 0.0025 J | 2.3 J | 0.11 J |
| 07 | 014 | 29363 | 21.0 | 0.110 | 0.190 | 0.184 | 0.0025 | 0.0025 J | 1.0 J | 1 |
| 07 | 014 | 29380 | 30.0 | 0.165 | 0.155 | 0.139 | 0.0026 | 0.0026 J | 2.4 J | 0.17 J |
| 07 | 015 | 29127 | 7.0 | 0.392 | 0.297 | 0.219 | 0.0025 | 0.0025 | 1.9 J | 0.13 J |
| 07 | 015 | 29144 | 17.0 | 0.125 | 0.137 | 0.165 | 0.0025 | 0.0025 | 1.0 J | 0.075 J |
| 07 | 015 | 29162 | 27.0 | 0.226 | 0.170 | 0.110 | 0.0026 | 0.0026 | 1.7 J | 0.11 J |
| 07 | 015 | 29165 | 30.0 | 0.129 | 0.167 | 0.132 | 0.0026 | 0.0026 | | |
| 07 | 016 | 29030 | 4.0 | 0.368 | 0.427 | 0.412 | 0.0025 | 0.0025 J | 1.7 J | 0.16 J |
| 07 | 016 | 29039 | 14.0 | 0.73 | 0.270 | 0.258 | 0.0026 | 0.0026 J | 0.68 J | 0.12 J |
| 07 | 016 | 29047 | 24.0 | 0.112 | 0.173 | 0.111 | 0.0026 | 0.0026 J | 0.65 J | 0.069 J |
| 07 | 016 | 29057 | 30.0 | 0.145 | 0.096 J | 0.099 J | 0.0026 | 0.0026 J | 1.1 J | 0.18 J |
| 07 | 017 | 28746 | 1.0 | 0.76 | 24.1 | 11.6 | 0.0027 | 0.0091 | 58.1 | 1.2 J |
| 07 | 017 | 28763 | 11.0 | 0.209 | 0.398 | 0.302 | 0.0025 | 0.0025 | 1.6 J | 0.20 J |
| 07 | 017 | 28772 | 21.0 | 0.233 | 0.152 J | 0.145 J | 0.0026 | 0.0026 | 1.6 J | 0.17 J |
| 07 | 017 | 28793 | 30.0 | 0.129 | 0.119 | 0.099 J | 0.0026 | 0.0026 | 2.4 J | 0.17 J |
| 07 | 018 | 28456 | 7.0 | 0.297 | 0.288 | 0.293 | 0.0025 | 0.0025 | 1.8 J | 0.19 J |
| 07 | 018 | 28475 | 17.0 | 0.219 | 0.169 | 0.230 | 0.0026 | 0.0026 | 4.1 J | 0.17 J |
| 07 | 018 | 28487 | 27.0 | 0.174 | 0.140 | 0.142 | 0.0025 | 0.0025 | 1.0 J | 0.076 J |
| 07 | 018 | 28489 | 30.0 | 0.223 | 0.201 | 0.182 | 0.0026 | 0.0026 | 1.3 J | 0.11 J |
| 07 | 022 | 29656 | 1.0 | 0.56 | 9.5 | 9.3 | 0.0025 | 0.0025 J | 9.9 | 0.42 J |
| 07 | 022 | 29677 | 11.0 | 0.206 | 0.245 | 0.246 | 0.0025 | 0.0025 | 1.3 J | 0.13 J |

Table 2
SU06 and SU07 Soil Boring Sample Results
Severn Trent Laboratories, Inc.

| Survey Unit | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | -234 (pCi/g) | -238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|--------------------|------------------------|------------------|---------------------|-----------------------|---------------------|---------------------|--------------------|--------------------|-------------------|-------------------|
| 07 | 022 | 29692 | 21.0 | 0.169 | 0.345 | 0.262 | 0.0025 | 0.0025 J | 1.5 J | 0.15 J |
| 07 | 022 | 29702 | 30.0 | 0.132 | 0.206 | 0.173 | 0.0025 | 0.0025 J | 1.7 J | 0.17 J |
| 07 | 023 | 29577 | 7.0 | 0.195 | 0.229 | 0.189 | 0.0025 | 0.0025 J | 1.3 J | 0.12 J |
| 07 | 023 | 29586 | 17.0 | 0.153 | 0.217 | 0.131 | 0.0025 | 0.0025 J | 0.97 J | 0.12 J |
| 07 | 023 | 29599 | 27.0 | 0.226 | 0.206 | 0.179 | 0.0025 | 0.0025 J | 2.0 J | 0.28 J |
| 07 | 023 | 29601 | 30.0 | 0.172 | 0.216 | 0.166 | 0.0026 | 0.0026 J | 1.9 J | 0.18 J |
| 07 | 024 | 29403 | 4.0 | 0.38 | 0.48 | 0.53 | 0.0025 | 0.0025 J | 1.2 J | 0.18 J |
| 07 | 024 | 29416 | 14.0 | 0.178 | 0.251 | 0.225 | 0.0025 | 0.0025 J | 1.8 J | 0.19 J |
| 07 | 024 | 29430 | 24.0 | 0.164 | 0.202 | 0.168 | 0.0025 | 0.0025 J | 1.3 J | 0.12 J |
| 07 | 024 | 29442 | 30.0 | 0.155 | 0.190 | 0.161 | 0.0025 | 0.0025 J | 0.62 J | 0.10 J |
| 07 | 025 | 29067 | 1.0 | 0.85 | 2.69 | 2.63 | 0.0025 | 0.0025 | 6.4 | 0.35 J |
| 07 | 025 | 29085 | 11.0 | 0.373 | 0.390 | 0.322 | 0.0025 | 0.0025 | 0.60 J | 0.10 J |
| 07 | 025 | 29099 | 21.0 | 0.185 | 0.216 | 0.179 | 0.0025 | 0.0025 | 1.6 J | 0.10 J |
| 07 | 025 | 29107 | 30.0 | 0.120 J | 0.201 | 0.213 | 0.0026 | 0.0026 | 2.1 J | 0.16 J |
| 07 | 026 | 28844 | 7.0 | 0.365 | 0.236 | 0.256 | 0.0025 | 0.0025 | 0.91 J | 0.069 J |
| 07 | 026 | 28858 | 17.0 | 0.104 | 0.114 | 0.125 | 0.0025 | 0.0025 | 1.0 J | 0.077 J |
| 07 | 026 | 28875 | 27.0 | 0.131 | 0.114 | 0.092 J | 0.0025 | 0.0025 | 1.1 J | 0.14 J |
| 07 | 026 | 28877 | 30.0 | 0.115 | 0.129 | 0.087 J | 0.0025 | 0.0025 | 1.7 J | 0.092 J |
| 07 | 027 | 28517 | 4.0 | 0.52 | 0.97 | 0.294 | 0.0025 | 0.0025 | 1.7 J | 0.13 J |
| 07 | 027 | 28525 | 14.0 | 0.270 | 0.257 | 0.209 | 0.0025 | 0.0025 | 1.4 J | 0.15 J |
| 07 | 027 | 28538 | 24.0 | 0.227 | 0.124 | 0.170 | 0.0025 | 0.0025 | 0.79 J | 0.10 J |
| 07 | 027 | 28551 | 30.0 | 0.244 | 0.194 | 0.145 | 0.0025 | 0.0025 | 0.63 J | 0.14 J |
| 07 | 031 | 29620 | 4.0 | 0.455 | 0.411 | 0.397 | 0.0025 | 0.0025 J | 3.0 J | 0.15 J |
| 07 | 031 | 29636 | 14.0 | 0.218 | 0.248 | 0.178 | 0.0025 | 0.0025 J | 1.4 J | 0.20 J |
| 07 | 031 | 29649 | 24.0 | 0.152 | 0.167 | 0.139 | 0.0025 | 0.0025 J | 1.1 J | 0.16 J |
| 07 | 031 | 29654 | 30.0 | 0.130 | 0.143 | 0.136 | 0.0025 | 0.0025 J | 1.8 J | 0.19 J |
| 07 | 032 | 29545 | 1.0 | 0.69 | 18.5 | 18.9 | 0.0027 | 0.0027 J | 23.9 | 0.37 J |
| 07 | 032 | 29553 | 11.0 | 0.252 | 0.423 | 0.386 | 0.0026 | 0.0026 J | 2.2 J | 0.15 J |
| 07 | 032 | 29561 | 21.0 | 0.167 | 0.201 | 0.178 | 0.0025 | 0.0025 J | 1.3 J | 0.17 J |
| 07 | 032 | 29569 | 30.0 | 0.126 | 0.184 | 0.166 | 0.0025 | 0.0025 J | 1.7 J | 0.18 J |
| 07 | 033 | 29500 | 7.0 | 0.52 | 0.38 | 0.282 | 0.0026 | 0.0026 J | 1.2 J | 0.16 J |
| 07 | 033 | 29516 | 17.0 | 0.184 | 0.117 | 0.178 | 0.0025 | 0.0025 J | 0.80 J | 0.15 J |
| 07 | 033 | 29531 | 27.0 | 0.157 | 0.151 | 0.156 | 0.0025 | 0.0025 J | 1.1 J | 0.13 J |
| 07 | 033 | 29533 | 31.0 | 0.097 J | 0.116 | 0.130 | 0.0025 | 0.0025 J | 1.4 J | 0.17 J |
| 07 | 034 | 28969 | 4.0 | 0.57 | 0.386 | 0.322 | 0.0026 | 0.0026 | 2.1 J | 0.21 J |
| 07 | 034 | 28979 | 14.0 | 0.298 | 0.228 | 0.234 | 0.0025 | 0.0025 J | 1.7 J | 0.13 J |
| 07 | 034 | 28994 | 24.0 | 0.346 | 0.234 | 0.238 | 0.0026 | 0.0026 J | 0.36 J | 0.082 J |
| 07 | 034 | 29004 | 30.0 | 0.220 | 0.165 | 0.160 | 0.0025 | 0.0025 J | 1.4 J | 0.15 J |
| 07 | 035 | 28902 | 1.0 | 0.93 | 32.4 | 10.3 | 0.0016 J | 0.022 | 15.1 | 0.37 J |
| 07 | 035 | 28916 | 11.0 | 0.294 | 0.307 | 0.337 | 0.0025 | 0.0025 | 1.8 J | 0.096 J |
| 07 | 035 | 28929 | 21.0 | 0.131 | 0.166 | 0.220 | 0.0026 | 0.0026 | 0.95 J | 0.11 J |
| 07 | 035 | 28944 | 30.0 | 0.282 | 0.206 | 0.262 | 0.0026 | 0.0026 | 1.3 J | 0.17 J |

Table 2
SU06 and SU07 Soil Boring Sample Results
Severn Trent Laboratories, Inc.

Analytics:

| | |
|-----------------------|-------------------------|
| Th-232 - Thorium-232 | PCE - Tetrachloroethene |
| U-234 - Uranium-234 | Ni - Nickel |
| U-238 - Uranium-238 | Be - Beryllium |
| TCE - Trichloroethene | |

Units:

pCi/g - picoCurie/gram
mg/kg - milligram/kilogram

Qualifiers:

U - Validation qualifier used to indicate that the result was qualified as non-detect.
J - Validation qualifier used to indicate that the result is considered an estimate.
UJ - Validation qualifier used to indicate that the result was qualified as non-detect and the associated reporting limit is considered an estimate.

Notes:

See Figure 1 for boring locations.

Table 3
LPH Soil Boring Sample Results

| Subcell | LPH | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|------------|-----------|-----------------|--------------|--------------|----------------|---------------|---------------|-----------------|-----------------|---------------|---------------|
| E08 | 34 | 01 | 28631 | 1.0 | 0.63 | | 1.01 UJ | | | <100 | |
| E08 | 34 | 01 | 28632 | 2.0 | 0.57 | | 2.21 | | | | |
| E08 | 34 | 01 | 28639 | 3.0 | 0.62 | | 4.22 | | | <100 | |
| E08 | 34 | 01 | 28640 | 4.0 | 0.63 | | 4.01 | | | | |
| E08 | 34 | 01 | 28645 | 5.0 | 0.34 | | 2.61 J | | | <100 | |
| E08 | 34 | 01 | 28646 | 6.0 | 0.42 | | 1.11 J | | | | |
| E08 | 34 | 01 | 28651 | 7.0 | 0.66 | | 2.28 J | | | <100 | |
| E08 | 34 | 01 | 28663 | 8.0 | 0.31 | | 0.50 J | | | | |
| E08 | 34 | 01 | 28664 | 9.0 | 0.33 | | 0.88 J | | | <100 | |
| E08 | 34 | 01 | 28667 | 10.0 | 0.37 | | 1.33 J | | | | |
| E08 | 34 | 01 | 28682 | 11.0 | 0.32 | | 1.08 J | | | <100 | |
| E08 | 34 | 01 | 28687 | 12.0 | 0.29 | | 0.70 J | | | | |
| E08 | 34 | 01 | 28694 | 13.0 | 0.42 | | 1.45 J | | | <100 | |
| E08 | 34 | 01 | 28695 | 14.0 | 0.27 | | 0.62 J | | | | |
| E08 | 34 | 01 | 28698 | 15.0 | 0.22 | | 0.92 J | | | <100 | |
| E08 | 34 | 01 | 28699 | 16.0 | 0.23 | | 1.37 | | | | |
| E08 | 34 | 01 | 28708 | 17.0 | 0.20 | | 0.62 J | | | <100 | |
| E08 | 34 | 01 | 28717 | 18.0 | 0.20 | | 4.00 J | | | | |
| E08 | 34 | 01 | 28723 | 19.0 | 0.23 | | 3.97 J | | | <100 | |
| E08 | 34 | 01 | 28732 | 20.0 | 0.23 | | 2.48 J | | | | |
| E08 | 34 | 01 | 28801 | 21.0 | 0.21 J | | 2.35 | | | <100 | |
| E08 | 34 | 01 | 28802 | 22.0 | 0.17 J | | 2.19 | | | | |
| E08 | 34 | 01 | 28803 | 23.0 | 0.23 | | 1.05 J | | | <100 | |
| E08 | 34 | 01 | 28811 | 24.0 | 0.18 J | | 1.08 | | | | |
| E08 | 34 | 01 | 28823 | 25.0 | 0.27 | | 0.59 J | | | <100 | |
| E08 | 34 | 01 | 28829 | 26.0 | 0.47 J | | 1.04 J | | | | |
| E08 | 34 | 01 | 28835 | 27.0 | 0.24 | | 0.44 J | | | <100 | |
| E08 | 34 | 01 | 28848 | 28.0 | 0.15 | | 0.40 | | | | |
| E08 | 34 | 01 | 28847 | 29.0 | 0.25 | | 0.72 J | | | <100 | |
| E08 | 34 | 01 | 28850 | 30.0 | 0.194 | 0.187 | 0.179 | 0.0026 U | 0.0026 U | 2.3 J | 0.17 J |
| E08 | 34 | 04 | 27455 | 1.0 | 0.66 | | 5.13 | | | <100 | |
| E08 | 34 | 04 | 27456 | 3.0 | NS | | NS | | | <100 | |
| E08 | 34 | 04 | 27461 | 9.0 | NS | | NS | | | <100 | |
| E08 | 34 | 04 | 27462 | 10.0 | 0.10 | | 5.66 | 0.0025 U | 0.0025 U | | |
| E08 | 34 | 04 | 27463 | 14.0 | 0.25 | | 1.11 | 0.094 | 0.094 | | |
| E08 | 34 | 04 | 27464 | 15.0 | 0.31 J | | 6.70 | | | <100 | |
| E08 | 34 | 04 | 27467 | 16.0 | 0.22 | | 5.87 | 0.113 | 0.113 | | |
| E08 | 34 | 04 | 27468 | 17.0 | 0.17 | | 3.94 | | | <100 | |
| E08 | 34 | 04 | 27469 | 18.0 | 0.31 | | 6.06 | 0.112 | 0.112 | | |
| E08 | 34 | 04 | 27470 | 19.0 | 0.17 | | 4.17 | | | <100 | |
| E08 | 34 | 04 | 27479 | 20.0 | 0.28 | | 5.01 | 0.0025 U | 0.0025 U | | |
| E08 | 34 | 04 | 27480 | 21.0 | 0.28 | | 4.41 | | | <100 | |
| E08 | 34 | 04 | 27481 | 22.0 | 0.22 | | 3.39 | 0.111 | 0.111 | | |
| E08 | 34 | 04 | 27482 | 23.0 | 0.17 | | 3.06 | | | <100 | |
| E08 | 34 | 04 | 27483 | 24.0 | 0.13 J | | 2.66 | 0.131 | 0.131 | | |
| E08 | 34 | 04 | 27484 | 25.0 | 0.24 | | 3.58 | | | <100 | |
| E08 | 34 | 04 | 27490 | 26.0 | 0.19 J | | 2.74 | 0.107 | 0.107 | | |
| E08 | 34 | 04 | 27491 | 27.0 | 0.16 | | 0.77 | | | <100 | |
| E08 | 34 | 04 | 27492 | 28.0 | 0.24 | | 9.45 | 0.109 | 0.109 | | |
| E08 | 34 | 04 | 27493 | 29.0 | 0.24 J | | 4.01 | | | <100 | |
| E08 | 34 | 04 | 27494 | 30.0 | 0.167 J | 4.47 | 4.41 | 0.0025 U | 0.0025 U | 0.14 J | 5.7 |
| E08 | 34 | 04 | 27506 | 32.0 | 0.18 | | 0.84 | 0.112 | 0.112 | | |
| E08 | 34 | 04 | 27507 | 33.0 | 0.19 | | 0.80 | | | <100 | |

Table 3
LPH Soil Boring Sample Results

| Subcell | LPH | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|---------|-----|-----------------|--------------|--------------|----------------|---------------|---------------|-----------------|------------------|---------------|----------------|
| E08 | 34 | 04 | 27508 | 34.0 | 0.22 | | 2.40 | 0.109 | 0.109 | | |
| E08 | 34 | 04 | 27509 | 35.0 | 0.19 | | 0.67 J | | | <100 | |
| E08 | 34 | 04 | 27515 | 36.0 | 0.04 | | 1.02 | 0.115 | 0.115 | | |
| E08 | 34 | 04 | 27516 | 37.0 | 0.24 J | | 0.94 | | | <100 | |
| E08 | 34 | 04 | 27517 | 38.0 | 0.02 UJ | | 0.24 | 0.115 | 0.115 | | |
| E08 | 34 | 04 | 27518 | 39.0 | 0.22 J | | 0.43 | | | <100 | |
| E08 | 34 | 04 | 27519 | 40.0 | 0.21 J | | 0.60 J | 0.0026 U | 0.0026 U | | |
| E08 | 34 | 04 | 27520 | 41.0 | 0.10 J | | 0.69 J | | | <100 | |
| E08 | 34 | 04 | 27527 | 42.0 | 0.17 J | | 0.73 | 0.116 | 0.116 | | |
| E08 | 34 | 04 | 27536 | 43.0 | 0.48 J | | 1.02 J | | | <100 | |
| E08 | 34 | 04 | 27537 | 44.0 | 0.46 J | | 0.57 | 0.115 | 0.115 | | |
| E08 | 34 | 04 | 27538 | 45.0 | 0.33 J | | 0.50 | | | <100 | |
| E08 | 34 | 04 | 27539 | 46.0 | 0.29 J | | 0.60 J | 0.135 | 0.135 | | |
| E08 | 34 | 04 | 27540 | 47.0 | 0.30 J | | 1.78 | | | <100 | |
| E08 | 34 | 04 | 27541 | 48.0 | 1.33 J | | 2.27 | 0.098 | 0.098 | | |
| E08 | 34 | 04 | 27542 | 49.0 | 1.12 J | | 3.15 | | | <100 | |
| E08 | 34 | 04 | 27545 | 50.0 | 0.82 J | | 2.22 J | 0.0030 U | 0.00089 U | | |
| E08 | 34 | 04 | 27546 | 51.0 | 0.67 J | | 2.39 J | | | <100 | |
| E08 | 34 | 04 | 27547 | 52.0 | 0.75 J | | 1.10 J | 0.093 | 0.093 | | |
| E08 | 34 | 04 | 27548 | 53.0 | 0.61 J | | 0.57 | | | <100 | |
| E08 | 34 | 04 | 27551 | 54.0 | 0.61 J | | 1.16 J | 0.115 | 0.115 | | |
| E08 | 34 | 04 | 27552 | 55.0 | 0.52 J | | 0.64 | | | <100 | |
| E08 | 34 | 04 | 27553 | 56.0 | 0.33 J | | 1.17 J | 0.111 | 0.111 | | |
| E08 | 34 | 04 | 27554 | 57.0 | 0.34 J | | 0.94 J | | | <100 | |
| E08 | 34 | 04 | 27557 | 58.0 | 0.41 J | | 2.11 | 0.112 | 0.112 | | |
| E08 | 34 | 04 | 27558 | 59.0 | 0.46 J | | 1.54 J | | | <100 | |
| E08 | 34 | 04 | 27559 | 60.0 | 0.54 J | | 1.30 | 0.115 | 0.115 | | |
| E08 | 34 | 04 | 27560 | 61.0 | 0.27 J | | 0.89 J | | | <100 | |
| E08 | 34 | 04 | 27562 | 62.0 | 0.36 J | | 0.70 J | 0.124 | 0.124 | | |
| E08 | 34 | 04 | 27563 | 63.0 | 0.32 J | | 1.89 | | | <100 | |
| E08 | 34 | 04 | 27564 | 64.0 | 0.50 J | 0.212 | 0.138 | 0.0027 U | 0.0027 U | 0.47 J | 0.072 J |
| E08 | 34 | 05 | 28751 | 1.0 | 0.71 | | 5.94 J | | | <100 | |
| E08 | 34 | 05 | 28752 | 2.0 | 0.87 | | 6.99 J | | | | |
| E08 | 34 | 05 | 28755 | 3.0 | 0.80 | | 7.10 J | | | <100 | |
| E08 | 34 | 05 | 28800 | 4.0 | 0.39 J | | 1.12 J | | | | |
| E08 | 34 | 05 | 28863 | 5.0 | 0.65 J | | 5.08 | | | <100 | |
| F08 | 34 | 03 | 29838 | 2.0 | 0.42 | | 2.79 | | | | |
| F08 | 34 | 03 | 29839 | 3.0 | 0.33 | | 1.37 J | | | <100 | |
| F08 | 34 | 03 | 29840 | 4.0 | 0.30 | | 1.17 | | | | |
| F08 | 34 | 03 | 29841 | 5.0 | 0.89 | | 1.72 J | | | <100 | |
| F08 | 34 | 03 | 29844 | 7.0 | 0.54 | | 1.69 | | | <100 | |
| F08 | 34 | 03 | 29845 | 8.0 | 0.35 | | 0.47 | | | | |
| F08 | 34 | 03 | 29846 | 9.0 | 0.33 | | 1.33 J | | | <100 | |
| F08 | 34 | 03 | 29856 | 10.0 | 0.09 | | 1.12 J | | | | |
| F08 | 34 | 03 | 29857 | 11.0 | 0.28 | | 1.52 J | | | <100 | |
| F08 | 34 | 03 | 29860 | 12.0 | 0.34 | | 1.93 J | | | | |
| F08 | 34 | 03 | 29861 | 13.0 | 0.30 | | 0.65 J | | | <100 | |
| F08 | 34 | 03 | 29863 | 14.0 | 0.26 | | 0.27 | | | | |
| F08 | 34 | 03 | 29864 | 15.0 | 0.19 | | 0.33 | | | <100 | |
| F08 | 34 | 03 | 29865 | 16.0 | 0.33 | | 1.50 | | | | |
| F08 | 34 | 03 | 29866 | 17.0 | 0.20 | | 0.90 J | | | <100 | |
| F08 | 34 | 03 | 29873 | 18.0 | 0.29 | | 0.49 | | | | |
| F08 | 34 | 03 | 29874 | 19.0 | 0.28 | | 1.50 | | | <100 | |

Table 3
LPH Soil Boring Sample Results

| Subcell | LPH | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|----------------|------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| F08 | 34 | 03 | 29875 | 20.0 | 0.46 | | 1.67 J | | | | |
| F08 | 34 | 03 | 29876 | 21.0 | 0.27 | | 0.96 J | | | <100 | |
| F08 | 34 | 03 | 29879 | 22.0 | 0.27 | | 1.29 J | | | | |
| F08 | 34 | 03 | 29880 | 23.0 | 0.28 | | 0.82 J | | | <100 | |
| F08 | 34 | 03 | 29884 | 24.0 | 0.36 | | 1.11 J | | | | |
| F08 | 34 | 03 | 29885 | 25.0 | 0.31 | | 0.53 | | | <100 | |
| F08 | 34 | 03 | 29886 | 26.0 | 0.25 | | 0.81 J | | | | |
| F08 | 34 | 03 | 29887 | 27.0 | 0.30 | | 0.93 J | | | <100 | |
| F08 | 34 | 03 | 29888 | 28.0 | 0.22 | | 1.21 | | | | |
| F08 | 34 | 03 | 29889 | 29.0 | 0.22 | | 0.48 | | | <100 | |
| F08 | 34 | 03 | 29890 | 30.0 | 0.140 | 0.117 | 0.084 J | 0.0025 U | 0.0025 UJ | 2.1 J | 1.0 |
| I06 | 21 | 01 | 19179 | 3.0 | NS | | NS | | | <100 | |
| I06 | 21 | 01 | 19187 | 5.0 | 0.80 | | 6.43 | | | <100 | |
| I06 | 21 | 01 | 19188 | 7.0 | 1.23 | | 33.35 | | | <100 | |
| I06 | 21 | 01 | 19197 | 9.0 | 0.85 | | 35.34 | | | <100 | |
| I06 | 21 | 01 | 19200 | 11.0 | 0.90 | | 39.73 | | | <100 | |
| I06 | 21 | 01 | 19201 | 12.0 | 0.65 | | 35.82 | | | | |
| I06 | 21 | 01 | 19202 | 13.0 | 1.09 | | 45.44 | | | <100 | |
| I06 | 21 | 01 | 19207 | 15.0 | 1.08 | | 46.15 | | | 43.3 J | |
| I06 | 21 | 01 | 19221 | 16.0 | 20.5 | 612 | 82 | 1600 | 40000 J | 125 J | 0.86 U |
| I06 | 21 | 01 | 19222 | 19.0 | 3.35 | | 11.49 | 33.412 | 1344.441 J | <100 | |
| I06 | 21 | 01 | 19227 | 21.0 | 0.75 | | 5.69 | 0.117 | 0.337 | <100 | |
| I06 | 21 | 01 | 19240 | 22.0 | NS | | NS | 0.113 | 0.219 | | |
| I06 | 21 | 01 | 19239 | 23.0 | 0.78 | | 5.27 J | | | <100 | |
| I06 | 21 | 01 | 19261 | 25.0 | 0.50 | | 4.33 | | | | |
| I06 | 21 | 01 | 19265 | 26.0 | 0.53 | | 1.15 | | | | |
| I06 | 21 | 01 | 19266 | 27.0 | 1.16 | | 16.82 J | | | | |
| I06 | 21 | 01 | 19278 | 29.0 | 0.34 | | 1.17 | | | | |
| I06 | 21 | 01 | 19279 | 30.0 | 0.250 | 7.27 | 4.74 | 0.0026 U | 0.0026 R | 2.4 J | 0.51 U |
| I06 | 21 | 02 | 19588 | 1.0 | 0.77 | | 7.18 J | | | <100 | |
| I06 | 21 | 02 | 19589 | 2.0 | 0.84 | | 4.74 J | | | | |
| I06 | 21 | 02 | 19590 | 3.0 | 1.40 J | | 1.51 | | | <100 | |
| I06 | 21 | 02 | 19599 | 4.0 | 0.40 | | 2.50 J | | | | |
| I06 | 21 | 02 | 19600 | 5.0 | 0.37 | | 1.07 J | | | <100 | |
| I06 | 21 | 02 | 19605 | 6.0 | 0.35 | | 0.96 J | | | | |
| I06 | 21 | 02 | 19606 | 7.0 | 0.56 | | 2.35 J | | | <100 | |
| I06 | 21 | 02 | 19611 | 8.0 | 0.77 | | 4.00 | | | | |
| I06 | 21 | 02 | 19612 | 9.0 | 0.36 | | 1.22 J | | | <100 | |
| I06 | 21 | 02 | 19613 | 10.0 | 0.29 | | 2.49 J | | | | |
| I06 | 21 | 02 | 19614 | 11.0 | 0.32 | | 1.61 J | | | <100 | |
| I06 | 21 | 02 | 19616 | 12.0 | 0.30 J | | 2.21 | | | | |
| I06 | 21 | 02 | 19617 | 13.0 | 0.43 J | | 0.80 | | | <100 | |
| I06 | 21 | 02 | 19618 | 14.0 | 0.22 | | 7.63 J | | | | |
| I06 | 21 | 02 | 19619 | 15.0 | 0.30 | | 9.07 J | | | <100 | |
| I06 | 21 | 02 | 19620 | 16.0 | 0.22 | | 9.73 | | | | |
| I06 | 21 | 02 | 19621 | 17.0 | 0.51 J | | 14.93 | | | <100 | |
| I06 | 21 | 02 | 19622 | 18.0 | 0.41 | | 7.88 J | | | | |
| I06 | 21 | 02 | 19623 | 19.0 | 0.20 | | 8.37 J | | | <100 | |
| I06 | 21 | 02 | 19624 | 21.0 | 0.42 | | 15.16 | | | <100 | |
| I06 | 21 | 02 | 19625 | 22.0 | 0.45 J | | 8.24 | | | | |
| I06 | 21 | 02 | 19626 | 23.0 | 0.34 | | 9.36 | | | <100 | |
| I06 | 21 | 02 | 19627 | 25.0 | 0.04 UJ | | 10.85 | | | <100 | |
| I06 | 21 | 02 | 19628 | 26.0 | 0.27 | | 11.38 | | | | |

Table 3
LPH Soil Boring Sample Results

| Subcell | LPH | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TGE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|------------|-----------|-----------------|--------------|--------------|----------------|---------------|---------------|-----------------|-----------------|--------------|----------------|
| I06 | 21 | 02 | 19629 | 27.0 | 0.06 UJ | | 13.78 | | | <100 | |
| I06 | 21 | 02 | 19637 | 28.0 | 0.32 J | | 15.68 | | | | |
| I06 | 21 | 02 | 19638 | 29.0 | 0.15 | | 9.09 | | | <100 | |
| I06 | 21 | 02 | 19641 | 30.0 | 0.132 | 6.58 | 5.97 | 0.0026 U | 0.0026 U | 1.6 J | 0.089 J |
| I06 | 21 | 03 | 19315 | 2.0 | 1.00 | | 16.87 J | | | | |
| I06 | 21 | 03 | 19316 | 3.0 | 1.15 | | 14.63 | | | <100 | |
| I06 | 21 | 03 | 19335 | 4.0 | 0.50 | | 11.59 | | | | |
| I06 | 21 | 03 | 19336 | 5.0 | 0.10 | | 11.55 | | | <100 | |
| I06 | 21 | 03 | 19342 | 6.0 | 0.33 | | 1.91 J | | | | |
| I06 | 21 | 03 | 19343 | 7.0 | 0.55 | | 2.65 | | | <100 | |
| I06 | 21 | 03 | 19348 | 9.0 | 0.90 | | 3.49 | | | <100 | |
| I06 | 21 | 03 | 19354 | 11.0 | 0.30 | | 2.96 | | | <100 | |
| I06 | 21 | 03 | 19359 | 12.0 | 0.36 | | 4.41 | | | | |
| I06 | 21 | 03 | 19360 | 13.0 | 0.30 | | 3.87 | | | <100 | |
| I06 | 21 | 03 | 19365 | 15.0 | 1.00 | | 10.93 | | | <100 | |
| I06 | 21 | 03 | 19371 | 16.0 | 1.30 | | 11.77 | | | | |
| I06 | 21 | 03 | 19372 | 17.0 | 2.44 | | 14.97 | | | <100 | |
| I06 | 21 | 03 | 19379 | 18.0 | 1.40 | | 9.13 | | | | |
| I06 | 21 | 03 | 19380 | 19.0 | 1.40 | | 3.47 | | | <100 | |
| I06 | 21 | 03 | 19384 | 20.0 | 1.36 | | 5.37 | | | | |
| I06 | 21 | 03 | 19385 | 21.0 | 0.85 | | 0.97 | | | <100 | |
| I06 | 21 | 03 | 19390 | 22.0 | 1.10 | | 10.74 | | | | |
| I06 | 21 | 03 | 19391 | 23.0 | 0.99 | | 7.34 | | | <100 | |
| I06 | 21 | 03 | 19407 | 25.0 | 0.88 | | 14.70 | | | <100 | |
| I06 | 21 | 03 | 19408 | 26.0 | 0.92 | | 17.11 | | | | |
| I06 | 21 | 03 | 19409 | 27.0 | 0.98 | | 22.38 | | | <100 | |
| I06 | 21 | 03 | 19420 | 28.0 | 0.68 | | 13.89 | | | | |
| I06 | 21 | 03 | 19421 | 29.0 | 0.46 | | 17.87 | | | <100 | |
| I06 | 21 | 03 | 19422 | 30.0 | 0.63 | 22.3 | 13.9 | 0.0026 U | 0.0026 R | 2.2 J | 0.12 J |
| I06 | 21 | 04 | 19497 | 3.0 | 1.45 | | 9.54 | | | <100 | |
| I06 | 21 | 04 | 19502 | 5.0 | 0.53 | | 1.49 | | | <100 | |
| I06 | 21 | 04 | 19503 | 6.0 | 0.51 | | 2.75 | | | | |
| I06 | 21 | 04 | 19504 | 7.0 | 0.69 | | 6.53 | | | <100 | |
| I06 | 21 | 04 | 19514 | 9.0 | 0.34 | | 1.04 J | | | <100 | |
| I06 | 21 | 04 | 19520 | 11.0 | 0.27 | | 3.18 | | | <100 | |
| I06 | 21 | 04 | 19521 | 12.0 | 0.20 | | 0.49 | | | | |
| I06 | 21 | 04 | 19522 | 13.0 | 0.48 | | 4.07 | | | <100 | |
| I06 | 21 | 04 | 19525 | 15.0 | 0.71 | | 3.76 | | | <100 | |
| I06 | 21 | 04 | 19526 | 16.0 | 0.78 | | 6.14 | | | | |
| I06 | 21 | 04 | 19529 | 17.0 | 1.62 | | 6.44 | | | <100 | |
| I06 | 21 | 04 | 19530 | 19.0 | 1.01 | | 6.18 | | | <100 | |
| I06 | 21 | 04 | 19528 | 21.0 | 0.72 | | 5.80 | | | <100 | |
| I06 | 21 | 04 | 19531 | 22.0 | 0.79 | | 2.49 | | | | |
| I06 | 21 | 04 | 19532 | 23.0 | 1.10 | | 3.97 | | | <100 | |
| I06 | 21 | 04 | 19538 | 25.0 | 0.99 | | 5.30 | | | <100 | |
| I06 | 21 | 04 | 19539 | 26.0 | 1.22 J | | 3.18 | | | | |
| I06 | 21 | 04 | 19540 | 27.0 | 2.77 | | 5.01 | | | <100 | |
| I06 | 21 | 04 | 19541 | 28.0 | 1.25 | | 3.96 J | | | | |
| I06 | 21 | 04 | 19542 | 29.0 | 1.12 | | 4.81 J | | | <100 | |
| I06 | 21 | 04 | 19578 | 30.0 | 0.62 | 13.4 | 8.07 | 0.0026 U | 0.0026 U | 1.3 J | 0.51 U |
| I06 | 21 | 05 | 19692 | 2.0 | 1.01 | | 18.35 | | | | |
| I06 | 21 | 05 | 19693 | 3.0 | 0.77 | | 9.66 | | | <100 | |
| I06 | 21 | 05 | 19694 | 4.0 | 0.76 | | 11.93 | | | | |

Table 3
LPH Soil Boring Sample Results

| Subcell | LPH | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|---------|-----|-----------------|--------------|--------------|----------------|----------------|---------------|-----------------|-----------------|--------------|---------------|
| I06 | 21 | 05 | 19695 | 5.0 | 2.97 | | 27.44 | | | <100 | |
| I06 | 21 | 05 | 19696 | 7.0 | 2.74 | | 46.94 | | | <100 | |
| I06 | 21 | 05 | 19697 | 9.0 | 0.93 | | 15.38 | | | <100 | |
| I06 | 21 | 05 | 19698 | 10.0 | 2.33 | | 59.20 | | | | |
| I06 | 21 | 05 | 19699 | 11.0 | 3.22 | | 33.89 | | | <100 | |
| I06 | 21 | 05 | 19703 | 13.0 | NS | | NS | | | <100 | |
| I06 | 21 | 05 | 19704 | 14.0 | 0.90 | | 3.75 | | | | |
| I06 | 21 | 05 | 19705 | 15.0 | 1.58 | | 7.06 | | | <100 | |
| I06 | 21 | 05 | 19706 | 16.0 | 1.54 | | 16.18 | | | | |
| I06 | 21 | 05 | 19707 | 17.0 | 1.14 | | 9.20 | | | <100 | |
| I06 | 21 | 05 | 19721 | 18.0 | 0.86 | | 7.55 | | | | |
| I06 | 21 | 05 | 19722 | 19.0 | 1.04 | | 13.45 | | | <100 | |
| I06 | 21 | 05 | 19723 | 21.0 | 1.00 | | 6.97 | | | <100 | |
| I06 | 21 | 05 | 19728 | 22.0 | 1.04 | | 7.08 | | | | |
| I06 | 21 | 05 | 19729 | 23.0 | 1.14 | | 4.02 | | | <100 | |
| I06 | 21 | 05 | 19737 | 24.0 | 1.27 | | 3.99 | | | | |
| I06 | 21 | 05 | 19738 | 25.0 | 0.98 | | 1.55 | | | <100 | |
| I06 | 21 | 05 | 19747 | 26.0 | 1.89 | | 4.04 | | | | |
| I06 | 21 | 05 | 19748 | 27.0 | 2.45 | | 3.79 | | | <100 | |
| I06 | 21 | 05 | 19753 | 28.0 | 1.33 | | 3.86 | | | | |
| I06 | 21 | 05 | 19754 | 29.0 | 1.65 | | 2.33 | | | <100 | |
| I06 | 21 | 05 | 19768 | 30.0 | 0.150 | 0.166 | 0.147 | 0.0025 U | 0.0025 U | 1.8 J | 0.51 U |
| I06 | 21 | 06 | 20602 | 1.0 | 0.82 | | 5.64 J | | | <100 | |
| I06 | 21 | 06 | 20603 | 2.0 | 0.93 | | 2.08 | | | | |
| I06 | 21 | 06 | 20604 | 3.0 | 1.02 | | 2.43 | | | <100 | |
| I06 | 21 | 06 | 20605 | 5.0 | 0.42 | | 14.28 | | | <100 | |
| I06 | 21 | 06 | 20607 | 6.0 | 0.37 | | 11.39 | | | | |
| I06 | 21 | 06 | 20608 | 7.0 | 0.53 | | 16.60 | | | <100 | |
| I06 | 21 | 06 | 20614 | 8.0 | 1.07 | | 13.41 | | | | |
| I06 | 21 | 06 | 20615 | 9.0 | 0.50 | | 3.36 J | | | <100 | |
| I06 | 21 | 06 | 20623 | 11.0 | 0.41 | | 1.20 J | | | <100 | |
| I06 | 21 | 06 | 20624 | 13.0 | 0.27 | | 2.84 | | | <100 | |
| I06 | 21 | 06 | 20652 | 15.0 | 0.36 | | 1.34 J | | | <100 | |
| I06 | 21 | 06 | 20653 | 16.0 | 0.32 | | 3.17 J | | | | |
| I06 | 21 | 06 | 20654 | 17.0 | 0.34 | | 3.82 | | | <100 | |
| I06 | 21 | 06 | 20661 | 19.0 | 0.29 | | 1.27 J | | | <100 | |
| I06 | 21 | 06 | 20662 | 21.0 | 0.27 | | 1.89 | | | <100 | |
| I06 | 21 | 06 | 20678 | 22.0 | 0.17 | | 1.09 J | | | | |
| I06 | 21 | 06 | 20679 | 23.0 | 0.25 | | 0.62 J | | | <100 | |
| I06 | 21 | 06 | 20684 | 25.0 | 0.02 | | 0.48 J | | | <100 | |
| I06 | 21 | 06 | 20685 | 26.0 | 0.02 | | 0.79 J | | | | |
| I06 | 21 | 06 | 20686 | 27.0 | 0.23 | | 0.51 | | | <100 | |
| I06 | 21 | 06 | 20689 | 29.0 | 0.04 | | 0.36 J | | | <100 | |
| I06 | 21 | 06 | 20700 | 30.0 | 0.137 | 0.097 J | 0.137 | 0.0025 U | 0.0025 U | 1.6 J | 0.14 J |
| I06 | 21 | 07 | 20709 | 1.0 | 0.60 | | 1.20 | | | <100 | |
| I06 | 21 | 07 | 20711 | 2.0 | 1.25 | | 8.38 | | | | |
| I06 | 21 | 07 | 20712 | 3.0 | 0.88 | | 3.16 | | | <100 | |
| I06 | 21 | 07 | 20713 | 5.0 | 0.41 | | 1.56 | | | <100 | |
| I06 | 21 | 07 | 20719 | 6.0 | 0.60 | | 1.93 | | | | |
| I06 | 21 | 07 | 20720 | 7.0 | 0.49 | | 1.51 | | | 43.1 J | |
| I06 | 21 | 07 | 20731 | 9.0 | 0.77 | | 0.85 J | | | <100 | |
| I06 | 21 | 07 | 20732 | 11.0 | 0.29 | | 2.57 | | | <100 | |
| I06 | 21 | 07 | 20751 | 13.0 | 0.05 | | 0.58 | | | <100 | |

Table 3
LPH Soil Boring Sample Results

| Subcell | LPH | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|---------|-----|-----------------|-----------|--------------|----------------|---------------|---------------|-------------|-------------|------------|------------|
| I06 | 21 | 07 | 20758 | 15.0 | 0.27 | | 1.10 | | | <100 | |
| I06 | 21 | 07 | 20762 | 16.0 | 0.25 | | 0.96 J | | | | |
| I06 | 21 | 07 | 20763 | 17.0 | 0.31 | | 0.77 J | | | <100 | |
| I06 | 21 | 07 | 20771 | 19.0 | 0.21 | | 1.43 | | | <100 | |
| I06 | 21 | 07 | 20772 | 21.0 | 0.25 | | 0.60 J | | | <100 | |
| I06 | 21 | 07 | 20780 | 22.0 | 0.22 | | 1.42 J | | | | |
| I06 | 21 | 07 | 20781 | 23.0 | 0.29 | | 0.90 | | | <100 | |
| I06 | 21 | 07 | 20791 | 25.0 | 0.24 | | 1.59 | | | <100 | |
| I06 | 21 | 07 | 20792 | 26.0 | 0.30 | | 3.97 | | | | |
| I06 | 21 | 07 | 20793 | 27.0 | 0.26 | | 8.07 | | | <100 | |
| I06 | 21 | 07 | 20804 | 29.0 | 0.27 | | 1.61 | | | <100 | |
| I06 | 21 | 07 | 20813 | 30.0 | 0.195 | 6.48 J | 7.06 J | 0.0025 U | 0.0025 U | 2.6 J | 0.32 J |
| I06 | 21 | 08 | 20400 | 1.0 | 0.99 | | 6.81 | | | <100 | |
| I06 | 21 | 08 | 20401 | 3.0 | 0.98 | | 1.66 J | | | <100 | |
| I06 | 21 | 08 | 20414 | 5.0 | 0.54 J | | 1.08 J | | | <100 | |
| I06 | 21 | 08 | 20427 | 7.0 | 0.91 | | 1.42 J | | | <100 | |
| I06 | 21 | 08 | 20428 | 9.0 | 0.51 | | 3.55 | | | <100 | |
| I06 | 21 | 08 | 20434 | 11.0 | 0.35 | | 0.96 J | | | <100 | |
| I06 | 21 | 08 | 20435 | 12.0 | 0.29 | | 0.62 | | | | |
| I06 | 21 | 08 | 20436 | 13.0 | 0.33 | | 0.70 J | | | <100 | |
| I06 | 21 | 08 | 20442 | 15.0 | 0.34 | | 1.27 J | | | <100 | |
| I06 | 21 | 08 | 20443 | 16.0 | 0.29 | | 1.40 | | | | |
| I06 | 21 | 08 | 20444 | 17.0 | 0.37 | | 1.58 J | | | <100 | |
| I06 | 21 | 08 | 20448 | 19.0 | 0.25 | | 5.96 | | | <100 | |
| I06 | 21 | 08 | 20454 | 21.0 | 0.31 | | 10.58 | | | <100 | |
| I06 | 21 | 08 | 20455 | 22.0 | 0.20 | | 5.32 | | | | |
| I06 | 21 | 08 | 20456 | 23.0 | 0.28 | | 10.16 | | | <100 | |
| I06 | 21 | 08 | 20475 | 25.0 | 0.07 | | 8.76 | | | 42.7 J | |
| I06 | 21 | 08 | 20476 | 26.0 | 0.30 | | 7.80 | | | | |
| I06 | 21 | 08 | 20477 | 27.0 | 0.29 | | 9.51 | | | <100 | |
| I06 | 21 | 08 | 20490 | 29.0 | 0.23 | | 10.70 | | | <100 | |
| I06 | 21 | 08 | 20500 | 30.0 | 0.124 | 6.06 | 5.91 | 0.0025 U | 0.0025 U | 0.85 J | 0.049 J |
| I06 | 21 | 09 | 20534 | 1.0 | 0.53 | | 2.11 | | | <100 | |
| I06 | 21 | 09 | 20535 | 2.0 | 1.41 | | 4.63 | | | | |
| I06 | 21 | 09 | 20536 | 3.0 | 1.45 | | 2.52 | | | <100 | |
| I06 | 21 | 09 | 20537 | 5.0 | 0.42 | | 0.96 J | | | 41.9 J | |
| I06 | 21 | 09 | 20545 | 6.0 | 0.67 | | 1.35 J | | | | |
| I06 | 21 | 09 | 20546 | 7.0 | 0.59 | | 3.18 | | | <100 | |
| I06 | 21 | 09 | 20553 | 9.0 | 1.22 | | 3.04 | | | <100 | |
| I06 | 21 | 09 | 20554 | 11.0 | 0.26 | | 0.94 J | | | <100 | |
| I06 | 21 | 09 | 20555 | 12.0 | 0.41 | | 0.53 | | | | |
| I06 | 21 | 09 | 20556 | 13.0 | 0.28 | | 0.68 J | | | 55.2 J | |
| I06 | 21 | 09 | 20561 | 14.0 | 0.09 | | 1.79 | | | | |
| I06 | 21 | 09 | 20562 | 15.0 | 0.29 | | 0.71 J | | | <100 | |
| I06 | 21 | 09 | 20563 | 16.0 | 0.34 | | 1.09 | | | | |
| I06 | 21 | 09 | 20564 | 17.0 | 0.35 | | 1.21 | | | <100 | |
| I06 | 21 | 09 | 20565 | 19.0 | 0.20 | | 1.42 J | | | <100 | |
| I06 | 21 | 09 | 20566 | 21.0 | 0.36 | | 2.27 | | | <100 | |
| I06 | 21 | 09 | 20569 | 22.0 | 0.33 | | 3.48 | | | | |
| I06 | 21 | 09 | 20570 | 23.0 | 0.31 | | 2.14 | | | <100 | |
| I06 | 21 | 09 | 20578 | 25.0 | 0.23 | | 1.47 | | | <100 | |
| I06 | 21 | 09 | 20587 | 27.0 | 0.20 | | 0.24 | | | 42.8 J | |
| I06 | 21 | 09 | 20590 | 29.0 | 0.28 | | 1.73 | | | <100 | |

Table 3
LPH Soil Boring Sample Results

| Subcell | LPH | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|---------|-----|-----------------|-----------|--------------|----------------|---------------|---------------|-------------|-------------|------------|------------|
| I06 | 21 | 09 | 20595 | 30.0 | 0.120 | 0.68 | 0.58 | 0.0026 U | 0.0026 U | 1.7 J | 0.11 J |
| I06 | 21 | 13 | 20294 | 1.0 | 0.93 | | 8.02 | | | <100 | |
| I06 | 21 | 13 | 20297 | 2.0 | 0.93 | | 14.35 | | | | |
| I06 | 21 | 13 | 20298 | 3.0 | 0.68 | | 0.70 J | | | <100 | |
| I06 | 21 | 13 | 20302 | 4.0 | 0.38 | | 1.29 | | | | |
| I06 | 21 | 13 | 20303 | 5.0 | 0.71 J | | 1.70 J | | | <100 | |
| I06 | 21 | 13 | 20304 | 7.0 | 0.08 | | 0.69 J | | | <100 | |
| I06 | 21 | 13 | 20305 | 8.0 | 0.90 | | 2.15 J | | | | |
| I06 | 21 | 13 | 20306 | 9.0 | 0.59 J | | 0.63 | | | <100 | |
| I06 | 21 | 13 | 20307 | 11.0 | 0.26 | | 0.82 | | | <100 | |
| I06 | 21 | 13 | 20309 | 12.0 | 0.42 | | 0.91 J | | | | |
| I06 | 21 | 13 | 20310 | 13.0 | 0.08 UJ | | 0.58 | | | <100 | |
| I06 | 21 | 13 | 20337 | 15.0 | 0.29 J | | 2.03 | | | <100 | |
| I06 | 21 | 13 | 20338 | 16.0 | 0.50 | | 1.45 J | | | | |
| I06 | 21 | 13 | 20339 | 17.0 | 0.21 J | | 1.02 J | | | <100 | |
| I06 | 21 | 13 | 20340 | 19.0 | 0.31 | | 1.42 | | | <100 | |
| I06 | 21 | 13 | 20354 | 21.0 | 0.28 J | | 0.95 | | | <100 | |
| I06 | 21 | 13 | 20355 | 22.0 | 0.26 | | 1.04 | | | | |
| I06 | 21 | 13 | 20356 | 23.0 | 0.33 | | 1.00 J | | | <100 | |
| I06 | 21 | 13 | 20360 | 25.0 | 0.27 | | 1.29 J | | | <100 | |
| I06 | 21 | 13 | 20369 | 26.0 | 0.26 J | | 1.17 J | | | | |
| I06 | 21 | 13 | 20370 | 27.0 | 0.18 | | 1.84 | | | <100 | |
| I06 | 21 | 13 | 20378 | 29.0 | 0.22 | | 1.21 | | | <100 | |
| I06 | 21 | 13 | 20385 | 30.0 | 0.144 | 0.165 | 0.202 | 0.0026 U | 0.0026 U | 3.2 J | 0.17 J |
| L05 | 20 | 01 | 19775 | 1.0 | 0.76 J | | 13.54 | | | 332 | |
| L05 | 20 | 01 | 19776 | 2.0 | 0.85 | | 0.72 | | | | |
| L05 | 20 | 01 | 19777 | 3.0 | 1.32 J | | 1.38 J | | | <100 | |
| L05 | 20 | 01 | 19785 | 4.0 | 0.52 J | | 1.38 J | | | | |
| L05 | 20 | 01 | 19782 | 5.0 | 0.37 J | | 1.37 J | | | <100 | |
| L05 | 20 | 01 | 19783 | 6.0 | 0.42 J | | 1.76 J | | | | |
| L05 | 20 | 01 | 19784 | 7.0 | 0.60 J | | 1.66 | | | <100 | |
| L05 | 20 | 01 | 19797 | 9.0 | 0.34 J | | 0.66 J | | | <100 | |
| L05 | 20 | 01 | 19798 | 11.0 | 0.18 J | | 0.64 J | | | <100 | |
| L05 | 20 | 01 | 19799 | 13.0 | 0.33 J | | 0.50 | | | <100 | |
| L05 | 20 | 01 | 19840 | 15.0 | 0.28 J | | 0.78 J | | | <100 | |
| L05 | 20 | 01 | 19841 | 17.0 | 0.26 J | | 0.39 | | | <100 | |
| L05 | 20 | 01 | 19842 | 18.0 | 0.06 UJ | | 0.55 J | | | | |
| L05 | 20 | 01 | 19843 | 19.0 | 0.31 J | | 0.92 | | | <100 | |
| L05 | 20 | 01 | 19844 | 20.0 | 0.33 J | | 1.51 J | | | | |
| L05 | 20 | 01 | 19845 | 21.0 | 0.18 J | | 0.75 J | | | <100 | |
| L05 | 20 | 01 | 19848 | 22.0 | 0.29 J | | 1.27 J | | | | |
| L05 | 20 | 01 | 19849 | 23.0 | 0.30 J | | 1.40 | | | <100 | |
| L05 | 20 | 01 | 19862 | 25.0 | 0.06 UJ | | 0.49 J | | | <100 | |
| L05 | 20 | 01 | 19861 | 26.0 | 0.18 J | | 0.79 J | | | | |
| L05 | 20 | 01 | 19863 | 27.0 | 0.20 J | | 0.55 J | | | 2.8 J | |
| L05 | 20 | 01 | 19877 | 29.0 | 0.05 UJ | | 0.29 | | | <100 | |
| L05 | 20 | 01 | 19882 | 30.0 | 0.101 | 0.135 | 0.158 | 0.0026 U | 0.0026 U | 2.5 J | 0.28 J |
| L05 | 20 | 02 | 19906 | 1.0 | 1.10 | | 4.56 J | | | 205 | |
| L05 | 20 | 02 | 19907 | 2.0 | 1.03 J | | 3.83 | | | | |
| L05 | 20 | 02 | 19908 | 3.0 | 1.75 J | | 2.06 J | | | <100 | |
| L05 | 20 | 02 | 19911 | 4.0 | 1.61 | | 3.01 J | 0.093 | 0.132 | | |
| L05 | 20 | 02 | 19912 | 5.0 | 0.99 J | | 3.15 | | | <100 | |
| L05 | 20 | 02 | 19913 | 6.0 | 0.54 J | | 1.60 J | | | | |

Table 3
LPH Soil Boring Sample Results

| Subcell | LPH | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|------------|-----------|-----------------|--------------|--------------|----------------|---------------|---------------|-----------------|------------------|--------------|---------------|
| L05 | 20 | 02 | 19914 | 7.0 | 0.65 | | 0.81 UJ | | | <100 | |
| L05 | 20 | 02 | 19916 | 9.0 | 0.42 J | | 0.81 J | | | 42.3 J | |
| L05 | 20 | 02 | 19919 | 11.0 | NS | | NS | | | <100 | |
| L05 | 20 | 02 | 19920 | 13.0 | 0.45 | | 0.45 UJ | | | <100 | |
| L05 | 20 | 02 | 19921 | 15.0 | 0.31 | | 0.70 J | | | <100 | |
| L05 | 20 | 02 | 19922 | 16.0 | 0.39 | | 1.51 J | | | | |
| L05 | 20 | 02 | 19923 | 17.0 | 0.48 | | 1.77 | | | <100 | |
| L05 | 20 | 02 | 19937 | 19.0 | 0.28 | | 1.24 | | | <100 | |
| L05 | 20 | 02 | 19938 | 21.0 | 0.33 J | | 1.06 J | | | <100 | |
| L05 | 20 | 02 | 19939 | 22.0 | 0.05 | | 0.40 J | | | | |
| L05 | 20 | 02 | 19940 | 23.0 | 0.07 | | 0.61 J | | | <100 | |
| L05 | 20 | 02 | 19951 | 25.0 | 0.24 J | | 1.49 | | | <100 | |
| L05 | 20 | 02 | 19952 | 26.0 | 0.28 | | 0.61 J | | | | |
| L05 | 20 | 02 | 19953 | 27.0 | 0.20 | | 0.94 J | | | <100 | |
| L05 | 20 | 02 | 19964 | 29.0 | 0.34 J | | 1.31 J | | | <100 | |
| L05 | 20 | 02 | 19974 | 30.0 | 0.145 | 0.153 | 0.155 | 0.0026 U | 0.00035 J | 2.6 J | 0.27 J |
| L05 | 20 | 03 | 20045 | 1.0 | 0.76 | | 14.02 | | | 85.2 J | |
| L05 | 20 | 03 | 20046 | 2.0 | 0.66 | | 7.98 | | | | |
| L05 | 20 | 03 | 20047 | 3.0 | 1.08 | | 6.86 | | | <100 | |
| L05 | 20 | 03 | 20063 | 4.0 | 0.37 | | 2.04 | | | | |
| L05 | 20 | 03 | 20064 | 5.0 | 0.96 | | 2.73 J | | | <100 | |
| L05 | 20 | 03 | 20065 | 6.0 | 0.54 | | 1.96 J | | | | |
| L05 | 20 | 03 | 20066 | 7.0 | 0.59 | | 1.90 J | | | <100 | |
| L05 | 20 | 03 | 20072 | 9.0 | 0.42 | | 2.19 | | | <100 | |
| L05 | 20 | 03 | 20076 | 11.0 | 0.43 | | 0.96 J | | | <100 | |
| L05 | 20 | 03 | 20079 | 13.0 | 0.49 | | 1.15 J | | | <100 | |
| L05 | 20 | 03 | 20087 | 15.0 | 0.27 | | 0.54 J | | | <100 | |
| L05 | 20 | 03 | 20088 | 16.0 | 0.41 | | 0.88 J | | | | |
| L05 | 20 | 03 | 20089 | 17.0 | 0.27 | | 2.16 J | | | <100 | |
| L05 | 20 | 03 | 20092 | 19.0 | 0.32 | | 2.17 J | | | <100 | |
| L05 | 20 | 03 | 20101 | 21.0 | 0.19 | | 1.12 J | | | <100 | |
| L05 | 20 | 03 | 20102 | 22.0 | 0.24 | | 1.77 J | | | | |
| L05 | 20 | 03 | 20103 | 23.0 | 0.30 | | 0.51 J | | | <100 | |
| L05 | 20 | 03 | 20110 | 25.0 | 0.37 | | 1.30 J | | | <100 | |
| L05 | 20 | 03 | 20111 | 26.0 | 0.26 | | 0.67 | | | | |
| L05 | 20 | 03 | 20112 | 27.0 | 0.23 | | 0.43 J | | | <100 | |
| L05 | 20 | 03 | 20121 | 29.0 | 0.24 | | 1.27 | | | <100 | |
| L05 | 20 | 03 | 20126 | 30.0 | 0.166 | 0.161 | 0.154 | 0.0026 U | 0.0026 U | 1.8 J | 0.51 U |
| L05 | 20 | 04 | 20133 | 1.0 | 0.92 | | 12.75 | | | 1105 J | |
| L05 | 20 | 04 | 20134 | 2.0 | NS | | NS | 0.088 | 0.482 | | |
| L05 | 20 | 04 | 20135 | 3.0 | 1.02 | | 7.06 | | | <100 | |
| L05 | 20 | 04 | 20136 | 5.0 | 0.43 | | 0.66 J | | | <100 | |
| L05 | 20 | 04 | 20144 | 7.0 | 0.98 | | 1.14 J | | | <100 | |
| L05 | 20 | 04 | 20145 | 9.0 | 0.50 | | 1.82 | | | <100 | |
| L05 | 20 | 04 | 20146 | 11.0 | 0.39 | | 1.64 J | | | <100 | |
| L05 | 20 | 04 | 20147 | 12.0 | 0.36 | | 0.68 J | | | | |
| L05 | 20 | 04 | 20148 | 13.0 | 0.24 | | 0.44 J | | | <100 | |
| L05 | 20 | 04 | 20149 | 15.0 | 0.20 | | 0.23 | | | <100 | |
| L05 | 20 | 04 | 20159 | 16.0 | 0.28 | | 1.20 | | | | |
| L05 | 20 | 04 | 20160 | 17.0 | 0.31 | | 1.03 J | | | <100 | |
| L05 | 20 | 04 | 20161 | 19.0 | 0.09 | | 0.82 J | | | <100 | |
| L05 | 20 | 04 | 20165 | 21.0 | 0.40 | | 0.71 J | | | <100 | |
| L05 | 20 | 04 | 20168 | 22.0 | 0.29 | | 0.22 UJ | | | | |

Table 3
LPH Soil Boring Sample Results

| Subcell | LPH | Boring Location | Sample ID | Depth (feet) | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) | TCE (mg/kg) | PCE (mg/kg) | Ni (mg/kg) | Be (mg/kg) |
|----------------|------------|------------------------|------------------|---------------------|-----------------------|----------------------|----------------------|--------------------|--------------------|-------------------|-------------------|
| L05 | 20 | 04 | 20169 | 23.0 | 0.27 | | 1.00 J | | | <100 | |
| L05 | 20 | 04 | 20172 | 25.0 | 0.24 | | 0.56 J | | | <100 | |
| L05 | 20 | 04 | 20179 | 26.0 | 0.24 | | 1.24 | | | | |
| L05 | 20 | 04 | 20180 | 27.0 | 0.17 | | 1.33 J | | | <100 | |
| L05 | 20 | 04 | 20181 | 29.0 | 0.16 | | 0.68 J | | | <100 | |
| L05 | 20 | 04 | 20182 | 30.0 | 0.141 | 0.159 | 0.124 | 0.0026 U | 0.0026 U | 2.1 J | 0.16 J |
| L05 | 20 | 05 | 19978 | 1.0 | 1.07 | | 40.07 J | | | 201 | |
| L05 | 20 | 05 | 19979 | 2.0 | 0.64 J | | 0.73 | 0.098 | 0.098 | | |
| L05 | 20 | 05 | 19980 | 3.0 | 1.17 J | | 2.19 | | | <100 | |
| L05 | 20 | 05 | 19981 | 5.0 | 0.63 | | 1.00 J | | | <100 | |
| L05 | 20 | 05 | 19982 | 6.0 | 0.59 | | 2.99 J | | | | |
| L05 | 20 | 05 | 19983 | 7.0 | 0.49 | | 1.24 J | | | <100 | |
| L05 | 20 | 05 | 19997 | 8.0 | 0.76 J | | 1.01 J | | | | |
| L05 | 20 | 05 | 19998 | 9.0 | 0.38 | | 1.33 J | | | <100 | |
| L05 | 20 | 05 | 19999 | 11.0 | 0.26 | | 0.69 J | | | <100 | |
| L05 | 20 | 05 | 20000 | 13.0 | 0.62 | | 0.85 | | | <100 | |
| L05 | 20 | 05 | 20007 | 15.0 | 0.37 | | 0.57 | | | <100 | |
| L05 | 20 | 05 | 20008 | 16.0 | 0.32 | | 0.48 | | | | |
| L05 | 20 | 05 | 20009 | 17.0 | 0.21 | | 0.61 J | | | <100 | |
| L05 | 20 | 05 | 20010 | 19.0 | 0.20 | | 0.69 J | | | <100 | |
| L05 | 20 | 05 | 20019 | 21.0 | 0.41 | | 1.52 | | | <100 | |
| L05 | 20 | 05 | 20020 | 22.0 | 0.28 | | 1.84 | | | | |
| L05 | 20 | 05 | 20021 | 23.0 | 0.26 | | 1.18 J | | | <100 | |
| L05 | 20 | 05 | 20026 | 25.0 | 0.28 | | 1.51 | | | <100 | |
| L05 | 20 | 05 | 20027 | 26.0 | 0.19 | | 0.47 | | | | |
| L05 | 20 | 05 | 20028 | 27.0 | 0.31 | | 0.62 J | | | <100 | |
| L05 | 20 | 05 | 20035 | 29.0 | 0.41 | | 1.21 | | | <100 | |
| L05 | 20 | 05 | 20041 | 30.0 | 0.161 | 0.147 | 0.182 | 0.0026 U | 0.0026 U | 2.8 J | 0.33 J |

Table 3
LPH Soil Boring Sample Results

Analytes:

| | |
|-----------------------|-------------------------|
| Th-232 - Thorium-232 | PCE - Tetrachloroethene |
| U-234 - Uranium-234 | Ni - Nickel |
| U-238 - Uranium-238 | Be - Beryllium |
| TCE - Trichloroethene | |

Units:

pCi/g - picoCurie/gram
mg/kg - milligram/kilogram

Qualifiers:

R - Validation qualifier used to indicate that the result is considered unusable.
U - Validation qualifier used to indicate that the result was qualified as non-detect.
J - Validation qualifier used to indicate that the result is considered an estimate.
UJ - Validation qualifier used to indicate that the result was qualified as non-detect and the associated reporting limit is considered an estimate.

Notes:

See Figure 3 for boring locations.

DL sample is analyzed on Site for radionuclides (Th-232 and U-238) using the gamma spectroscopy system

DL sample is analyzed on Site for Ni using x-ray fluorescence spectroscopy by Stone Environmental Inc. Ni result that is between the detection limit of 40 mg/kg and the reporting limit of 100 mg/kg is estimated. Ni result that is less than the detection limit of 40 mg/kg is reported as less than the reporting limit (<100 mg/kg).

DL sample is analyzed for volatile organic compounds (TCE and PCE) using solid phase microextraction and capillary gas chromatography by Stone Environmental Inc.

SP sample result is bold and indicates that analysis was performed off Site by Severn Trent Laboratories, Inc.

NS - Not sampled due to insufficient recovery.

Due to an artifact in the laboratory data reporting program, the on-Site analytical data should be interpreted to two significant figures.

Blank cell indicates analysis was not performed

Result is above Site cleanup level.

Figure 2
Intervals, Increments and Analyses for Samples

| | Row 1 | Row 2 | Row 3 |
|---------------|----------------------|--------------------|----------------------|
| SU Interval 1 | 0 -- No sample | 0 -- No sample | 0 -- No sample |
| | 1 SP | 1 DL Rad | 1 DL Rad |
| | 2 | 2 DL Rad | 2 DL Rad & Nickel |
| | 3 DL Rad | 3 DL Rad & Nickel | 3 DL Rad |
| | 4 DL Rad & Nickel | 4 SP | 4 DL Rad & Nickel |
| | 5 DL Rad | 5 | 5 DL Rad |
| | 6 DL Rad & Nickel | 6 DL Rad | 6 DL Rad & Nickel |
| | 7 DL Rad | 7 DL Rad & Nickel | 7 SP |
| | 8 DL Rad & Nickel | 8 DL Rad | 8 |
| | 9 DL Rad | 9 DL Rad & Nickel | 9 DL Rad |
| SU Interval 2 | 10 DL Rad & Nickel | 10 DL Rad | 10 DL Rad & Nickel |
| | 11 SP | 11 DL Rad & Nickel | 11 DL Rad |
| | 12 | 12 DL Rad | 12 DL Rad & Nickel |
| | 13 DL Rad | 13 DL Rad & Nickel | 13 DL Rad |
| | 14 DL Rad & Nickel | 14 SP | 14 DL Rad & Nickel |
| | 15 DL Rad | 15 | 15 DL Rad |
| | 16 DL Rad & Nickel | 16 DL Rad | 16 DL Rad & Nickel |
| | 17 DL Rad | 17 DL Rad & Nickel | 17 SP |
| | 18 DL Rad & Nickel | 18 DL Rad | 18 |
| | 19 DL Rad | 19 DL Rad & Nickel | 19 DL Rad |
| SU Interval 3 | 20 DL Rad & Nickel | 20 DL Rad | 20 DL Rad & Nickel |
| | 21 SP | 21 DL Rad & Nickel | 21 DL Rad |
| | 22 | 22 DL Rad | 22 DL Rad & Nickel |
| | 23 DL Rad (1' spoon) | 23 DL Rad & Nickel | 23 DL Rad |
| | 24 DL Rad | 24 SP | 24 DL Rad & Nickel |
| | 25 DL Rad & Nickel | 25 | 25 DL Rad |
| | 26 DL Rad | 26 DL Rad | 26 DL Rad & Nickel |
| | 27 DL Rad & Nickel | 27 DL Rad & Nickel | 27 SP |
| | 28 DL Rad | 28 DL Rad | 28 |
| | 29 DL Rad & Nickel | 29 DL Rad & Nickel | 29 DL Rad (1' spoon) |
| SP | 30 SP | 30 SP | 30 SP |
| | 31 | 31 | 31 |
| | 32 | 32 | 32 |

Notes:

Solid lines indicate the spoon increment (2')

Zero indicates the ground surface

Maximum depth at 30' bgs

Overview:

Row 1 = SP's (1-3', 11-13', 21-23' and 30-32')

Row 2 = SP's (4-6', 14-16', 24-26' and 30-32')

Row 3 = SP's (7-9', 17-19', 27-29' and 30-32')

All Rows = DL's at 1' increments between SP's

Analyses Intervals:

SU Interval 01:

All SP samples from rows 1, 2 and 3 that were collected between 0 - 10' bgs

SU Interval 02:

All SP samples from rows 1, 2 and 3 that were collected between 11 -20' bgs

SU Interval 03:

All SP samples from rows 1, 2 and 3 that were collected between 21 -30' bgs

Site Overview

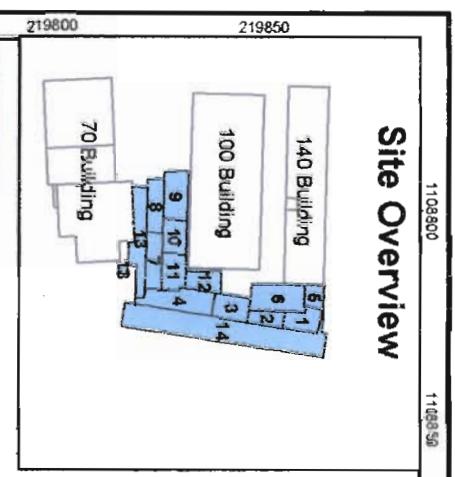
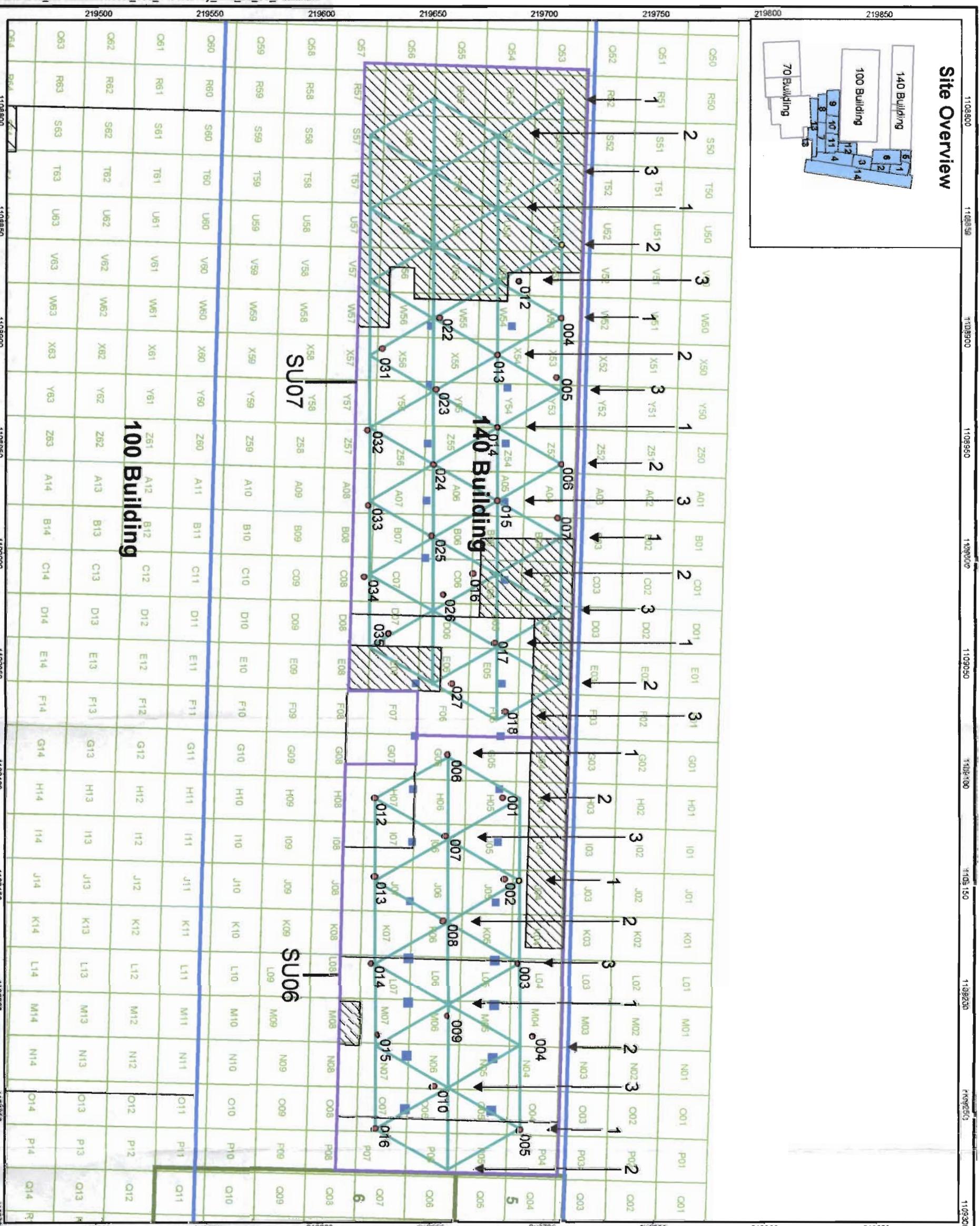


Figure 1
SU06 and SU07
Systematic Sampling
Locations

Legend

- Property Line
- Class 2 Survey Unit
- Subcell Boundary
- Interference Area
- 140 Building Column
- Systematic Sampling Grid

Row 1 SP samples at 1-3, 11-13, 21-23'
Row 2 SP samples at 4-6, 14-16, 24-26'
Row 3 SP samples at 7-9, 17-19, 27-29'
All Rows SP sample at 30-32'
All Rows DL samples at 1' increments
between SP samples
See Table 1 for summarized sample results.



DESTINY

RESOURCES, INC.

Site Overview

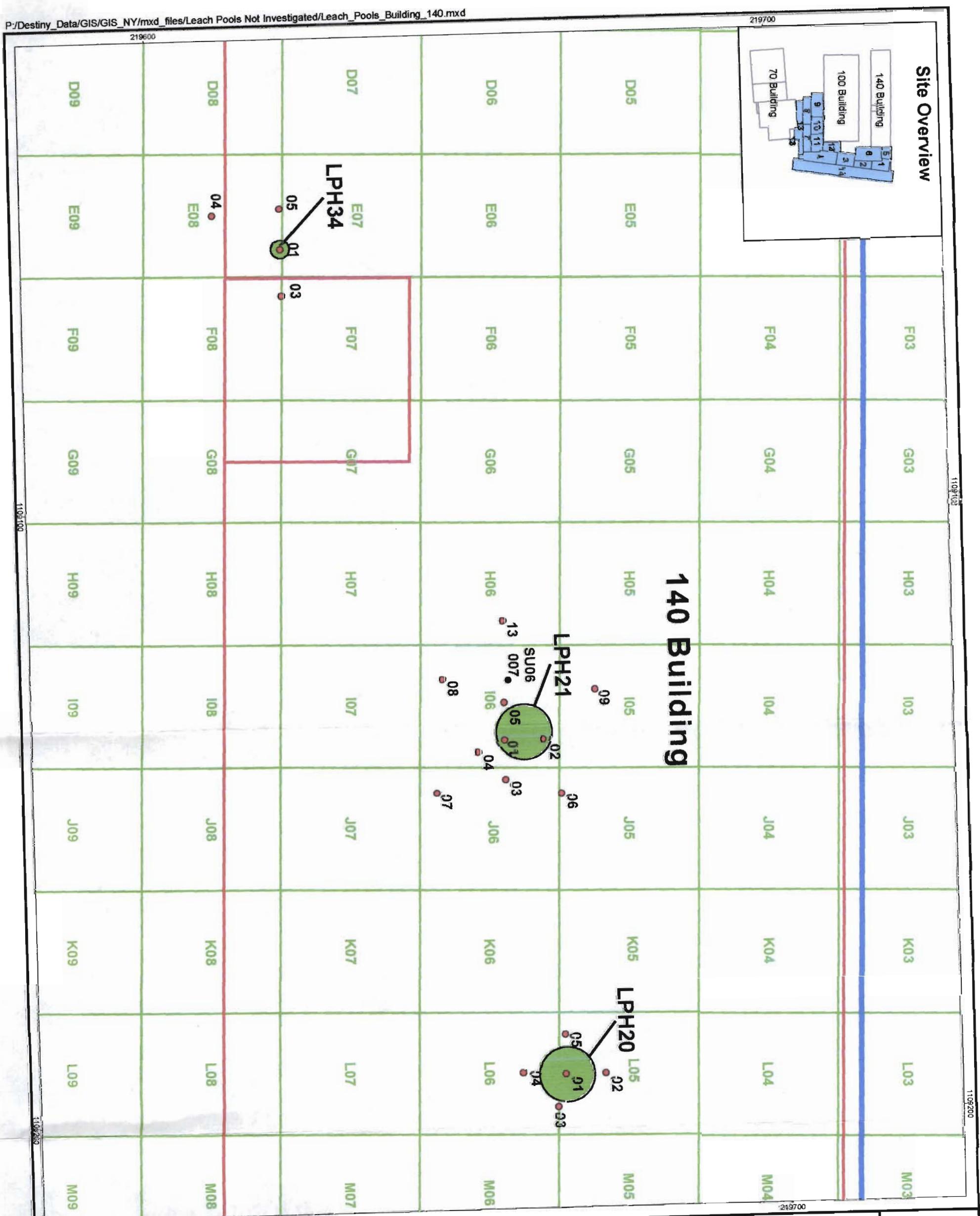
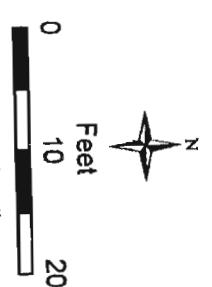


Figure 3 LPH Soil Boring Sample Results

See Table 3 for summarized sample results.
Note: Leach pool data provided by available historical maps



GTE OPERATIONS SUPPORT INCORPORATED
100 BROADWAY NEW YORK
NYSDEC V0089-1

Projection Information
State Plan Projection
Long Island Zone
North American Datum 1983
Feet

UR 82/10-039

DBI ID: 1006 H6754 RESOURCES, INC., September 29, 2005

**Systematic
Subsurface Soil Sampling and Analysis Plan
Beneath the 140 Building**

**Former Sylvania Electric Products Incorporated Facility
Hicksville, New York
GTE Operations Support Incorporated**

November 2004

This Systematic Subsurface Soil Sampling and Analysis Plan Beneath the 140 Building has been reviewed by URS Corporation – New York, and I am in agreement with the methods and procedures to be used in this investigation.

URS Corporation – New York



Robert D. Brathvode, P.E.
Engineer of Record

This Systematic Subsurface Soil Sampling and Analysis Plan Beneath the 140 Building has been reviewed by Professional Radiation Consulting, Inc. (PRCI) in accordance with Envirocon's New York State Department of Labor Radioactive Materials License No. 3095-4330, and I am in agreement with the methods and procedures to be used in this investigation.

S. Brightwell, CHP for Shane Brightwell

Shane Brightwell, CHP
President, PRCI
RSO, Radioactive Materials License No. 3095-4330

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FIGURES

Figure 1 – Survey Units Beneath the 140 Building

1.0 INTRODUCTION

This Systematic "Subsurface Soil Sampling and Analysis Plan" (SSSAP) has been prepared to characterize the soils in accessible areas beneath the 140 Building. This SSSAP describes applicable guidance, characterization (i.e., survey, design and sampling protocols), and laboratory analysis for the soils. The results of this SSSAP will enable GTE Operations Support Incorporated (GTEOSI) to determine the extent to which remedial activities are necessary beneath the 140 Building.

During the last two years, soils containing residual radionuclides of uranium (U) and thorium (Th) were excavated from the Former Sylvania Electric Products Incorporated (Sylvania) property in Hicksville, New York (the Site) and shipped off Site to an approved disposal facility. To date, remediation activities at the Site have focused primarily on the eastern portions of the 100 and 140 Properties. This eastern focus has been based on what is known regarding historical Sylvania facilities and operations, and findings of previous Site investigations.

Subsurface investigation was performed under the eastern portion of the 140 Building, which identified target analytes exceeding the cleanup criteria. Consequently, approximately 5,000 square feet (ft^2) of the eastern end of the 140 Building was razed to accommodate remediation. The remaining warehouse portion of the building footprint (approximately 49,000 ft^2) is the subject of this Plan.

The various sections of this SSSAP present the steps to be implemented to characterize the subsurface soils in the areas below the 140 Building. The characterization will include not only radionuclides, but also certain volatile organic compounds (VOCs) [(tetrachloroethene (PCE) and trichloroethene (TCE)] and nickel (Ni) (collectively, "target analytes"). Modification to these steps will be permitted when field conditions or sample results indicate the modifications would better support the intent and objective of this SSSAP as stated in Section 2.0 below. All modifications to steps in this Plan shall be made with the prior concurrence of the Radiation Safety Officer (or his designated alternate) and the prior approval of the Project Coordinator.

2.0 OBJECTIVE

The objective of this Plan is the characterization of soils in specified areas as shown in Figure 1. For radiological characterization purposes, these areas are referred to as "survey units" (SUs) as defined in NUREG 1575, *Multi-Agency Radiation Survey and Site Investigation Manual* (MARSSIM).

Note: The area designated as SU06 is the approximate eastern one-third of the 140 Building. Within SU06, a small portion of the southern area (control point area) and a portion of the northwestern area (sample storage) of the survey unit are not readily accessible for characterization (i.e., building alterations or relocation of structures would be required). The area designated as SU07 lies to the west of SU06, and comprises slightly less than two-thirds of the 140 Building area. Portions of the southeastern (lunch room) and northeastern corners (sample prep & lab area and sample storage area) of the survey unit and most of the western portion (office area) of the survey unit are not readily accessible for characterization (Figure 1).

3.0 APPLICABLE GUIDANCE

This SSSAP was prepared in accordance with Voluntary Cleanup Agreement, Site V-00089-1, Index W1-0903-01-12, between New York State Department of Environmental Conservation (NYSDEC) and

GTEOSI. Field procedures and analytical methods identified in the Site's approved *Comprehensive Soil Remediation Work Plan, Revision 5: June 2003* (Work Plan) have been incorporated in this SSSAP where appropriate. Guidance specific to radiological and chemical characterization are described in their associated sections, as applicable.

4.0 CHARACTERIZATION

The soils within SU06 and SU07 are not expected to contain target analytes at concentrations greater than the applicable target cleanup levels. (Note: the target cleanup levels are defined in the Work Plan). The following sources were reviewed during preparation of this SSSAP:

- **Historic maps, aerial photos, and historic documents** - These sources indicate that one building in which uranium fuel element fabrication occurred during the 1950s and 1960s occupied most of the southeastern half of SU06 and a small building historically occupied the southeastern corner of SU07.
- **Soil borings performed within the SUs during previous investigations** - Three shallow borings conducted in SU06 did not indicate the presence of target analytes above cleanup levels.
- **Excavation in adjacent cells** – Field surveys and sampling on the west side of Cell 5 and Cell 6 indicated that target analytes above cleanup levels did not continue to the west beyond the cell boundaries into SU06.

The radiological characterization is designed using guidance provided in MARSSIM as discussed below (Section 4.1). Concurrently, VOCs and Ni soil residuals will be characterized as described in Section 4.2.

4.1 RADIOLOGICAL

The following sections describe the radiological guidance and sampling parameters to be used to execute this SSSAP. This SSSAP has been developed using a combination of applicable MARSSIM guidance, historic documents, and knowledge of Site subsurface conditions gained during investigations and remediation.

4.1.1 Applicable Radiological Guidance

The investigation of soils to determine the presence (if any), concentrations, extent, and boundaries of radionuclides is termed a *characterization* survey. The principles for a characterization survey described in Chapter 5 of MARSSIM have been considered in developing this SSSAP. Specific methods recommended in MARSSIM for subsurface soil sampling have also been incorporated in this SSSAP.

4.1.2 Survey Unit

Classification

Both SU06 and SU07 were designated as MARSSIM Class 2 SUs since they are not expected to exhibit soil target analytes at concentrations exceeding the cleanup levels. A systematic triangular sampling pattern will be used to provide uniform lateral coverage of these SUs. This triangular grid based system, as prescribed by MARSSIM for Class 2 SUs, is useful as it accommodates both the radiological and chemical sampling.

Layout

SU06 is approximately 1,800 square meters (m^2) or 19,378 ft 2 . Of this total area, 1,634 m 2 (17,586 ft 2) are readily accessible for characterization. SU07 is approximately 2,760 m 2 (29,713 ft 2). Of this total area, only 1,410 m 2 (15,179 ft 2) are readily accessible for characterization. As indicated in Section 4.1.3, a triangular grid system will be used and nomenclature will be adopted from the Site grid system described below.

The Site is on a northing/easting planar grid coordinate system. The Site grid pattern was developed to accommodate excavation cells, and each cell is divided into subcells. Each subcell has a north-south length of 6.7 meters (m) or 22 feet (ft) and an east-west width of 6.1 m (20 ft). The subcells are uniquely identified by letter designations for north-south columns and number designations for east-west rows. This grid coordinate system will be used for defining the sample nomenclature within the SUs.

4.1.3 Sample Locations

Number of Horizontal Sample Locations

MARSSIM bases the number of samples (N) in a SU on how close the expected average concentration in the SU is to the cleanup level, how much variation there is in the observed or expected concentrations, and the sensitivity of equipment scanning capabilities with respect to the cleanup levels. For SU06 and SU07, the minimum number of samples to be collected in each SU is 13. Although MARSSIM indicates only 13 samples are sufficient, 16 sample locations per each SU were selected to provide lateral coverage and to ensure that the minimum number of 13 samples can be collected in the event field conditions do not allow collection of soil samples at all 16 locations. If sample locations fall outside the SU boundary due to the grid orientation, they may be relocated inside the grid using the criteria described in below.

Sample Start Point

MARSSIM suggests establishing a systematic sampling pattern using a random start point. A random number generator was used to select planar coordinates within the footprint of each of the SU boundaries. The associated systematic triangular sampling pattern, as described below, was established in each SU by placing one of the sample locations at the start point coordinates.

Horizontal Sample Locations

For each SU, once N, the SU size, the grid system pattern, and the start point were established, the sample locations were then selected and mapped. The calculated maximum east-west distance between sampling locations (L_N) and north-south distance between sampling rows (L'_N) are listed below.

| Survey Unit | N (samples) | L_N (meters) | L'_N (meters) |
|--------------------|--------------------|----------------------------------|-----------------------------------|
| SU06 | 16 | 10.86 | 9.40 |
| SU07 | 16 | 10.09 | 8.74 |

Some of the sample locations may have to be modified to avoid obstructions encountered in the field (i.e., utilities). Any sample location that must be relocated up to one-third of the diagonal distance between planned sample locations [$\leq 3.0\text{m}$ (9.8 ft) in SU06 or $\leq 3.4\text{ m}$ (11.2 ft) in SU07] will be relocated accordingly. Any sample location that must be relocated a distance greater than the applicable distance

specified above will be either eliminated or randomly relocated using the method for generating random coordinates as described previously.

If a sample location falls just outside of the SU boundary, the sample may be evaluated for relocation to within the SU boundary, depending on the required distance and obstructions. The result may be that the SU has more than the minimum number of sampling locations in order to provide as uniform coverage as practical. The addition of sample points does not reduce the effectiveness of the methods described in MARSSIM.

Vertical Sampling Depth

Vertical sampling and excavation depths on Site have been measured in feet below ground surface (bgs); therefore, vertical units are expressed here in both meters and feet (in parentheses). Based on the results of subsurface soil investigations and excavations, most impacts occur from the surface down to about 7.3 m (24 ft) bgs, with infrequent impacts identified greater than 7.3 m (24 ft) bgs. Impacts below 7.3 m (24 ft) bgs were usually identified based on shallow indicators. Given this history, a target maximum sampling depth of approximately 9 m (30 ft) bgs has been established to provide an additional 2-m (6-ft) buffer and to accommodate the pattern of the vertical sampling intervals as described below. If exceedences of the cleanup objectives are encountered at 9 m (30 ft) bgs, additional sampling will continue to define the vertical extent of impacts.

Vertical Sample Intervals

Based on the results of excavation and subsurface soil investigations performed during remediation on Site, impacts may be present in relatively thin soil veins. Specifically, concentrations may increase from not detected to greater than the cleanup levels in the next lower 0.3-m (1-ft) interval. Within the same boring, the concentrations may then decrease rapidly over the next 0.3- or 0.6-m (1- or 2-ft) intervals. Note that the measured depths of the soil layers with elevated radiological impacts may vary due to both depositional nature of the impacts and the assumption that the surface is a uniform elevation (measured bgs).

Based on the above information, the following subsurface soil sampling parameters were established.

- Characterization/Final Verification samples will be collected at 3-m (10-ft) intervals. These samples will be collected, documented, labeled, and analyzed by on-Site and off-Site analytical methods as Sample Point (SP) samples. SP samples are treated the same as Confirmation/Verification (CF/VF) samples as described in the Work Plan.
- The SP sample pattern was established so that each sample at the corner of an equilateral triangle is vertically staggered by 1 m (3.3 ft). For example:
 1. The first triangle corner (#1) sampling location will have SP samples collected from the top 1-ft segment of the 1-, 4-, and 7-m (1-, 11-, and 21-ft) intervals;
 2. The second triangle corner (#2) sampling location will have SP samples collected from the top 1-ft segment of the 2-, 5-, and 8-m (4-, 14-, and 24-ft) intervals; and
 3. The third triangle corner (#3) sampling location will have SP samples collected from the top 1-ft segment of the 3-, 6-, and 9-m (7-, 17-, and 27-ft) intervals.

The staggered vertical sample pattern result for a single set of three adjacent sample locations resembles a triangular "staircase" or helical pattern. This pattern works as follows*:

- a) The sample locations in the westernmost north-south oriented column are all sampled at the intervals outlined in #1 above;
- b) The sample locations in the second north-south oriented column to the east are all sampled at intervals outlined in #2 above;
- c) The sample locations in the third north-south oriented column to the east are all sampled at the intervals outlined in #3 above;
- d) The sample locations in the fourth north-south oriented column to the east are all sampled at the intervals outlined in #1 above;
- e) The sample locations in the fifth north-south oriented column to the east are all sampled at the intervals outlined in #2 above; and.
- f) The sample locations in the sixth north-south oriented column to the east are all sampled at the intervals outlined in #3 above.

* The pattern repeats after every third column.

- The 0.3-m (1-ft) interval samples between the SP sample intervals will be collected and analyzed on Site as Delineation (DL) Samples. This will provide additional assurance that any relatively thin veins of impacts present between the SP interval samples will be identified.

4.2 CHEMICAL

As indicated in the introduction of this SSSAP, the potential for residual VOCs and Ni impacts in the SUs will be evaluated concurrently with the radiological impacts. The triangular grid system established under MARSSIM and the vertical interval sampling were evaluated for this purpose and accepted. This system provides both vertical and lateral coverage to adequately evaluate the potential for chemical impacts. If elevated concentrations of VOCs and/or Ni are detected, the soils around the location will be considered for additional investigation or remedial action, as appropriate.

4.3 MATERIALS AND METHODS

The following narrative describes the sample collection, analysis, and evaluation methodology to be used to execute this SSSAP.

4.3.1 Soil Sampling Equipment

A hollow-stem auger drill rig with split-spoon sampling capabilities will be used to collect soil samples. The split spoon [0.6 m (2 ft) in length and 0.08 m (3 inches) in diameter] will be advanced in 0.6-m (2-ft) intervals. Two, 0.3-m (1-ft) interval samples will be collected per split-spoon.

4.3.2 Sample Field Screening and Preparation

Each sample will be initially field-screened with a 3-inch sodium iodide (NaI) gamma detector to evaluate potential residual radiological impacts and a photoionization detector (PID) to evaluate the presence of VOCs. In addition, an x-ray fluorescence (XRF) spectrometer will be used on Site to screen samples for Ni. Sample descriptions and field observations will be documented on the boring logs.

4.3.3 Sample Collection

A minimum of two samples will be collected per split spoon barring loss or incomplete recovery. These samples will be designated as either DL or SP, as applicable. DL samples will be collected at the intervals between SP samples from the surface down to the bottom sampling depth of approximately 9 m (30 ft) bgs.

Samples collected for radiological analysis will be placed in 1-liter Marinelli containers. DL samples will be used for radiological screening and analyzed on Site using gamma spectroscopy. The SP samples will be analyzed for radionuclides on Site and off Site, consistent with the Work Plan criteria for CF/VF sampling.

Samples collected for chemical analysis will be placed in pre-preserved methanol vials and non-preserved 40-ml vials. DL samples are not analyzed for VOCs or Ni unless field screening/observations support collection of a chemical sample. DL samples with PID screening readings of 50 parts per million (ppm) or higher will be collected for VOC analysis by Severn Trent Laboratories (STL), Earth City, Missouri. The SP samples will be collected for VOCs both on Site and off Site, consistent with the Work Plan criteria for CF/VF sampling.

A geologist will describe the samples in general accordance with the Unified Soil Classification System (USCS). Sample descriptions will include soil type, color, moisture, and other visual observations and field readings. This information will be documented on soil boring logs.

All samples will be logged into the Site sample tracking and barcode system.

4.3.4 Sample Analysis

Each DL sample will be analyzed for 10 minutes by on-Site gamma spectroscopy (providing a nominal detection limit of approximately 0.014 pCi/g for Th-232 and 3.6 pCi/g for U-238, both of which are far below the Site cleanup levels) to quantify the concentrations of target radionuclides of U and Th. Each SP sample will be analyzed for 30 minutes by on-Site gamma spectroscopy (providing a nominal detection limit of approximately 0.008 pCi/g for Th-232 and 2.0 pCi/g for U-238, both of which are far below the Site cleanup levels) as well as by alpha spectroscopy at STL for isotopic U and Th.

If DL samples are collected for chemical analyses, they may be screened using XRF for Ni and analyzed for VOCs on Site by Stone Environmental. Each SP sample will be analyzed for VOCs on Site by Stone Environmental as well as by STL for VOCs and Ni. SP samples will also be analyzed for beryllium (Be).

5.0 SAMPLING/ANALYSIS PROCEDURE

The following is the step-by-step procedure for sample collection and subsequent analysis.

1. The applicable Chemical/Radiological Work Permit (C/RWP) and Activity Hazards Analysis (AHA) will be in place prior to commencement of sampling.
2. The field crew will be briefed on this procedure prior to commencement of sampling.
3. Each sampling location will be located and surveyed in the field using either a laser positioning system (LPS) or global positioning system (GPS) surveying system.
4. Each sample location will be investigated for utilities and obstructions prior to saw cutting any pavement or commencement of sampling. If a sample location is in an area where utilities or obstructions have been identified, then the sample location shall be adjusted to a safe, practical location as close to the proposed location as possible, but no more distant than 3.0 m (9.8 ft) in SU06 or 3.4 m (11.2 ft) in SU07. Any sample location that cannot be relocated within these criteria will be eliminated or randomly relocated per Section 4.1.3.
5. The split-spoon sampler will be advanced to the predetermined maximum depth range of approximately 9 m (30 ft) bgs, in 0.6-m (2-ft) intervals, collecting two, 0.3-m (1-ft) samples per sampling cycle.
6. Radiological field screening of samples will be conducted on each sample using a NaI gamma detector.
7. Chemical field screening of samples for VOCs will be conducted on each sample using a PID. An XRF spectrometer will be used for on-Site Ni screening of every other sample beginning with the second sample in the boring, continuing with the fourth sample, sixth sample, etc. Soil samples (~100 g) for Ni screening by XRF will be collected in Ziploc® bags if the soils are relatively dry and in glass jars if the moisture content is approximately 20% or higher. The samples will be delivered to Stone Environmental for either direct screening by XRF, or for drying in an oven, and then screening by XRF. For those DL quality control (QC) samples to be submitted to STL, the soils will be transferred from the Ziploc® bags to 40-ml glass vials in the sample preparation area. For QC purposes, every tenth sample will be screened by XRF and then submitted to STL for duplicate analysis. SP samples will be analyzed for Be.
8. A geologist will log the borings and record observations and measurements consistent with the USCS nomenclature and procedures, noting indications of soil impacts by chemicals and other potential contributors to contamination.
9. DL screening samples will be collected at the intervals between SP samples prescribed in Section 4.1.3. Radiological DL samples will be analyzed by on-Site gamma spectroscopy for a 10-minute count time. If field conditions warrant and chemical DL samples are collected, they will be analyzed for VOCs on Site by Stone Environmental. Chemical DL samples with PID readings of 50 ppm or greater will be submitted for analysis to STL.
10. SP samples will be collected at the intervals prescribed in Section 4.1.3 and will be treated in the same manner as CF/VF samples. Radiological SP samples will be analyzed by on-Site gamma spectroscopy for a 30-minute count time as well as off-Site isotopic analyses by STL. Chemical SP samples will be collected and placed in vials with methanol for on-Site analysis by

Stone Environmental and in 40-ml glass vials for submission to STL for analysis of VOCs, Ni, and Be.

11. If oily soils are encountered, they will be collected while sampling as either DL or SP samples. Pursuant to the NYSDEC request, these soils will be submitted to STL for analysis of polychlorinated biphenyls (PCBs) and semi-volatile organic compounds (SVOCs) base/neutral fraction. The soils collected for PCBs and SVOC analyses will be placed in 250-ml glass jars; a minimum of 100g is needed to accommodate both analyses. The containers for the other analyses will follow the instructions provided above. (If sufficient sample volume of oily soils is not available, the chemical analyses for VOCs, SVOCs, PCBs, Ni and Be will take precedence over samples for radiological analyses.)
12. After the completion of sampling from a given location, the borehole will be backfilled with clean cuttings and/or clean on-Site backfill material to within 0.1 to 0.15 m (4 to 6 inches) of the top of the borehole. The remaining 0.1 to 0.15 m (4 to 6 inches) will be filled with asphalt or other applicable surfacing material.
13. Decontamination of sampling equipment will be performed in accordance with SOP-RAD-011, *Equipment Decontamination* and in accordance with the chemical decontamination procedures.

6.0 TARGET CONCENTRATIONS

The soil concentrations will be compared to the Site cleanup levels as defined in the Work Plan.

7.0 ASSESSMENT

Currently, the SUs are beneath Building 140. As a result, performing surface radiation scans as surveys are not practical to detect the presence of surface or subsurface radiological impacts in excess of cleanup criteria. MARSSIM allows for modifications to the survey design to address subsurface soils. However, in order to classify SUs as non-impacted, or to facilitate remediation planning, subsurface characterization is required. In addition, the data quality objectives process also allows that, based on the data needs for a survey, the decision can be made that sampling and analysis are necessary.

7.1 RADIOLOGICAL

7.1.1 Survey Unit Assessment

Each SU will be characterized/verified vertically at 3-m (10-ft) staggered intervals. This approach for subsurface soils is not directly addressed in MARSSIM, which provides characterization and final verification guidance primarily on surface soils. Therefore, each 3-m (10-ft) depth interval will be evaluated independently as if that interval were representative of an undulating soil surface, using the MARSSIM approach to surface soils. The SP samples within each 3-m (10-ft) depth interval will be treated as if they were collected from a continuous varying surface that existed at their corresponding depths [i.e., all samples in the 0 to 3-m (0 to 10-ft) interval will be evaluated independently using a MARSSIM statistical test and all samples in the 3- to 6-m (10- to 20-ft) interval will be evaluated independently using the MARSSIM statistical test]. This approach will be used for each of the 3-m (10-ft) intervals.

7.1.2 Decision Analysis

The radiological analytical results will be evaluated using the default null hypothesis recommended in MARSSIM, which states: "The residual radioactivity in the survey unit exceeds the release criterion." The MARSSIM "Sign Test" (assuming no contribution from background radionuclides) will be used to reject the null hypothesis. When the null hypothesis is rejected, then the SU will pass and qualify for release. If the null hypothesis cannot be rejected, further investigation or remedial action may be necessary.

As stated earlier, each 3-m (10-ft) sampling interval data set will be evaluated independently as a soil (undulating planar) surface sample set generated from all SP samples within that 3-m (10-ft) interval. Therefore, there will be at least three independent evaluations of the surface and subsurface soils within each SU.

7.2 CHEMICAL

The chemical analytical results will be evaluated independently and compared to the Site cleanup levels specified in the Work Plan, NYSDEC Technical and Administrative Guidance Memorandum (TAGM) #4060, or Site background concentrations. Exceedences will be considered for additional investigation or remedial action, as appropriate.

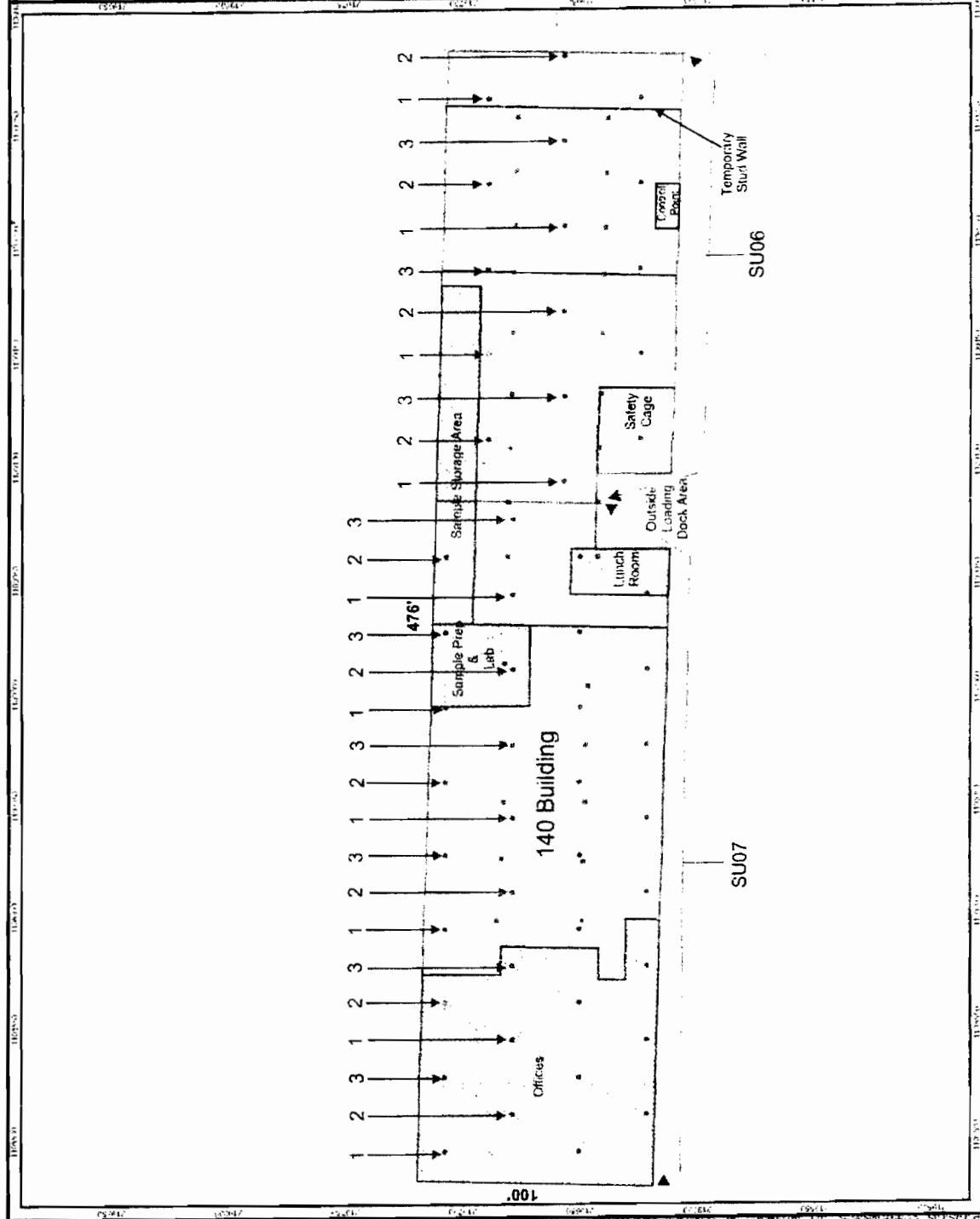
8.0 SCHEUDLE

The work described in this SSSAP is scheduled to start in December 2004.

Figure 1
**Survey Units - Beneath
the 140 Building**

Legend

- Random Sample Starting Points
- Sample Locations
- Sample Grid Layout
- Structure Columns Building 140
- Class 2 Survey Unit
- Cell Boundaries
- Not Accessible to Drilling Equipment
- Cell Number
- 1-Meter Vertical Sampling Start Interval
- 2-Meter Vertical Sampling Start Interval
- 3-Meter Vertical Sampling Start Interval



DRI ID: 1006-H6245

November 03, 2004

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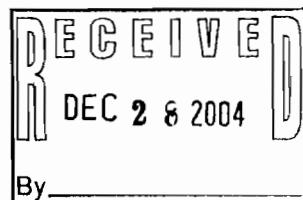
New York State Department of Environmental Conservation
Division of Environmental Remediation, Region One
Building 40 - SUNY, Stony Brook, New York 11790-2356
Phone: (631) 444-0240 • FAX: (631) 444-0248
Website: www.dec.state.ny.us



Erin M. Crotty
Commissioner

December 20, 2004

Jean Agostinelli
Vice President - Controller
GTE Operations Support Inc.
600 Hidden Ridge Drive (HQE03E75)
Irving, TX 75038



Re: Systematic Subsurface Soil Sampling and Analysis Plan Beneath the 140 Building and
Systematic Subsurface Soil Sampling and Analysis Plan Beneath the 100 Building
Former Sylvania Electric Products Facility, #V00089-1

Dear Ms. Agostinelli:

The Department offers the following comments on the subject documents:

1) 100 Building - Vertical Sampling Depth

Please clarify ground surface reference point particularly as it relates to the loading dock area of the 100 property. The loading dock floor is approximately four to five feet below the 100 building's floor. The Department wants to ensure that the six foot buffer built into your sampling plan is not lost.

2) Soil Gas Sampling

Based on a preliminary analysis of the groundwater sampling results, there may still be undiscovered source areas for chlorinated solvents in the western and central portions of the site. As another tool in identifying the location of these volatile organic compounds, the Department requests that a soil gas sample be collected from each borehole after the proposed shallow samples have been removed. Please propose a depth at which to collect these soil gas samples which is somewhere between three feet and ten feet below the building slab. The samples could be analyzed by a PID in a head space sample or by your on-site laboratory, whichever you prefer.

3) Additional Investigation Borings Between Survey Units SU05 and SU04 and Between Survey Units SU04 and SU05 for the 100 Building

There is a space between survey units SU04 and SU05 and between SU03 and SU04. It is not necessary to alter the survey units. However, I am requesting five additional investigation

borings at the locations shown in the attached figure to give better coverage.

The space between SU04 and SU05 is by western portion of the chemical processing area for the former AEC building on the south portion of the gap and by an historical metal storage tank and stucco building on the north portion of the gap. Groundwater data suggests the presence of potential nickel and VOC source areas near this gap. The nickel and radiological contamination found in cell 9 probably extends to under the 100 building.

The space between SU03 and SU04 is just north of the process tank found in the northwest corner of cell 10 and is near the eastern wall of the former AEC building. The piping leading from the 100 building to the former reservoir in the rear of the 100 property apparently originated near the northeast corner of the AEC building. Based on an old figure, there was a pump in the cellar of this portion of the building which probably was used to pump water to the reservoir. This area is of interest due to contamination discovered in the reservoir. Additionally, the source of the radiological contamination in MW-2, which is downgradient of this area, has apparently not been found yet.

It is for the above reasons that I am requesting the additional investigation borings.

4) Historical Leaching Pool by the 140 Building Loading Dock

There is one historical leaching reportedly located inside the 140 building, just west of the loading dock, that was not investigated in the recent leaching pool investigation. It is just west of the former Building 2, the earlier commercial manufacturing building, and just east of a two-story frame building which I believe to be the "farm house". The farm house may have been used historically for machining operations. In SU07 for the 140 building, the survey point in the southeast corner of this survey unit comes very near the location of this former leaching pool. Please move this survey point slightly so that is located over the expected center of this pool. This pool must be investigated due to the high concentrations of PCE that were detected in nearby LPH21. Since the sediment sample in LPH21 detected percent concentrations, degreasing operations were most likely located historically somewhere near this pool. The leaching pool apparently is within the area identified as the "Lunch Room" on your figure. Please let me know if this presents a difficulty in investigating this pool.

If high soil gas readings are detected in any of the grid samples near the "Safety Cage" by the western portion of Building 2, additional borings will be requested around this area later. The western portion of that building would be the most likely source of the solvents that were found in LPH21.

Please address these comments in a revised work plan to be submitted within 30 days of your receipt of this letter. Please do not hesitate to call me at (631) 444-0244 if you have any questions or disagree with these comments.

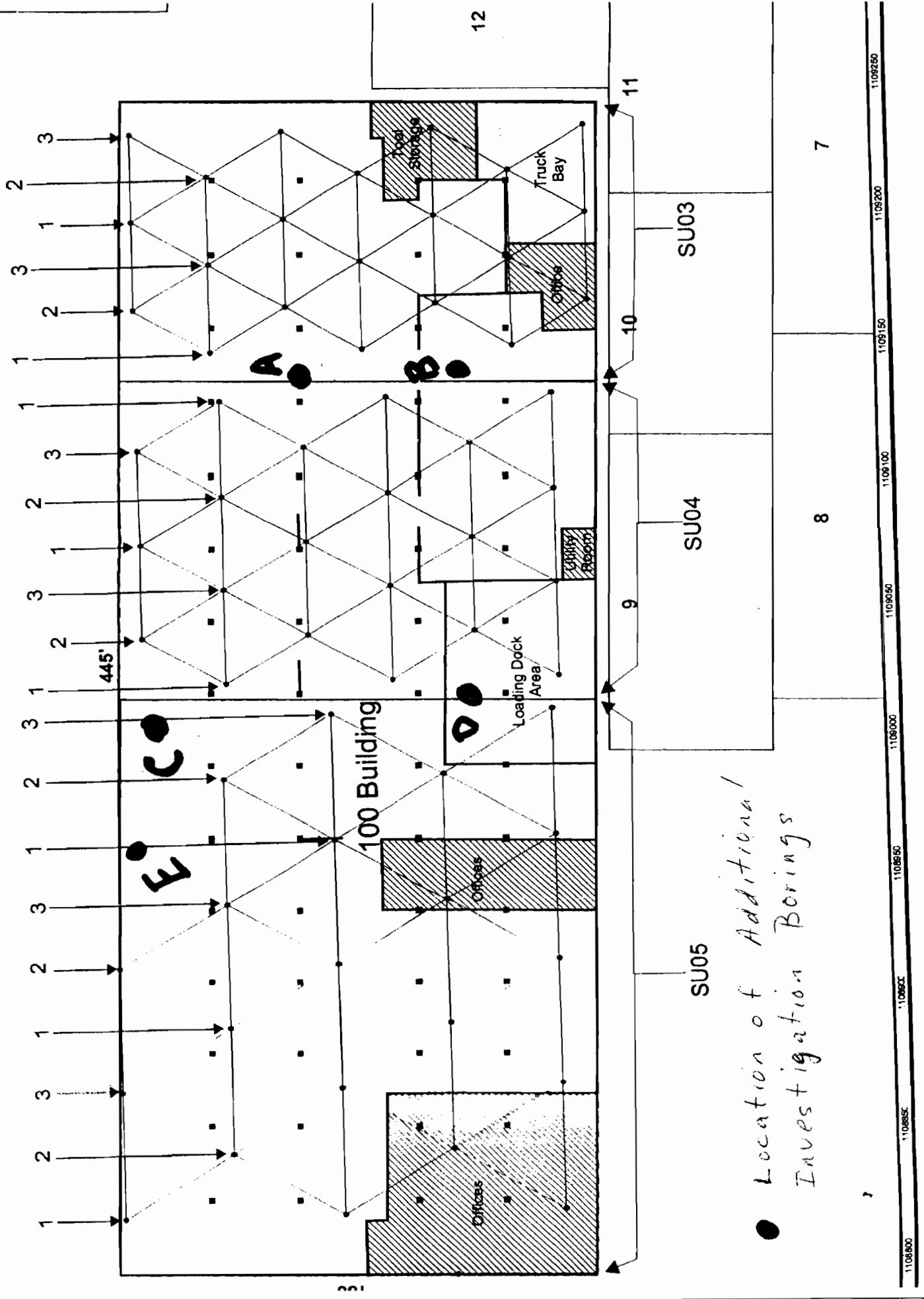
Sincerely,



Robert R. Stewart
Environmental Engineer I

Enclosure

cc: W. Parish
K. Carpenter
J. Riggi
J. Nealon, NYSDOH



● Location of Additional /
 Investigation Boring s



GTE Operations Support Incorporated
600 Hidden Ridge Drive (HQE03E75)
Irving, Texas 75038
(972) 718-4806

January 20, 2005

Mr. Robert Stewart
Division of Environmental Remediation
New York State Department of Environmental Conservation
SUNY Campus Loop Bldg. 40
Stony Brook, New York 11790-2356

Re: **Response to NYSDEC Comments of December 20, 2004 on the
*Systematic Subsurface Soil Sampling and Analysis Plan Beneath the 140 Building and
Systematic Subsurface Soil Sampling and Analysis Plan Beneath the 100 Building
Former Sylvania Electric Products Facility, #V00089-1***

Dear Mr. Stewart:

Thank you for your December 20, 2004 response to our November 17, 2004 submittal of the referenced Work Plans. To address your comments, the following responses have been prepared for your consideration. The comment responses are presented below, in full or in part, in the order that they appeared in your letter.

Comment 1: 100 Building - Vertical Sampling Depth

Please clarify ground surface reference point particularly as it relates to the loading dock area of the 100 property. The loading dock floor is approximately four to five feet below the 100 building's floor. The Department wants to ensure that the six foot buffer built into your sampling plan is not lost.

Response: *We are standardizing these borings to a baseline elevation on Site, therefore we will be able to maintain a consistent sampling depth interval applicable to the survey units. Based on this approach, the 6-foot buffer described in the Vertical Sampling Depth section of both plans is preserved.*

Comment 2: Soil Gas Sampling

Based on a preliminary analysis of the groundwater sampling results, there may still be undiscovered source areas for chlorinated solvents in the western and central portions of the site. As another tool in identifying the location of these volatile organic compounds, the Department requests that a soil gas sample be collected from each borehole after the proposed shallow samples have been removed.

Mr. Robert Stewart
January 20, 2005
Page 2

Please propose a depth at which to collect these soil gas samples which is somewhere between three feet and ten feet below the building slab. The samples could be analyzed by a PID in a head space sample or by your on-site laboratory, whichever you prefer.

Response: *As part of the standard operating procedures for sample recovery, every soil sample that is recovered is screened for soil gases using a PID as the sampler is opened. If a sample shows indications of volatile organic compounds above 10 parts per million, an additional soil sample is sent to the on-Site laboratory for analysis. The depths of sample recovery are defined within the plans and all sample locations in the Systematic Subsurface Soil Sampling protocol have at least one sample recovered from the 3- to 10-foot depth interval as requested.*

After the analytical data is available, we can evaluate the need for additional information with the NYSDEC.

Comment 3: Additional Investigation Borings Between Survey Units SU03 and SU04 and Between Survey Units SU04 and SU05 for the 100 Building

There is a space between survey units SU04 and SU05 and between SU03 and SU04. It is not necessary to alter the survey units. However, I am requesting five additional investigation borings at the locations shown in the attached figure to give better coverage.

The space between SU04 and SU05 is by western portion of the chemical processing area for the former AEC building on the south portion of the gap and by an historical metal storage tank and stucco building on the north portion of the gap. Groundwater data suggests the presence of potential nickel and VOC source areas near this gap. The nickel and radiological contamination found in cell 9 probably extends to under the 100 building.

The space between SU03 and SU04 is just north of the process tank found in the northwest corner of cell 10 and is near the eastern wall of the former AEC building. The piping leading from the 100 building to the former reservoir in the rear of the 100 property apparently originated near the northeast corner of the AEC building. Based on an old figure, there was a pump in the cellar of this portion of the building which probably was used to pump water to the reservoir. This area is of interest due to contamination discovered in the reservoir. Additionally, the source of the radiological contamination in MW-2, which is downgradient of this area, has apparently not been found yet.

It is for the above reasons that I am requesting the additional investigation borings.

Response: *We will add Borings A and B to SU03. Boring D will be added as a biased sample location in SU04 since it will not fall into the Systematic Sampling Protocol. Borings C and E will be added to SU05. The borings will be renamed to comply with the existing boring nomenclature used for the survey units, assigned to appropriate sampling interval columns, and sampled in accordance with the Systematic Sampling Protocol.*

Mr. Robert Stewart
January 20, 2005
Page 3

Comment 4: Historical Leaching Pool by the 140 Building Loading Dock

There is one historical leaching reportedly located inside the 140 building, just west of the loading dock, that was not investigated in the recent leaching pool investigation. It is just west of the former Building 2, the earlier commercial manufacturing building, and just east of a two-story frame building which I believe to be the "farm house". The farm house may have been used historically for machining operations. In SU07 for the 140 building, the survey point in the southeast corner of this survey unit comes very near the location of this former leaching pool. Please move this survey point slightly so that is located over the expected center of this pool. This pool must be investigated due to the high concentrations of PCE that were detected in nearby LPH21. Since the sediment sample in LPH21 detected percent concentrations, degreasing operations were most likely located historically somewhere near this pool. The leaching pool apparently is within the area identified as the "Lunch Room" on your figure. Please let me know if this presents a difficulty in investigating this pool.

If high soil gas readings are detected in any of the grid samples near the "Safety Cage" by the western portion of Building 2, additional borings will be requested around this area later. The western portion of that building would be the most likely source of the solvents that were found in LPH21.

Response: *This historic leaching pool, designated as LPH34, will be added and evaluated under the LPH Sampling Protocol. Reasonable attempts will be made to locate LPH34 and sample as many locations as possible using the LPH Sampling Protocol; however, several obstructions are present in this area (lunch room, loading dock, safety cage, equipment, etc.) that may impede access. Please note that we do not have any information regarding the historical use of this LPH.*

This letter will be attached as an addendum to the referenced work plans. We plan to begin work described in the subject work plans in mid January.

If you have any questions or require additional information, please do not hesitate to contact me. I can be reached at (214) 724-2506 or via facsimile (972) 719-0065.

Sincerely,


Jean M. Agostinelli
Vice President and Controller

Mr. Robert Stewart
January 20, 2005
Page 4

Walter Perish
Division of Environmental Remediation,
Region One
New York State Department of
Environmental Conservation
Building 40 – SUNY
Stony Brook, NY 11790-0248

Jerry Riggi
Division of Solid and Hazardous Materials
Bureau of Hazardous Waste & Radiation
Management
New York State Department of
Environmental Conservation
625 Broadway
Albany, NY 12233-7255

Jacquelyn Nealon
Bureau of Environmental Exposure
Investigation
New York State Department of Health
Flannegan Square, Rm 300
547 River Street
Troy, NY 12180-2216

Kevin Carpenter
Division of Environmental Remediation
New York State Department of
Environmental Conservation
625 Broadway
Albany, NY 12233-7015

Figure 100 Building Survey Units - Beneath

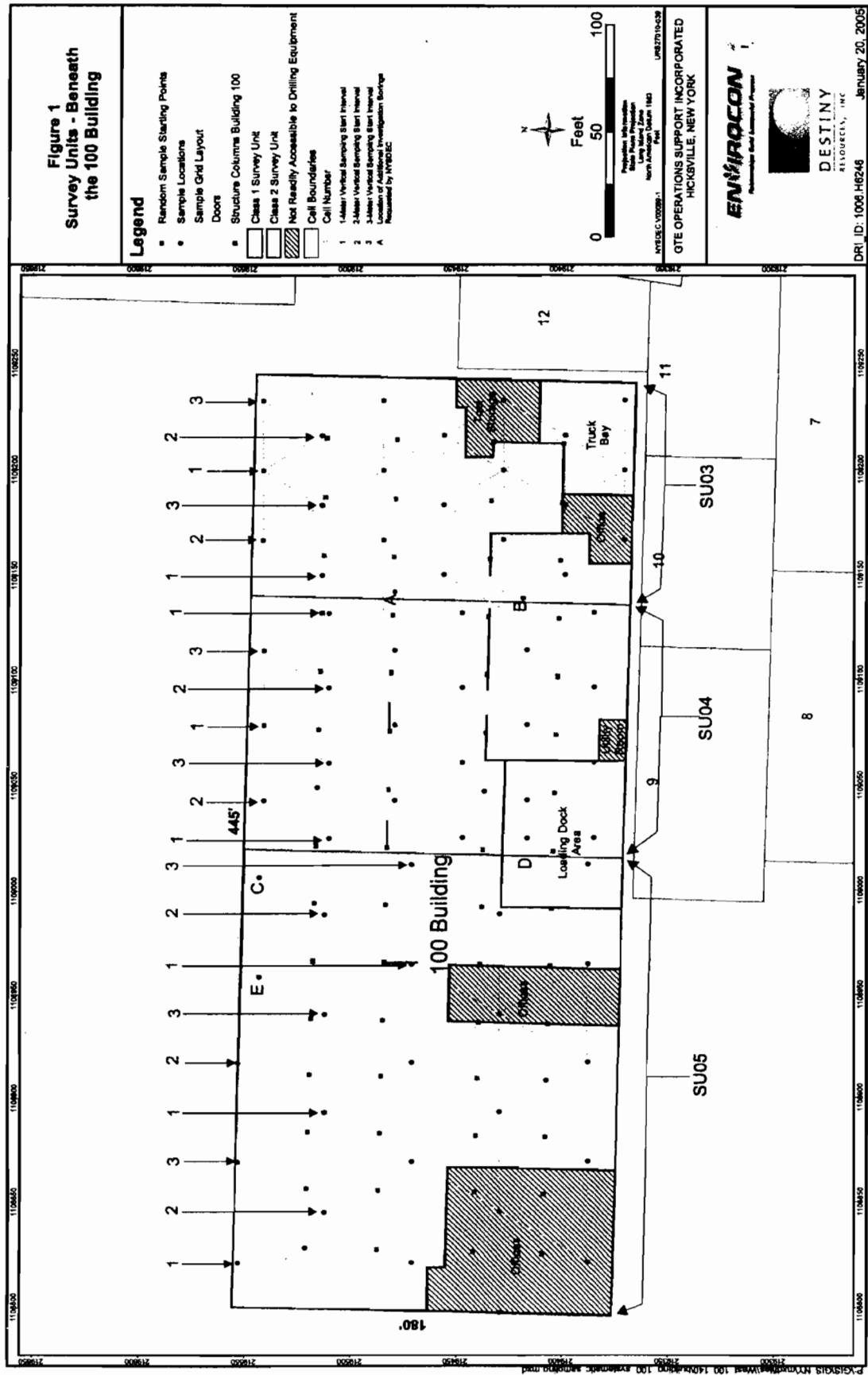
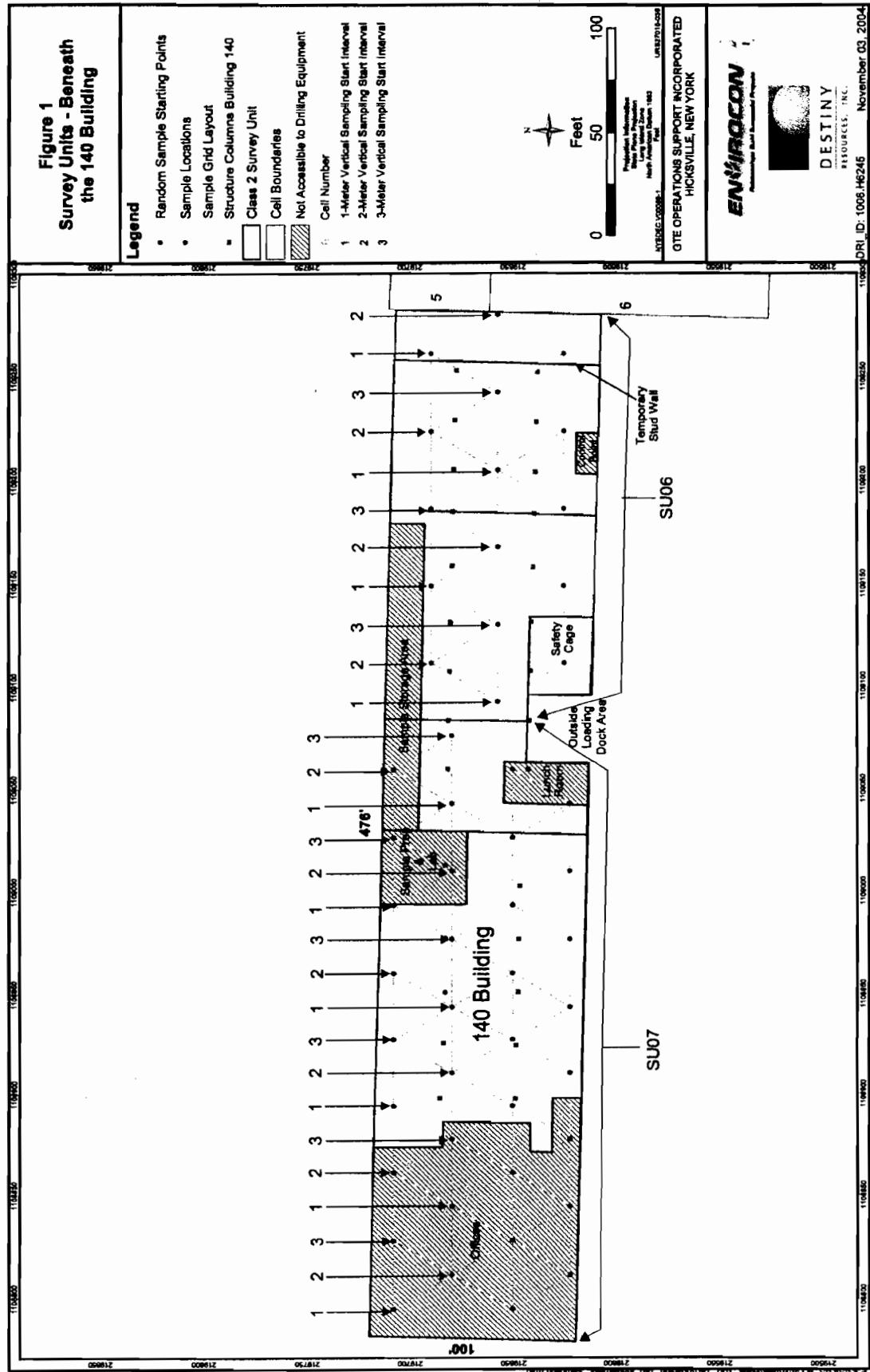


Figure 1
Survey Units - Beneath
the 140 Building



**New York State Department of Environmental Conservation
Division of Environmental Remediation, Region One**

Building 40 - SUNY, Stony Brook, New York 11790-2356

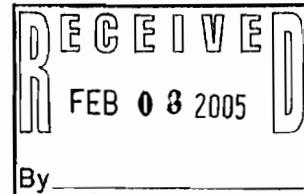
Phone: (631) 444-0240 • FAX: (631) 444-0248

Website: www.dec.state.ny.us



January 31, 2005

Jean Agostinelli
Vice President - Controller
GTE Operations Support, Inc.
600 Hidden Ridge Drive (HQE03E75)
Irving, TX 75038



Re: January 20, 2005 Response to NYSDEC Comments of December 20, 2004 on the SSSAP
Beneath the 140 Building and the SSSAP Beneath the 100 Building
Former Sylvania Electric Products Facility; Site # V00089-1

Dear Ms. Agostinelli:

As indicated in my conference call with your staff, the proposed changes to the Subsurface Soil Sampling and Analysis Plan (SSSAP) Beneath the 140 Building, November 2004 and the SSSAP Beneath the 100 Building, November 2004, as stated in your letter dated January 20, 2005 are acceptable. With a copy of the January 20, 2005 letter attached to each of the November 2004 SSSA Plans, these documents are both hereby approved.

As you know, the Department requested that a soil gas survey be performed in conjunction with the two investigations noted above. However, your staff indicated that it would be difficult to add this sampling to the proposed work. Instead, you have committed to perform a soil gas survey on a grid later to evaluate soil gases beneath the buildings. I am attaching a copy of an e-mail message documenting your commitment to perform the soil gas survey.

You may proceed with these investigations. I am requesting that after you complete each borehole that you backfill them with clean, sandy fill of the similar porosity in each boring. If this presents any difficulties to you, please let me know. After you have completed each survey unit, the Department plans to perform a preliminary soil gas survey for each survey unit by inserting a soil gas probe into the backfilled soils to approximately 31 inches in each borehole. The soils will be pushed down around the probe at the surface to prevent drawing in vapors from above the borehole. The soil probe will be connected to an HNu with a 10.2 eV probe calibrated to benzene. Peak and steady-state soil gas readings will be recorded. The purpose of these preliminary soil gas surveys for SU-03 through SU-07 is to help determine the grid spacing and analytical requirements for the subsequent soil gas surveys for these survey units that you will perform later. It is also expected that the results of the preliminary soil gas surveys will help the Department with its interpretation of the results of your soil sampling for volatile organic compounds. Of course, you may oversee this sampling and I'll share my results with you.

The Department realizes that the preliminary soil gas surveys performed by the Department are just a preliminary screening tool. Consequently, no formal report will be prepared.

If you have any questions, please do not hesitate to call me.

Sincerely,



Robert R. Stewart

Environmental Engineer I

Enclosure

cc: W. Parish
 J. Riggi
 K. Carpenter
 J. Nealon, NYSDOH

From: <elie.a.ghannoum@verizon.com>
To: "Robert Stewart" <rrstewar@gw.dec.state.ny.us>, "Walter Parish"
<wjparish@gw.dec.state.ny.us>
Date: 1/27/05 1:38PM
Subject: January 26, 05 Conference Call

Bob, per our conference call as of yesterday (1/26/05) with you and Walter, if the Department feels that it is necessary to conduct soil vapor sampling within the survey units 3 through 7 of the 140 and 100 Buildings once the soil investigation beneath the Buildings are completed and the results of the investigation are presented to the Department, GTEOSI will submit to NYSDEC a sampling grid pattern and established protocol by which such sampling will be conducted. With the understanding as described above, GTEOSI, with your approval, will commence the work as outlined in our letter to you dated November 17, 2004 and our January 20, 2005 response to your comments of December 20, 2004 on the Systematic Subsurface Soil Sampling and Analysis Plan Beneath the 140 Building and Systematic Subsurface Soil Sampling and Analysis Plan Beneath the 100 Building.

Thanks

Elie

(Embedded image moved to file:
pic06903.gif)

CC: "Lucky Tabor" <LTabor@envirocon.com>, <Rob_Brathovde@URSCorp.com>, <Carol_Scholl@URSCorp.com>, <Michael_Ander@URSCorp.com>, <jean.agostinelli@verizon.com>

SU06 MARSSIM Evaluation Results Using Severn Trent Laboratories, Inc. Sample Results

SU06, Intervals 1, 2, and 3 passed the MARSSIM¹ Sign Test and the associated soils are considered releasable from a radiological perspective. These intervals consist of SP samples collected and analyzed in the 0 to 3-m, 3 to 6-m, and 6 to 9-m depth ranges, respectively. The MARSSIM protocol uses a non-parametric statistical analysis test that evaluates all of the SP sample results for a single interval separately. Therefore, there were three independent evaluations within the three-dimensional footprint of SU06.

There were a total of 15 SP sample results in Interval 1, Interval 2, and Interval 3, respectively. All samples were analyzed for radiological analytes of interest (Th-232, U-234, and U-238) for purposes of this evaluation. The sample results for each of the samples are presented in **Table 2** and are the results reported by STL.

The charts on the subsequent pages of this appendix were generated by the COMPASS² computer code. As shown on the first page of the COMPASS Surface Soil Survey Plan for Intervals 1 and 2, a minimum of 13 soil sample analyses were sufficient for the MARSSIM-based analysis to be statistically significant. As shown on the first page of the COMPASS Surface Soil Survey Plan for Interval 3, a minimum of 14 soil sample analyses were sufficient for the MARSSIM-based analysis to be statistically significant. As stated earlier, this MARSSIM-based analysis for Intervals 1, 2, and 3 in this SU were each based on 15 soil sample analyses, respectively.

Included in the assessment of SU06 are three reports. The cover report is titled *Site Report* and provides information the radiological contaminants and their respective DCGLw³ (the Site cleanup levels specified in the Work Plan) used in the evaluation of each interval.

Each interval assessment is comprised of two COMPASS reports. The first report is titled *Surface Soil Survey Plan*. This report contains information that was used in the planning phase of the survey or soil sample collection. This information was based on the Site's cleanup levels and cell parameters or is information that was derived from these parameters. The last section of this report contains information that, by design, was an estimate of the average concentration and the standard deviation anticipated to be present in the survey unit interval for each radionuclide. The values in this report were based on the actual average concentration and standard deviation of each radionuclide as calculated from the sample results.

The second report is titled *DQA Surface Soil Report*. This report presents the results of performing a non-parametric statistical analysis called the Sign Test on the samples results. On the first page of this report is given the *Assessment Conclusion* which is *Reject Null Hypothesis (Survey Unit PASSES)* for all three intervals. The only other possible conclusion is if the survey unit did not pass. Other information presented in the report is either input information that is echoed back in the report or is information related to the performance of the Sign Test. Also included in the report is a table titled *Basic Statistical Quantities Summary*. The average or mean SOR is shown in this table. This SOR value is high (conservative) by approximately a factor of 2 due to the use of individual uranium radionuclides in the evaluation and the limitations on the flexibility of this version of COMPASS. The information in this table supports the earlier stated conclusion as it demonstrates that the average concentration of radiological contaminants is significantly below the cleanup levels.

¹ NUREG-1575, Multi-Agency Radiation Survey and Site Investigation Manual (MARSSIM), August 2000.

² COMPASS Code Version 1.0.0 was developed under the sponsorship of the U. S. Nuclear Regulatory Commission for implementing the MARSSIM in support of the decommissioning license termination rule (10 CFR Part 20, Subpart E).

³ For these purposes, the term DCGL is synonymous with the term cleanup level.



Site Report

Site Summary

Site Name: GTEOSI - Hicksville Site

Planner(s): Shane Brightwell

Contaminant Summary

NOTE: Surface soil DCGLw units are pCi/g.
Building surface DCGLw units are dpm/100 cm².

| Contaminant | Type | DCGLw | Screening Value Used? | Area (m ²) | Area Factor |
|-------------|--------------|-------|-----------------------|------------------------|-------------|
| Th-232 | Surface Soil | 2.80 | No | 1 | 12.3 |
| | | | | 3 | 6.08 |
| | | | | 10 | 3.12 |
| | | | | 30 | 2.24 |
| | | | | 100 | 1.75 |
| | | | | 300 | 1.47 |
| | | | | 1,000 | 1.05 |
| | | | | 3,000 | 1.03 |
| | | | | 10,000 | 1 |
| | | | | | |
| U-234 | Surface Soil | 50.00 | No | 1 | 30.5 |
| | | | | 3 | 18.3 |
| | | | | 10 | 11.1 |
| | | | | 30 | 5.73 |
| | | | | 100 | 2.27 |
| | | | | 300 | 1.43 |
| | | | | 1,000 | 1.04 |
| | | | | 3,000 | 1.01 |
| | | | | 10,000 | 1 |
| | | | | | |
| U-238 | Surface Soil | 50.00 | No | 1 | 30.5 |
| | | | | 3 | 18.3 |
| | | | | 10 | 11.1 |
| | | | | 30 | 5.73 |
| | | | | 100 | 2.27 |
| | | | | 300 | 1.43 |
| | | | | 1,000 | 1.04 |
| | | | | 3,000 | 1.01 |
| | | | | 10,000 | 1 |
| | | | | | |

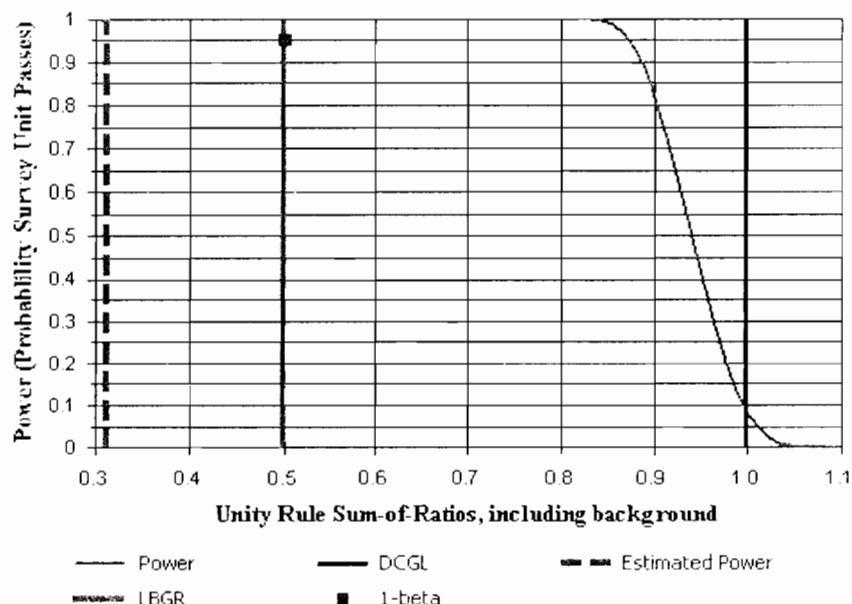


Surface Soil Survey Plan

Survey Plan Summary

| | | | |
|-------------------------|--------------------------|------------------------|------|
| Site: | GTEOSI - Hicksville Site | | |
| Planner(s): | Shane Brightwell | | |
| Survey Unit Name: | SU06 Interval 1 01 | | |
| Comments: | SU06 Interval 1 Run 01 | | |
| Area (m ²): | 1,635 | Classification: | 2 |
| Selected Test: | Sign | Estimated Sigma (SOR): | 0.12 |
| DCGL (SOR): | 1 | Sample Size (N): | 13 |
| LBGR (SOR): | 0.5 | Estimated Conc. (SOR): | 0.31 |
| Alpha: | 0.050 | Estimated Power: | 1 |
| Beta: | 0.050 | | |

Prospective Power Curve





Surface Soil Survey Plan

Contaminant Summary

| Contaminant | DCGLw (pCi/g) | Inferred Contaminant | Ratio | Modified DCGLw (pCi/g) | Scan MDC (pCi/g) |
|-------------|------------------|-------------------------|-------|---------------------------|---------------------|
| Th-232 | 2.80 | N/A | N/A | N/A | N/A |
| U-234 | 50.00 | N/A | N/A | N/A | N/A |
| U-238 | 50.00 | N/A | N/A | N/A | N/A |

| Contaminant | Survey Unit Estimate (Mean ± 1-Sigma) (pCi/g) | Reference Area Estimate (Mean ± 1-Sigma) (pCi/g) |
|-------------|---|--|
| Th-232 | 0.631 ± 0.278 | N/A |
| U-234 | | N/A |
| U-238 | | N/A |

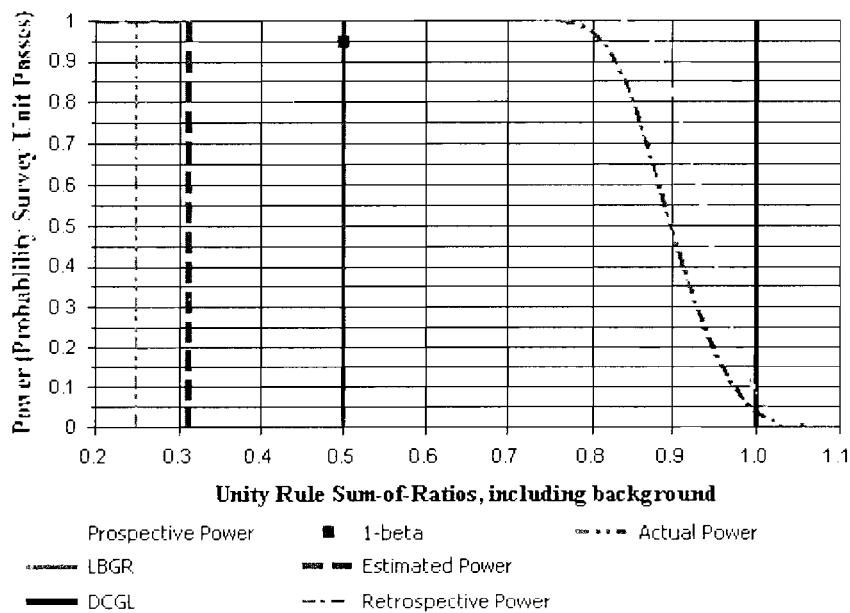


DQA Surface Soil Report

Assessment Summary

Site: GTEOSI - Hicksville Site
Planner(s): Shane Brightwell
Survey Unit Name: SU06 Interval 1 01
Report Number: 1
Survey Unit Samples: 15
Reference Area Samples: 0
Test Performed: Sign Test Result: Not Performed
Judgmental Samples: 0 EMC Result: Not Performed
Assessment Conclusion: ***Reject Null Hypothesis (Survey Unit PASSES)***

Retrospective Power Curve





DQA Surface Soil Report

Survey Unit Data

NOTE: Type = "S" indicates survey unit sample.
Type = "R" indicates reference area sample.

| Sample Number | Type | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) |
|---------------|------|----------------|---------------|---------------|
| 27977 | S | 0.47 | 2.44 | 1.19 |
| 26851 | S | 0.83 | 2.37 | 1.87 |
| 28398 | S | 0.58 | 0.5 | 0.61 |
| 27682 | S | 0.97 | 7.4 | 6.06 |
| 28278 | S | 0.64 | 5.19 | 1.93 |
| 27060 | S | 0.72 | 5.76 | 5.42 |
| 28342 | S | 0.38 | 1.08 | 0.77 |
| 27318 | S | 0.65 | 0.69 | 0.41 |
| 27882 | S | 0.36 | 1.91 | 0.83 |
| 28205 | S | 0.79 | 3.19 | 2.33 |
| 27776 | S | 1.07 | 4.62 | 4.89 |
| 27421 | S | 1.08 | 0.75 | 0.76 |
| 28107 | S | 0.42 | 0.42 | 0.38 |
| 27593 | S | 0.22 | 0.29 | 0.27 |
| 27502 | S | 0.29 | 0.32 | 0.23 |

Modified Data (Unity Rule SOR)

NOTE: Type = "S" indicates survey unit sample.
Type = "R" indicates reference area sample.

| Sample Number | Type | Sum-of-Ratios (SOR) |
|---------------|------|---------------------|
| 27977 | S | 0.24 |
| 26851 | S | 0.38 |
| 28398 | S | 0.23 |
| 27682 | S | 0.62 |
| 28278 | S | 0.37 |
| 27060 | S | 0.48 |
| 28342 | S | 0.17 |
| 27318 | S | 0.25 |
| 27882 | S | 0.18 |
| 28205 | S | 0.39 |
| 27776 | S | 0.57 |
| 27421 | S | 0.42 |
| 28107 | S | 0.17 |
| 27593 | S | 0.09 |
| 27502 | S | 0.11 |



DQA Surface Soil Report

Basic Statistical Quantities Summary

| Statistic | Survey Unit | Background | DQO Results |
|------------------|-------------|------------|-------------|
| Sample Number | 15 | N/A | N=13 |
| Mean (SOR) | 0.31 | N/A | 0.31 |
| Median (SOR) | 0.25 | N/A | N/A |
| Std Dev (SOR) | 0.16 | N/A | 0.12 |
| High Value (SOR) | 0.62 | N/A | N/A |
| Low Value (SOR) | 0.09 | N/A | N/A |

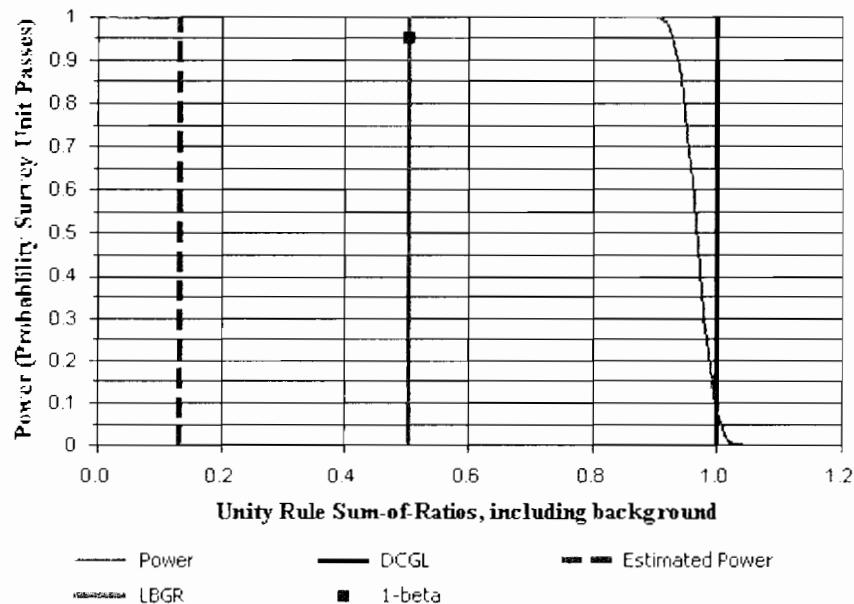


Surface Soil Survey Plan

Survey Plan Summary

| | | | |
|-------------------------|--------------------------|------------------------|------|
| Site: | GTEOSI - Hicksville Site | | |
| Planner(s): | Shane Brightwell | | |
| Survey Unit Name: | SU06 Interval 2 01 | | |
| Comments: | SU06 Interval 2 Run 01 | | |
| Area (m ²): | 1,635 | Classification: | 2 |
| Selected Test: | Sign | Estimated Sigma (SOR): | 0.07 |
| DCGL (SOR): | 1 | Sample Size (N): | 13 |
| LBGR (SOR): | 0.5 | Estimated Conc. (SOR): | 0.13 |
| Alpha: | 0.050 | Estimated Power: | 1 |
| Beta: | 0.050 | | |

Prospective Power Curve





Surface Soil Survey Plan

Contaminant Summary

| Contaminant | DCGLw (pCi/g) | Inferred Contaminant | Ratio | Modified DCGLw (pCi/g) | Scan MDC (pCi/g) |
|-------------|------------------|-------------------------|-------|---------------------------|---------------------|
| Th-232 | 2.80 | N/A | N/A | N/A | N/A |
| U-234 | 50.00 | N/A | N/A | N/A | N/A |
| U-238 | 50.00 | N/A | N/A | N/A | N/A |

| Contaminant | Survey Unit Estimate (Mean \pm 1-Sigma) (pCi/g) | Reference Area Estimate (Mean \pm 1-Sigma) (pCi/g) |
|-------------|---|--|
| Th-232 | 0.224 ± 0.075 | N/A |
| U-234 | 1.788 ± 0.945 | N/A |
| U-238 | 0.945 ± 2.837 | N/A |

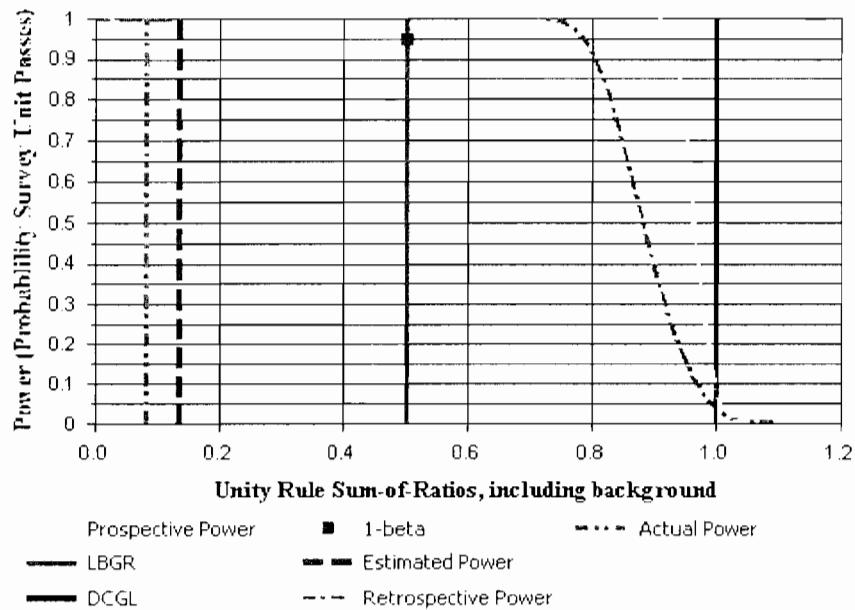


DQA Surface Soil Report

Assessment Summary

Site: GTEOSI - Hicksville Site
Planner(s): Shane Brightwell
Survey Unit Name: SU06 Interval 2 01
Report Number: 1
Survey Unit Samples: 15
Reference Area Samples: 0
Test Performed: Sign Test Result: Not Performed
Judgmental Samples: 0 EMC Result: Not Performed
Assessment Conclusion: ***Reject Null Hypothesis (Survey Unit PASSES)***

Retrospective Power Curve





DQA Surface Soil Report

Survey Unit Data

NOTE: Type = "S" indicates survey unit sample.
Type = "R" indicates reference area sample.

| Sample Number | Type | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) |
|---------------|------|----------------|---------------|---------------|
| 28008 | S | 0.42 | 0.32 | 0.33 |
| 26873 | S | 0.27 | 0.24 | 0.3 |
| 28413 | S | 0.25 | 0.23 | 0.24 |
| 27705 | S | 0.27 | 0.31 | 0.24 |
| 28299 | S | 0.21 | 0.22 | 0.22 |
| 27082 | S | 0.17 | 0.21 | 0.24 |
| 28359 | S | 0.19 | 0.19 | 0.22 |
| 27335 | S | 0.26 | 0.21 | 0.21 |
| 27911 | S | 0.15 | 0.24 | 0.18 |
| 28223 | S | 0.17 | 0.21 | 0.16 |
| 27791 | S | 0.26 | 0.16 | 0.18 |
| 27436 | S | 0.19 | 0.2 | 0.17 |
| 28144 | S | 0.28 | 23.8 | 11.2 |
| 27609 | S | 0.1 | 0.13 | 0.13 |
| 27528 | S | 0.17 | 0.14 | 0.15 |

Modified Data (Unity Rule SOR)

NOTE: Type = "S" indicates survey unit sample.
Type = "R" indicates reference area sample.

| Sample Number | Type | Sum-of-Ratios (SOR) |
|---------------|------|---------------------|
| 28008 | S | 0.16 |
| 26873 | S | 0.11 |
| 28413 | S | 0.1 |
| 27705 | S | 0.11 |
| 28299 | S | 0.08 |
| 27082 | S | 0.07 |
| 28359 | S | 0.08 |
| 27335 | S | 0.1 |
| 27911 | S | 0.06 |
| 28223 | S | 0.07 |
| 27791 | S | 0.1 |
| 27436 | S | 0.07 |
| 28144 | S | 0.8 |
| 27609 | S | 0.04 |
| 27528 | S | 0.07 |



DQA Surface Soil Report

Basic Statistical Quantities Summary

| Statistic | Survey Unit | Background | DQO Results |
|------------------|-------------|------------|-------------|
| Sample Number | 15 | N/A | N=13 |
| Mean (SOR) | 0.13 | N/A | 0.13 |
| Median (SOR) | 0.08 | N/A | N/A |
| Std Dev (SOR) | 0.19 | N/A | 0.07 |
| High Value (SOR) | 0.80 | N/A | N/A |
| Low Value (SOR) | 0.04 | N/A | N/A |

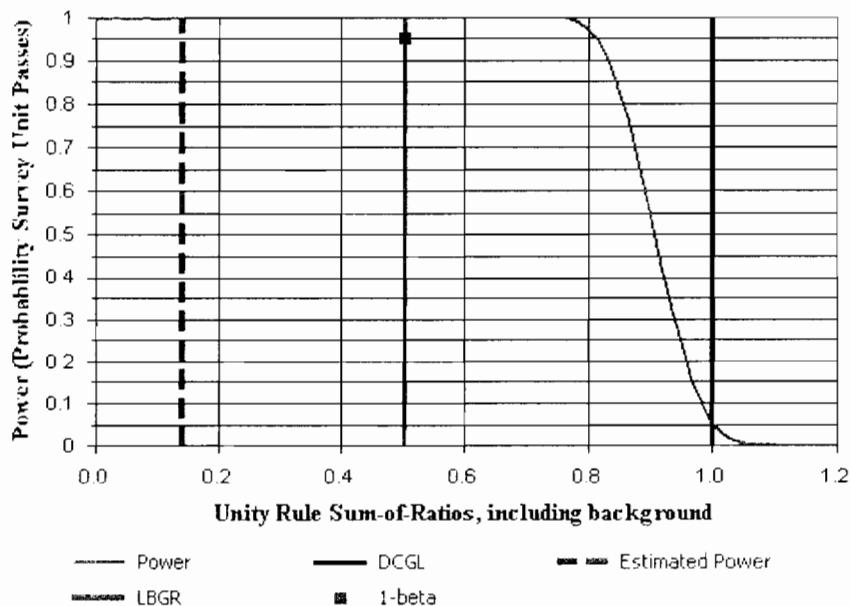


Surface Soil Survey Plan

Survey Plan Summary

| | | | |
|-------------------------|--------------------------|------------------------|------|
| Site: | GTEOSI - Hicksville Site | | |
| Planner(s): | Shane Brightwell | | |
| Survey Unit Name: | SU06 Interval 3 01 | | |
| Comments: | SU06 Interval 3 Run 01 | | |
| Area (m ²): | 1,635 | Classification: | 2 |
| Selected Test: | Sign | Estimated Sigma (SOR): | 0.17 |
| DCGL (SOR): | 1 | Sample Size (N): | 14 |
| LBGR (SOR): | 0.5 | Estimated Conc. (SOR): | 0.14 |
| Alpha: | 0.050 | Estimated Power: | 1 |
| Beta: | 0.050 | | |

Prospective Power Curve





Surface Soil Survey Plan

Contaminant Summary

| Contaminant | DCGLw (pCi/g) | Inferred Contaminant | Ratio | Modified DCGLw (pCi/g) | Scan MDC (pCi/g) |
|-------------|------------------|-------------------------|-------|---------------------------|---------------------|
| Th-232 | 2.80 | N/A | N/A | N/A | N/A |
| U-234 | 50.00 | N/A | N/A | N/A | N/A |
| U-238 | 50.00 | N/A | N/A | N/A | N/A |

| Contaminant | Survey Unit Estimate (Mean \pm 1-Sigma) (pCi/g) | Reference Area Estimate (Mean \pm 1-Sigma) (pCi/g) |
|-------------|---|--|
| Th-232 | 0.218 ± 0.055 | N/A |
| U-234 | 2.125 ± 7.435 | N/A |
| U-238 | 1.167 ± 3.827 | N/A |

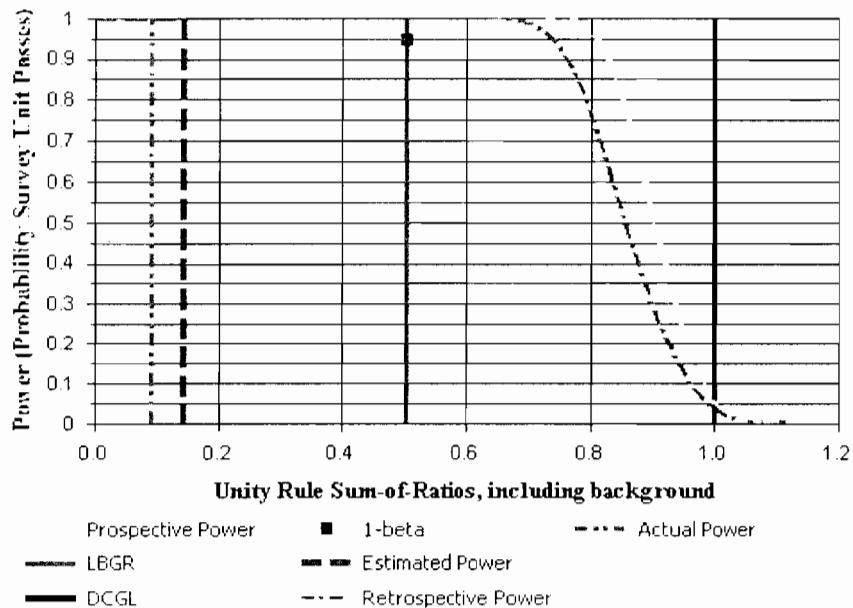


DQA Surface Soil Report

Assessment Summary

Site: GTEOSI - Hicksville Site
Planner(s): Shane Brightwell
Survey Unit Name: SU06 Interval 3 01
Report Number: 1
Survey Unit Samples: 15
Reference Area Samples: 0
Test Performed: Sign Test Result: Not Performed
Judgmental Samples: 0 EMC Result: Not Performed
Assessment Conclusion: ***Reject Null Hypothesis (Survey Unit PASSES)***

Retrospective Power Curve





DQA Surface Soil Report

Survey Unit Data

NOTE: Type = "S" indicates survey unit sample.
Type = "R" indicates reference area sample.

| Sample Number | Type | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) |
|---------------|------|----------------|---------------|---------------|
| 28017 | S | 0.14 | 0.18 | 0.21 |
| 26899 | S | 0.24 | 0.22 | 0.23 |
| 28420 | S | 0.22 | 0.18 | 0.17 |
| 27720 | S | 0.25 | 0.17 | 0.18 |
| 28318 | S | 0.3 | 0.19 | 0.14 |
| 27094 | S | 0.33 | 0.32 | 0.33 |
| 28371 | S | 0.16 | 0.2 | 0.13 |
| 27365 | S | 0.19 | 0.18 | 0.18 |
| 27931 | S | 0.26 | 0.2 | 0.17 |
| 28257 | S | 0.18 | 0.3 | 0.16 |
| 27816 | S | 0.17 | 0.13 | 0.14 |
| 27453 | S | 0.26 | 0.27 | 0.18 |
| 28171 | S | 0.24 | 29 | 15 |
| 27635 | S | 0.18 | 0.16 | 0.13 |
| 27555 | S | 0.17 | 0.16 | 0.17 |

Modified Data (Unity Rule SOR)

NOTE: Type = "S" indicates survey unit sample.
Type = "R" indicates reference area sample.

| Sample Number | Type | Sum-of-Ratios (SOR) |
|---------------|------|---------------------|
| 28017 | S | 0.06 |
| 26899 | S | 0.09 |
| 28420 | S | 0.09 |
| 27720 | S | 0.1 |
| 28318 | S | 0.11 |
| 27094 | S | 0.13 |
| 28371 | S | 0.06 |
| 27365 | S | 0.07 |
| 27931 | S | 0.1 |
| 28257 | S | 0.07 |
| 27816 | S | 0.07 |
| 27453 | S | 0.1 |
| 28171 | S | 0.97 |
| 27635 | S | 0.07 |
| 27555 | S | 0.07 |



DQA Surface Soil Report

Basic Statistical Quantities Summary

| Statistic | Survey Unit | Background | DQO Results |
|------------------|-------------|------------|-------------|
| Sample Number | 15 | N/A | N=14 |
| Mean (SOR) | 0.14 | N/A | 0.14 |
| Median (SOR) | 0.09 | N/A | N/A |
| Std Dev (SOR) | 0.23 | N/A | 0.17 |
| High Value (SOR) | 0.97 | N/A | N/A |
| Low Value (SOR) | 0.06 | N/A | N/A |

SU07 MARSSIM Evaluation Results Using Severn Trent Laboratories, Inc. Sample Results

SU07, Intervals 1, 2, and 3 passed the MARSSIM¹ Sign Test and the associated soils are considered releasable from a radiological perspective. These intervals consist of SP samples collected and analyzed in the 0 to 3-m, 3 to 6-m, and 6 to 9-m depth ranges, respectively. The MARSSIM protocol uses a non-parametric statistical analysis test that evaluates all of the SP sample results for a single interval separately. Therefore, there were three independent evaluations within the three-dimensional footprint of SU07.

There were a total of 22 SP sample results in Interval 1, Interval 2, and Interval 3, respectively. All samples were analyzed for radiological analytes of interest (Th-232, U-234, and U-238) for purposes of this evaluation. The sample results for each of the samples are presented in **Table 2** and are the results reported by STL.

The charts on the subsequent pages of this appendix were generated by the COMPASS² computer code. As shown on the first page of the COMPASS Surface Soil Survey Plan for Interval 1, a minimum of 15 soil sample analyses were sufficient for the MARSSIM-based analysis to be statistically significant. As shown on the first page of the COMPASS Surface Soil Survey Plan for Intervals 2 and 3, a minimum of 13 soil sample analyses were sufficient for the MARSSIM-based analyses to be statistically significant. As stated earlier, this MARSSIM-based analysis for Intervals 1, 2, and 3 in this SU were each based on 22 soil sample analyses, respectively.

Included in the assessment of SU07 are three reports. The cover report is titled *Site Report* and provides information the radiological contaminants and their respective DCGLw³ (the Site cleanup levels specified in the Work Plan) used in the evaluation of each interval.

Each interval assessment is comprised of two COMPASS reports. The first report is titled *Surface Soil Survey Plan*. This report contains information that was used in the planning phase of the survey or soil sample collection. This information was based on the Site's cleanup levels and cell parameters or is information that was derived from these parameters. The last section of this report contains information that, by design, was an estimate of the average concentration and the standard deviation anticipated to be present in the survey unit interval for each radionuclide. The values in this report were based on the actual average concentration and standard deviation of each radionuclide as calculated from the sample results.

The second report is titled *DQA Surface Soil Report*. This report presents the results of performing a non-parametric statistical analysis called the Sign Test on the samples results. On the first page of this report is given the *Assessment Conclusion* which is *Reject Null Hypothesis (Survey Unit PASSES)* for all three intervals. The only other possible conclusion is if the survey unit did not pass. Other information presented in the report is either input information that is echoed back in the report or is information related to the performance of the Sign Test. Also included in the report is a table titled *Basic Statistical Quantities Summary*. The average or mean SOR is shown in this table. This SOR value is high (conservative) by approximately a factor of 2 due to the use of individual uranium radionuclides in the evaluation and the limitations on the flexibility of this version of COMPASS. The information in this table supports the earlier stated conclusion as it demonstrates that the average concentration of radiological contaminants is significantly below the cleanup levels.

¹ NUREG-1575, Multi-Agency Radiation Survey and Site Investigation Manual (MARSSIM), August 2000.

² COMPASS Code Version 1.0.0 was developed under the sponsorship of the U. S. Nuclear Regulatory Commission for implementing the MARSSIM in support of the decommissioning license termination rule (10 CFR Part 20, Subpart E).

³ For these purposes, the term DCGL is synonymous with the term cleanup level.



Site Report

Site Summary

Site Name: GTEOSI - Hicksville Site
Planner(s): Shane Brightwell

Contaminant Summary

NOTE: Surface soil DCGLw units are pCi/g.
Building surface DCGLw units are dpm/100 cm²

| Contaminant | Type | DCGLw | Screening Value Used? | Area (m ²) | Area Factor |
|-------------|--------------|-------|-----------------------|------------------------|-------------|
| Th-232 | Surface Soil | 2.80 | No | 1 | 12.3 |
| | | | | 3 | 6.08 |
| | | | | 10 | 3.12 |
| | | | | 30 | 2.24 |
| | | | | 100 | 1.75 |
| | | | | 300 | 1.47 |
| | | | | 1,000 | 1.05 |
| | | | | 3,000 | 1.03 |
| | | | | 10,000 | 1 |
| | | | | | |
| U-234 | Surface Soil | 50.00 | No | 1 | 30.5 |
| | | | | 3 | 18.3 |
| | | | | 10 | 11.1 |
| | | | | 30 | 5.73 |
| | | | | 100 | 2.27 |
| | | | | 300 | 1.43 |
| | | | | 1,000 | 1.04 |
| | | | | 3,000 | 1.01 |
| | | | | 10,000 | 1 |
| | | | | | |
| U-238 | Surface Soil | 50.00 | No | 1 | 30.5 |
| | | | | 3 | 18.3 |
| | | | | 10 | 11.1 |
| | | | | 30 | 5.73 |
| | | | | 100 | 2.27 |
| | | | | 300 | 1.43 |
| | | | | 1,000 | 1.04 |
| | | | | 3,000 | 1.01 |
| | | | | 10,000 | 1 |
| | | | | | |

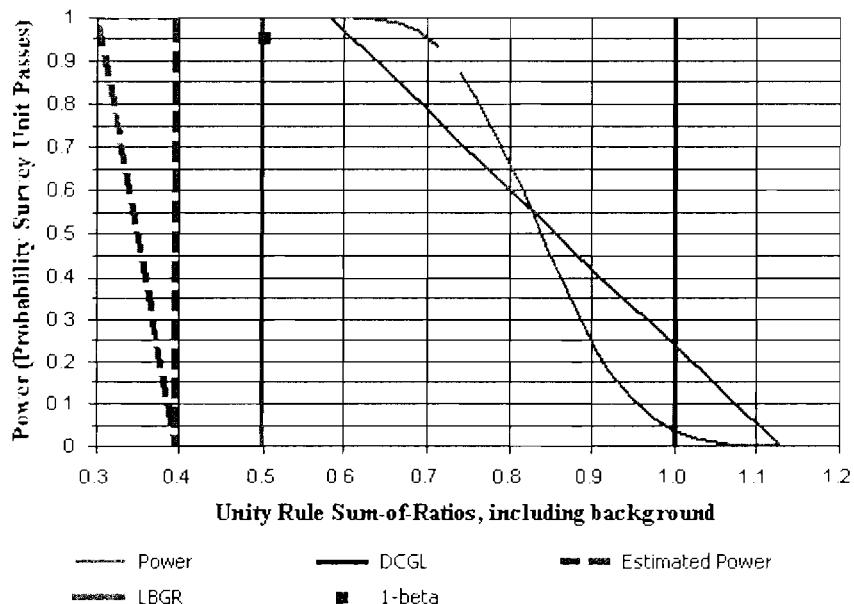


Surface Soil Survey Plan

Survey Plan Summary

| | | | |
|-------------------------|--------------------------|------------------------|------|
| Site: | GTEOSI - Hicksville Site | | |
| Planner(s): | Shane Brightwell | | |
| Survey Unit Name: | SU07 Interval 1 01 | | |
| Comments: | SU07 Interval 1 Run 01 | | |
| Area (m ²): | 1,411 | Classification: | 2 |
| Selected Test: | Sign | Estimated Sigma (SOR): | 0.26 |
| DCGL (SOR): | 1 | Sample Size (N): | 15 |
| LBGR (SOR): | 0.5 | Estimated Conc. (SOR): | 0.4 |
| Alpha: | 0.050 | Estimated Power: | 1 |
| Beta: | 0.050 | | |

Prospective Power Curve





Surface Soil Survey Plan

Contaminant Summary

| Contaminant | DCGLw (pCi/g) | Inferred Contaminant | Ratio | Modified DCGLw (pCi/g) | Scan MDC (pCi/g) |
|-------------|------------------|-------------------------|-------|---------------------------|---------------------|
| Th-232 | 2.80 | N/A | N/A | N/A | N/A |
| U-234 | 50.00 | N/A | N/A | N/A | N/A |
| U-238 | 50.00 | N/A | N/A | N/A | N/A |

| Contaminant | Survey Unit Estimate (Mean \pm 1-Sigma) (pCi/g) | Reference Area Estimate (Mean \pm 1-Sigma) (pCi/g) |
|-------------|---|--|
| Th-232 | 0.513 ± 0.206 | N/A |
| U-234 | 6.279 ± 10.16 | N/A |
| U-238 | 4.335 ± 7.145 | N/A |

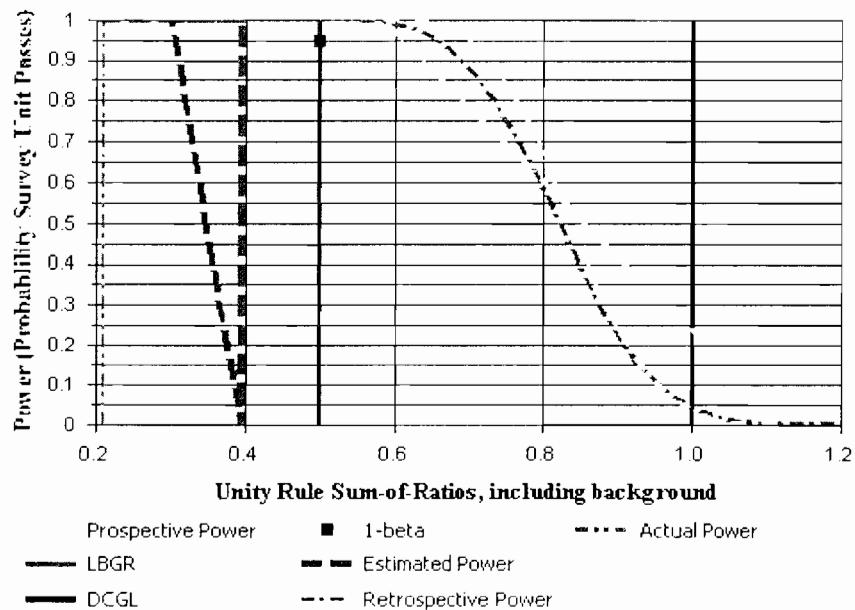


DQA Surface Soil Report

Assessment Summary

Site: GTEOSI - Hicksville Site
Planner(s): Shane Brightwell
Survey Unit Name: SU07 Interval 1 01
Report Number: 1
Survey Unit Samples: 22
Reference Area Samples: 0
Test Performed: Sign Test Result: Pass
Judgmental Samples: 0 EMC Result: Not Performed
Assessment Conclusion: ***Reject Null Hypothesis (Survey Unit PASSES)***

Retrospective Power Curve





DQA Surface Soil Report

Survey Unit Data

NOTE: Type = "S" indicates survey unit sample.
Type = "R" indicates reference area sample.

| Sample Number | Type | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) |
|---------------|------|----------------|---------------|---------------|
| 29454 | S | 0.39 | 0.53 | 0.47 |
| 29209 | S | 0.73 | 15.3 | 8.8 |
| 29346 | S | 0.43 | 26.8 | 26.6 |
| 28746 | S | 0.76 | 24.1 | 11.6 |
| 29656 | S | 0.56 | 9.5 | 9.3 |
| 29067 | S | 0.85 | 2.69 | 2.63 |
| 29545 | S | 0.69 | 18.5 | 18.9 |
| 28902 | S | 0.93 | 32.4 | 10.3 |
| 29256 | S | 0.78 | 0.62 | 0.55 |
| 29717 | S | 0.57 | 3.04 | 2.7 |
| 29030 | S | 0.37 | 0.43 | 0.41 |
| 29403 | S | 0.38 | 0.48 | 0.53 |
| 28517 | S | 0.52 | 0.97 | 0.29 |
| 29620 | S | 0.46 | 0.41 | 0.4 |
| 28969 | S | 0.57 | 0.39 | 0.32 |
| 29306 | S | 0.36 | 0.32 | 0.3 |
| 29791 | S | 0.18 | 0.22 | 0.01 |
| 29127 | S | 0.39 | 0.3 | 0.22 |
| 28456 | S | 0.3 | 0.29 | 0.29 |
| 29577 | S | 0.2 | 0.23 | 0.19 |
| 28844 | S | 0.36 | 0.24 | 0.26 |
| 29500 | S | 0.52 | 0.38 | 0.28 |

Modified Data (Unity Rule SOR)

NOTE: Type = "S" indicates survey unit sample.
Type = "R" indicates reference area sample.

| Sample Number | Type | Sum-of-Ratios (SOR) |
|---------------|------|---------------------|
| 29454 | S | 0.16 |
| 29209 | S | 0.74 |
| 29346 | S | 1.22 |
| 28746 | S | 0.99 |
| 29656 | S | 0.58 |
| 29067 | S | 0.41 |
| 29545 | S | 0.99 |
| 28902 | S | 1.19 |
| 29256 | S | 0.3 |
| 29717 | S | 0.32 |
| 29030 | S | 0.15 |
| 29403 | S | 0.16 |
| 28517 | S | 0.21 |
| 29620 | S | 0.18 |
| 28969 | S | 0.22 |
| 29306 | S | 0.14 |
| 29791 | S | 0.07 |
| 29127 | S | 0.15 |



DQA Surface Soil Report

Modified Data (Unity Rule SOR)

NOTE: Type = "S" indicates survey unit sample.
Type = "R" indicates reference area sample.

| Sample Number | Type | Sum-of-Ratios (SOR) |
|---------------|------|---------------------|
| 28456 | S | 0.12 |
| 29577 | S | 0.08 |
| 28844 | S | 0.14 |
| 29500 | S | 0.2 |



DQA Surface Soil Report

Basic Statistical Quantities Summary

| Statistic | Survey Unit | Background | DQO Results |
|------------------|-------------|------------|-------------|
| Sample Number | 22 | N/A | N=15 |
| Mean (SOR) | 0.40 | N/A | 0.4 |
| Median (SOR) | 0.21 | N/A | N/A |
| Std Dev (SOR) | 0.38 | N/A | 0.26 |
| High Value (SOR) | 1.22 | N/A | N/A |
| Low Value (SOR) | 0.07 | N/A | N/A |

Statistical Test Summary

S+: 20
Critical Value: 15
Result: Pass

| Data | DCGLw - Data | Sign |
|------|--------------|------|
| 0.16 | 0.84 | + |
| 0.74 | 0.26 | + |
| 1.22 | -0.22 | - |
| 0.99 | 0.01 | + |
| 0.58 | 0.42 | + |
| 0.41 | 0.59 | + |
| 0.99 | 0.01 | + |
| 1.19 | -0.19 | - |
| 0.3 | 0.70 | + |
| 0.32 | 0.68 | + |
| 0.15 | 0.85 | + |
| 0.16 | 0.84 | + |
| 0.21 | 0.79 | + |
| 0.18 | 0.82 | + |
| 0.22 | 0.78 | + |
| 0.14 | 0.86 | + |
| 0.07 | 0.93 | + |
| 0.15 | 0.85 | + |
| 0.12 | 0.88 | + |
| 0.08 | 0.92 | + |
| 0.14 | 0.86 | + |
| 0.2 | 0.80 | + |

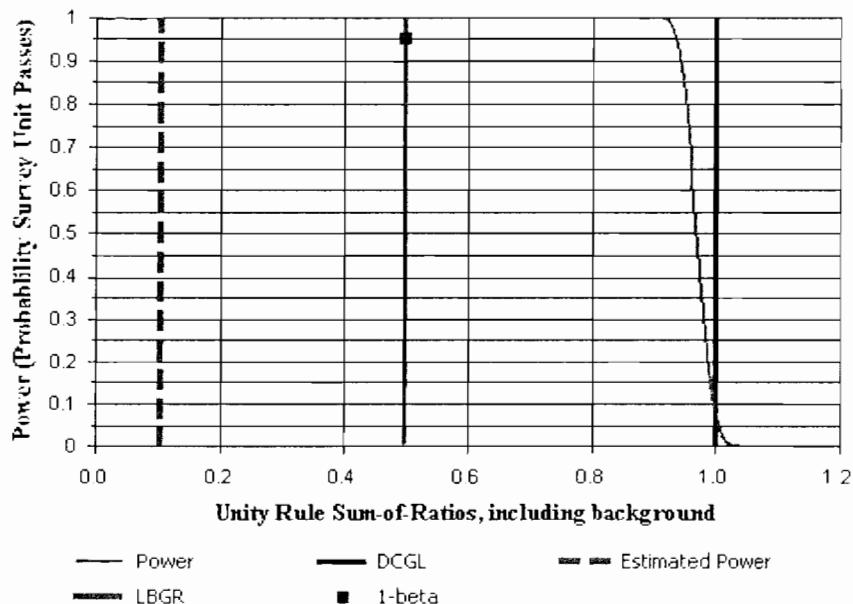


Surface Soil Survey Plan

Survey Plan Summary

Site: GTEOSI - Hicksville Site
Planner(s): Shane Brightwell
Survey Unit Name: SU07 Interval 2 01
Comments: SU07 Interval 2 Run 01
Area (m²): 1,411 Classification: 2
Selected Test: Sign Estimated Sigma (SOR): 0.06
DCGL (SOR): 1 Sample Size (N): 13
LBGR (SOR): 0.5 Estimated Conc. (SOR): 0.1
Alpha: 0.050 Estimated Power: 1
Beta: 0.050

Prospective Power Curve





Surface Soil Survey Plan

Contaminant Summary

| Contaminant | DCGLw (pCi/g) | Inferred Contaminant | Ratio | Modified DCGLw (pCi/g) | Scan MDC (pCi/g) |
|-------------|------------------|-------------------------|-------|---------------------------|---------------------|
| Th-232 | 2.80 | N/A | N/A | N/A | N/A |
| U-234 | 50.00 | N/A | N/A | N/A | N/A |
| U-238 | 50.00 | N/A | N/A | N/A | N/A |

| Contaminant | Survey Unit Estimate (Mean \pm 1-Sigma) (pCi/g) | Reference Area Estimate (Mean \pm 1-Sigma) (pCi/g) | |
|-------------|---|--|--|
| Th-232 | 0.259 ± 0.167 | N/A | |
| U-234 | 0.27 ± 0.121 | N/A | |
| U-238 | 0.247 ± 0.087 | N/A | |

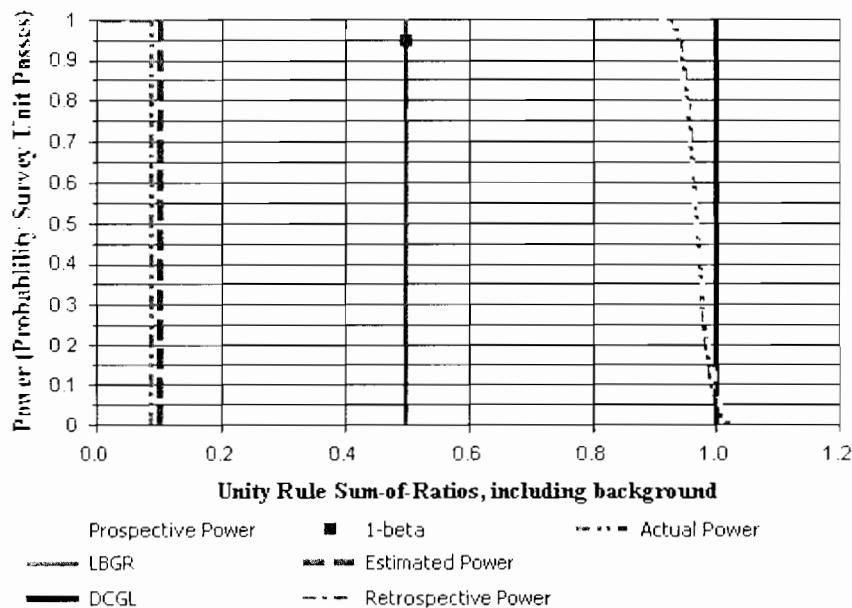


DQA Surface Soil Report

Assessment Summary

Site: GTEOSI - Hicksville Site
Planner(s): Shane Brightwell
Survey Unit Name: SU07 Interval 2 01
Report Number: 1
Survey Unit Samples: 22
Reference Area Samples: 0
Test Performed: Sign Test Result: Not Performed
Judgmental Samples: 0 EMC Result: Not Performed
Assessment Conclusion: ***Reject Null Hypothesis (Survey Unit PASSES)***

Retrospective Power Curve





DQA Surface Soil Report

Survey Unit Data

NOTE: Type = "S" indicates survey unit sample.
Type = "R" indicates reference area sample.

| Sample Number | Type | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) |
|---------------|------|----------------|---------------|---------------|
| 29463 | S | 0.74 | 0.64 | 0.46 |
| 29222 | S | 0.22 | 0.32 | 0.3 |
| 29355 | S | 0.15 | 0.34 | 0.3 |
| 28763 | S | 0.21 | 0.4 | 0.3 |
| 29677 | S | 0.21 | 0.24 | 0.25 |
| 29085 | S | 0.37 | 0.39 | 0.32 |
| 29553 | S | 0.25 | 0.42 | 0.39 |
| 28916 | S | 0.29 | 0.31 | 0.34 |
| 29269 | S | 0.25 | 0.3 | 0.27 |
| 29732 | S | 0.22 | 0.27 | 0.29 |
| 29039 | S | 0.73 | 0.27 | 0.26 |
| 29416 | S | 0.18 | 0.25 | 0.22 |
| 28525 | S | 0.27 | 0.26 | 0.21 |
| 29636 | S | 0.22 | 0.25 | 0.18 |
| 28979 | S | 0.3 | 0.23 | 0.23 |
| 29320 | S | 0.18 | 0.16 | 0.19 |
| 29814 | S | 0.12 | 0.15 | 0.11 |
| 29144 | S | 0.12 | 0.14 | 0.16 |
| 28475 | S | 0.22 | 0.17 | 0.23 |
| 29586 | S | 0.15 | 0.22 | 0.13 |
| 28858 | S | 0.1 | 0.11 | 0.12 |
| 29516 | S | 0.18 | 0.12 | 0.18 |

Modified Data (Unity Rule SOR)

NOTE: Type = "S" indicates survey unit sample.
Type = "R" indicates reference area sample.

| Sample Number | Type | Sum-of-Ratios (SOR) |
|---------------|------|---------------------|
| 29463 | S | 0.29 |
| 29222 | S | 0.09 |
| 29355 | S | 0.07 |
| 28763 | S | 0.09 |
| 29677 | S | 0.08 |
| 29085 | S | 0.15 |
| 29553 | S | 0.11 |
| 28916 | S | 0.12 |
| 29269 | S | 0.1 |
| 29732 | S | 0.09 |
| 29039 | S | 0.27 |
| 29416 | S | 0.07 |
| 28525 | S | 0.11 |
| 29636 | S | 0.09 |
| 28979 | S | 0.12 |
| 29320 | S | 0.07 |
| 29814 | S | 0.05 |
| 29144 | S | 0.05 |



DQA Surface Soil Report

Modified Data (Unity Rule SOR)

NOTE: Type = "S" indicates survey unit sample.
Type = "R" indicates reference area sample.

| Sample Number | Type | Sum-of-Ratios (SOR) |
|---------------|------|---------------------|
| 28475 | S | 0.09 |
| 29586 | S | 0.06 |
| 28858 | S | 0.04 |
| 29516 | S | 0.07 |



DQA Surface Soil Report

Basic Statistical Quantities Summary

| Statistic | Survey Unit | Background | DQO Results |
|------------------|-------------|------------|-------------|
| Sample Number | 22 | N/A | N=13 |
| Mean (SOR) | 0.10 | N/A | 0.1 |
| Median (SOR) | 0.09 | N/A | N/A |
| Std Dev (SOR) | 0.06 | N/A | 0.06 |
| High Value (SOR) | 0.29 | N/A | N/A |
| Low Value (SOR) | 0.04 | N/A | N/A |

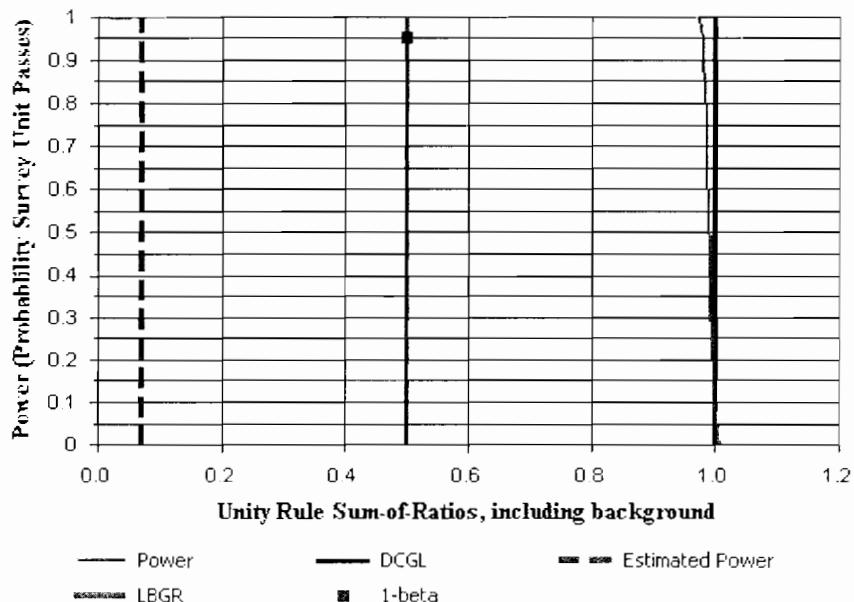


Surface Soil Survey Plan

Survey Plan Summary

Site: GTEOSI - Hicksville Site
Planner(s): Shane Brightwell
Survey Unit Name: SU07 Interval 3 02
Comments: SU07 Interval 3 Run 02
Area (m²): 1,411 Classification: 2
Selected Test: Sign Estimated Sigma (SOR): 0.02
DCGL (SOR): 1 Sample Size (N): 13
LBGR (SOR): 0.5 Estimated Conc. (SOR): 0.07
Alpha: 0.050 Estimated Power: 1
Beta: 0.050

Prospective Power Curve





Surface Soil Survey Plan

Contaminant Summary

| Contaminant | DCGLw (pCi/g) | Inferred Contaminant | Ratio | Modified DCGLw (pCi/g) | Scan MDC (pCi/g) |
|-------------|------------------|-------------------------|-------|---------------------------|---------------------|
| Th-232 | 2.80 | N/A | N/A | N/A | N/A |
| U-234 | 50.00 | N/A | N/A | N/A | N/A |
| U-238 | 50.00 | N/A | N/A | N/A | N/A |

| Contaminant | Survey Unit Estimate (Mean \pm 1-Sigma) (pCi/g) | Reference Area Estimate (Mean \pm 1-Sigma) (pCi/g) |
|-------------|---|--|
| Th-232 | 0.185 ± 0.052 | N/A |
| U-234 | 0.193 ± 0.056 | N/A |
| U-238 | 0.174 ± 0.05 | N/A |

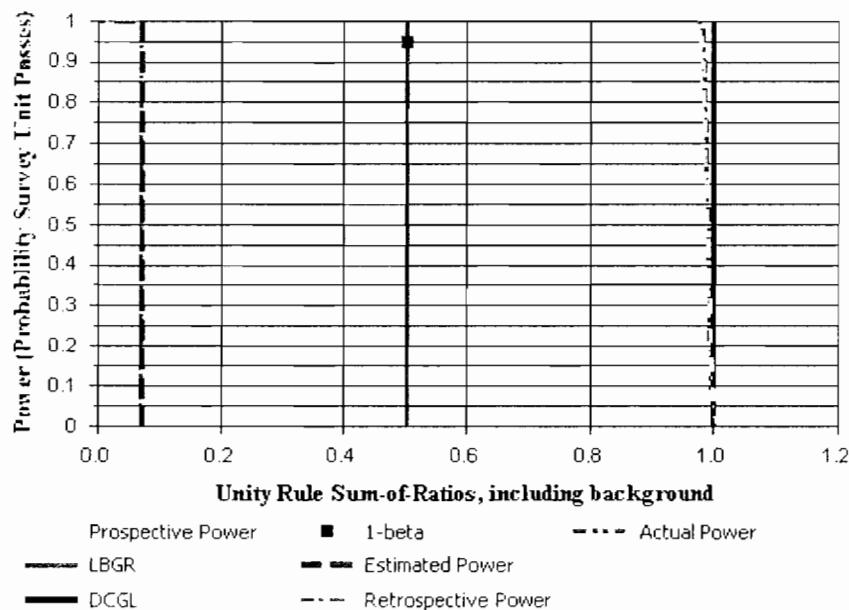


DQA Surface Soil Report

Assessment Summary

Site: GTEOSI - Hicksville Site
Planner(s): Shane Brightwell
Survey Unit Name: SU07 Interval 3 02
Report Number: 1
Survey Unit Samples: 22
Reference Area Samples: 0
Test Performed: Sign Test Result: Not Performed
Judgmental Samples: 0 EMC Result: Not Performed
Assessment Conclusion: ***Reject Null Hypothesis (Survey Unit PASSES)***

Retrospective Power Curve





DQA Surface Soil Report

Survey Unit Data

NOTE: Type = "S" indicates survey unit sample.
Type = "R" indicates reference area sample.

| Sample Number | Type | Th-232 (pCi/g) | U-234 (pCi/g) | U-238 (pCi/g) |
|---------------|------|----------------|---------------|---------------|
| 29474 | S | 0.21 | 0.22 | 0.15 |
| 29237 | S | 0.14 | 0.23 | 0.17 |
| 29363 | S | 0.11 | 0.19 | 0.18 |
| 28772 | S | 0.23 | 0.15 | 0.14 |
| 29692 | S | 0.17 | 0.34 | 0.26 |
| 29099 | S | 0.18 | 0.22 | 0.18 |
| 29561 | S | 0.17 | 0.2 | 0.18 |
| 28929 | S | 0.13 | 0.17 | 0.22 |
| 29283 | S | 0.21 | 0.32 | 0.31 |
| 29746 | S | 0.22 | 0.21 | 0.16 |
| 29047 | S | 0.11 | 0.17 | 0.11 |
| 29430 | S | 0.16 | 0.2 | 0.17 |
| 28538 | S | 0.23 | 0.12 | 0.17 |
| 29649 | S | 0.15 | 0.17 | 0.14 |
| 28994 | S | 0.35 | 0.23 | 0.24 |
| 29334 | S | 0.2 | 0.16 | 0.18 |
| 29833 | S | 0.18 | 0.16 | 0.18 |
| 29162 | S | 0.23 | 0.17 | 0.11 |
| 28487 | S | 0.17 | 0.14 | 0.14 |
| 29599 | S | 0.23 | 0.21 | 0.18 |
| 28875 | S | 0.13 | 0.11 | 0.09 |
| 29531 | S | 0.16 | 0.15 | 0.16 |

Modified Data (Unity Rule SOR)

NOTE: Type = "S" indicates survey unit sample.
Type = "R" indicates reference area sample.

| Sample Number | Type | Sum-of-Ratios (SOR) |
|---------------|------|---------------------|
| 29474 | S | 0.08 |
| 29237 | S | 0.06 |
| 29363 | S | 0.05 |
| 28772 | S | 0.09 |
| 29692 | S | 0.07 |
| 29099 | S | 0.07 |
| 29561 | S | 0.07 |
| 28929 | S | 0.05 |
| 29283 | S | 0.09 |
| 29746 | S | 0.08 |
| 29047 | S | 0.05 |
| 29430 | S | 0.07 |
| 28538 | S | 0.09 |
| 29649 | S | 0.06 |
| 28994 | S | 0.13 |
| 29334 | S | 0.08 |
| 29833 | S | 0.07 |
| 29162 | S | 0.09 |



DQA Surface Soil Report

Modified Data (Unity Rule SOR)

NOTE: Type = "S" indicates survey unit sample.
Type = "R" indicates reference area sample.

| Sample Number | Type | Sum-of-Ratios (SOR) |
|---------------|------|---------------------|
| 28487 | S | 0.07 |
| 29599 | S | 0.09 |
| 28875 | S | 0.05 |
| 29531 | S | 0.06 |



DQA Surface Soil Report

Basic Statistical Quantities Summary

| Statistic | Survey Unit | Background | DQO Results |
|------------------|-------------|------------|-------------|
| Sample Number | 22 | N/A | N=13 |
| Mean (SOR) | 0.07 | N/A | 0.07 |
| Median (SOR) | 0.07 | N/A | N/A |
| Std Dev (SOR) | 0.02 | N/A | 0.02 |
| High Value (SOR) | 0.13 | N/A | N/A |
| Low Value (SOR) | 0.05 | N/A | N/A |

