**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| 11/21/08 | 39.8 | 2.3 | 10.4 | 85.1 | 1.4 | 9.5 | 478.7 | 0.0 | 9.1 | yes[1] | 0.4 | 0.0 | 0.0 | 0.8 | 0.1 | 0.1 | 0.4 | 0.2 | 0.2 | no |
| 11/24/08 | 227.0 | 19.9 | 45.6 | 172.8 | 16.4 | 28.8 | 201.5 | 5.6 | 16.4 | yes[1] | 1.1 | 0.1 | 0.1 | 0.4 | 0.1 | 0.1 | 3.8 | 0.0 | 1.0 | no |
| 11/25/08 | 40.6 | 14.4 | 24.6 | 74.6 | 14.4 | 24.6 | 22.0 | 8.1 | 13.0 | no | 0.3 | 0.1 | 0.2 | 14.7 | 0.2 | 5.7 | 0.3 | 0.1 | 0.2 | yes[1] |
| 11/26/08 | 57.1 | 15.8 | 28.4 | 42.3 | 11.1 | 23.4 | 19.8 | 2.5 | 8.5 | no | 0.1 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.1 | no |
| 12/01/08 | 42.1 | 15.6 | 27.4 | 35.9 | 11.2 | 21.2 | 42.5 | 4.6 | 14.6 | no | 0.2 | 0.1 | 0.1 | 0.3 | 0.0 | 0.1 | 1.3 | 0.1 | 0.3 | no |
| 12/02/08 | 29.0 | 8.4 | 14.4 | 30.0 | 16.3 | 6.0 | 28.8 | 4.4 | 0.8 | no | 0.2 | 0.2 | 0.2 | 1.8 | 0.0 | 0.5 | 0.2 | 0.0 | 0.1 | no |
| 12/03/08 | 46.5 | 30.4 | 38.8 | 65.8 | 25.6 | 36.3 | 13.1 | 8.2 | 9.8 | no | 0.3 | 0.1 | 0.2 | 0.7 | 0.0 | 0.5 | 0.2 | 0.0 | 0.1 | no |
| 12/04/08 | 363.9 | 45.6 | 77.2 | 110.7 | 39.0 | 57.9 | 173.4 | 13.9 | 33.0 | yes[2] | 0.3 | 0.1 | 0.2 | 1.4 | 0.0 | 0.6 | 0.2 | 0.0 | 0.2 | no |
| 12/05/08 | 21.7 | 9.4 | 13.0 | 28.4 | 7.3 | 14.6 | 2.2 | 0.1 | 5.1 | no | 0.5 | 0.4 | 0.4 | 0.9 | 0.0 | 0.6 | 0.3 | 0.1 | 0.2 | no |
| 12/06/08 | 50.1 | 25.8 | 32.7 | 57.0 | 19.2 | 26.7 | 17.7 | 5.3 | 7.9 | no | 0.7 | 0.3 | 0.4 | 2.2 | 0.2 | 0.7 | 0.1 | 0.1 | 0.1 | no |
| 12/08/08 | 50.7 | 7.0 | 13.4 | 127.3 | 4.3 | 28.8 | 27.6 | 0.2 | 2.7 | no | 0.3 | 0.3 | 0.3 | 1.8 | 0.1 | 1.2 | 0.1 | 0.0 | 0.0 | no |
| 12/09/08 | 78.4 | 18.3 | 40.9 | 10.4 | 1.7 | 4.4 | 42.9 | 6.4 | 19.5 | no | 0.3 | 0.1 | 0.2 | 0.4 | 0.0 | 0.1 | 0.2 | 0.0 | 0.1 | no |
| 12/10/08 | 350.6 | 20.2 | 91.1 | 166.7 | 2.3 | 39.1 | 86.2 | 0.6 | 40.8 | yes[3] | 0.4 | 0.0 | 0.3 | 0.6 | 0.0 | 0.5 | 0.4 | 0.0 | 0.3 | no |
| 12/11/08 | 9.8 | 0.0 | 0.2 | 6.9 | 0.0 | 0.3 | 49.6 | 0.0 | 9.5 | no | 0.7 | 0.0 | 0.2 | 0.9 | 0.0 | 0.6 | 0.5 | 0.0 | 0.3 | no |
| 12/12/08 | 0.6 | 0.0 | 0.0 | nr[4] | nr[4] | nr[4] | 0.1 | 0.0 | 0.0 | no | 0.2 | 0.0 | 0.1 | 1.3 | 0.0 | 0.8 | 0.4 | 0.0 | 0.2 | no |
| 12/13/08 | 0.0 | 0.0 | 0.0 | nr[4] | nr[4] | nr[4] | 1.8 | 0.0 | 0.2 | no | 0.1 | 0.0 | 0.0 | 1.0 | 0.0 | 0.6 | 0.0 | 0.0 | 0.0 | no |
| 12/15/08 | 51.2 | 29.6 | 41.1 | nr[4] | nr[4] | nr[4] | 21.4 | 11.4 | 17.2 | no | 0.3 | 0.1 | 0.2 | 0.3 | 0.1 | 0.2 | 0.3 | 0.1 | 0.1 | no |
| 12/16/08 | 34.5 | 17.7 | 25.1 | 25.7 | 8.2 | 11.8 | 16.9 | 3.6 | 8.3 | no | 0.1 | 0.0 | 0.0 | 0.4 | 0.1 | 0.2 | 0.2 | 0.0 | 0.0 | no |
| 12/17/08 | 101.1 | 8.9 | 50.8 | 37.4 | 1.9 | 16.4 | 48.9 | 1.4 | 22.2 | no | 0.1 | 0.0 | 0.0 | 0.6 | 0.0 | 0.5 | 0.2 | 0.0 | 0.0 | no |
| 12/18/08 | 64.9 | 22.6 | 39.6 | 77.1 | 7.1 | 24.7 | 14.6 | 0.7 | 5.4 | no | 0.1 | 0.0 | 0.0 | 0.9 | 0.0 | 0.5 | 0.2 | 0.0 | 0.0 | no |
| 12/19/08 | 71.8 | 28.0 | 40.2 | 97.1 | 39.2 | 61.0 | 29.0 | 10.1 | 17.6 | no | 0.0 | 0.0 | 0.0 | 0.5 | 0.0 | 0.3 | 0.1 | 0.0 | 0.0 | no |
| 12/20/08 | 40.2 | 8.7 | 22.2 | 12.0 | 5.6 | 9.4 | 2.3 | 0.0 | 1.0 | no | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.2 | 0.1 | 0.0 | 0.0 | no |
| 12/22/08 | 37.9 | 19.3 | 27.4 | 135.3 | 10.9 | 23.9 | 10.3 | 6.8 | 8.9 | no | 0.0 | 0.0 | 0.0 | 0.7 | 0.0 | 0.5 | 0.0 | 0.0 | 0.0 | no |
| 12/23/08 | 66.0 | 17.8 | 33.8 | 140.1 | 10.4 | 25.6 | 20.1 | 5.0 | 10.3 | no | 0.1 | 0.0 | 0.0 | 0.8 | 0.0 | 0.5 | 0.1 | 0.0 | 0.0 | no |
| 12/29/08 | 17.8 | 12.1 | 14.4 | 13.3 | 3.1 | 6.2 | 5.3 | 2.6 | 3.6 | no | 0.0 | 0.0 | 0.0 | 0.4 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | no |
| 12/30/08 | 8.0 | 5.3 | 6.4 | 8.0 | 0.5 | 3.4 | 8.6 | 1.1 | 2.5 | no | 0.0 | 0.0 | 0.0 | 0.5 | 0.0 | 0.3 | 0.0 | 0.0 | 0.0 | no |
| 12/31/08 | 41.7 | 20.0 | 28.5 | 8.7 | 3.3 | 4.4 | 49.7 | 0.0 | 0.9 | no | 0.0 | 0.0 | 0.0 | 0.4 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |

**NOTES:**

(1) Dust exceedences caused by humidity due to dust suppression water. No visible off-site dust observed.
(2) Dust exceedences was caused by sidewalk work along Water Street not associated with this project.
(3) Dust exceedences due to false positives likely caused by inclement weather.
(4) Not recorded due to equipment malfunction. Monitor replaced on 12/16/08.

**NOTES:**

(1) VOCs exceedance due to equipment malfunction.

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| 1/5/09 | 82.5 | 20.0 | 37.9 | 23.9 | 4.3 | 10.8 | 23.5 | 9.0 | 14.4 | no | 0.0 | 0.0 | 0.0 | 0.5 | 0.0 | 0.2 | 0.1 | 0.0 | 0.0 | no |
| 1/6/09 | 31.5 | 10.3 | 21.0 | 8.0 | 1.3 | 3.2 | 21.9 | 2.0 | 7.8 | no | 0.0 | 0.0 | 0.0 | 0.6 | 0.0 | 0.3 | 0.0 | 0.0 | 0.0 | no |
| 1/7/09 | 67.2 | 7.2 | 22.9 | 54.6 | 0.7 | 19.2 | 38.8 | 4.0 | 18.2 | no | 0.1 | 0.0 | 0.0 | 0.9 | 0.1 | 0.7 | 0.2 | 0.0 | 0.2 | no |
| 1/8/09 | 51.7 | 28.8 | 37.1 | 7.5 | 0.0 | 0.0 | 13.5 | 0.0 | 1.9 | no | 0.0 | 0.0 | 0.0 | 0.7 | 0.0 | 0.5 | 0.2 | 0.0 | 0.1 | no |
| 1/9/09 | 11.6 | 8.0 | 9.7 | 1.7 | 0.0 | 0.1 | 4.6 | 0.3 | 1.8 | no | 0.0 | 0.0 | 0.0 | 0.8 | 0.0 | 0.5 | 0.0 | 0.0 | 0.0 | no |
| 1/12/09 | 42.7 | 15.5 | 23.1 | 26.4 | 0.0 | 0.4 | 15.2 | 4.3 | 6.9 | no | 0.0 | 0.0 | 0.0 | 0.8 | 0.1 | 0.5 | 0.1 | 0.0 | 0.0 | no |
| 1/13/09 | 124.6[1] | 52.3 | 72.0 | 92.7 | 32.5 | 52.0 | 56.0 | 19.1 | 25.8 | no | 0.1 | 0.0 | 0.0 | 0.7 | 0.1 | 0.5 | 0.2 | 0.0 | 0.1 | no |
| 1/14/09 | 21.9 | 9.4 | 14.6 | 54.4 | 3.0 | 7.8 | 4.9 | 0.8 | 2.1 | no | 0.0 | 0.0 | 0.0 | 0.9 | 0.0 | 0.6 | 0.0 | 0.0 | 0.0 | no |
| 1/15/09 | 20.3 | 10.2 | 13.3 | 11.4 | 1.4 | 3.1 | 5.7 | 3.7 | 4.5 | no | 0.0 | 0.0 | 0.0 | 0.5 | 0.0 | 0.4 | 0.0 | 0.0 | 0.0 | no |
| 1/16/09 | 35.8 | 16.9 | 26.7 | 26.1 | 4.7 | 8.1 | 10.8 | 4.2 | 7.5 | no | 0.0 | 0.0 | 0.0 | 0.5 | 0.0 | 0.3 | 0.0 | 0.0 | 0.0 | no |
| 1/20/09 | 45.9 | 41.7 | 44.2 | 33.6 | 14.9 | 18.8 | 18.1 | 13.3 | 15.3 | no | 0.0 | 0.0 | 0.0 | 0.8 | 0.1 | 0.6 | 0.1 | 0.0 | 0.0 | no |
| 1/21/09 | 46.2 | 20.7 | 28.5 | 99.5 | 13.3 | 36.1 | 15.6 | 7.3 | 10.0 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 1/22/09 | 96.5 | 42.1 | 58.4 | 140.7 | 19.8 | 44.1 | 227.6 | 14.4 | 25.9 | yes[2] | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | 0.3 | 0.0 | 0.1 | no |
| 1/23/09 | 134.0 | 53.2 | 83.9 | 42.8 | 13.1 | 24.8 | 45.3 | 12.3 | 25.1 | no | 0.1 | 0.0 | 0.1 | 0.2 | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | no |
| 1/26/09 | 39.2 | 16.8 | 26.0 | 31.6 | 3.5 | 8.2 | 30.2 | 5.1 | 9.4 | no | 0.0 | 0.0 | 0.0 | 0.5 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | no |
| 1/27/09 | 10.4 | 6.6 | 8.1 | 135.3 | 12.5 | 32.7 | 71.9 | 16.1 | 25.8 | no | 0.1 | 0.0 | 0.1 | 0.5 | 0.0 | 0.1 | 0.3 | 0.0 | 0.1 | no |
| 1/28/09 | 168.8 | 24.0 | 62.7 | 275.6 | 8.1 | 87.7 | 86.2 | 7.5 | 44.3 | yes[3] | 0.1 | 0.0 | 0.0 | 1.0 | 0.0 | 0.4 | 0.6 | 0.0 | 0.1 | no |
| 1/29/09 | 26.6 | 7.2 | 11.6 | 123.6 | 0.0 | 24.5 | 14.1 | 0.0 | 1.0 | no | 0.0 | 0.0 | 0.0 | 0.5 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | no |
| 1/30/09 | nr[4] | nr[4] | nr[4] | 70.9 | 21.0 | 27.4 | 10.8 | 4.2 | 7.5 | no | 0.1 | 0.0 | 0.1 | 0.4 | 0.0 | 0.2 | nr[1] | nr[1] | nr[1] | no |
| 1/31/09 | 11.7 | 8.0 | 9.6 | 109.8 | 3.4 | 10.0 | 49.9 | 1.8 | 5.9 | no | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | nr[1] | nr[1] | nr[1] | no |

**NOTES:**

(1) Dust exceednance due to equipment malfunction.
(2) Caused by an instantaneous spike of 2,072.2 µg/m³ at 6:07pm (during reagent delivery).
(3) Dust exceedences due to false positives likely caused by inclement weather.
(4) Not recorded due to equipment malfunction.

**NOTES:**

(1) Not recorded due to equipment malfunction.

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| | | | | | | | | | | | | | | | | | | | | |
| 2/2/09 | 38.2 | 6.4 | 18.5 | 31.5 | 7.3 | 14.2 | 28.5 | 2.0 | 10.6 | no | 0.1 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | nr[1] | nr[1] | nr[1] | no |
| 2/3/09 | 21.8 | 3.8 | 13.3 | 21.1 | 1.2 | 9.0 | 90.0 | 2.1 | 13.8 | no | 0.0 | 0.0 | 0.0 | 0.5 | 0.0 | 0.3 | 0.0 | 0.0 | 0.0 | no |
| 2/4/09 | 16.8 | 10.6 | 12.3 | 12.6 | 1.5 | 4.2 | 105.5 | 3.3 | 19.2 | no | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 2/5/09 | nr[1] | nr[1] | nr[1] | 16.5 | 0.0 | 1.4 | 5.7 | 1.4 | 2.9 | no | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 2/6/09 | 32.1 | 15.5 | 21.0 | 134.9 | 0.0 | 40.8 | 94.0 | 8.6 | 17.4 | no | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | no |
| 2/7/09 | 62.1 | 28.5 | 39.7 | nr[1] | nr[1] | nr[1] | 128.7 | 25.1 | 43.2 | no | 0.0 | 0.0 | 0.0 | 0.4 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | no |
| 2/9/09 | 27.5 | 6.5 | 11.5 | 39.1 | 0.0 | 1.9 | 18.3 | 8.2 | 11.7 | no | 0.1 | 0.0 | 0.0 | 0.4 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | no |
| 2/10/09 | 103.1 | 20.3 | 37.5 | 64.4 | 6.7 | 14.8 | nr[1] | nr[1] | nr[1] | no | 0.1 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.2 | 0.0 | 0.0 | no |
| 2/11/09 | nr[1] | nr[1] | nr[1] | 124.0 | 0.0 | 17.9 | 313.6 | 82.1 | 164.2 | yes[2] | 0.1 | 0.0 | 0.1 | 0.2 | 0.0 | 0.2 | 1.1 | 0.0 | 0.1 | no |
| 2/12/09 | 20.3 | 2.1 | 5.3 | 6.3 | 1.7 | 3.3 | 14.0 | 3.3 | 6.6 | no | 0.1 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 2/13/09 | 2.4 | 0.4 | 1.0 | 26.6 | 1.8 | 6.0 | 33.6 | 5.0 | 14.4 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.1 | no |
| 2/14/09 | 27.0 | 16.2 | 19.8 | 16.0 | 2.7 | 6.3 | nr[1] | nr[1] | nr[1] | no | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 2/16/09 | 11.9 | 1.9 | 4.3 | 45.8 | 0.9 | 9.4 | 25.5 | 5.0 | 9.9 | no | 0.2 | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 2/17/09 | 77.7 | 2.6 | 10.8 | 57.8 | 1.8 | 11.5 | 48.3 | 10.3 | 19.3 | no | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | no |
| 2/18/09 | 268.0 | 24.7 | 55.1 | 156.9 | 17.0 | 54.2 | 25.7 | 2.9 | 6.7 | yes[2] | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 2/19/09 | 35.9 | 0.2 | 10.2 | 75.1 | 0.0 | 3.1 | nr[1] | nr[1] | nr[1] | no | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 2/20/09 | 84.0 | 3.7 | 21.1 | 44.3 | 3.5 | 26.4 | 80.3 | 7.4 | 19.5 | no | 0.0 | 0.0 | 0.0 | 0.5 | 0.0 | 0.3 | 0.3 | 0.0 | 0.0 | no |
| 2/21/09 | 15.8 | 3.7 | 6.1 | 39.7 | 4.6 | 12.5 | 36.8 | 7.4 | 14.8 | no | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 2/23/09 | 13.5 | 3.6 | 6.3 | 46.6 | 6.0 | 16.1 | 36.8 | 7.4 | 14.8 | no | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | no |
| 2/24/09 | 7.4 | 2.1 | 4.2 | 80.8 | 5.1 | 26.0 | 56.7 | 1.7 | 5.8 | no | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | no |
| 2/25/09 | 80.8 | 4.4 | 21.2 | 113.6 | 5.3 | 22.9 | 49.6 | 4.9 | 10.8 | no | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 2/26/09 | 69.8 | 34.5 | 50.4 | 133.4 | 16.6 | 38.7 | 53.3 | 13.0 | 20.2 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 2/27/09 | 121.9 | 28.5 | 57.4 | 64.1 | 12.9 | 21.9 | 33.8 | 5.3 | 11.6 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 2/28/09 | 5.4 | 3.7 | 4.7 | 20.0 | 3.8 | 9.6 | 59.2 | 4.0 | 17.6 | no | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |

**NOTES:**

(1) Not recorded due to equipment malfunction.

(2) Dust exceedance due to upwind spike than lasted less than 2 minutes.

**NOTES:**

(1) Not recorded due to equipment malfunction.

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| | | | | | | | | | | | | | | | | | | | | |
| 3/3/09 | 41.9 | 2.7 | 5.1 | 39.1 | 7.5 | 12.4 | 123.3 | 2.7 | 27.8 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.9 | 0.0 | 0.8 | no |
| 3/4/09 | 27.8 | 5.8 | 9.4 | 41.3 | 8.0 | 14.1 | 34.3 | 5.2 | 9.2 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | no |
| 3/5/09 | 60.9 | 19.8 | 34.8 | 78.2 | 11.3 | 23.2 | 141.3 | 16.6 | 40.3 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/6/09 | 60.7 | 25.1 | 37.1 | 31.4 | 13.6 | 19.7 | 142.8 | 15.1 | 42.1 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.5 | 0.1 | 0.4 | no |
| 3/7/09 | 43.8 | 32.7 | 36.9 | 37.7 | 27.2 | 30.5 | 91.6 | 28.1 | 32.8 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.4 | 0.0 | 0.1 | no |
| 3/9/09 | 72.6 | 7.6 | 23.2 | 41.8 | 2.8 | 14.7 | 95.8 | 1.7 | 9.7 | no | 0.4 | 0.0 | 0.3 | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.1 | no |
| 3/10/09 | 44.3 | 2.6 | 13.8 | 19.7 | 6.4 | 12.6 | 41.3 | 5.1 | 13.6 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.6 | 0.0 | 0.2 | no |
| 3/11/09 | 36.5 | 23.8 | 27.8 | 110.3 | 15.1 | 42.8 | 102.1 | 6.2 | 31.8 | no | 0.7 | 0.0 | 0.4 | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | no |
| 3/12/09 | 4.3 | 0.1 | 1.2 | 43.9 | 5.4 | 16.5 | 56.2 | 2.9 | 10.8 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/13/09 | 123.4 | 4.3 | 20.5 | 20.4 | 4.3 | 7.5 | 60.0 | 3.8 | 15.6 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.4 | 0.0 | 0.1 | no |
| 3/14/09 | 144.9 | 25.3 | 49.8 | 50.3 | 17.8 | 33.1 | 81.2 | 15.2 | 29.9 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.4 | 0.0 | 0.1 | no |
| 3/16/09 | 123.2 | 27.2 | 58.4 | 131.4 | 19.9 | 39.5 | 119.4 | 6.6 | 33.6 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.6 | 0.0 | 0.2 | no |
| 3/17/09 | 44.6 | 11.8 | 21.0 | 22.5 | 7.1 | 14.7 | 88.5 | 6.0 | 11.3 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | no |
| 3/18/09 | 52.1 | 26.8 | 38.1 | 40.5 | 14.5 | 25.9 | 40.0 | 9.6 | 18.9 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | no |
| 3/19/09 | 52.4 | 4.1 | 12.8 | 17.5 | 4.4 | 8.0 | 46.2 | 1.6 | 8.1 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/20/09 | 25.7 | 4.3 | 10.2 | 14.7 | 6.5 | 11.6 | 68.8 | 4.7 | 17.2 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/21/09 | 33.6 | 4.4 | 9.3 | 10.2 | 4.1 | 5.5 | 29.8 | 4.7 | 10.1 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/23/09 | 19.7 | 2.9 | 6.1 | 64.0 | 3.1 | 9.2 | 59.0 | 4.7 | 19.6 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/24/09 | 23.8 | 3.7 | 8.7 | 16.1 | 4.4 | 8.7 | 80.8 | 4.8 | 32.4 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/25/09 | 129.7 | 5.4 | 28.1 | 32.3 | 2.4 | 7.2 | 37.4 | 4.6 | 12.7 | no | 0.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/26/09 | 116.5 | 23.3 | 50.3 | 38.6 | 11.3 | 19.8 | 38.2 | 9.6 | 19.2 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/27/09 | 145.0 | 9.2 | 54.5 | 23.5 | 9.7 | 15.4 | 81.3 | 9.2 | 21.5 | no | 4.0 | 0.0 | 0.7 | 0.0 | 0.0 | 0.0 | 0.8 | 0.0 | 0.1 | no |
| 3/28/09 | 138.8 | 9.8 | 39.0 | 71.5 | 2.3 | 11.4 | 41.0 | 4.2 | 15.1 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/30/09 | 97.9 | 1.5 | 9.7 | 81.7 | 2.0 | 14.2 | 59.7 | 1.4 | 8.9 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/31/09 | 59.2 | 1.2 | 6.7 | 78.9 | 1.9 | 7.0 | 143.4 | 0.2 | 31.3 | no | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| | | | | | | | | | | | | | | | | | | | | |
| 4/1/09 | 65.1 | 16.6 | 31.1 | 49.1 | 10.9 | 16.7 | 18.5 | 6.8 | 10.1 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/2/09 | 124.1 | 13.1 | 45.7 | 88.8 | 2.0 | 16.8 | 83.9 | 6.8 | 20.9 | no | 1.1 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/3/09 | 48.6 | 12.9 | 22.5 | 18.6 | 1.8 | 6.7 | 34.3 | 2.4 | 6.8 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/6/09 | 34.7 | 5.2 | 20.9 | 26.5 | 7.0 | 14.9 | 88.2 | 0.0 | 5.9 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/7/09 | 116.9 | 0.0 | 5.6 | 101.0 | 0.7 | 14.8 | 25.5 | 0.0 | 0.0 | no | 1.3 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/8/09 | 131.2 | 5.4 | 20.1 | 107.7 | 5.3 | 29.9 | 79.0 | 0.0 | 5.3 | no | 2.1 | 0.0 | 0.3 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/9/09 | 120.2 | 5.9 | 17.6 | 127.2 | 3.7 | 30.1 | 36.5 | 0.0 | 3.4 | no | 3.0 | 0.0 | 0.4 | 0.2 | 0.0 | 0.1 | 0.5 | 0.1 | 0.4 | no |
| 4/10/09 | 114.2 | 18.2 | 54.2 | 146.0 | 9.8 | 25.7 | 75.4 | 9.0 | 17.3 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.4 | 0.3 | 0.3 | no |
| 4/13/09 | 11.0 | 3.1 | 4.1 | 24.6 | 8.3 | 11.7 | 22.6 | 3.2 | 4.3 | no | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.4 | 0.0 | 0.3 | no |
| 4/14/09 | 18.0 | 4.8 | 11.0 | 17.2 | 4.7 | 8.9 | 9.9 | 3.8 | 6.9 | no | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | 0.5 | 0.0 | 0.4 | no |
| 4/15/09 | 12.3 | 3.2 | 6.3 | 15.4 | 3.5 | 4.9 | 9.2 | 3.1 | 4.2 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.4 | 0.1 | 0.4 | no |
| 4/16/09 | 134.6 | 7.0 | 22.0 | 110.8 | 2.8 | 12.0 | 21.7 | 4.3 | 6.9 | no | 0.6 | 0.1 | 0.3 | 0.2 | 0.0 | 0.1 | 3.0 | 0.0 | 0.3 | no |
| 4/17/09 | 26.1 | 6.6 | 13.5 | 107.3 | 2.4 | 17.8 | 14.8 | 4.0 | 7.9 | no | 0.5 | 0.0 | 0.2 | 0.2 | 0.0 | 0.1 | 0.5 | 0.0 | 0.4 | no |
| 4/18/09 | 12.7 | 10.1 | 10.9 | 8.9 | 6.3 | 6.8 | 11.1 | 6.6 | 7.0 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | no |
| 4/20/09 | 23.5 | 10.0 | 14.6 | 16.3 | 7.0 | 11.8 | 9.1 | 2.0 | 4.3 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | no |
| 4/21/09 | 97.4 | 2.5 | 50.4 | 60.8 | 2.9 | 28.1 | 51.6 | 3.6 | 27.7 | no | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.3 | no |
| 4/22/09 | 61.6 | 10.6 | 30.4 | 134.4 | 10.9 | 35.5 | 87.7 | 9.2 | 20.0 | no | 1.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.2 | no |
| 4/23/09 | 23.3 | 1.6 | 7.7 | 25.1 | 0.9 | 8.2 | 11.4 | 0.0 | 1.1 | no | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | no |
| 4/24/09 | 52.7 | 4.9 | 16.4 | 76.2 | 0.8 | 10.7 | 33.5 | 5.9 | 13.3 | no | 0.6 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.1 | no |
| 4/27/09 | 53.2 | 23.1 | 36.9 | 11.4 | 5.2 | 7.4 | 47.0 | 23.2 | 31.0 | no | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | no |
| 4/28/09 | 137.9 | 15.1 | 27.1 | 19.3 | 1.2 | 5.4 | 32.5 | 14.4 | 19.1 | no | 0.4 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | no |
| 4/29/09 | 27.1 | 2.1 | 10.2 | 31.9 | 0.8 | 3.1 | 33.6 | 4.0 | 10.7 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | no |
| 4/30/09 | 85.1 | 9.5 | 19.0 | 25.7 | 4.0 | 7.0 | 43.1 | 10.1 | 16.2 | no | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | no |

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| 5/1/09 | 135.8 | 76.7 | 102.3 | 68.7 | 40.3 | 52.8 | 129.4 | 74.6 | 97.1 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | no |
| 5/6/09 | 61.4 | 1.1 | 17.4 | 35.8 | 0.0 | 9.0 | 60.4 | 1.8 | 17.9 | no | 0.1 | 0.0 | 0.1 | 0.2 | 0.0 | 0.1 | 1.9 | 0.0 | 0.3 | no |
| 5/7/09 | 52.8 | 13.5 | 35.3 | 22.9 | 5.4 | 16.3 | 47.5 | 12.4 | 33.7 | no | 0.3 | 0.0 | 0.2 | 0.2 | 0.0 | 0.1 | 0.4 | 0.0 | 0.3 | no |
| 5/8/09 | 39.7 | 5.1 | 19.4 | 25.6 | 2.4 | 10.7 | 42.5 | 9.3 | 21.7 | no | 0.2 | 0.0 | 0.1 | 0.3 | 0.0 | 0.1 | 0.4 | 0.1 | 0.3 | no |
| 5/11/09 | 117.0 | 4.3 | 12.0 | 11.1 | 1.9 | 5.6 | 63.6 | 6.8 | 13.6 | no | 0.2 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.4 | 0.0 | 0.2 | no |
| 5/12/09 | 19.3 | 5.5 | 8.9 | 46.4 | 2.2 | 11.5 | 25.1 | 6.0 | 11.3 | no | 0.3 | 0.0 | 0.1 | 0.3 | 0.0 | 0.2 | 0.4 | 0.0 | 0.2 | no |
| 5/13/09 | 62.4 | 9.3 | 20.5 | 15.7 | 2.4 | 5.1 | 31.8 | 4.5 | 12.8 | no | 0.8 | 0.0 | 0.2 | 0.4 | 0.0 | 0.3 | 0.1 | 0.0 | 0.0 | no |
| 5/14/09 | 82.5 | 17.1 | 41.2 | 65.2 | 6.8 | 15.2 | 54.0 | 18.3 | 31.1 | no | 0.5 | 0.0 | 0.2 | 0.3 | 0.0 | 0.2 | 0.4 | 0.0 | 0.2 | no |
| 5/15/09 | 79.5 | 19.7 | 38.9 | 39.4 | 11.2 | 23.1 | 76.0 | 22.1 | 38.1 | no | 0.2 | 0.0 | 0.1 | 0.3 | 0.0 | 0.1 | 0.4 | 0.1 | 0.3 | no |
| 5/18/09 | 9.5 | 3.2 | 4.3 | 7.0 | 2.1 | 3.3 | 10.6 | 6.0 | 7.2 | no | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.2 | 0.0 | 0.1 | no |
| 5/19/09 | 64.5 | 4.3 | 10.7 | 9.5 | 0.2 | 1.7 | 18.8 | 4.9 | 8.3 | no | nr[1] | nr[1] | nr[1] | 0.4 | 0.0 | 0.2 | 0.4 | 0.0 | 0.2 | no |
| 5/20/09 | nr[1] | nr[1] | nr[1] | 94.9 | 21.8 | 44.4 | 35.0 | 6.3 | 16.6 | no | nr[1] | nr[1] | nr[1] | 0.4 | 0.2 | 0.3 | 0.4 | 0.2 | 0.2 | no |
| 5/21/09 | 85.6 | 5.3 | 16.8 | 8.3 | 0.5 | 2.5 | 24.7 | 8.4 | 13.3 | no | 0.6 | 0.0 | 0.4 | 0.3 | 0.0 | 0.2 | nr[2] | nr[2] | nr[2] | no |
| 5/22/09 | 30.4 | 9.9 | 16.7 | nr[1] | nr[1] | nr[1] | 22.2 | 11.0 | 15.5 | no | 0.7 | 0.0 | 0.2 | 0.3 | 0.0 | 0.2 | 0.3 | 0.0 | 0.1 | no |
| 5/26/09 | 19.1 | 5.3 | 9.8 | 8.4 | 0.7 | 1.8 | 19.0 | 8.1 | 12.9 | no | 0.1 | 0.0 | 0.0 | 0.3 | 0.0 | 0.2 | 1.0 | 0.0 | 0.1 | no |
| 5/27/09 | 46.9 | 12.3 | 20.4 | 15.8 | 3.2 | 6.6 | 28.3 | 10.6 | 18.5 | no | nr[2] | nr[2] | nr[2] | 0.3 | 0.0 | 0.3 | 18.3[3] | 17.7[3] | 18.1[3] | yes[3] |
| 5/28/09 | 31.2 | 11.2 | 17.2 | 11.8 | 3.6 | 5.7 | 26.8 | 11.3 | 15.3 | no | 0.1 | 0.0 | 0.1 | 0.3 | 0.0 | 0.2 | 0.1 | 0.0 | 0.1 | no |
| 5/29/09 | 73.9 | 0.9 | 35.8 | 55.9 | 0.8 | 11.9 | 39.8 | 4.8 | 21.1 | no | nr[2] | nr[2] | nr[2] | nr[2] | nr[2] | nr[2] | nr[2] | nr[2] | nr[2] | no |
| 5/30/09 | 13.6 | 8.3 | 10.2 | 133.5 | 4.0 | 29.5 | 31.0 | 11.7 | 15.7 | no | 0.2 | 0.0 | 0.0 | nr[2] | nr[2] | nr[2] | nr[2] | nr[2] | nr[2] | no |

**NOTES:**

(1) Not recorded due to equipment malfunction.

**NOTES:**

(1) Data not recorded because monitor was used for sonic drilling head space readings.
(2) Data not recorded due to equipment malfunction. Manual monitoring conducted and no exceedences.
(3) VOCs exceedences due to false positives likely caused humidity.

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background



VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| | | | | | | | | | | | | | | | | | | | | |
| 6/1/09 | 115.0 | 2.6 | 15.6 | 54.6 | 0.1 | 5.6 | 17.0 | 3.5 | 7.3 | no | 0.3 | 0.0 | 0.1 | 0.5 | 0.0 | 0.3 | 0.1 | 0.0 | 0.0 | no |
| 6/2/09 | 136.5 | 15.8 | 25.9 | 147.6 | 6.1 | 34.1 | 46.8 | 15.8 | 23.2 | no | 1.3 | 0.0 | 0.2 | 0.4 | 0.0 | 0.2 | 0.5 | 0.0 | 0.1 | no |
| 6/3/09 | 24.5 | 7.1 | 11.3 | 84.3 | 2.6 | 18.7 | 42.4 | 8.4 | 13.5 | no | 0.0 | 0.0 | 0.0 | 0.4 | 0.0 | 0.2 | 0.2 | 0.0 | 0.1 | no |
| 6/4/09 | 16.1 | 8.4 | 10.9 | 7.6 | 1.8 | 4.2 | 14.2 | 7.9 | 10.7 | no | 0.5 | 0.0 | 0.1 | 0.5 | 0.0 | 0.3 | 0.1 | 0.0 | 0.0 | no |
| 6/5/09 - 6/12/09 CAMP not set up due to limited site activities | | | | | | | | | | | 6/5/09 - 6/12/09 CAMP not set up due to limited site activities | | | | | | | | | |
| 6/15/09 | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | no | 2.2 | 0.0 | 0.2 | 1.1 | 0.0 | 0.2 | 0.1 | 0.0 | 0.0 | no |
| 6/16/09 | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | no | 0.6 | 0.0 | 0.1 | 0.3 | 0.0 | 0.2 | 0.1 | 0.0 | 0.0 | no |
| 6/17/09 | 22.4 | 3.4 | 7.3 | 143.0 | 0.0 | 9.0 | 14.1 | 5.6 | 8.8 | no | 0.2 | 0.0 | 0.0 | 1.4 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | no |
| 6/18/09 | 56.5 | 18.9 | 35.1 | 35.2 | 0.3 | 10.7 | 91.9 | 11.7 | 32.0 | no | 3.1 | 0.0 | 1.4 | 1.4 | 0.0 | 0.5 | 0.1 | 0.0 | 0.1 | no |
| 6/19/09 | 29.2 | 0.0 | 2.5 | 141.0 | 0.0 | 8.9 | 117.5 | 0.0 | 2.1 | no | 0.1 | 0.0 | 0.0 | 1.3 | 0.0 | 0.1 | 0.4 | 0.0 | 0.1 | no |
| 6/25/09 | nr[1] | nr[1] | nr[1] | 1.6 | 0.0 | 0.1 | 12.7 | 2.8 | 6.4 | no | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | no |
| 6/26/09 | 12.7 | 0.6 | 5.8 | 39.4 | 9.6 | 21.2 | 106.1 | 22.0 | 52.2 | no | 0.2 | 0.0 | 0.0 | 0.6 | 0.0 | 0.2 | 0.2 | 0.0 | 0.0 | no |
| 6/27/09 | 22.7 | 4.7 | 8.7 | 115.5 | 2.6 | 9.7 | 144.7 | 10.8 | 34.1 | no | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 6/29/09 | nr[1] | nr[1] | nr[1] | 35.3 | 6.5 | 20.1 | 140.3 | 17.4 | 47.4 | no | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 6/30/09 | 49.4 | 17.1 | 31.1 | 20.9 | 5.2 | 12.8 | 40.5 | 17.1 | 24.7 | no | 0.2 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |

**NOTES:**

(1) Not recorded due to equipment malfunction.

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background



VOC action levels:
Based on 15 min avg
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Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| 7/1/09 | 46.7 | 19.5 | 30.5 | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | no | 0.1 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | no |
| 7/2/09 | 48.5 | 28.9 | 35.7 | 19.7 | 11.4 | 14.4 | 35.9 | 24.2 | 28.6 | no | 0.2 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | no |
| 7/6/09 | nr[2] | nr[2] | nr[2] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[2] | 0.1 | 0.0 | 0.0 | 0.3 | 0.0 | 0.2 | 0.1 | 0.0 | 0.0 | no |
| 7/7/09 | nr[1] | nr[1] | nr[1] | 66.6 | 1.2 | 13.0 | 56.1 | 8.9 | 25.3 | no | 0.4 | 0.0 | 0.1 | 0.3 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 7/8/09 | 143.1 | 4.9 | 54.3 | 77.0 | 1.4 | 18.4 | 98.7 | 3.9 | 12.7 | no | 0.0 | 0.0 | 0.0 | 0.4 | 0.0 | 0.3 | 0.3 | 0.0 | 0.0 | no |
| 7/9/09 | 97.9 | 11.4 | 28.4 | 15.0 | 1.3 | 4.3 | 55.8 | 6.5 | 16.0 | no | 1.4 | 0.0 | 0.2 | 0.3 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | no |
| 7/10/09 | 85.1 | 6.9 | 23.9 | 40.8 | 1.0 | 6.4 | 122.4 | 9.7 | 27.1 | no | 1.8 | 0.0 | 0.3 | 0.3 | 0.1 | 0.2 | 0.1 | 0.0 | 0.0 | no |
| 7/11/09 | 79.3 | 9.4 | 26.6 | 48.1 | 2.8 | 4.4 | 28.2 | 12.9 | 18.4 | no | 3.1 | 0.4 | 0.9 | 0.1 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 7/13/09 | nr[1] | nr[1] | nr[1] | 59.0 | 5.3 | 11.4 | 36.0 | 8.5 | 22.6 | no | 0.6 | 0.0 | 0.2 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 7/15/09 | nr[1] | nr[1] | nr[1] | 139.7 | 26.3 | 62.7 | 53.8 | 4.5 | 12.8 | no | 0.9 | 0.0 | 0.2 | 0.4 | 0.0 | 0.3 | 0.1 | 0.0 | 0.0 | no |
| 7/16/09 | nr[1] | nr[1] | nr[1] | 25.7 | 0.1 | 1.4 | 21.6 | 5.9 | 8.6 | no | 2.1 | 0.1 | 0.6 | 0.2 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | no |
| 7/17/09 | 107.9 | 4.0 | 11.6 | 43.3 | 5.7 | 15.1 | 127.0 | 25.8 | 44.6 | no | nr[1] | nr[1] | nr[1] | 0.2 | 0.0 | 0.1 | nr[1] | nr[1] | nr[1] | no |
| 7/18/09 | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | 24.0 | 4.1 | 5.6 | no | 0.1 | 0.0 | 0.0 | 0.1 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 7/21/09 | nr[1] | nr[1] | nr[1] | 50.7 | 1.4 | 9.2 | 27.1 | 9.9 | 15.0 | no | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | no |
| 7/23/09 | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | 78.4 | 6.2 | 13.7 | no | 0.9 | 0.0 | 0.1 | 0.3 | 0.0 | 0.2 | nr[1] | nr[1] | nr[1] | no |
| 7/24/09 | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | 132.8 | 25.1 | 53.4 | no | nr[1] | nr[1] | nr[1] | 0.3 | 0.0 | 0.1 | nr[1] | nr[1] | nr[1] | no |
| 7/25/09 | nr[1] | nr[1] | nr[1] | 78.0 | 5.8 | 23.3 | 36.5 | 3.9 | 12.3 | no | nr[1] | nr[1] | nr[1] | 0.2 | 0.0 | 0.1 | nr[1] | nr[1] | nr[1] | no |
| 7/27/09 | nr[1] | nr[1] | nr[1] | 49.0 | 8.3 | 14.6 | 70.7 | 30.9 | 53.4 | no | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | no |
| 7/28/09 | 117.1 | 30.0 | 51.8 | 123.9 | 15.6 | 29.3 | 110.1 | 24.6 | 44.0 | no | nr[1] | nr[1] | nr[1] | 0.1 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | no |
| 7/29/09 | 112.9 | 63.5 | 82.4 | 79.2 | 32.3 | 46.7 | 67.5 | 54.3 | 59.9 | no | 0.1 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | no |
| 7/31/09 | 94.7 | 34.3 | 52.8 | 103.4 | 49.5 | 62.1 | 122.1 | 46.4 | 59.4 | no | 0.2 | 0.0 | 0.0 | 0.3 | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | no |

**NOTES:**
(1) Not recorded due to equipment malfunction

**NOTES:**
(1) Not recorded due to equipment malfunction

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| | | | | | | | | | | | | | | | | | | | | |
| 8/1/09 | 82.6 | 36.6 | 49.7 | 61.7 | 37.3 | 57.9 | 106.9 | 29.8 | 34.2 | no | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 8/3/09 | 124.0 | 59.4 | 66.7 | 77.7 | 36.4 | 52.9 | 72.8 | 39.8 | 51.1 | no | 0.2 | 0.0 | 0.1 | 0.2 | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | no |
| 8/4/09 | 72.6 | 36.6 | 49.7 | 59.1 | 27.6 | 52.2 | 81.9 | 26.7 | 35.4 | no | 0.1 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | no |
| 8/5/09 | 85.2 | 38.8 | 59.7 | 67.2 | 31.9 | 42.7 | 65.4 | 37.6 | 38.6 | no | 0.2 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | no |
| 8/6/09 | 111.1 | 49.2 | 55.5 | 79.4 | 26.7 | 51.7 | 77.9 | 36.4 | 52.7 | no | 0.2 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | no |
| 8/6/09 - 8/14/09 CAMP not set up due to limited site activities | | | | | | | | | | | 8/6/09 - 8/14/09 CAMP not set up due to limited site activities | | | | | | | | | |
| 8/17/09 | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | 44.9 | 10.3 | 21.6 | no | 0.5 | 0.0 | 0.0 | 0.4 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | no |
| 8/18/09 | nr[1] | nr[1] | nr[1] | 15.5 | 0.0 | 3.1 | 139.9 | 50.3 | 77.6 | no | 2.6 | 0.0 | 0.0 | 0.6 | 0.1 | 0.2 | nr[1] | nr[1] | nr[1] | no |
| 8/19/09 | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | no | 0.5 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | no |
| 8/20/09 | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | no | 0.0 | 0.0 | 0.0 | 0.4 | 0.0 | 0.2 | nr[1] | nr[1] | nr[1] | no |
| 8/21/09 | nr[1] | nr[1] | nr[1] | 113.6 | 7.9 | 51.0 | nr[1] | nr[1] | nr[1] | no | 1.4 | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | no |
| 8/24/09 | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | 118.0 | 7.9 | 53.5 | no | nr[1] | nr[1] | nr[1] | 0.2 | 0.0 | 0.1 | nr[1] | nr[1] | nr[1] | no |
| 8/25/09 | 133.7 | 6.8 | 18.0 | nr[1] | nr[1] | nr[1] | 110.3 | 15.4 | 46.0 | no | 0.2 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | no |
| 8/26/09 | 82.0 | 23.1 | 39.8 | 116.8 | 6.4 | 35.0 | 113.2 | 25.2 | 48.5 | no | 0.8 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 8/27/09 | 43.3 | 3.4 | 8.7 | 116.8 | 6.4 | 35.0 | nr[1] | nr[1] | nr[1] | no | 0.8 | 0.0 | 0.1 | 0.3 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | no |
| 8/28/09 | 31.2 | 10.3 | 22.0 | 49.6 | 13.5 | 37.9 | 72.4 | 3.1 | 11.3 | no | 0.2 | 0.0 | 0.0 | 0.3 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | no |

NOTES:
(1) Not recorded due to equipment malfunction

NOTES:
(1) Not recorded due to equipment malfunction

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| 9/1/09 | nr[1] | nr[1] | nr[1] | 19.0 | 3.8 | 8.7 | nr[1] | nr[1] | nr[1] | no | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 9/2/09 | 33.0 | 6.6 | 11.9 | 54.8 | 3.8 | 8.8 | nr[1] | nr[1] | nr[1] | no | 0.8 | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 9/3/09 | 58.8 | 12.3 | 22.7 | 65.8 | 7.7 | 20.5 | 668.4 | 8.6 | 43.7 | yes[2] | 0.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 9/4/09 | 49.4 | 12.4 | 20.6 | 133.7 | 9.7 | 22.1 | 30.5 | 11.7 | 17.1 | no | 0.1 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 9/5/09 | 13.3 | 7.4 | 8.5 | 46.5 | 7.2 | 8.3 | 18.5 | 7.9 | 9.3 | no | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.2 | 0.3 | 0.2 | 0.2 | no |
| 9/8/09 | 104.1 | 19.0 | 30.8 | 34.5 | 6.4 | 12.6 | 135.1 | 21.6 | 35.8 | no | 1.2 | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 9/9/09 | 66.6 | 16.3 | 24.1 | 81.1 | 8.4 | 19.6 | 133.8 | 18.8 | 39.7 | no | nr[1] | nr[1] | nr[1] | 0.1 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 9/10/09 | nr[1] | nr[1] | nr[1] | 29.9 | 1.1 | 6.4 | 50.6 | 13.1 | 22.9 | no | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | 0.0 | 0.0 | 0.0 | no |
| 9/14/09 | 34.5 | 2.4 | 8.2 | 110.0 | 4.5 | 25.8 | 77.3 | 3.0 | 16.5 | no | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 9/15/09 | 28.8 | 15.5 | 20.1 | 104.0 | 12.2 | 39.5 | 82.5 | 15.7 | 28.7 | no | 0.2 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 9/16/09 | 24.8 | 8.4 | 14.2 | 144.4 | 5.7 | 21.7 | 86.0 | 7.1 | 14.8 | no | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 9/17/09 | 14.6 | 4.2 | 7.5 | 143.7 | 3.3 | 31.4 | 72.7 | 6.9 | 16.9 | no | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | no |
| 9/18/09 | 38.7 | 20.9 | 27.4 | 127.8 | 13.5 | 41.8 | 48.0 | 21.5 | 32.5 | no | 0.8 | 0.0 | 0.1 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 9/19/09 | 2.3 | 0.1 | 0.4 | 140.2 | 0.7 | 29.8 | 42.0 | 0.5 | 9.7 | no | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 9/21/09 | 116.5 | 7.0 | 25.6 | 135.6 | 3.2 | 19.3 | 144.6 | 5.7 | 27.2 | no | 0.5 | 0.0 | 0.1 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 9/22/09 | 39.6 | 13.9 | 24.2 | 103.0 | 3.3 | 7.8 | 41.4 | 11.5 | 23.1 | no | 1.0 | 0.0 | 0.2 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 9/23/09 | nr[1] | nr[1] | nr[1] | 36.4 | 4.3 | 10.1 | 119.9 | 13.6 | 25.0 | no | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 9/24/09 | 111.4 | 12.1 | 36.9 | 63.6 | 8.1 | 13.8 | 100.6 | 17.9 | 39.5 | no | 0.3 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | no |
| 9/25/09 | 95.9 | 12.1 | 36.3 | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | no | 0.7 | 0.0 | 0.1 | 0.2 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | no |
| 9/26/09 | 21.1 | 3.8 | 8.7 | 24.4 | 3.2 | 5.1 | 23.6 | 4.9 | 10.3 | no | 0.0 | 0.0 | 0.0 | 0.9 | 0.0 | 0.3 | 0.0 | 0.0 | 0.0 | no |
| 9/28/09 | 164.1 | 23.4 | 47.4 | 86.6 | 11.1 | 22.7 | 164.7 | 21.3 | 50.1 | yes[2] | 0.4 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 9/29/09 | 25.8 | 6.3 | 11.4 | 89.6 | 3.4 | 13.0 | 63.6 | 9.6 | 16.5 | no | 0.9 | 0.0 | 0.2 | 0.3 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | no |
| 9/30/09 | 10.7 | 2.0 | 3.7 | 92.2 | 1.4 | 19.3 | 130.0 | 1.3 | 14.3 | no | 0.0 | 0.0 | 0.0 | 0.4 | 0.0 | 0.3 | 0.0 | 0.0 | 0.0 | no |

NOTES:
(1) Not recorded due to equipment malfunction
(2) Exceedence caused by dust spikes from reagent silos.

NOTES:
(1) Not recorded due to equipment malfunction

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| | | | | | | | | | | | | | | | | | | | | |
| 10/1/09 | 21.5 | 4.4 | 10.6 | 76.6 | 3.0 | 16.0 | 30.5 | 6.2 | 11.4 | no | 0.2 | 0.0 | 0.0 | 0.4 | 0.0 | 0.3 | 0.0 | 0.0 | 0.0 | no |
| 10/2/09 | 38.7 | 9.8 | 16.5 | 55.8 | 3.7 | 8.9 | 29.8 | 8.4 | 16.8 | no | 0.5 | 0.0 | 0.2 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 10/5/09 | 17.2 | 3.7 | 6.5 | 112.3 | 2.3 | 27.9 | 35.8 | 2.9 | 10.7 | no | 0.0 | 0.0 | 0.0 | 0.4 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | no |
| 10/6/09 | 47.0 | 1.7 | 7.6 | 82.4 | 3.7 | 26.8 | 50.3 | 1.2 | 13.3 | no | 0.2 | 0.0 | 0.0 | 0.3 | 0.0 | 0.3 | 0.0 | 0.0 | 0.0 | no |
| 10/7/09 | 32.7 | 5.7 | 10.1 | 93.7 | 4.8 | 28.9 | 25.5 | 4.0 | 12.0 | no | 0.4 | 0.0 | 0.1 | 0.4 | 0.0 | 0.2 | 0.5 | 0.3 | 0.4 | no |
| 10/8/09 | 10.6 | 1.3 | 3.3 | 123.9 | 1.7 | 32.8 | 45.4 | 1.5 | 11.3 | no | 0.2 | 0.0 | 0.1 | 0.5 | 0.0 | 0.3 | 0.6 | 0.3 | 0.4 | no |
| 10/9/09 | 45.1 | 16.8 | 30.1 | 98.2 | 6.5 | 21.4 | 50.7 | 16.5 | 29.9 | no | 1.2 | 0.1 | 0.4 | 0.5 | 0.0 | 0.2 | 0.6 | 0.4 | 0.5 | no |
| 10/10/09 | 4.6 | 0.5 | 2.1 | 140.8 | 1.1 | 38.9 | 34.6 | 2.5 | 8.0 | no | 0.1 | 0.0 | 0.0 | 0.2 | 0.0 | 0.1 | 0.4 | 0.3 | 0.4 | no |
| 10/12/09 | 9.6 | 2.8 | 5.0 | 129.4 | 0.8 | 8.5 | 75.5 | 3.9 | 12.0 | no | 0.2 | 0.0 | 0.1 | 0.1 | 0.0 | 0.1 | 0.4 | 0.3 | 0.4 | no |
| 10/13/09 | 25.9 | 9.3 | 18.5 | 49.0 | 7.2 | 24.7 | 149.2 | 11.2 | 29.4 | no | 0.1 | 0.0 | 0.1 | 0.4 | 0.0 | 0.2 | 0.5 | 0.3 | 0.4 | no |
| 10/14/09 | 12.1 | 2.3 | 4.2 | 73.3 | 0.7 | 11.4 | 16.4 | 2.5 | 6.8 | no | 0.2 | 0.0 | 0.1 | 0.2 | 0.0 | 0.2 | 0.5 | 0.3 | 0.4 | no |
| 10/15/09 | 79.0 | 7.7 | 26.6 | 138.4 | 2.9 | 31.9 | 105.3 | 8.6 | 22.5 | no | 0.9 | 0.0 | 0.2 | 0.6 | 0.0 | 0.3 | 0.4 | 0.3 | 0.4 | no |
| 10/16/09 | 73.6 | 3.7 | 9.0 | 109.0 | 0.0 | 9.9 | nr[1] | nr[1] | nr[1] | no | 0.2 | 0.0 | 0.1 | 0.3 | 0.0 | 0.3 | 0.5 | 0.3 | 0.4 | no |
| 10/19/09 | 20.0 | 4.1 | 7.0 | 8.6 | 0.0 | 0.0 | 28.0 | 4.5 | 11.2 | no | 0.2 | 0.0 | 0.1 | 0.3 | 0.0 | 0.2 | 0.4 | 0.2 | 0.3 | no |
| 10/20/09 | 39.2 | 12.1 | 20.0 | 26.0 | 0.0 | 1.4 | 128.2 | 10.5 | 30.3 | no | 0.3 | 0.0 | 0.0 | 0.4 | 0.1 | 0.3 | 0.6 | 0.4 | 0.5 | no |
| 10/21/09 | 110.1 | 20.9 | 34.3 | 25.2 | 2.8 | 4.6 | 141.2 | 19.2 | 45.4 | no | 2.1 | 0.0 | 0.4 | 0.3 | 0.0 | 0.2 | 0.6 | 0.4 | 0.5 | no |
| 10/23/09 | 111.3 | 4.9 | 18.1 | 39.8 | 1.8 | 6.4 | 101.5 | 5.1 | 24.5 | no | 0.2 | 0.0 | 0.2 | 0.6 | 0.0 | 0.3 | 0.7 | 0.4 | 0.6 | no |
| 10/24/09 | 107.5 | 58.6 | 79.7 | 26.0 | 10.0 | 14.2 | 122.3 | 61.2 | 70.4 | no | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.2 | 0.4 | 0.3 | 0.4 | no |
| 10/26/09 | 45.3 | 0.0 | 5.4 | 36.7 | 1.6 | 9.9 | 29.1 | 4.5 | 13.1 | no | 0.7 | 0.0 | 0.2 | 0.3 | 0.0 | 0.1 | 0.7 | 0.3 | 0.5 | no |
| 10/27/09 | 33.5 | 16.0 | 26.8 | 5.6 | 1.8 | 3.5 | 67.3 | 16.2 | 26.2 | no | 3.2 | 0.0 | 1.4 | 0.4 | 0.0 | 0.2 | 0.5 | 0.3 | 0.4 | no |
| 10/28/09 | nr[1] | nr[1] | nr[1] | 4.0 | 1.0 | 2.8 | 13.2 | 5.4 | 8.0 | no | 29.7[1] | 0.0 | 10.8 | 0.3 | 0.0 | 0.2 | 0.5 | 0.3 | 0.5 | yes[1] |
| 10/29/09 | 31.0 | 3.7 | 13.5 | 21.6 | 3.8 | 7.7 | 57.9 | 8.0 | 19.1 | no | 0.2 | 0.0 | 0.1 | 0.2 | 0.0 | 0.1 | 0.6 | 0.3 | 0.5 | no |
| 10/30/09 | 30.7 | 14.0 | 19.2 | 10.4 | 3.8 | 5.7 | 60.5 | 18.5 | 28.2 | no | 0.5 | 0.0 | 0.2 | 0.2 | 0.0 | 0.1 | 0.5 | 0.3 | 0.5 | no |

NOTES:
(1) Not recorded due to equipment malfunction

NOTES:
(1) VOCs exceedences due to false positives likely caused by humidity.

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| | | | | | | | | | | | | | | | | | | | | |
| 11/2/09 | 63.4 | 1.0 | 6.5 | 55.4 | 0.6 | 12.8 | 146.2 | 3.1 | 17.0 | no | 0.6 | 0.0 | 0.3 | 0.1 | 0.0 | 0.1 | 0.5 | 0.4 | 0.4 | no |
| 11/3/09 | 124.8 | 11.2 | 20.0 | 21.1 | 3.3 | 10.1 | 39.5 | 13.5 | 27.9 | no | 0.8 | 0.0 | 0.2 | 0.3 | 0.0 | 0.2 | 0.6 | 0.3 | 0.5 | no |
| 11/4/09 | 20.5 | 3.4 | 8.9 | 19.7 | 0.8 | 4.5 | 67.9 | 3.6 | 15.7 | no | 0.5 | 0.0 | 0.3 | 0.2 | 0.0 | 0.1 | 0.7 | 0.3 | 0.4 | no |
| 11/5/09 | 80.7 | 0.1 | 31.4 | 15.7 | 4.1 | 7.4 | 45.0 | 14.4 | 26.6 | no | 0.3 | 0.0 | 0.2 | 0.2 | 0.0 | 0.1 | 0.5 | 0.3 | 0.4 | no |
| 11/6/09 | 6.9 | 1.8 | 3.9 | 17.6 | 1.0 | 2.8 | 149.5 | 2.5 | 21.4 | no | 0.2 | 0.0 | 0.2 | 0.4 | 0.0 | 0.2 | 0.6 | 0.3 | 0.5 | no |
| 11/7/09 | 28.9 | 5.7 | 17.7 | 16.3 | 2.6 | 4.9 | 36.6 | 7.4 | 18.5 | no | 0.4 | 0.0 | 0.2 | 0.5 | 0.2 | 0.4 | 0.5 | 0.2 | 0.4 | no |
| 11/9/09 | 143.0 | 48.5 | 67.3 | 27.1 | 11.5 | 16.2 | 141.3 | 52.3 | 70.1 | no | 1.9 | 0.0 | 0.3 | 0.1 | 0.0 | 0.1 | 0.6 | 0.3 | 0.5 | no |
| 11/10/09 | 30.4 | 6.0 | 12.4 | 147.2 | 36.3 | 82.9 | 137.2 | 30.8 | 68.7 | no | 0.2 | 0.0 | 0.1 | 0.2 | 0.0 | 0.1 | 0.6 | 0.3 | 0.5 | no |
| 11/11/09 | 14.4 | 0.0 | 2.2 | 50.2 | 1.5 | 4.2 | 141.7 | 6.1 | 22.5 | no | 0.4 | 0.0 | 0.2 | 0.1 | 0.0 | 0.0 | 0.7 | 0.3 | 0.4 | no |
| 11/12/09 | 14.4 | 0.0 | 2.2 | 22.2 | 1.5 | 4.7 | 92.9 | 6.9 | 18.0 | no | 0.2 | 0.0 | 0.2 | 0.2 | 0.0 | 0.1 | 0.5 | 0.2 | 0.4 | no |
| 11/13/09 | 13.0 | 6.4 | 9.8 | 35.3 | 2.6 | 4.8 | 65.7 | 14.5 | 24.7 | no | 0.2 | 0.0 | 0.1 | 0.2 | 0.0 | 0.1 | 0.5 | 0.2 | 0.4 | no |
| 11/14/09 | 0.4 | 0.0 | 0.1 | 110.0 | 0.7 | 4.9 | 18.4 | 3.8 | 9.5 | no | 3.9 | 0.0 | 1.5 | 0.4 | 0.0 | 0.2 | 0.6 | 0.2 | 0.4 | no |
| 11/16/09 | 89.6 | 5.8 | 33.0 | 28.4 | 0.1 | 2.0 | 147.6 | 3.8 | 31.1 | no | 0.3 | 0.0 | 0.2 | 0.6 | 0.0 | 0.3 | 1.0 | 0.2 | 0.5 | no |
| 11/17/09 | 119.7 | 5.8 | 10.1 | 60.8 | 0.4 | 3.3 | 134.1 | 7.8 | 33.7 | no | 1.2 | 0.0 | 0.2 | 0.4 | 0.0 | 0.3 | 0.8 | 0.4 | 0.7 | no |
| 11/18/09 | 114.2 | 13.2 | 25.5 | 85.5 | 5.6 | 21.1 | 70.9 | 13.6 | 26.6 | no | 0.3 | 0.0 | 0.2 | 0.6 | 0.0 | 0.3 | 0.7 | 0.4 | 0.6 | no |
| 11/19/09 | 148.1 | 25.8 | 82.1 | 33.1 | 6.4 | 12.0 | 74.7 | 17.4 | 38.8 | no | 3.8 | 0.0 | 0.4 | 0.4 | 0.0 | 0.3 | 0.6 | 0.3 | 0.5 | no |
| 11/20/09 | 132.1 | 5.1 | 30.4 | 63.0 | 7.7 | 18.0 | 143.3 | 10.1 | 19.3 | no | 0.9 | 0.0 | 0.1 | 0.4 | 0.0 | 0.2 | 0.7 | 0.4 | 0.6 | no |
| 11/23/09 | 89.4 | 11.6 | 34.4 | 42.9 | 11.7 | 16.7 | 48.1 | 15.8 | 23.5 | no | 0.4 | 0.0 | 0.1 | 0.4 | 0.0 | 0.2 | 0.5 | 0.2 | 0.5 | no |
| 11/24/09 | 108.9 | 4.9 | 34.0 | 76.5 | 4.6 | 13.9 | 89.7 | 4.6 | 15.1 | no | 3.1 | 0.0 | 0.3 | 0.4 | 0.0 | 0.3 | 1.0 | 0.2 | 0.5 | no |
| 11/25/09 | 142.3 | 0.0 | 49.9 | 48.1 | 7.6 | 21.0 | 69.7 | 13.2 | 32.2 | no | 1.6 | 0.1 | 0.8 | 0.2 | 0.0 | 0.1 | 0.5 | 0.3 | 0.5 | no |
| 11/30/09 | 87.2 | 2.5 | 13.3 | 130.7 | 0.0 | 29.3 | 38.0 | 5.5 | 17.6 | no | 0.6 | 0.0 | 0.3 | 3.5 | 0.0 | 0.2 | 0.8 | 0.3 | 0.6 | no |

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| 12/1/09 | 87.2 | 2.5 | 13.3 | 130.7 | 0.0 | 29.3 | 38.0 | 5.5 | 17.6 | no | 0.6 | 0.0 | 0.3 | nr[1] | nr[1] | nr[1] | 0.8 | 0.3 | 0.6 | no |
| 12/2/09 | 55.9 | 16.4 | 33.6 | 89.3 | 14.8 | 29.0 | 128.8 | 25.5 | 42.8 | no | 1.1 | 0.1 | 0.5 | 0.3 | 0.0 | 0.2 | 0.9 | 0.4 | 0.7 | no |
| 12/3/09 | 57.0 | 0.1 | 11.8 | 44.0 | 0.7 | 4.9 | 15.6 | 2.4 | 7.0 | no | 0.2 | 0.0 | 0.1 | 0.3 | 0.0 | 0.1 | 0.7 | 0.3 | 0.5 | no |
| 12/4/09 | 1.8 | 0.0 | 0.1 | 66.7 | 5.3 | 15.9 | 98.7 | 6.3 | 17.4 | no | 0.3 | 0.0 | 0.1 | 0.3 | 0.0 | 0.2 | 1.0 | 0.4 | 0.7 | no |
| 12/7/09 | 93.7 | 35.5 | 56.0 | 103.4 | 46.2 | 66.4 | 117.1 | 51.3 | 75.8 | no | 0.4 | 0.0 | 0.3 | 0.3 | 0.0 | 0.2 | 0.7 | 0.3 | 0.6 | no |
| 12/8/09 | 51.8 | 12.2 | 18.6 | 143.2 | 19.5 | 36.4 | 123.7 | 16.5 | 28.3 | no | 0.3 | 0.0 | 0.2 | 0.5 | 0.0 | 0.3 | 0.8 | 0.3 | 0.6 | no |
| 12/9/09 | nr[1] | nr[1] | nr[1] | 68.2 | 25.7 | 45.5 | 71.7 | 39.3 | 55.9 | no | 1.3 | 0.3 | 0.8 | 0.6 | 0.4 | 0.6 | 0.7 | 0.3 | 0.6 | no |
| 12/10/09 | 17.6 | 2.3 | 7.9 | 125.8 | 0.9 | 48.5 | 106.2 | 4.7 | 12.1 | no | 0.5 | 0.1 | 0.3 | 0.4 | 0.0 | 0.2 | 0.7 | 0.3 | 0.6 | no |
| 12/11/09 | nr[1] | nr[1] | nr[1] | 112.8 | 9.0 | 26.0 | 58.1 | 13.2 | 19.2 | no | 0.8 | 0.3 | 0.6 | 0.6 | 0.0 | 0.4 | 0.2 | 0.0 | 0.2 | no |
| 12/14/09 | 119.8 | 0.0 | 63.0 | 106.1 | 7.7 | 24.4 | 74.8 | 10.2 | 39.6 | no | 0.6 | 0.1 | 0.4 | 0.7 | 0.4 | 0.6 | 0.7 | 0.3 | 0.6 | no |
| 12/15/09 | 72.6 | 8.8 | 26.4 | 142.8 | 0.0 | 43.5 | 69.2 | 11.5 | 35.3 | no | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.7 | 0.2 | 0.6 | no |
| 12/16/09 | 36.7 | 4.1 | 11.8 | 54.7 | 5.2 | 23.4 | 54.8 | 4.1 | 14.0 | no | nr[1] | nr[1] | nr[1] | 0.0 | 0.0 | 0.0 | 2.6 | 1.1 | 2.1 | no |
| 12/17/09 | 13.9 | 2.5 | 5.8 | 86.1 | 7.8 | 29.4 | 146.7 | 2.3 | 15.7 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 12/18/09 | 50.5 | 7.6 | 14.9 | 124.3 | 8.2 | 23.2 | nr[1] | nr[1] | nr[1] | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.8 | 0.0 | 1.2 | no |
| 12/21/09 | 13.5 | 2.7 | 5.5 | 105.8 | 12.8 | 32.9 | 141.4 | 6.4 | 13.9 | no | 0.0 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | 3.3 | 0.8 | 2.2 | no |
| 12/22/09 | nr[1] | nr[1] | nr[1] | 46.8 | 5.3 | 15.4 | 28.9 | 6.6 | 11.5 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.8 | 1.2 | 2.3 | no |

NOTES:
(1) Not recorded due to equipment malfunction

NOTES:
(1) Not recorded due to equipment malfunction

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| 1/4/10 | 20.9 | 6.7 | 10.1 | 72.8 | 5.3 | 28.8 | nr[1] | nr[1] | nr[1] | no | nr[1] | nr[1] | nr[1] | 0.0 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | no |
| 1/5/10 | 68.7 | 6.7 | 22.6 | 15.0 | 4.1 | 7.0 | nr[1] | nr[1] | nr[1] | no | nr[1] | nr[1] | nr[1] | 0.0 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | no |
| 1/6/10 | 22.9 | 0.1 | 6.2 | 103.4 | 6.1 | 24.4 | 63.5 | 0.7 | 7.5 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.5 | 1.3 | 2.1 | no |
| 1/7/10 | 74.1 | 3.5 | 18.3 | 113.9 | 11.1 | 30.8 | 73.7 | 2.9 | 9.8 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.9 | 0.2 | 0.6 | no |
| 1/8/10 | 58.7 | 2.8 | 18.0 | 139.1 | 6.4 | 37.9 | 53.1 | 0.0 | 16.9 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.5 | 0.2 | 0.4 | no |
| 1/11/10 | 45.2 | 10.6 | 17.6 | 121.9 | 15.5 | 30.7 | 27.9 | 8.8 | 14.4 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.5 | 0.2 | 0.4 | no |
| 1/12/10 | 21.8 | 3.9 | 11.7 | 89.7 | 14.0 | 36.3 | 37.4 | 5.5 | 12.4 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.6 | 0.1 | 0.4 | no |
| 1/13/10 | 38.3 | 6.8 | 15.1 | 168.9 | 16.7 | 35.7 | 29.4 | 8.2 | 14.3 | yes[2] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.4 | 0.2 | 0.4 | no |
| 1/14/10 | 79.8 | 22.5 | 43.0 | 56.6 | 19.4 | 37.2 | 16.4 | 4.8 | 8.6 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.7 | 0.3 | 0.5 | no |
| 1/15/10 | 140.9 | 18.6 | 46.2 | 86.1 | 15.7 | 30.2 | 68.6 | 16.4 | 26.8 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.5 | 0.2 | 0.5 | no |
| 1/16/10 | nr[1] | nr[1] | nr[1] | 6.4 | 2.3 | 3.1 | nr[1] | nr[1] | nr[1] | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | no |
| 1/18/10 | nr[1] | nr[1] | nr[1] | 64.6 | 1.7 | 12.3 | 17.0 | 1.2 | 5.0 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 1/19/10 | nr[1] | nr[1] | nr[1] | 267.1 | 13.6 | 47.6 | 252.3 | 104.5 | 176.7 | yes[2] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 1/20/10 | 131.4 | 11.8 | 45.5 | 18.9 | 5.1 | 9.6 | 75.3 | 0.0 | 14.4 | no | nr[1] | nr[1] | nr[1] | 0.0 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | no |
| 1/21/10 | 31.4 | 7.3 | 17.4 | 139.3 | 8.8 | 30.8 | 150.8 | 0.0 | 56.2 | no[3] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 1/22/10 | 25.2 | 5.7 | 13.6 | 102.3 | 0.1 | 41.3 | 161.3 | 5.8 | 17.1 | no[4] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 1/23/10 | 23.9 | 13.4 | 18.0 | 32.2 | 11.3 | 20.3 | 7.0 | 1.2 | 3.3 | no | 0.0 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | no |
| 1/25/10 | 105.3 | 10.4 | 41.1 | 33.8 | 15.4 | 25.2 | 62.5 | 24.9 | 37.5 | no | 61.7 | 0.0 | 21.1 | 9999.0 | 0.0 | 3679.4 | 0.0 | 0.0 | 0.0 | yes[2] |
| 1/26/10 | 1.4 | 0.0 | 0.0 | 227.6 | 1.8 | 18.7 | 31.3 | 0.0 | 1.2 | yes[2] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 1/27/10 | 16.7 | 0.0 | 1.1 | 57.1 | 13.7 | 27.2 | 38.1 | 7.3 | 12.6 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 1/28/10 | 80.9 | 7.0 | 38.4 | 483.3 | 13.1 | 33.6 | 83.5 | 3.2 | 21.6 | yes[2] | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 1/29/10 | 94.4 | 3.2 | 12.0 | 75.7 | 10.6 | 22.0 | 20.4 | 1.7 | 3.6 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |

NOTES:
(1) Not recorded due to equipment malfunction
(2) Dust exceedence was the result of excessive dust from reagent delivery truck off-loading into a silo.
(3) The relative (downwind minus upwind) dust level did not exceed action level.
(4) The relative (nearest receptor minus upwind) dust level did not exceed action level.

NOTES:
(1) Not recorded due to equipment malfunction
(2) VOCs exceedence due to false positives likely caused by inclement weather.

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| 2/1/10 | 42.7 | 13.9 | 23.8 | 149.8 | 10.7 | 26.4 | 78.5 | 3.9 | 16.6 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 2/2/10 | 82.9 | 12.9 | 23.9 | 45.7 | 8.1 | 14.9 | 35.3 | 8.9 | 17.8 | no | nr[1] | nr[1] | nr[1] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 2/3/10 | 85.8 | 34.1 | 46.5 | 159.4 | 23.1 | 41.9 | 62.8 | 15.1 | 24.4 | no[1] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 2/4/10 | nr[2] | nr[2] | nr[2] | 147.8 | 4.8 | 29.5 | 73.0 | 3.4 | 13.1 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | no |
| 2/5/10 | nr[2] | nr[2] | nr[2] | 193.9 | 17.1 | 31.4 | 55.2 | 10.4 | 17.3 | yes[3] | nr[1] | nr[1] | nr[1] | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 | no |
| 2/8/10 | 35.7 | 4.0 | 8.4 | 180.1 | 4.4 | 12.9 | 19.7 | 4.5 | 7.1 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.5 | 0.0 | 0.0 | no |
| 2/9/10 | 75.2 | 1.0 | 8.5 | 12.2 | 4.3 | 8.2 | 94.4 | 4.2 | 13.8 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 2/11/10 | 33.5 | 0.0 | 15.7 | 148.0 | 2.3 | 27.5 | 93.0 | 0.0 | 19.3 | no | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | no |
| 2/12/10 | 105.7 | 6.1 | 15.3 | 64.1 | 7.4 | 22.4 | 47.4 | 3.9 | 11.5 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 2/15/10 | 70.1 | 12.5 | 22.4 | 108.3 | 8.3 | 21.0 | 13.1 | 1.7 | 5.0 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 2/16/10 | 71.3 | 22.6 | 35.1 | 152.3 | 18.3 | 47.1 | 17.8 | 3.1 | 7.6 | no[1] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | no |
| 2/17/10 | 34.5 | 1.5 | 10.5 | 2.7 | 1.2 | 2.3 | 20.4 | 2.0 | 7.8 | no | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | no |
| 2/18/10 | 31.6 | 0.9 | 7.8 | 47.0 | 7.2 | 21.7 | 34.9 | 2.4 | 14.2 | no | 0.0 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | 3.5 | 0.0 | 0.1 | no |
| 2/19/10 | 25.1 | 1.8 | 5.2 | 39.6 | 4.8 | 11.8 | 7.5 | 0.0 | 2.4 | no | 0.0 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | no |
| 2/22/10 | 134.1 | 0.0 | 12.6 | 35.8 | 3.9 | 9.4 | nr[2] | nr[2] | nr[2] | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | no |
| 2/23/10 | 57.0 | 4.9 | 24.4 | 21.8 | 3.6 | 11.6 | 18.1 | 0.7 | 2.8 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.1 | 0.0 | 0.2 | no |
| 2/24/10 | 129.8 | 0.5 | 18.7 | 64.5 | 9.8 | 22.1 | 8.0 | 0.1 | 1.3 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | no |
| 2/25/10 - 2/26/10 CAMP not set up due to limited site activities | | | | | | | | | | | 2/25/10 - 2/26/10 CAMP not set up due to limited site activities | | | | | | | | | |

NOTES:
(1) The relative (nearest receptor minus upwind) dust level did not exceed action levels.
(2) Not recorded due to equipment malfunction.
(3) Dust exceedence was the result of excessive dust from reagent delivery truck off-loading into a silo.

NOTES:
(1) Not recorded due to equipment malfunction.

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| 3/1/10 | 146.6 | 2.1 | 28.9 | 103.0 | 4.8 | 20.0 | 311.5 | 69.5 | 81.8 | yes[1] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | no |
| 3/2/10 | 141.2 | 3.7 | 18.4 | 62.8 | 3.1 | 12.0 | 32.7 | 0.0 | 0.6 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/3/10 | 116.2 | 8.9 | 39.4 | 330.9 | 2.7 | 15.2 | 53.5 | 2.3 | 10.8 | yes[1] | 0.0 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | 0.0 | 0.0 | 0.0 | no |
| 3/4/10 | 33.9 | 3.1 | 11.0 | nr[2] | nr[2] | nr[2] | nr[2] | nr[2] | nr[2] | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/5/10 | nr[2] | nr[2] | nr[2] | 273.8 | 5.6 | 17.2 | 24.0 | 2.6 | 5.2 | yes[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | nr[1] | no |
| 3/8/10 | nr[2] | nr[2] | nr[2] | nr[2] | nr[2] | nr[2] | 28.8 | 7.1 | 16.2 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/9/10 | 41.1 | 4.9 | 13.9 | 700.1 | 5.3 | 296.4 | 95.5 | 5.4 | 22.4 | yes[1] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/10/10 | 62.5 | 10.3 | 30.3 | 36.9 | 4.3 | 9.6 | 27.7 | 3.7 | 8.0 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/11/10 | 50.8 | 16.1 | 32.8 | 111.2 | 13.6 | 23.2 | 115.7 | 10.4 | 23.5 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/12/10 | 31.2 | 0.3 | 21.8 | 22.3 | 10.5 | 15.0 | 20.6 | 9.3 | 13.6 | no | 1.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/15/10 | 27.8 | 0.9 | 5.6 | 16.8 | 2.7 | 6.8 | 5.0 | 0.1 | 2.0 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/16/10 | 35.5 | 1.1 | 7.5 | 284.7[1] | 4.1 | 37.0 | 32.5 | 0.1 | 4.6 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/17/10 | 20.5 | 3.9 | 9.8 | 56.2 | 5.5 | 20.2 | 74.1 | 3.1 | 12.2 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/18/10 | 70.7 | 0.0 | 16.9 | 43.3 | 4.0 | 16.8 | 21.1 | 3.5 | 9.3 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/19/10 | 92.7 | 1.3 | 23.4 | 64.7 | 7.8 | 25.9 | 22.8 | 6.7 | 11.8 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/22/10 | 65.3 | 29.1 | 43.6 | 75.9 | 29.0 | 44.5 | 86.0 | 25.9 | 38.6 | no | 0.7 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/23/10 | 47.7 | 0.0 | 9.2 | 47.4 | 10.3 | 32.5 | 40.2 | 6.4 | 23.1 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/24/10 | 35.2 | 1.2 | 7.4 | nr[2] | nr[2] | nr[2] | 107.0 | 0.0 | 6.8 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/25/10 | 40.8 | 13.7 | 26.5 | 63.8 | 8.3 | 15.9 | 14.0 | 2.7 | 5.2 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/26/10 | 52.8 | 5.1 | 13.1 | 22.8 | 6.5 | 11.5 | 10.9 | 1.2 | 2.7 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 | no |
| 3/29/10 | 143.7 | 24.0 | 55.0 | 39.9 | 10.2 | 18.9 | 20.4 | 3.1 | 6.3 | no | 62.6[2] | 0.0 | 27.1[2] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | yes[2] |
| 3/30/10 | 2.7 | 0.0 | 0.2 | 18.0 | 2.9 | 9.3 | 5.5 | 1.0 | 2.1 | no | 3.0 | 0.0 | 0.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 3/31/10 | 0.0 | 0.0 | 0.0 | 41.5 | 1.5 | 9.3 | 4.1 | 0.2 | 1.5 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |

NOTES:
(1) Dust exceedence was the result of excessive dust from reagent delivery truck off-loading into a silo.
(2) Not recorded due to equipment malfunction.

NOTES:
(1) Not recorded due to equipment malfunction.
(2) VOCs exceedences due to false positives likely caused by humidity.

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| 4/1/10 | 0.0 | 0.0 | 0.0 | 46.1 | 6.3 | 16.8 | 5.1 | 1.3 | 2.3 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/2/10 | 0.0 | 0.0 | 0.0 | 34.4 | 2.4 | 7.6 | 9.4 | 2.5 | 4.6 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/5/10 | 4.5 | 0.0 | 0.2 | 20.7 | 0.8 | 3.8 | 129.3 | 2.7 | 63.4 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/6/10 | 58.6 | 17.1 | 28.5 | 131.7 | 11.1 | 27.8 | 158.0 | 18.6 | 44.3 | no[1] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/7/10 | 112.0 | 15.3 | 43.5 | 120.3 | 11.0 | 34.3 | 220.0 | 5.6 | 55.7 | yes[2] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/8/10 | 70.6 | 29.6 | 48.2 | 44.9 | 21.6 | 31.6 | 77.5 | 17.2 | 38.1 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/9/10 | 38.2 | 3.7 | 9.7 | 71.6 | 7.0 | 22.0 | 38.2 | 0.2 | 10.8 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | no |
| 4/12/10 | 90.0 | 0.0 | 16.9 | 38.5 | 1.5 | 7.5 | 8.5 | 0.0 | 0.1 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/13/10 | 36.6 | 6.4 | 13.5 | 28.6 | 3.3 | 7.2 | 15.3 | 0.9 | 5.5 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/14/10 | 113.6 | 1.8 | 28.7 | 242.0 | 4.1 | 21.2 | 12.1 | 0.0 | 2.1 | yes[3] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/15/10 | 56.6 | 7.8 | 15.9 | 29.5 | 8.8 | 14.1 | 56.7 | 8.7 | 15.1 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/16/10 | 72.4 | 0.7 | 20.9 | 12.3 | 7.3 | 8.4 | 134.6 | 5.6 | 19.2 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | no |
| 4/17/10 | 49.3 | 0.1 | 8.9 | 28.3 | 1.0 | 6.6 | 49.4 | 1.3 | 7.2 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/19/10 | 55.0 | 3.1 | 13.8 | 13.2 | 2.3 | 5.1 | 92.7 | 1.6 | 9.8 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/20/10 | 50.4 | 0.0 | 2.7 | 11.0 | 0.5 | 3.7 | 68.3 | 1.7 | 11.4 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/21/10 | 80.8 | 17.3 | 36.1 | 24.0 | 7.6 | 15.5 | nr[4] | nr[4] | nr[4] | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | no |
| 4/22/10 | 113.3 | 14.4 | 33.4 | 41.0 | 8.3 | 19.1 | 24.6 | 10.1 | 16.9 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/23/10 | 23.5 | 5.5 | 11.0 | 13.3 | 4.7 | 8.3 | 48.1 | 4.6 | 8.5 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | no |
| 4/24/10 | 67.8 | 0.1 | 11.4 | 6.0 | 0.8 | 1.3 | 12.9 | 3.8 | 4.6 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | no |
| 4/26/10 | 28.0 | 4.9 | 16.7 | 20.1 | 5.2 | 11.1 | 14.5 | 3.9 | 7.5 | no | 0.7 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | nr[1] | nr[1] | nr[1] | no |
| 4/27/10 | 29.2 | 0.8 | 13.3 | 25.7 | 0.9 | 13.2 | 7.4 | 1.7 | 3.7 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/28/10 | 13.5 | 1.8 | 4.7 | 21.1 | 2.4 | 5.0 | 46.6 | 1.8 | 6.0 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/29/10 | 77.6 | 1.4 | 12.8 | 7.0 | 1.7 | 3.0 | 12.0 | 1.1 | 5.8 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 4/30/10 | 44.4 | 0.0 | 13.6 | 16.7 | 3.3 | 8.9 | 16.9 | 4.0 | 6.5 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |

NOTES:
(1) The relative (downward minus upwind) dust level did not exceed action levels.
(2) Dust exceedence due to off-site activity (i.e., leaf blower in Hamilton Street parking lot).
(3) Dust exceedence due to cleaning out silos.
(4) Not recorded due to equipment malfunction.

NOTES:
(1) Not recorded due to equipment malfunction.

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | | | | VOCs | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | SIDEWALK* (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | SIDEWALK VOC* (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| 5/3/10 | 7.2 | 0.0 | 0.7 | 16.0 | 9.8 | 11.8 | nr[2] | nr[2] | nr[2] | - | - | - | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | - | - | - | no |
| 5/4/10 | 32.9 | 4.1 | 9.0 | 45.5 | 0.5 | 4.7 | 15.1 | 4.4 | 7.0 | - | - | - | no | 0.2 | 0.0 | 0.1 | 0.1 | 0.0 | 0.1 | 0.1 | 0.0 | 0.0 | - | - | - | no |
| 5/5/10 | 16.7 | 2.8 | 6.0 | 75.0 | 2.1 | 7.8 | 8.2 | 3.7 | 5.5 | - | - | - | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | - | - | - | no |
| 5/6/10 | 174.1 | 19.2 | 80.5 | 76.4 | 2.9 | 31.8 | 35.3 | 7.1 | 18.2 | - | - | - | yes[1] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.2 | - | - | - | no |
| 5/7/10 | 55.3 | 0.0 | 6.1 | nr[2] | nr[2] | nr[2] | 17.0 | 1.8 | 4.3 | - | - | - | no | 0.1 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | 2.4 | 0.0 | 0.1 | - | - | - | no |
| 5/10/10 | 29.2 | 2.6 | 7.3 | 32.2 | 2.5 | 8.8 | 15.5 | 3.6 | 7.4 | - | - | - | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | - | - | - | no |
| 5/11/10 | 60.2 | 0.0 | 7.6 | 128.6 | 2.7 | 8.0 | 37.2 | 3.1 | 9.1 | 91.6 | 3.1 | 18.5 | no | 0.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | no |
| 5/12/10 | 142.0 | 8.7 | 22.9 | 18.2 | 5.3 | 6.9 | 73.2 | 2.9 | 5.9 | 83.5 | 5.9 | 16.2 | no | 5.5 | 0.0 | 1.7 | 0.1 | 0.0 | 0.1 | 2.9 | 0.0 | 0.5 | 27.3 | 0.0 | 13.9 | yes[1] |
| 5/13/10 | 27.8 | 0.9 | 6.4 | 26.0 | 2.1 | 4.7 | 14.7 | 0.0 | 2.8 | 129.9 | 5.2 | 29.4 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 5/14/10 | 45.6 | 37.1 | 40.9 | 37.3 | 15.8 | 21.0 | 44.1 | 15.5 | 31.2 | 66.4 | 32.9 | 51.7 | no | 0.4 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 10.0 | 0.0 | 2.7 | yes[1] |
| 5/17/10 | 32.7 | 4.1 | 13.7 | 9.7 | 2.8 | 3.8 | 18.9 | 3.1 | 7.5 | 14.8 | 6.6 | 10.9 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 5/18/10 | 48.1 | 11.7 | 19.3 | 47.2 | 11.0 | 15.5 | 20.3 | 9.7 | 13.4 | 111.7 | 14.0 | 24.7 | no | 0.2 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.7 | 0.0 | 0.3 | no |
| 5/19/10 | 7.6 | 0.5 | 2.6 | 5.2 | 0.4 | 2.6 | 8.0 | 0.2 | 3.2 | - | - | - | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | - | - | - | no |
| 5/20/10 | 19.2 | 0.8 | 4.1 | 20.5 | 0.1 | 4.1 | 10.1 | 1.2 | 4.2 | - | - | - | no | nr[2] | nr[2] | nr[2] | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | - | - | - | no |
| 5/21/10 | 19.4 | 9.5 | 12.6 | 31.5 | 9.5 | 13.3 | 25.5 | 9.4 | 12.9 | - | - | - | no | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | - | - | - | no |
| 5/24/10 | 147.2 | 58.7 | 100.5 | 67.5 | 11.4 | 39.7 | 53.3 | 11.9 | 31.5 | - | - | - | no | 1.7 | 0.0 | 0.6 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | - | - | - | no |
| 5/25/10 | 130.8 | 0.0 | 11.2 | 48.0 | 3.6 | 6.5 | 34.8 | 0.0 | 10.9 | - | - | - | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | - | - | - | no |
| 5/26/10 | 23.0 | 9.9 | 13.2 | 57.3 | 11.5 | 19.2 | 59.0 | 0.3 | 16.0 | - | - | - | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | - | - | - | no |
| 5/27/10 | 0.0 | 0.0 | 0.0 | 102.5 | 6.7 | 20.4 | 39.4 | 0.0 | 2.7 | - | - | - | no | 0.3 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | - | - | - | no |

NOTES:
(1) Exceedence caused by construction dust blowing from the west side of the site.
(2) Not recorded due to equipment malfunction.
"-" Data not collected because there was no investigation work in the sidewalk area.
* = Nearest Receptor CAMP station used for Water Street sidewalk investigation work.

NOTES:
(1) VOCs exceedence due to false positives likely caused by humidity.
(2) Not recorded due to equipment malfunction.
"-" Data not collected because there was no investigation work in the sidewalk area.
* = Nearest Receptor CAMP station used for Water Street sidewalk investigation work.

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| 6/2/10 | 85.9 | 15.2 | 38.1 | nr[1] | nr[1] | nr[1] | 57.7 | 6.4 | 17.7 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 6/3/10 | 22.8 | 15.9 | 19.7 | 66.8 | 13.2 | 36.0 | 33.6 | 0.1 | 13.0 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 6/4/10 | 52.0 | 1.4 | 15.6 | 34.3 | 1.0 | 4.9 | 47.3 | 8.0 | 13.0 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 3.3 | 0.0 | 0.1 | no |
| 6/7/10 | 12.5 | 0.1 | 3.5 | 65.7 | 2.4 | 9.5 | 26.5 | 0.0 | 5.4 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 6/8/10 | 5.1 | 1.2 | 3.0 | 36.2 | 2.1 | 6.8 | 4.7 | 0.0 | 0.0 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 6/9/10 | 15.7 | 5.4 | 9.3 | 55.1 | 5.2 | 9.8 | 2.3 | 0.1 | 0.6 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 6/10/10 | nr[1] | nr[1] | nr[1] | 29.1 | 2.1 | 12.9 | 48.8 | 14.1 | 21.1 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 6/11/10 | 10.2 | 2.5 | 6.0 | 79.3 | 3.1 | 8.0 | 32.2 | 1.2 | 10.9 | no | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 6/14/10 | 168.5 | 67.0 | 104.5 | 99.4 | 38.8 | 60.5 | 284.6 | 7.1 | 115.5 | yes[2] | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 6/15/10 | 13.9 | 8.1 | 9.4 | 152.0 | 9.5 | 17.3 | 19.4 | 2.2 | 10.7 | no[3] | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 6/16/10 | 71.2 | 13.1 | 19.9 | 72.8 | 10.8 | 16.2 | 5.5 | 1.3 | 2.6 | no | 0.5 | 0.1 | 0.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 6/17/10 | 33.6 | 1.3 | 6.1 | 84.6 | 0.4 | 6.7 | 6.6 | 1.3 | 2.4 | no | 0.6 | 0.2 | 0.3 | 0.0 | 0.0 | 0.0 | 3.5 | 0.0 | 0.1 | no |
| 6/18/10 | 24.7 | 17.4 | 19.6 | 64.8 | 18.8 | 26.6 | 2.7 | 0.7 | 1.9 | no | 0.4 | 0.1 | 0.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 6/21/10 | 18.3 | 0.0 | 4.4 | 48.0 | 2.3 | 7.1 | 4.4 | 0.5 | 1.2 | no | 0.4 | 0.3 | 0.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 6/22/10 | 34.0 | 9.9 | 16.8 | 67.7 | 9.4 | 14.6 | 6.2 | 1.0 | 2.7 | no | 0.4 | 0.1 | 0.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 6/23/10 | 137.1 | 6.2 | 34.1 | 130.8 | 7.4 | 21.1 | 30.3 | 3.1 | 6.8 | no | 3.7 | 0.5 | 0.7 | 0.1 | 0.0 | 0.1 | 11.1 | 0.0 | 0.4 | yes[1] |
| 6/24/10 | 103.3 | 0.0 | 23.4 | 60.9 | 28.3 | 34.0 | 7.7 | 4.6 | 5.9 | no | 1.3 | 0.3 | 0.4 | 0.1 | 0.0 | 0.1 | 2.5 | 0.0 | 0.0 | no |
| 6/25/10 | 24.9 | 0.0 | 5.1 | 52.6 | 5.1 | 11.2 | 3.1 | 0.4 | 1.5 | no | 0.4 | 0.1 | 0.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | no |
| 6/28/10 | 0.7 | 0.0 | 0.0 | 89.1 | 19.0 | 30.4 | 11.4 | 4.6 | 6.7 | no | 0.8 | 0.8 | 0.8 | 0.1 | 0.0 | 0.1 | 0.2 | 0.0 | 0.0 | no |
| 6/29/10 | 112.8 | 6.3 | 17.0 | 76.7 | 3.9 | 15.3 | 93.6 | 6.4 | 21.0 | no | 6.6 | 0.5 | 0.8 | 0.1 | 0.0 | 0.1 | 11.1 | 0.0 | 0.4 | yes[1] |

NOTES:
(1) Not recorded due to equipment malfunction.
(2) Dust exceedences due to false positives likely caused by humidity.
(3) The relative (nearest receptor minus upwind) dust level did not exceed action levels.

NOTES:
(1) VOCs exceedences due to false positives likely caused by humidity.

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| 7/7/10 | 69.2 | 34.6 | 41.0 | 65.3 | 53.4 | 57.2 | 58.3 | 0.0 | 5.2 | no | 0.5 | 0.3 | 0.4 | 0.2 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | no |
| 7/8/10 | 320.7 | 26.4 | 79.6 | 128.7 | 23.5 | 58.8 | 131.8 | 11.7 | 32.8 | yes[1] | 8.4 | 0.6 | 2.0 | 0.1 | 0.0 | 0.1 | 29.9 | 0.0 | 2.0 | yes[1] |
| 7/9/10 | 10.2 | 0.0 | 0.8 | 37.7 | 1.0 | 5.6 | 17.9 | 1.3 | 5.8 | no | 7.9 | 0.5 | 0.8 | 0.2 | 0.0 | 0.1 | 16.3 | 0.0 | 0.5 | yes[1] |
| 7/12/10 | 145.7 | 13.7 | 42.0 | 74.3 | 7.9 | 17.0 | 67.8 | 7.2 | 16.1 | no | 8.9 | 0.6 | 1.7 | 0.2 | 0.0 | 0.1 | 5.3 | 0.0 | 0.2 | yes[1] |
| 7/13/10 | 122.5 | 13.9 | 43.6 | 97.7 | 9.6 | 25.4 | 59.8 | 5.4 | 14.2 | no | 6.0 | 0.3 | 0.6 | 0.1 | 0.0 | 0.0 | 29.9 | 0.6 | 2.6 | yes[1] |
| 7/15/10 | 105.9 | 0.0 | 7.4 | 73.9 | 4.1 | 10.4 | 19.7 | 2.8 | 7.5 | no | 9.4 | 0.3 | 1.3 | 0.2 | 0.0 | 0.1 | 0.7 | 0.5 | 0.6 | yes[1] |
| 7/16/10 | 144.8 | 49.8 | 60.4 | 101.5 | 52.4 | 63.4 | 34.6 | 2.5 | 22.3 | no | 9.0 | 0.2 | 0.7 | 0.2 | 0.1 | 0.1 | 30.5 | 0.4 | 2.5 | yes[1] |
| 7/19/10 | 37.5 | 15.7 | 27.2 | 91.9 | 4.8 | 30.6 | 74.5 | 0.0 | 23.9 | no | 8.1 | 0.0 | 1.5 | 0.2 | 0.0 | 0.1 | 3.3 | 0.4 | 0.9 | yes[2] |
| 7/20/10 | 64.9 | 0.0 | 8.8 | 103.0 | 10.2 | 30.6 | 25.2 | 4.0 | 9.8 | no | 12.2 | 0.2 | 0.9 | 0.3 | 0.0 | 0.2 | 24.9 | 0.5 | 2.4 | yes[1] |
| 7/21/10 | 70.5 | 18.1 | 28.5 | 154.0 | 24.6 | 45.9 | 27.3 | 7.0 | 12.2 | no[2] | 7.8 | 0.1 | 0.4 | 0.3 | 0.0 | 0.2 | 23.6 | 0.5 | 1.9 | yes[1] |
| 7/22/10 | 20.6 | 5.1 | 8.0 | 42.9 | 6.2 | 11.1 | nr[5] | nr[5] | nr[5] | no | 0.6 | 0.1 | 0.2 | 0.1 | 0.0 | 0.1 | 3.1 | 0.3 | 0.4 | no |
| 7/23/10 | 51.3 | 13.2 | 24.4 | 112.4 | 11.9 | 22.6 | 16.4 | 2.9 | 4.5 | no | 0.8 | 0.0 | 0.3 | 0.2 | 0.0 | 0.1 | 1.2 | 0.2 | 0.5 | no |
| 7/26/10 | 24.7 | 1.5 | 5.2 | 101.0 | 4.2 | 14.7 | 10.9 | 0.5 | 2.8 | no | 0.2 | 0.0 | 0.1 | 0.2 | 0.0 | 0.1 | 1.0 | 0.2 | 0.3 | no |
| 7/27/10 | 19.4 | 7.0 | 11.4 | 92.6 | 12.9 | 23.9 | 170.0 | 4.7 | 19.1 | yes[3] | 0.2 | 0.0 | 0.1 | 0.3 | 0.0 | 0.1 | 1.1 | 0.0 | 0.4 | no |
| 7/28/10 | 54.1 | 25.7 | 37.9 | 105.4 | 21.7 | 34.1 | 137.9 | 17.7 | 31.6 | no | 0.3 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 2.9 | 0.3 | 0.4 | no |
| 7/29/10 | 1564.9 | 8.5 | 201.4 | 276.2 | 7.2 | 47.0 | 1262.8 | 5.8 | 146.6 | yes[1] | 14.8 | 0.3 | 2.0 | 0.2 | 0.0 | 0.1 | 176.6 | 0.3 | 9.4 | yes[1] |
| 7/30/10 | 206.6 | 12.0 | 39.7 | 75.5 | 14.1 | 24.1 | 110.1 | 13.0 | 24.3 | yes[4] | 0.3 | 0.0 | 0.2 | 0.7 | 0.0 | 0.1 | 0.4 | 0.1 | 0.2 | no |

NOTES:
(1) Dust exceedences due to false positives likely caused by humidity.
(2) The relative (nearest receptor minus upwind) dust level did not exceed action levels.
(3) Dust exceedence caused by street curb excavation adjacent to dust monitor.
(4) Dust exceedence caused by inorganic dust during restoration construction work.
(5) Not recorded due to equipment malfunction.

NOTES:
(1) VOCs exceedence due to false positives likely caused by humidity.
(2) VOCs exceedence due to false positives likely caused by inclement weather.

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.1**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**CAMP Summary Table**

| DATE | DUST | | | | | | | | | | VOCs | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | UPWIND (µg/m³) | | | DOWNWIND (µg/m³) | | | NEAREST RECEPTOR (µg/m³) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? | UPWIND (ppm) | | | DOWNWIND (ppm) | | | NEAREST RECEPTOR (ppm) | | | EXCEED ACTION LEVEL FOR 15 MIN AVG. INTERVAL? |
| | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | HIGH | LOW | AVERAGE | |
| | | | | | | | | | | | | | | | | | | | | |
| 8/3/10 | 131.3 | 0.0 | 17.4 | 69.0 | 12.2 | 29.4 | 201.6 | 95.1 | 140.0 | yes[1] | nr[1] | nr[1] | nr[1] | 0.0 | 0.0 | 0.0 | 4.1 | 0.8 | 2.0 | no |
| 8/4/10 | 106.2 | 15.2 | 32.8 | 129.6 | 13.5 | 31.2 | 10.5 | 3.1 | 5.2 | no | 0.5 | 0.3 | 0.4 | 0.1 | 0.0 | 0.0 | 0.5 | 0.4 | 0.5 | no |
| 8/5/10 | 87.6 | 41.2 | 58.6 | 136.7 | 12.1 | 42.1 | 15.8 | 1.8 | 5.5 | no | 4.5 | 0.2 | 0.4 | 0.1 | 0.0 | 0.1 | 15.3 | 0.4 | 0.7 | yes[2] |
| 8/6/10 | 61.7 | 20.1 | 32.4 | 140.0 | 20.1 | 41.2 | 107.8 | 14.7 | 38.6 | no | 0.2 | 0.0 | 0.2 | 0.1 | 0.0 | 0.1 | 4.3 | 0.3 | 1.0 | no |

NOTES:
(1) Dust exceedence caused by inorganic dust during restoration construction work.

NOTES:
(1) Not recorded due to equipment malfunction.
(2) VOCs exceedences due to false positives likely caused by humidity.

Dust action levels:
Based on 15 min avg
Primary = 100 ug/m3 above background
Secondary = 150 ug/m3 above background

VOC action levels:
Based on 15 min avg
Primary = 5 PPM above background
Secondary = 10 ppm above background

**Table 4.3**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Excavator-ISS Tracking Log**

| Date | Cell ID | Estimated Cell Dimensions | | | | Water Added (GAL) | Reagents Added | | | Grout Added | | Estimated % Reagent Added | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | Width (FT) | Length (FT) | Depth Range (FT) | Avg Depth (FT) | | Slag (LBS) | Portland (LBS) | Total (LBS) | Total (GAL) | # Batches | | |
| 1/22/09 | TP-1 | 17 | 18 | 14 | 14 | 3,720 | 5,196 | 1,732 | 6,928 | | 4 | | (1) |
| 1/26/09 | TP-1A | 17 | 18 | 14 | 14 | 4,600 | 34,887 | 11,629 | 46,516 | | 6 | | |
| " | TP-1/1A | | | | | 8,320 | 40,083 | 13,361 | 53,444 | | 10 | 10.35 | (2) (6) |
| 1/27/09 | TP-2 | 17 | 18 | 12-14 | 13 | 4,510 | 50,166 | 16,722 | 66,888 | 7,216 | 8 | 13.95 | (6) |
| 1/28/09 | TP-3 | 18 | 34 | 12 | 12 | 8,711 | 95,674 | 31,891 | 127,565 | 13,871 | 7 | 14.41 | (6) |
| 1/29/09 | TP-4 | 17 | 25 | 12-16 | 14 | 7,201 | 81,470 | 27,157 | 108,627 | 11,595 | 12 | 15.15 | (6) |
| 1/30/09 | TP-5 | 17 | 25 | 12 | 12 | | | | | | | | (3) (7) |
| " | TP-5 | 14 | 21 | 12 | 12 | 10,806 | 122,258 | 40,753 | 163,011 | 17,400 | | | (7) |
| " | TP-5 | | | | | 10,806 | 122,258 | 40,753 | 163,011 | 17,400 | 18 | 15.68 | " |
| 2/2/09 | P-7 | 16 | 15 | 8 | 8 | 2,397 | 26,568 | 8,856 | 35,424 | 3,830 | 4 | 15.31 | " |
| " | P-8 | 16 | 15 | 10 | 10 | 3,002 | 33,449 | 11,150 | 44,599 | 4,806 | 5 | 15.42 | " |
| 2/2 & 2/3/09 | P-9 | 15 | 29 | 13 | 13 | 6,600 | 74,169 | 24,723 | 98,892 | 10,601 | 11 | 14.51 | (4) (7) |
| 2/3/09 | P-10 | 15 | 26 | 13 | 13 | 6,301 | 70,877 | 23,626 | 94,503 | 10,124 | 10.5 | 15.47 | (7) |
| 2/4/09 | P-11 | 15 | 26 | 15.5 | 15.5 | 6,306 | 70,266 | 23,422 | 93,688 | 7,237 | 10.5 | 12.86 | " |
| 2/6/09 | P-12 | 15 | 27 | 16 | 16 | 7,801 | 86,880 | 28,960 | 115,840 | 12,487 | 13 | 14.84 | " |
| " | P-6 | 15 | 16 | 10 | 10 | 3,005 | 31,666 | 10,555 | 42,221 | 4,325 | 5 | 14.60 | " |
| 2/7/09 | P-13 | 16 | 16 | 15 | 15 | (5) | 53,019 | 17,673 | 70,692 | (5) | (5) | 15.28 | " |
| 2/9/09 | P-14 | 10 | 11 | 13 | 13 | 2,400 | 26,602 | 8,867 | 35,469 | 3,835 | 4 | 20.58 | " |
| 2/9/09 | P-15 | 15 | 20 | 15 | 15 | 6,007 | 66,705 | 22,235 | 88,940 | 9,605 | 10 | 16.40 | (7) |
| 2/10/09 | EM-1 | 11 | 20 | 15 | 15 | 4,506 | 49,856 | 16,619 | 66,475 | 7,195 | 7.5 | 16.72 | (8) |
| " | EM-2 | 14 | 20 | 11 | 11 | 4,202 | 46,634 | 15,545 | 62,179 | 6,717 | 7 | 16.75 | " |
| " | EM-3 | 14 | 20 | 11 | 11 | 4,202 | 46,399 | 15,466 | 61,865 | 6,704 | 7 | 16.67 | " |
| 2/11/09 | EM-4 | 16 | 18 | 11 | 11 | 5,105 | 58,313 | 19,438 | 77,751 | 8,250 | 8.5 | 20.37 | " |
| " | P-5 | 16 | 20 | 11 | 11 | 4,803 | 54,877 | 18,293 | 73,170 | 7,783 | 8 | 17.25 | " |
| 2/13/09 | P-4 | 11 | 19 | 8 | 8 | 2,100 | 24,248 | 8,083 | 32,331 | | 3.5 | 16.05 | " |

**Table 4.3**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Excavator-ISS Tracking Log**

| Date | Cell ID | Estimated Cell Dimensions | | | | Water Added (GAL) | Reagents Added | | | Grout Added | | Estimated % Reagent Added | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | Width (FT) | Length (FT) | Depth Range (FT) | Avg Depth (FT) | | Slag (LBS) | Portland (LBS) | Total (LBS) | Total (GAL) | # Batches | | |
| 2/16/09 | P-3 | 16 | 21 | 13 | 13 | 6,608 | 75,650 | 25,217 | 100,867 | 10,688 | 11 | 19.16 | " |
| " | P-16 | 4 | 21 | 6 | 6 | 1,200 | 13,890 | 4,630 | 18,520 | 1,949 | 2 | 30.49 | " |
| 2/17/09 | EM-5 | 7 | 18 | 13.5 | 13.5 | 2,406 | 27,609 | 9,203 | 36,812 | 3,895 | 4 | 17.96 | " |
| " | EM-6 | 11 | 21 | 15 | 15 | 4,504 | 52,444 | 17,481 | 69,925 | 7,332 | 7.5 | 16.75 | " |
| 2/18/09 | EM-7 | 14 | 18 | 12.5 | 12.5 | 3,905 | 45,141 | 15,047 | 60,188 | 6,340 | 6.5 | 15.86 | " |
| " | P-17 | 19 | 17 | 17 | 17 | 6,906 | 79,760 | 26,587 | 106,347 | 11,208 | 11.5 | 16.07 | " |
| 2/19/09 | TP-2 (Remix) | 17 | 18 | 13 | 13 | 5,096 | 59,665 | 19,888 | 79,553 | 8,314 | 8.5 | 16.60 | " |
| 2/20/09 | TP-1 (Remix) | 17 | 18 | 14-15 | 14.5 | 5,701 | 65,818 | 21,939 | 87,757 | 9,251 | 9.5 | 16.41 | " |
| 2/21/09 | P-2 | 17 | 20 | 12.5 | 12.5 | 5,405 | 61,966 | 20,655 | 82,621 | 8,747 | 9 | 16.13 | " |
| 2/23/09 | EM-8 | 17 | 21 | 11 | 11 | 5,103 | 58,529 | 19,510 | 78,039 | 8,259 | 8.5 | 16.49 | " |
| " | P-1 | 17 | 20 | 14 | 14 | 6,302 | 72,896 | 24,299 | 97,195 | 10,233 | 10.5 | 16.95 | " |
| 2/24/09 | EM-9 | 18 | 20 | 13.5 | 13.5 | 6,002 | 67,576 | 22,525 | 90,101 | 9,647 | 10 | 15.39 | " |
| 2/25/09 | EM-10 | 14 | 27 | 16 | 16 | 7,507 | 84,230 | 28,077 | 112,307 | 12,050 | 12.5 | 15.41 | " |
| 2/26/09 | EM-11 | 10 | 27 | 14 | 14 | 4,803 | 53,704 | 17,901 | 71,605 | 7,700 | 8 | 15.72 | " |
| " | P-11 (Remix) | 15.5 | 20 | 11 | 11 | 4,509 | 50,709 | 16,903 | 67,612 | 7,231 | 7.5 | 16.45 | " |
| 2/27/09 | EM-12 | 10 | 20 | 16 | 16 | 5,105 | 58,073 | 19,358 | 77,431 | 8,237 | 8.5 | 20.08 | " |
| " | EM-13 | 10 | 31 | 16 | 16 | 6,611 | 75,205 | 25,068 | 100,273 | 10,667 | 11 | 16.78 | " |

**(1)** Grout flow meter not working. After 4 batches of grout, cement silo became inoperable. Mixing stopped @ 1500 due to inadequate amount of grout.
**(2)** Grout pumped is the total for TP-1 and TP-1A
**(3)** TP-5 was excavated and mixed in two separate cells and combined into one at the end of the day.
**(4)** Began P-9 at 1300 on 2/2/09 but ran out of slag, that portion was re-excavated and re-mixed on 2/3/09.
**(5)** Awaiting Contractor's data.
**(6)** Contractor used incorrect soil density = 114.3 lbs/ft$^3$
**(7)** Contractor used incorrect soil density = 120.4 lbs/ft$^3$
**(8)** Contractor began using correct soil density = 120.5 lbs/ft$^3$
10.35 Cells with less than 15% reagent
The above weights and volumes were provided by WRScompass and are based on a water/slag density of 100 lbs/cf and a water/slag/cement density of 109 lbs/cf

**Table 4.4**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Auger-ISS Tracking Log**

| Date | Column ID | # Full Mixing Passes | Column Elevations | | Column Dimensions | | | Water Added | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | Top (FT) | Bottom (FT) | Diameter (FT) | Length (FT) | # Overlaps | (GAL) | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| **3/30/09** | M10 | 4 | 181.73 | 161.40 | 9 | 20.33 | 0 | 3,074 | 25,569 | 9,846 | 35,415 | 22.72 | **Test column** |
| **3/31/09** | N15 | 4 | 183.18 | 160.24 | 9 | 22.93 | 1 | 3,011 | 25,058 | 8,340 | 33,398 | 20.38 | **Test column.** Test core indicates column is approx 10 feet short of bedrock. |
| " | N14 | 4 | 183.18 | 156.79 | 9 | 26.39 | 2 | 2,429 | 20,120 | 6,881 | 27,001 | 15.44 | **Test column** |
| **4/2/09** | N5 | 4 | 182.04 | 139.70 | 9 | 42.34 | 0 | 4,807 | 39,825 | 14,375 | 54,200 | 16.70 | |
| " | N6 | | 182.04 | 149.87 | 9 | 32.17 | 1 | 4,208 | 35,196 | 11,892 | 47,088 | 20.00 | Could not drill to refusal due to auger "walking" |
| **4/3/09** | N7 | 2 | 182.04 | 145.10 | 9 | 36.94 | 1 | 4,257 | 34,930 | 13,546 | 48,476 | 18.37 | Incomplete due to only 2 auger passes |
| **4/7/09** | M3 | 4 | 181.12 | 146.84 | 8 | 34.28 | 0 | 3,006 | 25,272 | 8,342 | 33,614 | 16.19 | **Began use of scale to weigh freagents at batch plant** |
| " | N6 Remix (P7) | - | 184.34 | 176.21 | 8 | 8.13 | 0 | 2,405 | 20,044 | 6,696 | 26,740 | 54.30 | Contractor attempted N-6 (aka P-7) again on 4/7 with an 8' diameter auger, but stopped although progress was slowly being made (4' in 47 mins.). |
| **4/8/09** | L3 | 4 | 181.35 | 147.62 | 8 | 33.73 | 1 | 3,016 | 25,069 | 9,268 | 34,337 | 18.03 | |
| " | N3 | 4 | 181.96 | 145.50 | 8 | 36.46 | 1 | 3,611 | 29,984 | 10,140 | 40,124 | 19.46 | |
| " | L2 | 4 | 182.23 | 146.28 | 8 | 35.95 | 2 | 3,611 | 29,994 | 10,308 | 40,302 | 21.42 | |
| **4/9/09** | K2 | 6 | 182.50 | 148.59 | 8 | 33.91 | 2 | 2,720 | 22,708 | 7,588 | 30,296 | 17.06 | |
| " | J2 | 6 | 181.22 | 150.04 | 8 | 31.18 | 1 | 3,018 | 25,114 | 8,599 | 33,713 | 19.15 | |
| " | J3 | 4 | 182.20 | 150.83 | 8 | 31.37 | 2 | 2,405 | 20,094 | 6,976 | 27,070 | 16.48 | |
| " | I2 | 6 | 181.95 | 152.73 | 8 | 29.22 | 2 | 2,409 | 20,110 | 6,784 | 26,894 | 17.57 | |
| " | I1 | 4 | 181.82 | 148.39 | 8 | 33.43 | 2 | 2,715 | 22,670 | 7,990 | 30,660 | 17.51 | |
| **4/10/09** | N2 | 4 | 183.91 | 141.76 | 8 | 42.15 | 1 | 3,908 | 32,774 | 11,096 | 43,870 | 18.44 | |
| " | M2 | - | 183.92 | 157.32 | 8 | 26.60 | 4 | 3,026 | 20,084 | 6,768 | 26,852 | 22.83 | Bent Kelly bar during installation. Incomplete. |
| **4/16/09** | 7h1 | 6 | 179.95 | 152.30 | 7 | 27.65 | 0 | 2,105 | 16,744 | 5,576 | 22,320 | 17.40 | |
| " | 7n1 | 4 | 184.78 | 142.81 | 7 | 41.97 | 0 | 3,617 | 28,070 | 10,119 | 38,189 | 19.62 | Auger advanced slowly @ 15' & 25' |
| " | 7m1 | - | 184.00 | 146.17 | 7 | 37.83 | 1 | 3,010 | 23,076 | 7,727 | 30,803 | 18.84 | Auger advanced slowly @ 15' |
| **4/17/09** | 7m1 (north) | 4 | 185.80 | 181.39 | 7 | 4.41 | 2 | 1,200 | NA | NA | NA | NA | Batch plant log unavailable |
| **4/22/09** | 7003 | 6 | 184.86 | 161.76 | 7 | 23.10 | 0 | 1,813 | 14,954 | 5,116 | 20,070 | 18.74 | |
| " | 7004 | 6 | 184.62 | 163.65 | 7 | 20.97 | 1 | 1,514 | 12,180 | 4,054 | 16,234 | 17.92 | |
| " | 7009 | 4 | 183.88 | 165.19 | 7 | 18.69 | 1 | 1,504 | 10,018 | 3,398 | 13,416 | 16.61 | |
| " | 7010 | 4 | 182.00 | 166.98 | 7 | 15.02 | 1 | 1,205 | 9,400 | 3,194 | 12,594 | 19.40 | |
| " | 7002 | | | | | | | | | | | | Could not drill column between brick foundation and test columns. |
| " | 7011 | 4 | 183.28 | 164.00 | 7 | 19.28 | 2 | 1,505 | 11,494 | 3,970 | 15,464 | 20.01 | |
| " | 7008 | 4 | 184.00 | 163.82 | 7 | 20.18 | 3 | 1,208 | 7,968 | 2,554 | 10,522 | 14.11 | |
| **4/23/09** | 7021 | - | 183.23 | 173.69 | 7 | 9.54 | 1 | 1,201 | 9,460 | 3,154 | 12,614 | 30.60 | Hit wood debris which caused refusal. Column not drilled to full depth. Column relocated |
| " | 7P10 | 4 | 181.33 | 162.87 | 7 | 18.46 | 1 | 1,502 | 11,942 | 3,960 | 15,902 | 19.94 | Column relocated |
| " | 7O11 | 6 | 181.54 | 163.26 | 7 | 18.28 | 1 | 901 | 9,154 | 3,058 | 12,212 | 15.46 | |
| " | 7N12 | 6 | 181.43 | 167.02 | 7 | 14.41 | 2 | 901 | 6,805 | 2,320 | 9,125 | 15.80 | Hit wood debris which caused refusal. Column not drilled to full depth. |
| " | 7M11 | 4 | 181.51 | 164.85 | 7 | 16.66 | 1 | 1,203 | 8,913 | 3,084 | 11,997 | 16.66 | |
| " | 7L10 | 4 | 181.62 | 163.27 | 7 | 18.35 | 1 | 8,380 | 8,380 | 2,858 | 11,238 | 14.17 | |
| " | 7N11 | 4 | 181.61 | 162.77 | 7 | 18.84 | 3 | 1,211 | 7,670 | 2,550 | 10,220 | 14.68 | |
| " | 7o10 | 4 | 181.87 | 160.90 | 7 | 20.97 | 3 | 1,208 | 9,170 | 3,110 | 12,280 | 15.85 | |
| " | 7M10 | 4 | 182.22 | 162.00 | 7 | 20.22 | 3 | 1,204 | 9,210 | 3,070 | 12,280 | 16.44 | |

**Table 4.4**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Auger-ISS Tracking Log**

| Date | Column ID | # Full Mixing Passes | Column Elevations | | Column Dimensions | | | Water Added | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | Top (FT) | Bottom (FT) | Diameter (FT) | Length (FT) | # Overlaps | (GAL) | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| **4/24/09** | 7u17 | 4 | 189.30 | 154.35 | 7 | 34.95 | 0 | 3,003 | 24,895 | 8,210 | 33,105 | 20.43 | Column relocated |
| " | 7k9 | 6 | 182.65 | 162.81 | 7 | 19.84 | 1 | 1,201 | 9,930 | 3,412 | 13,342 | 15.56 | |
| " | 7L9 | 4 | 182.60 | 160.87 | 7 | 21.73 | 3 | 1,202 | 8,366 | 2,810 | 11,176 | 13.92 | |
| " | 7m9 | 4 | 183.26 | 160.01 | 7 | 23.25 | 2 | 1,200 | 9,999 | 3,340 | 13,339 | 14.31 | |
| " | 7n10 | 4 | 182.34 | 161.10 | 7 | 21.24 | 4 | 1,208 | 7,738 | 2,594 | 10,332 | 14.39 | |
| " | 7o9 | 4 | 182.37 | 158.16 | 7 | 24.21 | 2 | 1,207 | 9,190 | 3,040 | 12,230 | 12.60 | |
| " | 7p9 | 4 | 182.93 | 156.93 | 7 | 26.00 | 1 | 1,517 | 12,314 | 4,037 | 16,351 | 14.55 | Column relocated |
| " | 7q8 | 4 | 182.04 | 155.90 | 7 | 26.14 | 1 | 1,509 | 12,425 | 4,130 | 16,555 | 14.66 | |
| " | 7k8 | 4 | 182.07 | 159.65 | 7 | 22.42 | 2 | 1,202 | 10,440 | 3,624 | 14,064 | 15.65 | |
| **4/27/09** | 7o9 (remix) | 4 | 183.30 | 162.03 | 7 | 21.27 | 2 | 6,022 | 50,726 | 17,450 | 68,176 | 79.98 | |
| **4/28/09** | 7L9 (Remix) | 6 | 184.29 | 168.74 | 7 | 15.55 | 5 | 3,018 | 19,271 | 6,536 | 25,807 | 54.10 | 7.87 feet short of original depth |
| " | 7k7 | 4 | 184.41 | 158.55 | 7 | 25.86 | 1 | 2,404 | 16,145 | 5,426 | 21,571 | 19.30 | |
| " | 7L8 | - | 184.67 | 158.92 | 7 | 25.75 | 4 | 1,202 | 10,090 | 3,928 | 14,018 | 16.10 | Stopped due to movement of Kelley bar. |
| " | 7m8 | 4 | 184.93 | NA | 7 | NA | 2 | 1,501 | 10,705 | 3,569 | 14,274 | NA | Stopped due to obstruction |
| " | 7p8 | 4 | 184.85 | 155.01 | 7 | 29.84 | 0 | 2,714 | 19,588 | 6,490 | 26,078 | 18.85 | |
| **4/29/09** | 7L8 (Remix) | 4 | 184.67 | 159.02 | 7 | 25.65 | 5 | 2,102 | 17,922 | 6,058 | 23,980 | 30.47 | Stopped due to movement of Kelley bar. |
| " | 7m8 (Remix) | 4 | 184.53 | 157.97 | 7 | 26.56 | 2 | 2,418 | 16,600 | 5,597 | 22,197 | 20.85 | Stopped due to movement of Kelley bar. |
| **4/30/09** | 7L7 | 4 | 185.36 | 158.02 | 7 | 27.34 | 3 | 2,406 | 18,050 | 6,108 | 24,158 | 23.92 | |
| **5/12/09** | 6U14 | 4 | 182.48 | 153.55 | 6 | 28.93 | 0 | 1,803 | 12,856 | 4,295 | 17,151 | 17.40 | |
| " | 6V23 | 4 | 183.76 | 153.90 | 6 | 29.86 | 1 | 1,800 | 15,690 | 5,270 | 20,960 | 22.11 | |
| " | 6T13 | 4 | 183.63 | 151.98 | 6 | 31.65 | 0 | 2,401 | 21,280 | 7,343 | 28,623 | 26.55 | |
| **5/29/09** | 4q16 | 4 | 185.47 | 161.89 | 4 | 23.58 | 0 | 2,421 | 8,102 | 3,185 | 11,287 | 31.60 | Stopped due to movement of Kelly bar. |
| " | 4ai11 | 4 | 184.70 | 138.54 | 4 | 46.16 | 0 | 2,416 | 17,904 | 6,074 | 23,978 | 34.29 | |
| " | 4aj19 | 4 | 189.04 | 146.12 | 4 | 42.92 | 0 | 2,407 | 14,683 | 5,696 | 20,379 | 31.35 | |
| " | 4o2 | 4 | 185.16 | 152.53 | 4 | 32.63 | 0 | 1,809 | 11,705 | 3,847 | 15,552 | 31.47 | |
| **5/30/09** | 4b11 | 4 | 185.87 | 154.97 | 4 | 30.90 | 0 | 2,414 | 12,958 | 4,129 | 17,087 | 36.51 | |
| **6/1/09** | 8test-1 | 4 | 186.24 | 155.47 | 8 | 30.77 | 0 | 3,019 | 21,359 | 7,471 | 28,830 | 15.47 | |
| " | 8test-2 | 4 | 185.99 | 156.65 | 8 | 29.34 | 0 | 3,016 | 21,526 | 7,320 | 28,846 | 16.23 | |
| " | 8test-3 | 4 | 185.93 | 151.58 | 8 | 34.35 | 0 | 3,615 | 28,425 | 10,170 | 38,595 | 18.55 | |
| **6/2/09** | 8test-4 | 4 | 186.80 | 150.94 | 8 | 35.86 | 0 | 3,912 | 30,137 | 9,927 | 40,064 | 18.44 | Stopped due to movement of Kelly bar. |
| " | 8a2 | 4 | 183.60 | 151.28 | 8 | 32.32 | 0 | 3,011 | 22,093 | 7,655 | 29,748 | 15.19 | |
| " | 8a3 | 4 | 182.84 | 150.75 | 8 | 32.09 | 1 | 3,003 | 22,163 | 7,614 | 29,777 | 16.44 | |
| " | 8b1 | 4 | 182.77 | 154.35 | 8 | 28.42 | 1 | 3,009 | 20,392 | 7,030 | 27,422 | 17.10 | |
| " | 8e1 | 4 | 182.52 | 158.55 | 8 | 23.97 | 1 | 2,439 | 19,040 | 6,214 | 25,254 | 18.67 | |
| **6/3/09** | 8d1 | 4 | 180.64 | 159.81 | 8 | 20.83 | 1 | 1,804 | 15,690 | 5,250 | 20,940 | 17.81 | |
| " | 8c2 | 4 | 181.03 | 165.93 | 8 | 15.10 | 2 | 1,205 | 9,066 | 3,050 | 12,116 | 15.33 | |
| **6/15/09** | 8a5 | 4 | 185.16 | 160.62 | 8 | 24.54 | 0 | 2,104 | 17,437 | 5,870 | 23,307 | 15.68 | |

**Table 4.4**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Auger-ISS Tracking Log**

| Date | Column ID | # Full Mixing Passes | Column Elevations | | Column Dimensions | | | Water Added | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | Top (FT) | Bottom (FT) | Diameter (FT) | Length (FT) | # Overlaps | (GAL) | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| **6/19/09** | 8b3 | 4 | 183.35 | 156.49 | 8 | 26.86 | 0 | 2,704 | 19,835 | 6,200 | 26,035 | 16.00 | |
| " | 8b4 | 4 | 183.69 | 154.42 | 8 | 29.27 | 1 | 2,701 | 19,540 | 6,781 | 26,321 | 15.93 | |
| " | 8b5 | 4 | 184.08 | 157.07 | 8 | 27.01 | 1 | 2,401 | 18,957 | 6,458 | 25,415 | 16.67 | |
| " | 8b6 | 4 | 184.12 | 157.14 | 8 | 26.98 | 1 | 2,403 | 17,240 | 5,805 | 23,045 | 15.13 | |
| " | 8b7 | 4 | 184.89 | 159.14 | 8 | 25.75 | 1 | 2,403 | 17,260 | 5,750 | 23,010 | 15.83 | |
| " | 8c3 | 4 | 184.51 | 156.71 | 8 | 27.80 | 1 | 2,702 | 19,389 | 6,497 | 25,886 | 16.50 | |
| " | 8d2 | 4 | 184.34 | 161.20 | 8 | 23.14 | 1 | 2,103 | 15,504 | 5,324 | 20,828 | 15.95 | |
| **7/6/09** | 8c4 | 4 | 182.91 | 156.20 | 8 | 26.71 | 0 | 2,707 | 19,665 | 6,700 | 26,365 | 16.30 | |
| " | 8c5 | 4 | 183.74 | 157.46 | 8 | 26.28 | 1 | 2,400 | 17,520 | 5,965 | 23,485 | 15.83 | |
| " | 8c6 | 4 | 184.27 | 158.53 | 8 | 25.74 | 1 | 2,405 | 17,276 | 5,714 | 22,990 | 15.82 | |
| " | 8c7 | 4 | 184.86 | 157.69 | 8 | 27.17 | 1 | 2,404 | 17,165 | 5,790 | 22,955 | 14.97 | |
| " | 8e2 | 4 | 182.67 | 162.87 | 8 | 19.80 | 0 | 1,803 | 13,749 | 4,600 | 18,349 | 15.30 | |
| " | 8f1 | 4 | 183.11 | 163.10 | 8 | 20.01 | 1 | 1,805 | 12,800 | 4,270 | 17,070 | 15.11 | |
| " | 8d4 | 4 | 183.64 | 154.70 | 8 | 28.94 | 2 | 2,403 | 18,198 | 6,110 | 24,308 | 16.05 | |
| " | 8d5 | 4 | 184.36 | 158.16 | 8 | 26.20 | 3 | 2,405 | 21,009 | 7,105 | 28,114 | 22.23 | |
| **7/7/09** | 8d6 | 4 | 183.32 | 157.75 | 8 | 25.57 | 3 | 1,801 | 15,750 | 5,340 | 21,090 | 17.09 | |
| " | 8d7 | 4 | 185.25 | 158.41 | 8 | 26.84 | 2 | 1,803 | 15,940 | 5,411 | 21,351 | 15.20 | |
| " | 8e3 | 4 | 182.43 | 162.45 | 8 | 19.98 | 1 | 1,805 | 12,800 | 4,260 | 17,060 | 15.13 | |
| " | 8f2 | 4 | 183.00 | 161.68 | 8 | 21.32 | 3 | 1,201 | 11,610 | 3,885 | 15,495 | 15.06 | |
| " | 8e4 | 4 | 183.26 | 152.40 | 8 | 30.86 | 2 | 2,401 | 18,267 | 6,096 | 24,363 | 15.08 | |
| " | 8e5 | 4 | 183.89 | 157.57 | 8 | 26.32 | 3 | 1,805 | 15,795 | 5,280 | 21,075 | 16.59 | |
| " | 8e6 | 4 | 184.20 | 157.24 | 8 | 26.96 | 3 | 1,805 | 14,670 | 4,888 | 19,558 | 15.03 | |
| " | 8e7 | 4 | 184.79 | 157.23 | 8 | 27.56 | 3 | 1,803 | 15,195 | 5,250 | 20,445 | 15.37 | |
| **7/8/09** | 8f3 | 4 | 182.90 | 151.38 | 8 | 31.52 | 3 | 2,403 | 17,208 | 5,730 | 22,938 | 15.08 | |
| " | 8f4 | 4 | 183.72 | 153.03 | 8 | 30.69 | 3 | 2,401 | 17,329 | 5,910 | 23,239 | 15.69 | |
| " | 8f5 | 4 | 184.73 | 157.93 | 8 | 26.80 | 3 | 2,102 | 15,035 | 5,070 | 20,105 | 15.54 | |
| " | 8f6 | 4 | 184.89 | 156.95 | 8 | 27.94 | 3 | 1,801 | 15,214 | 5,085 | 20,299 | 15.05 | |
| " | 8f7 | 4 | 184.96 | 157.68 | 8 | 27.28 | 2 | 2,101 | 16,275 | 6,160 | 22,435 | 15.71 | |
| " | 8g1 | 4 | 184.69 | 151.48 | 8 | 33.21 | 2 | 2,411 | 19,571 | 6,530 | 26,101 | 15.01 | |
| " | 8g2 | 4 | 185.01 | 155.09 | 8 | 29.92 | 3 | 2,406 | 18,040 | 6,100 | 24,140 | 16.72 | |
| " | 8g3 | 4 | 185.00 | 154.39 | 8 | 30.61 | 3 | 2,403 | 17,450 | 5,923 | 23,373 | 15.82 | |
| **7/9/09** | 8f8 | 4 | 183.23 | 160.37 | 8 | 22.86 | 1 | 2,109 | 16,345 | 5,427 | 21,772 | 16.87 | |
| " | 8g4 | 4 | 185.04 | 156.39 | 8 | 28.65 | 3 | 2,401 | 17,585 | 6,282 | 23,867 | 17.26 | |
| " | 8g5 | 4 | 183.07 | 158.06 | 8 | 25.01 | 3 | 1,805 | 13,819 | 4,700 | 18,519 | 15.34 | |
| " | 8g6 | 4 | 183.59 | 158.45 | 8 | 25.14 | 3 | 1,802 | 15,035 | 5,290 | 20,325 | 16.75 | |
| " | 8h2 | 4 | 183.93 | 150.84 | 8 | 33.09 | 2 | 2,408 | 19,504 | 6,646 | 26,150 | 15.10 | |
| " | 8h3 | 4 | 185.50 | 152.83 | 8 | 32.67 | 3 | 2,405 | 18,032 | 6,174 | 24,206 | 15.35 | |
| " | 8h4 | 4 | 184.79 | 157.11 | 8 | 27.68 | 3 | 2,106 | 18,510 | 5,517 | 24,027 | 17.99 | |

**Table 4.4**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Auger-ISS Tracking Log**

| Date | Column ID | # Full Mixing Passes | Column Elevations | | Column Dimensions | | | Water Added | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | Top (FT) | Bottom (FT) | Diameter (FT) | Length (FT) | # Overlaps | (GAL) | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| **7/10/09** | 8h5 | 4 | 183.46 | 155.83 | 8 | 27.63 | 3 | 2,103 | 16,250 | 5,704 | 21,954 | 16.46 | |
| " | 8h6 | 4 | 184.37 | 157.17 | 8 | 27.20 | 3 | 2,104 | 16,285 | 5,625 | 21,910 | 16.69 | |
| " | 8i6 | 4 | 184.74 | 154.02 | 8 | 30.72 | 2 | 2,406 | 18,600 | 6,305 | 24,905 | 15.49 | |
| " | 8i4 | 4 | 184.84 | 152.23 | 8 | 32.61 | 1 | 3,006 | 21,431 | 7,379 | 28,810 | 15.65 | |
| " | 8i5 | 4 | 184.61 | 151.56 | 8 | 33.05 | 4 | 2,401 | 16,870 | 6,045 | 22,915 | 15.70 | |
| " | 8i7 | 4 | 184.86 | 155.19 | 8 | 29.67 | 3 | 2,404 | 18,178 | 6,333 | 24,511 | 17.12 | |
| " | 8i8 | 4 | 185.07 | 156.09 | 8 | 28.98 | 3 | 2,103 | 16,104 | 5,459 | 21,563 | 15.42 | |
| **7/11/09** | 8a9 | 4 | 185.10 | 170.52 | 8 | 14.58 | 1 | 1,200 | 10,520 | 3,712 | 14,232 | 17.29 | |
| " | 8b8 | 4 | 185.65 | 162.91 | 8 | 22.74 | 1 | 1,802 | 16,030 | 5,525 | 21,555 | 16.79 | |
| " | 8b9 | 4 | 185.10 | 164.40 | 8 | 20.70 | 3 | 1,801 | 13,005 | 4,800 | 17,805 | 17.82 | |
| " | 8a6 | 4 | 185.04 | 163.52 | 8 | 21.52 | 0 | 1,801 | 15,220 | 5,190 | 20,410 | 15.66 | |
| " | 8a7 | 4 | 185.60 | 165.27 | 8 | 20.33 | 1 | 1,805 | 14,550 | 5,165 | 19,715 | 17.18 | |
| " | 8a8 | 4 | 185.36 | 169.41 | 8 | 15.95 | 1 | 1,802 | 13,985 | 4,735 | 18,720 | 20.79 | |
| **7/13/09** | 8b10 | 4 | 182.66 | 167.30 | 8 | 15.36 | 3 | 1,801 | 12,310 | 4,935 | 17,245 | 23.26 | |
| " | 8b11 | 4 | 183.52 | 169.72 | 8 | 13.80 | 3 | 1,200 | 9,960 | 3,369 | 13,329 | 20.01 | |
| " | 8c9 | 4 | 183.56 | 163.12 | 8 | 20.44 | 0 | 2,402 | 17,871 | 5,699 | 23,570 | 19.04 | |
| " | 8c10 | 4 | 184.45 | 165.25 | 8 | 19.20 | 3 | 1,800 | 11,673 | 3,915 | 15,588 | 16.82 | |
| " | 8c11 | 4 | 184.60 | 167.50 | 8 | 17.10 | 3 | 1,200 | 11,210 | 3,890 | 15,100 | 18.30 | |
| " | 8c12 | 4 | 184.68 | 171.79 | 8 | 12.89 | 2 | 1,200 | 9,965 | 3,365 | 13,330 | 19.76 | |
| " | 8d8 | 4 | 184.80 | 163.42 | 8 | 21.38 | 1 | 1,801 | 15,842 | 5,498 | 21,340 | 17.68 | |
| " | 8d9 | 4 | 185.24 | 163.62 | 8 | 21.62 | 3 | 1,500 | 11,826 | 4,140 | 15,966 | 15.30 | |
| " | 8d10 | 4 | 185.48 | 165.50 | 8 | 19.98 | 3 | 1,501 | 11,901 | 4,220 | 16,121 | 16.72 | |
| " | 8d11 | 4 | 185.51 | 167.16 | 8 | 18.35 | 3 | 1,201 | 10,980 | 4,028 | 15,008 | 16.95 | |
| **7/14/09** | 8e9 | 4 | 182.29 | 162.71 | 8 | 19.58 | 2 | 1,801 | 13,250 | 4,614 | 17,864 | 17.43 | |
| " | 8e10 | 4 | 182.77 | 164.09 | 8 | 18.68 | 3 | 1,200 | 10,705 | 3,650 | 14,355 | 15.92 | |
| " | 8e11 | 4 | 183.04 | 165.87 | 8 | 17.17 | 3 | 1,200 | 11,030 | 3,795 | 14,825 | 17.89 | |
| " | 8f9 | 4 | 184.00 | 163.09 | 8 | 20.91 | 2 | 1,801 | 17,115 | 6,227 | 23,342 | 21.33 | |
| " | 8f10 | 4 | 184.13 | 164.24 | 8 | 19.89 | 3 | 1,501 | 11,526 | 3,991 | 15,517 | 16.17 | |
| **7/16/09** | 8q3 | 4 | 186.24 | 135.52 | 8 | 50.72 | 0 | 7,209 | 52,405 | 18,070 | 70,475 | 22.94 | |
| " | 8p3 | 4 | 186.44 | 135.23 | 8 | 51.21 | 1 | 6,008 | 46,781 | 16,102 | 62,883 | 21.76 | |
| " | 8p4 | 4 | 186.76 | 135.52 | 8 | 51.24 | 1 | 5,409 | 43,328 | 15,106 | 58,434 | 20.20 | |
| **7/17/09** | 8q10 | 4 | 185.52 | 149.06 | 8 | 36.46 | 0 | 5,407 | 41,719 | 14,406 | 56,125 | 25.41 | |
| " | 8p5 | | | | | | | | | | | | early refusal, bottom elevation was not surveyed |
| " | 8q8 | 4 | 184.53 | 144.78 | 8 | 39.75 | 0 | 5,404 | 43,118 | 14,646 | 57,764 | 23.99 | |
| " | 8q7 | 4 | 185.89 | 144.73 | 8 | 41.16 | 0 | 4,205 | 30,244 | 10,857 | 41,101 | 17.69 | |
| **7/18/09** | 8p10 | 4 | 185.90 | 156.34 | 8 | 29.56 | 0 | 2,701 | 21,266 | 7,406 | 28,672 | 16.01 | |
| | 8p9 | 4 | 184.18 | 149.04 | 8 | 35.14 | 1 | 3,303 | 24,627 | 9,492 | 34,119 | 17.20 | |
| | 8p8 | 4 | 182.47 | 148.17 | 8 | 34.30 | 2 | 3,904 | 30,158 | 10,526 | 40,684 | 22.66 | |

**Table 4.4**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Auger-ISS Tracking Log**

| Date | Column ID | # Full Mixing Passes | Column Elevations | | Column Dimensions | | | Water Added | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | Top (FT) | Bottom (FT) | Diameter (FT) | Length (FT) | # Overlaps | (GAL) | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| **7/21/09** | 8p7 | 4 | 182.59 | 148.18 | 8 | 34.41 | 2 | 3,604 | 29,013 | 9,717 | 38,730 | 21.50 | |
| " | 8p6 | 4 | 182.83 | 158.38 | 8 | 24.45 | 1 | 2,402 | 17,951 | 6,331 | 24,282 | 17.60 | |
| " | 8o8 | 4 | 182.95 | 150.43 | 8 | 32.52 | 2 | 3,003 | 23,200 | 8,072 | 31,272 | 18.37 | |
| " | 8o7 | 4 | 183.75 | 148.52 | 8 | 35.23 | 3 | 2,401 | 20,737 | 6,964 | 27,701 | 16.29 | |
| " | 8o6 | 4 | 183.90 | 148.07 | 8 | 35.83 | 3 | 2,701 | 21,477 | 7,513 | 28,990 | 16.77 | |
| **7/22/09** | 8o5 | 4 | 180.19 | 149.33 | 8 | 30.86 | 2 | 2,401 | 18,481 | 6,331 | 24,812 | 15.36 | |
| " | 8n6 | 4 | 181.92 | 164.28 | 8 | 17.64 | 2 | 3,603 | 27,685 | 9,424 | 37,109 | 40.19 | |
| " | 8n5 | 4 | 181.92 | 149.26 | 8 | 32.66 | 3 | 2,701 | 20,231 | 7,167 | 27,398 | 17.38 | |
| " | 8n4 | 4 | 184.01 | 152.46 | 8 | 31.55 | 3 | 2,402 | 17,879 | 6,345 | 24,224 | 15.91 | |
| " | 8n3 | 4 | 183.20 | 149.87 | 8 | 33.33 | 3 | 2,701 | 19,450 | 6,949 | 26,399 | 16.41 | |
| " | 8n2 | 4 | 183.57 | 148.94 | 8 | 34.63 | 3 | 2,703 | 19,579 | 6,882 | 26,461 | 15.83 | |
| **7/23/09** | 8n6 | 4 | 181.92 | 164.39 | 8 | 17.53 | 2 | 3,603 | 27,685 | 9,424 | 37,109 | 40.44 | Started on 7/22. Completed on 7/23 |
| " | 8m6 | 4 | 183.24 | 153.85 | 8 | 29.39 | 1 | 2,403 | 18,849 | 6,295 | 25,144 | 15.16 | |
| " | 8m5 | 4 | 182.98 | 155.72 | 8 | 27.26 | 3 | 3,001 | 20,537 | 7,010 | 27,547 | 20.94 | |
| " | 8m4 | 4 | 183.48 | 150.77 | 8 | 32.71 | 3 | 3,004 | 20,725 | 7,204 | 27,929 | 17.69 | |
| " | 8m3 | 4 | 183.53 | 149.85 | 8 | 33.68 | 3 | 2,704 | 18,599 | 6,478 | 25,077 | 15.43 | |
| " | 8m2 | 4 | 183.70 | 150.93 | 8 | 32.77 | 3 | 2,701 | 21,342 | 7,381 | 28,723 | 18.16 | |
| **7/24/09** | 8m1 | 4 | 183.93 | 150.62 | 8 | 33.31 | 2 | 2,701 | 20,773 | 7,030 | 27,803 | 15.95 | |
| " | 8L6 | 4 | 180.22 | 156.58 | 8 | 23.64 | 0 | 2,101 | 16,385 | 5,885 | 22,270 | 15.55 | |
| " | 8L5 | 4 | 182.07 | 157.71 | 8 | 24.36 | 2 | 2,402 | 17,843 | 6,191 | 24,034 | 18.85 | |
| " | 8L4 | 4 | 183.32 | 156.77 | 8 | 26.55 | 3 | 2,401 | 18,217 | 6,188 | 24,405 | 19.05 | |
| " | 8L3 | 4 | 184.00 | 152.19 | 8 | 31.81 | 3 | 2,404 | 18,260 | 6,482 | 24,742 | 16.12 | |
| " | 8L2 | 4 | 184.38 | 151.18 | 8 | 33.20 | 3 | 2,403 | 18,060 | 6,100 | 24,160 | 15.08 | |
| **7/25/09** | 8L1 | 4 | 184.48 | 150.41 | 8 | 34.07 | 3 | 2,701 | 18,588 | 6,385 | 24,973 | 15.19 | |
| " | 8K5 | 4 | 182.86 | 157.55 | 8 | 25.31 | 2 | 2,402 | 17,813 | 6,118 | 23,931 | 18.06 | |
| " | 8K4 | 4 | 183.55 | 153.90 | 8 | 29.65 | 3 | 2,401 | 18,236 | 6,275 | 24,511 | 17.13 | |
| " | 8K3 | 4 | 184.04 | 151.72 | 8 | 32.32 | 3 | 2,703 | 18,878 | 6,455 | 25,333 | 16.24 | |
| " | 8K2 | 4 | 184.76 | 151.67 | 8 | 33.09 | 3 | 2,700 | 18,863 | 6,765 | 25,628 | 16.05 | |
| **7/27/09** | 8K1 | 4 | 186.16 | 151.77 | 8 | 34.39 | 2 | 3,600 | 27,744 | 9,353 | 37,097 | 20.61 | |
| " | 8J7 | 4 | 185.10 | 162.21 | 8 | 22.89 | 2 | 1,801 | 13,610 | 4,745 | 18,355 | 15.32 | |
| " | 8J6 | 4 | 183.56 | 160.96 | 8 | 22.60 | 3 | 2,401 | 18,262 | 6,350 | 24,612 | 22.57 | |
| " | 8J5 | 4 | 183.93 | 162.42 | 8 | 21.51 | 3 | 2,401 | 16,935 | 5,758 | 22,693 | 21.86 | |
| " | 8J4 | 4 | 184.42 | 154.54 | 8 | 29.88 | 3 | 2,403 | 16,950 | 5,781 | 22,731 | 15.76 | |
| " | 8J3 | 4 | 184.55 | 154.59 | 8 | 29.96 | 2 | 3,304 | 25,656 | 8,715 | 34,371 | 21.92 | |
| **7/28/09** | 8x1 | 4 | 181.80 | 166.16 | 8 | 15.64 | 0 | 1,801 | 12,991 | 4,320 | 17,311 | 18.27 | |
| " | 8x2 | 4 | 183.48 | 166.80 | 8 | 16.68 | 1 | 1,201 | 10,815 | 3,667 | 14,482 | 15.38 | |
| " | 8x4 | 4 | 184.35 | 167.57 | 8 | 16.78 | 1 | 1,500 | 11,606 | 4,072 | 15,678 | 16.55 | |
| " | 8x3 | 4 | 184.28 | 165.66 | 8 | 18.62 | 2 | 1,501 | 11,505 | 4,003 | 15,508 | 15.91 | |
| " | 8x5 | 4 | 184.55 | 165.79 | 8 | 18.76 | 2 | 1,201 | 11,380 | 3,755 | 15,135 | 15.41 | |

**Table 4.4**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Auger-ISS Tracking Log**

| Date | Column ID | # Full Mixing Passes | Column Elevations | | Column Dimensions | | | Water Added | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | Top (FT) | Bottom (FT) | Diameter (FT) | Length (FT) | # Overlaps | (GAL) | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| **7/29/09** | 4xy5 | 4 | 182.79 | 164.21 | 4 | 18.58 | 0 | 1,200 | 9,205 | 3,145 | 12,350 | 43.88 | |
| " | 4xy2 | 4 | 182.79 | 160.31 | 4 | 22.48 | 0 | 1,200 | 5,703 | 2,110 | 7,813 | 22.95 | |
| " | 4xy8 | 4 | 183.04 | 159.33 | 4 | 23.71 | 1 | 1,200 | 4,915 | 1,600 | 6,515 | 19.46 | |
| " | 4xy12 | 4 | 183.68 | 158.97 | 4 | 24.71 | 1 | 900 | 5,604 | 1,755 | 7,359 | 21.09 | |
| " | 4xy11 | 4 | 183.81 | 157.21 | 4 | 26.60 | 2 | 900 | 5,624 | 1,650 | 7,274 | 20.88 | |
| **7/30/09** | 4xx4 | 4 | 182.49 | 160.87 | 4 | 21.62 | 0 | 900 | 7,350 | 2,470 | 9,820 | 29.99 | |
| " | 4xx5 | 4 | 185.25 | 158.18 | 4 | 27.07 | 0 | 1,200 | 9,711 | 3,402 | 13,113 | 31.98 | |
| " | 4xx1 | 4 | 184.23 | 150.52 | 4 | 33.71 | 0 | 1,200 | 9,616 | 3,140 | 12,756 | 24.98 | |
| " | 4xx2 | 4 | 184.90 | 174.35 | 4 | 10.55 | 1 | 1,200 | 7,206 | 2,442 | 9,648 | 64.75 | |
| " | 4xz9 | 4 | 185.57 | 172.30 | 4 | 13.27 | 0 | 1,200 | 4,830 | 1,520 | 6,350 | 31.59 | |
| " | 4xz6 | 4 | 185.87 | 182.75 | 4 | 3.12 | 0 | 600 | 4,645 | 1,625 | 6,270 | 132.68 | early refusal |
| " | 4xz4 | 4 | 185.94 | 136.20 | 4 | 49.74 | 0 | 1,500 | 13,712 | 5,247 | 18,959 | 25.16 | |
| **7/31/09** | 4xz1 | 4 | 185.93 | 138.85 | 4 | 47.08 | 1 | 1,801 | 14,297 | 4,985 | 19,282 | 29.00 | |
| " | 4xz6 | 4 | | | 4 | NA | NA | NA | NA | NA | NA | NA | early refusal, bottom elevation was not surveyed |
| " | 4xz19 | 4 | 187.34 | 167.46 | 4 | 19.88 | 0 | 1,200 | 9,073 | 2,662 | 11,735 | 38.97 | |
| " | 4xz11 | 4 | 185.66 | 163.29 | 4 | 22.37 | 1 | 900 | 6,660 | 2,275 | 8,935 | 28.28 | |
| " | 4xy16 | 4 | 186.06 | 176.57 | 4 | 9.49 | 0 | 900 | 3,382 | 1,152 | 9,068 | 31.54 | |
| " | 4xz2 | 4 | 185.77 | 145.38 | 4 | 40.39 | 0 | 1,050 | 11,130 | 3,590 | 11,179 | 24.06 | |
| **8/3/09** | 4xy14 | 4 | 183.95 | 181.39 | 4 | 2.56 | 0 | 1,201 | 8,988 | 2,942 | 11,930 | 307.67 | early refusal, bottom elevation was not surveyed |
| " | 4xy13 | 4 | 179.45 | 152.64 | 4 | 26.81 | 0 | 1,500 | 11,039 | 3,720 | 14,759 | 36.34 | |
| " | 4xy7 | 4 | 182.94 | 173.11 | 4 | 9.83 | 0 | 300 | 2,123 | 742 | 2,865 | 19.24 | |
| " | 4xy10 | 4 | 183.92 | 175.91 | 4 | 8.01 | 2 | 600 | 4,180 | 1,410 | 5,590 | 53.28 | |
| " | 4xy6 | 4 | 183.72 | 172.57 | 4 | 11.15 | 0 | 300 | 2,215 | 715 | 2,930 | 17.35 | |
| " | 4xy1 | 4 | 183.59 | 178.29 | 4 | 5.30 | 0 | 300 | 2,215 | 715 | 2,930 | 36.50 | |
| " | 4xy15 | 4 | 185.02 | 157.32 | 4 | 27.70 | 0 | 1,500 | 11,501 | 4,116 | 15,617 | 37.22 | |
| **8/4/09** | 4xz13 | 4 | 186.38 | | 4 | NA | 0 | NA | NA | NA | NA | NA | early refusal, bottom elevation was not surveyed |
| " | 4xz12 | 4 | 187.40 | 181.76 | 4 | 5.64 | 0 | 900 | 6,691 | 2,088 | 8,779 | 102.76 | |
| " | 4xx3 | 4 | 183.39 | 180.59 | 4 | 2.80 | 0 | 900 | 6,751 | 2,252 | 9,003 | 212.28 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added (GAL) | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 6/26/09 | JG-Test-1 | | 161.26 | 153.26 | 4.9 | 8.00 | Full | 951.68 | 5,962 | 1,987 | 7,950 | 43.73 | **Test Column** |
| 6/27/09 | JG-Test-2 | | 183.23 | 153.23 | 4.9 | 30.00 | Full | 2562.21 | 16,052 | 5,351 | 21,403 | 33.70 | **Test Column** |
| 6/29/09 | JG-Test-3 | | 183.13 | 155.13 | 4.9 | 28.00 | Full | 2762.71 | 17,309 | 5,770 | 23,078 | 41.96 | **Test Column** |
| 6/30/09 | JG-Test-4 | | 142.43 | 129.31 | 4.9 | 13.12 | Full | 986.71 | 6,182 | 2,061 | 8,242 | 27.64 | **Test Column** |
| 7/1/09 | JG-Test-5 | | 183.60 | 133.60 | 4.9 | 50.00 | Full | 4369.95 | 27,378 | 9,126 | 36,504 | 34.48 | **Test Column** |
| 7/1/09 | JG-Test-6 | | 183.85 | 131.85 | 4.9 | 52.00 | Full | 4295.25 | 26,910 | 8,970 | 35,880 | 35.13 | **Test Column** |
| 8/21/09 | WO-11 | 139.89 | 177.19 | 139.90 | 4.9 | 37.29 | Full | 4392.36 | 27,518 | 9,173 | 36,691 | 43.30 | |
| 8/24/09 | WO-13 | 136.81 | 182.84 | 136.82 | 4.9 | 46.02 | Full | 7979.45 | 49,992 | 16,664 | 66,656 | 63.73 | |
| 8/25/09 | WO-14 | 141.32 | 183.30 | 141.32 | 4.9 | 41.98 | Full | 7174.19 | 44,947 | 14,982 | 59,929 | 67.43 | |
| 8/26/09 | WO-15 | 138.14 | 151.07 | 138.14 | 4.9 | 12.93 | Full | 1756.94 | 11,007 | 3,669 | 14,676 | 53.61 | |
| " | WO-16 | 135.88 | 145.68 | 135.88 | 4.9 | 9.80 | Full | 1244.50 | 7,797 | 2,599 | 10,396 | 50.10 | |
| " | WO-17 | 134.88 | 146.68 | 134.88 | 4.9 | 11.80 | Full | 1830.15 | 11,466 | 3,822 | 15,288 | 61.19 | |
| " | WO-18 | 133.44 | 186.95 | 186.95 | 4.9 | 0.00 | - | - | - | - | - | - | Grouting stopped early due to excessive spoils near rig. Completed on 8/27. |
| 8/27/09 | WO-19 | 134.61 | 183.91 | 134.61 | 4.9 | 49.30 | Full | 7979.45 | 49,992 | 16,664 | 66,656 | 63.86 | |
| " | WO-18 | 133.44 | 183.95 | 133.44 | 4.9 | 50.51 | Full | 8052.66 | 50,450 | 16,817 | 67,267 | 62.90 | Started grouting on 8/26. Completed grouting on 8/27. |
| 9/1/09 | WO-20 | 133.14 | 142.19 | 133.14 | 4.9 | 9.05 | Full | 1683.74 | 10,549 | 3,516 | 14,065 | 73.41 | |
| " | WO-11 | 139.89 | 182.41 | 139.90 | 4.9 | 42.51 | Full | 3587.09 | 22,473 | 7,491 | 29,964 | 31.02 | |
| " | WO-12 | 143.10 | 149.00 | 143.06 | 4.9 | 5.94 | Full | 951.68 | 5,962 | 1,987 | 7,950 | 68.14 | |
| " | WI-10 | 141.77 | 181.75 | 141.73 | 4.9 | 40.02 | Full | 3733.51 | 23,391 | 7,797 | 31,188 | 36.81 | |
| " | WI-11 | 143.21 | 155.53 | 143.16 | 4.9 | 12.37 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 57.32 | |
| " | WI-12 | 143.75 | 154.15 | 143.09 | 4.9 | 11.06 | Full | 1317.71 | 8,256 | 2,752 | 11,007 | 54.95 | |
| 9/2/09 | WI-13 | 140.58 | 154.48 | 143.68 | 4.9 | 10.80 | Full | 1390.91 | 8,714 | 2,905 | 11,619 | 59.40 | |
| " | WI-14 | 142.05 | 168.58 | 141.94 | 4.9 | 26.64 | Full | 2781.83 | 17,428 | 5,809 | 23,238 | 48.16 | |
| " | WI-15 | 137.95 | 151.20 | 137.88 | 4.9 | 13.32 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 53.23 | |
| 9/3/09 | WI-16 | 136.70 | 182.75 | 136.65 | 4.9 | 46.10 | Full | 4611.98 | 28,894 | 9,631 | 38,526 | 46.14 | |
| " | WI-17 | 134.70 | 162.97 | 134.62 | 4.9 | 28.35 | Full | 2708.62 | 16,970 | 5,657 | 22,626 | 44.07 | |
| " | WI-18 | 134.92 | 146.44 | 134.89 | 4.9 | 11.55 | Full | 1390.91 | 8,714 | 2,905 | 11,619 | 55.54 | |
| " | WI-19 | 132.60 | 145.17 | 132.60 | 4.9 | 12.57 | Full | 1464.12 | 9,173 | 3,058 | 12,230 | 53.72 | |
| " | WO-9 | 138.04 | 155.29 | 138.03 | 4.9 | 17.26 | Full | 1903.36 | 11,925 | 3,975 | 15,900 | 40.53 | |
| 9/4/09 | WO-10 | 138.86 | 156.39 | 138.80 | 4.9 | 17.59 | Full | 1976.56 | 12,383 | 4,128 | 16,511 | 47.79 | |
| " | WI-8 | 139.13 | 155.29 | 139.08 | 4.9 | 16.21 | Full | 1903.36 | 11,925 | 3,975 | 15,900 | 46.33 | |
| 9/5/09 | WI-9 | 139.29 | 183.24 | 139.28 | 4.9 | 43.96 | Full | 3953.12 | 24,767 | 8,256 | 33,022 | 41.48 | |
| " | Int-01 | 150.07 | 183.45 | 150.07 | 4.9 | 33.38 | Full | 3001.45 | 18,804 | 6,268 | 25,072 | 33.05 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added (GAL) | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 9/8/09 | Int-02 | 148.15 | 183.41 | 149.65 | 4.9 | 33.76 | Full | 3733.51 | 23,391 | 7,797 | 31,188 | 43.63 | |
| " | Int-03 | 142.51 | 183.32 | 141.85 | 4.9 | 41.47 | Full | 4026.33 | 25,225 | 8,408 | 33,634 | 35.69 | |
| " | Int-04 | 147.14 | 183.29 | 147.14 | 4.9 | 36.15 | Full | 3221.06 | 20,180 | 6,727 | 26,907 | 32.75 | |
| " | Int-07 | 148.53 | 183.17 | 147.87 | 4.9 | 35.30 | Full | 3221.06 | 20,180 | 6,727 | 26,907 | 33.54 | |
| 9/9/09 | WO-18A | 186.46 | 183.47 | 155.42 | 4.9 | 28.05 | Full | 2196.18 | 13,759 | 4,586 | 18,346 | 43.49 | |
| " | Int-5 | 144.71 | 183.08 | 144.67 | 4.9 | 38.41 | Full | 3294.27 | 20,639 | 6,880 | 27,518 | 31.52 | |
| " | Int-6 | 146.89 | 183.79 | 146.84 | 4.9 | 36.95 | Full | 3367.48 | 21,097 | 7,032 | 28,130 | 35.96 | |
| " | Int-8 | 186.37 | 183.45 | 150.61 | 4.9 | 32.84 | Full | 3733.51 | 23,391 | 7,797 | 31,188 | 41.79 | |
| " | Int-9 | 151.49 | 183.91 | 151.49 | 4.9 | 32.42 | Full | 3001.45 | 18,804 | 6,268 | 25,072 | 34.03 | |
| " | Int-11 | 141.37 | 183.58 | 141.36 | 4.9 | 42.22 | Full | 4392.36 | 27,518 | 9,173 | 36,691 | 38.24 | |
| 9/10/09 | WI-14A | 144.41 | 182.15 | 145.91 | 4.9 | 36.24 | Full | 4904.80 | 30,729 | 10,243 | 40,972 | 62.42 | |
| " | Int-39 | 141.27 | 183.22 | 142.77 | 4.9 | 40.45 | Full | 5490.45 | 34,398 | 11,466 | 45,864 | 68.43 | |
| " | WO-9A | 150.30 | 182.94 | 151.77 | 4.9 | 31.17 | Full | 2928.24 | 18,346 | 6,115 | 24,461 | 47.36 | |
| " | WO-10A | 151.61 | 182.16 | 151.91 | 4.9 | 30.25 | Full | 3147.86 | 19,722 | 6,574 | 26,295 | 57.80 | |
| 9/11/09 | WO-19A | 137.28 | 184.35 | 138.78 | 4.9 | 45.57 | Full | 5417.24 | 33,939 | 11,313 | 45,252 | 54.83 | |
| 9/12/09 | WO-29 | 130.70 | 187.72 | 130.70 | 4.9 | 57.02 | Full | 5929.69 | 37,150 | 12,383 | 49,533 | 38.22 | |
| " | WO-24 | 130.43 | 186.88 | 130.38 | 4.9 | 56.50 | Full | 5710.07 | 35,774 | 11,925 | 47,699 | 37.15 | |
| 9/14/09 | WO-22 | 130.27 | 182.54 | 132.03 | 4.9 | 50.51 | Full | 5417.24 | 33,939 | 11,313 | 45,252 | 39.42 | |
| " | WO-26 | 131.13 | 182.54 | 129.35 | 4.9 | 53.19 | Full | 6076.10 | 38,067 | 12,689 | 50,756 | 41.99 | Lost return at 7.53 bgs. WO-26 completed on 9/16. |
| 9/15/09 | WI-20 | 134.27 | 185.51 | 134.26 | 4.9 | 51.25 | Full | 7613.42 | 47,699 | 15,900 | 63,598 | 63.18 | |
| " | WO-21 | 133.57 | 185.42 | 133.54 | 4.9 | 51.88 | Full | 5417.24 | 33,939 | 11,313 | 45,252 | 48.16 | |
| " | WI-22 | 131.52 | 186.92 | 131.48 | 4.9 | 55.44 | Full | 5710.07 | 35,774 | 11,925 | 47,699 | 43.80 | |
| 9/16/09 | WO-25 | 130.12 | 187.16 | 130.15 | 4.9 | 57.01 | Full | 6002.89 | 37,608 | 12,536 | 50,145 | 44.78 | |
| " | WI-28 | 130.14 | 188.29 | 130.14 | 4.9 | 58.15 | Full | 6222.51 | 38,984 | 12,995 | 51,979 | 39.33 | |
| " | WO-26 | 132.04 | 182.54 | 132.03 | 4.9 | 50.51 | Full | 5417.24 | 33,939 | 11,313 | 45,252 | 54.07 | WO-26 started on 9/14. Completed on 9/16. |
| 9/17/09 | WI-29 | 130.56 | 188.04 | 130.54 | 4.9 | 57.50 | Full | 6002.89 | 37,608 | 12,536 | 50,145 | 41.19 | |
| 9/18/09 | WI-24 | 129.64 | 187.61 | 129.58 | 4.9 | 58.03 | Full | 6076.10 | 38,067 | 12,689 | 50,756 | 41.31 | |
| " | WO-23 | 128.45 | 185.99 | 128.44 | 4.9 | 57.55 | Full | 6954.57 | 43,571 | 14,524 | 58,094 | 55.74 | |
| " | WI-23 | 128.89 | 187.25 | 128.88 | 4.9 | 58.37 | Full | 6222.51 | 38,984 | 12,995 | 51,979 | 53.75 | |
| 9/19/09 | WI-27 | 130.11 | 187.98 | 130.11 | 4.9 | 57.87 | Full | 6368.92 | 39,902 | 13,301 | 53,202 | 46.81 | |
| " | WI-26 | 130.38 | 187.88 | 130.37 | 4.9 | 57.51 | Full | 6149.30 | 38,526 | 12,842 | 51,368 | 49.32 | |
| 9/21/09 | WO-27 | 129.63 | 187.46 | 129.62 | 4.9 | 57.84 | Full | 6076.10 | 38,067 | 12,689 | 50,756 | 48.45 | |
| " | WO-28 | 130.90 | 188.01 | 130.83 | 4.9 | 57.18 | Full | 4904.80 | 30,729 | 10,243 | 40,972 | 39.56 | |
| " | WO-30 | 128.43 | 188.23 | 129.93 | 4.9 | 58.30 | Full | 5783.27 | 36,233 | 12,078 | 48,310 | 50.01 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | (GAL) | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 9/22/09 | WI-25 | 130.39 | 187.74 | 130.39 | 4.9 | 57.35 | Full | 5856.48 | 36,691 | 12,230 | 48,922 | 51.48 | |
| " | Int-50 | 142.00 | 165.19 | 142.00 | 4.9 | 23.19 | Full | 3074.65 | 19,263 | 6,421 | 25,684 | 48.73 | |
| " | Int-49 | 143.30 | 156.65 | 143.30 | 4.9 | 13.35 | Full | 1830.15 | 11,466 | 3,822 | 15,288 | 54.09 | |
| " | Int-48 | 144.63 | 161.15 | 144.63 | 4.9 | 16.52 | Full | 2342.59 | 14,676 | 4,892 | 19,569 | 55.95 | |
| " | Int-47 | 145.71 | 164.14 | 145.71 | 4.9 | 18.43 | Full | 2562.21 | 16,052 | 5,351 | 21,403 | 54.85 | |
| " | Int-42 | 144.10 | 156.85 | 144.10 | 4.9 | 12.75 | Full | 2196.18 | 13,759 | 4,586 | 18,346 | 79.45 | |
| 9/23/09 | WI-21 | 132.30 | 142.86 | 132.30 | 4.9 | 10.56 | Full | 1683.74 | 10,549 | 3,516 | 14,065 | 67.81 | |
| " | Int-41 | 143.60 | 153.35 | 143.60 | 4.9 | 9.75 | Full | 2562.21 | 16,052 | 5,351 | 21,403 | 121.21 | |
| " | Int-43 | 143.89 | 154.61 | 143.89 | 4.9 | 10.72 | Full | 1756.94 | 11,007 | 3,669 | 14,676 | 75.59 | |
| 9/24/09 | Int-15 | 133.40 | 185.75 | 133.40 | 4.9 | 52.35 | Full | 4758.39 | 29,812 | 9,937 | 39,749 | 35.86 | |
| " | Int-44 | 146.70 | 154.99 | 146.70 | 4.9 | 8.29 | Full | 1390.91 | 8,714 | 2,905 | 11,619 | 77.39 | |
| " | Int-46 | 148.76 | 158.27 | 148.76 | 4.9 | 9.51 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 59.42 | |
| " | Int-40 | 145.74 | 156.10 | 145.74 | 4.9 | 10.36 | Full | 1756.94 | 11,007 | 3,669 | 14,676 | 85.50 | |
| " | Int-45 | 147.07 | 158.29 | 147.07 | 4.9 | 11.22 | Full | 1683.74 | 10,549 | 3,516 | 14,065 | 69.21 | |
| 9/25/09 | Int-16 | 138.77 | 185.97 | 138.77 | 4.9 | 47.20 | Full | 4465.57 | 27,977 | 9,326 | 37,303 | 37.33 | |
| " | Int-10 | 144.85 | 155.70 | 144.85 | 4.9 | 10.85 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 60.26 | |
| " | Int-168 | 143.42 | 150.86 | 143.42 | 4.9 | 7.44 | Full | 1171.30 | 7,338 | 2,446 | 9,784 | 62.12 | |
| " | Int-12 | 139.26 | 185.47 | 139.26 | 4.9 | 46.21 | Full | 5124.42 | 32,105 | 10,702 | 42,806 | 47.16 | |
| " | Int-161 | 140.08 | 185.58 | 140.08 | 4.9 | 45.50 | Full | 4831.60 | 30,270 | 10,090 | 40,360 | 41.90 | |
| " | Int-162 | 142.71 | 153.79 | 142.71 | 4.9 | 11.08 | Full | 1683.74 | 10,549 | 3,516 | 14,065 | 59.96 | |
| 9/26/09 | Int-14 | 142.28 | 185.53 | 142.28 | 4.9 | 43.25 | Full | 3879.92 | 24,308 | 8,103 | 32,411 | 35.39 | |
| " | Int-165 | 142.02 | 157.11 | 142.02 | 4.9 | 15.09 | Full | 2269.39 | 14,218 | 4,739 | 18,957 | 63.96 | |
| 9/28/09 | Int-163 | 142.37 | 155.45 | 142.37 | 4.9 | 13.08 | Full | 1976.56 | 12,383 | 4,128 | 16,511 | 69.70 | |
| " | Int-164 | 140.81 | 154.53 | 140.81 | 4.9 | 13.72 | Full | 2122.97 | 13,301 | 4,434 | 17,734 | 61.05 | |
| " | Int-166 | 142.43 | 154.10 | 142.43 | 4.9 | 11.67 | Full | 1903.36 | 11,925 | 3,975 | 15,900 | 75.23 | |
| " | Int-167 | 142.64 | 154.47 | 142.64 | 4.9 | 11.83 | Full | 1830.15 | 11,466 | 3,822 | 15,288 | 65.79 | |
| " | Int-142 | 132.12 | 145.23 | 132.12 | 4.9 | 13.11 | Full | 2122.97 | 13,301 | 4,434 | 17,734 | 68.87 | |
| 9/29/09 | Int-143 | 134.83 | 154.77 | 134.83 | 4.9 | 19.94 | Full | 3074.65 | 19,263 | 6,421 | 25,684 | 71.12 | |
| " | Int-144 | 135.65 | 157.17 | 135.65 | 4.9 | 21.52 | Full | 3587.09 | 22,473 | 7,491 | 29,964 | 65.77 | |
| " | Int-17 | 137.26 | 185.60 | 137.06 | 4.9 | 48.54 | Full | 4026.33 | 25,225 | 8,408 | 33,634 | 38.26 | |
| " | Int-145 | 138.07 | 152.92 | 138.07 | 4.9 | 14.85 | Full | 2196.18 | 13,759 | 4,586 | 18,346 | 62.90 | |
| " | Int-146 | 138.34 | 149.71 | 138.30 | 4.9 | 11.41 | Full | 2196.18 | 13,759 | 4,586 | 18,346 | 81.86 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | (GAL) | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 9/30/09 | Int-152 | 138.80 | 151.16 | 138.80 | 4.9 | 12.36 | Full | 1756.94 | 11,007 | 3,669 | 14,676 | 56.08 | |
| " | Int-18 | 141.65 | 186.26 | 141.65 | 4.9 | 44.61 | Full | 4465.57 | 27,977 | 9,326 | 37,303 | 39.50 | |
| " | Int-19 | 140.96 | 186.13 | 140.96 | 4.9 | 45.17 | Full | 4319.15 | 27,060 | 9,020 | 36,080 | 44.10 | |
| " | Int-20 | 138.64 | 185.90 | 138.64 | 4.9 | 47.26 | Full | 4245.95 | 26,601 | 8,867 | 35,468 | 38.21 | |
| " | Int-22 | 134.51 | 186.34 | 134.51 | 4.9 | 51.83 | Full | 4831.60 | 30,270 | 10,090 | 40,360 | 39.65 | |
| 10/1/09 | Int-147 | 140.45 | 152.51 | 140.45 | 4.9 | 12.06 | Full | 2049.77 | 12,842 | 4,281 | 17,123 | 72.28 | |
| " | Int-154 | 137.97 | 153.74 | 137.97 | 4.9 | 15.77 | Full | 2342.59 | 14,676 | 4,892 | 19,569 | 63.18 | |
| 10/2/09 | Int-155 | 139.95 | 152.34 | 139.95 | 4.9 | 12.39 | Full | 1976.56 | 12,383 | 4,128 | 16,511 | 67.85 | |
| " | WO-31 | 127.42 | 186.79 | 127.42 | 4.9 | 59.37 | Full | 5197.63 | 32,563 | 10,854 | 43,418 | 37.23 | |
| " | SO-1 | 126.66 | 186.52 | 124.93 | 4.9 | 61.59 | Full | 5344.04 | 33,481 | 11,160 | 44,641 | 31.89 | |
| " | SO-7 | 133.00 | 187.12 | 130.00 | 4.9 | 57.12 | Full | 5051.21 | 31,646 | 10,549 | 42,195 | 32.50 | |
| 10/5/09 | WO-32 | 126.19 | 184.91 | 126.19 | 4.9 | 58.72 | Full | 5490.45 | 34,398 | 11,466 | 45,864 | 36.89 | density of sample = 122 lb/ft³ |
| " | SO-3 | 127.58 | 186.46 | 125.07 | 4.9 | 61.39 | Full | 5417.24 | 33,939 | 11,313 | 45,252 | 32.44 | |
| " | SO-9 | 132.97 | 187.00 | 132.97 | 4.9 | 54.03 | Full | 4538.77 | 28,436 | 9,479 | 37,914 | 30.88 | |
| 10/6/09 | WO-33 | 126.04 | 186.36 | 126.04 | 4.9 | 60.34 | Full | 5197.63 | 32,563 | 10,854 | 43,418 | 36.63 | density of sample = 121 lb/ft³ |
| " | WI-30 | 127.49 | 186.90 | 127.49 | 4.9 | 59.41 | Full | 5856.48 | 36,691 | 12,230 | 48,922 | 41.92 | |
| " | SO-6 | 131.18 | 187.15 | 128.42 | 4.9 | 58.73 | Full | 4904.80 | 30,729 | 10,243 | 40,972 | 32.95 | |
| " | SO-12 | 134.80 | 187.42 | 134.80 | 4.9 | 52.62 | Full | 5270.83 | 33,022 | 11,007 | 44,029 | 36.82 | |
| 10/7/09 | SO-2 | 129.04 | 187.15 | 127.99 | 4.9 | 59.16 | Full | 5270.83 | 33,022 | 11,007 | 44,029 | 41.09 | |
| " | SO-8 | 133.69 | 187.10 | 132.00 | 4.9 | 55.10 | Full | 6515.33 | 40,819 | 13,606 | 54,425 | 50.29 | |
| " | SO-5 | 128.41 | 186.54 | 128.41 | 4.9 | 58.13 | Full | 7833.04 | 49,074 | 16,358 | 65,433 | 53.17 | |
| 10/8/09 | SO-4 | 128.53 | 187.08 | 128.35 | 4.9 | 58.73 | Full | 6734.95 | 42,195 | 14,065 | 56,260 | 45.25 | |
| " | SI-3A | 127.92 | 187.19 | 127.88 | 4.9 | 59.31 | Full | 6515.33 | 40,819 | 13,606 | 54,425 | 46.72 | |
| " | SI-2 | 128.74 | 187.04 | 126.41 | 4.9 | 60.63 | Full | 7247.39 | 45,405 | 15,135 | 60,540 | 55.13 | |
| 10/9/09 | SI-3 | 126.00 | 140.98 | 126.00 | 4.9 | 14.98 | Full | 2342.59 | 14,676 | 4,892 | 19,569 | 66.51 | |
| " | SO-10 | 132.77 | 187.13 | 132.73 | 4.9 | 54.40 | Full | 6588.54 | 41,278 | 13,759 | 55,037 | 47.79 | |
| 10/10/09 | WI-31 | 126.28 | 187.20 | 126.24 | 4.9 | 60.96 | Full | 7320.60 | 45,864 | 15,288 | 61,152 | 60.54 | |
| 10/12/09 | Int-153 | 135.49 | 185.75 | 135.49 | 4.9 | 50.26 | Full | 6442.13 | 40,360 | 13,453 | 53,814 | 59.12 | |
| 10/13/09 | SI-1 | 127.83 | 187.50 | 127.83 | 4.9 | 59.67 | Full | 6076.10 | 38,067 | 12,689 | 50,756 | 51.34 | |
| " | Int-35 | 134.78 | 187.50 | 134.78 | 4.9 | 52.72 | Full | 5783.27 | 36,233 | 12,078 | 48,310 | 46.65 | |
| 10/14/09 | Int-34 | 134.85 | 187.60 | 134.85 | 4.9 | 52.75 | Full | 5856.48 | 36,691 | 12,230 | 48,922 | 47.22 | |
| " | Int-37 | 135.05 | 187.18 | 135.05 | 4.9 | 52.13 | Full | 5563.66 | 34,857 | 11,619 | 46,476 | 45.39 | |
| 10/15/09 | Int-38 | 135.04 | 186.81 | 135.04 | 4.9 | 51.77 | Full | 6149.30 | 38,526 | 12,842 | 51,368 | 50.52 | |
| " | Int-32 | 135.11 | 187.08 | 135.11 | 4.9 | 51.97 | Full | 5563.66 | 34,857 | 11,619 | 46,476 | 49.38 | |
| " | Int-33 | 135.07 | 187.01 | 135.07 | 4.9 | 51.94 | Full | 5563.66 | 34,857 | 11,619 | 46,476 | 54.00 | |
| 10/16/09 | SI-4 | 126.50 | 140.41 | 126.40 | 4.9 | 14.01 | Full | 2196.18 | 13,759 | 4,586 | 18,346 | 72.30 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added (GAL) | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 10/19/09 | Int-36 | 134.90 | 161.77 | 134.90 | 4.9 | 26.87 | Full | 3513.89 | 22,015 | 7,338 | 29,353 | 60.32 | |
| " | SI-5 | 130.34 | 187.48 | 130.34 | 4.9 | 57.14 | Full | 6442.13 | 40,360 | 13,453 | 53,814 | 56.84 | |
| " | Int-31 | 135.00 | 187.36 | 135.00 | 4.9 | 52.36 | Full | 5490.45 | 34,398 | 11,466 | 45,864 | 44.60 | |
| 10/20/09 | SI-6 | 132.71 | 187.89 | 132.71 | 4.9 | 55.18 | Full | 6002.89 | 37,608 | 12,536 | 50,145 | 46.27 | |
| " | Int-30 | 135.06 | 187.16 | 135.06 | 4.9 | 52.10 | Full | 6076.10 | 38,067 | 12,689 | 50,756 | 49.60 | |
| " | SO-11 | 134.73 | 187.61 | 134.73 | 4.9 | 52.88 | Full | 5856.48 | 36,691 | 12,230 | 48,922 | 43.70 | |
| 10/21/09 | SI-7 | 133.33 | 187.23 | 133.33 | 4.9 | 53.90 | Full | 5856.48 | 36,691 | 12,230 | 48,922 | 50.11 | |
| " | Int-343 | 135.38 | 186.50 | 135.38 | 4.9 | 51.12 | Full | 5417.24 | 33,939 | 11,313 | 45,252 | 45.07 | |
| " | Int-340 | 135.49 | 186.35 | 135.49 | 4.9 | 50.86 | Full | 5636.86 | 35,315 | 11,772 | 47,087 | 43.73 | |
| 10/22/09 | SI-8 | 137.28 | 187.17 | 134.65 | 4.9 | 52.52 | Full | 5929.69 | 37,150 | 12,383 | 49,533 | 56.92 | |
| " | Int-344 | 134.39 | 187.04 | 134.39 | 4.9 | 52.65 | Full | 5710.07 | 35,774 | 11,925 | 47,699 | 50.02 | |
| " | Int-345 | 134.57 | 186.80 | 134.57 | 4.9 | 52.23 | Full | 5929.69 | 37,150 | 12,383 | 49,533 | 44.79 | |
| " | SO-13 | 135.13 | 186.46 | 135.13 | 4.9 | 51.33 | Full | 5710.07 | 35,774 | 11,925 | 47,699 | 43.89 | |
| 10/23/09 | Int-341 | 132.73 | 186.55 | 132.73 | 4.9 | 53.82 | Full | 6076.10 | 38,067 | 12,689 | 50,756 | 52.07 | |
| | SI-9 | - | - | - | - | - | - | - | - | - | - | - | Cementitious material encountered to 53.79'. No jet grouting. |
| " | SI-10 | 133.07 | 186.60 | 133.07 | 4.9 | 53.53 | Full | 5856.48 | 36,691 | 12,230 | 48,922 | 46.53 | |
| " | SO-14 | 135.34 | 187.29 | 135.34 | 4.9 | 51.95 | Full | 6881.36 | 43,112 | 14,371 | 57,483 | 52.26 | |
| " | Int-28 | 132.88 | 143.23 | 132.88 | 4.9 | 10.35 | Full | 1610.53 | 10,090 | 3,363 | 13,453 | 71.77 | |
| 10/24/09 | Int-29 | 132.35 | 144.09 | 132.35 | 4.9 | 11.74 | Full | 2049.77 | 12,842 | 4,281 | 17,123 | 96.98 | |
| " | Int-27 | 132.96 | 157.10 | 132.96 | 4.9 | 24.14 | Full | 3147.86 | 19,722 | 6,574 | 26,295 | 55.46 | |
| " | Int-149 | 133.25 | 152.70 | 133.25 | 4.9 | 19.45 | Full | 2781.83 | 17,428 | 5,809 | 23,238 | 72.11 | |
| 10/26/09 | SI-9 | 132.93 | - | - | - | - | - | - | - | - | - | - | Cementitious material encountered. No jet grouting. |
| " | SO-18 | 137.16 | 186.50 | 137.16 | 4.9 | 49.34 | Full | 5051.21 | 31,646 | 10,549 | 42,195 | 37.63 | |
| " | Int-342 | 133.43 | 152.94 | 133.43 | 4.9 | 19.51 | Full | 2928.24 | 18,346 | 6,115 | 24,461 | 63.83 | |
| " | Int-150 | 132.99 | 162.15 | 132.99 | 4.9 | 29.16 | Full | 3806.71 | 23,849 | 7,950 | 31,799 | 65.82 | |
| 10/27/09 | Int-151 | 135.20 | 149.00 | 135.20 | 4.9 | 13.80 | Full | 2122.97 | 13,301 | 4,434 | 17,734 | 77.56 | |
| " | SO-18A | 137.58 | 186.56 | 137.58 | 4.9 | 48.98 | Full | 5270.83 | 33,022 | 11,007 | 44,029 | 42.46 | |
| " | SO-23 | 148.34 | 186.49 | 148.34 | 4.9 | 38.15 | Full | 3879.92 | 24,308 | 8,103 | 32,411 | 37.38 | |
| 10/28/09 | SO-15 | 136.42 | 187.47 | 136.42 | 4.9 | 51.05 | Full | 6149.30 | 38,526 | 12,842 | 51,368 | 47.53 | |
| 10/29/09 | SO-20 | 139.17 | 185.16 | 139.17 | 4.9 | 45.99 | Full | 5124.42 | 32,105 | 10,702 | 42,806 | 40.96 | |
| " | SO-25 | 145.23 | 185.61 | 145.23 | 4.9 | 40.38 | Full | 4319.15 | 27,060 | 9,020 | 36,080 | 39.32 | |
| " | SO-28 | 151.51 | 186.19 | 151.51 | 4.9 | 34.68 | Full | 3733.51 | 23,391 | 7,797 | 31,188 | 39.57 | |
| " | SO-30 | 156.38 | 185.84 | 156.48 | 4.9 | 29.36 | Full | 3367.48 | 21,097 | 7,032 | 28,130 | 42.16 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added (GAL) | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 10/30/09 | SO-17 | 134.99 | 186.88 | 134.99 | 4.9 | 51.89 | Full | 5710.07 | 35,774 | 11,925 | 47,699 | 43.42 | |
| " | SO-22 | 142.61 | 185.12 | 142.14 | 4.9 | 42.98 | Full | 4685.18 | 29,353 | 9,784 | 39,137 | 43.01 | |
| " | SI-11 | 134.96 | 187.05 | 134.96 | 4.9 | 52.09 | Full | 5710.07 | 35,774 | 11,925 | 47,699 | 50.56 | |
| " | SI-12 | 135.04 | 187.03 | 135.04 | 4.9 | 51.99 | Full | 5563.66 | 34,857 | 11,619 | 46,476 | 49.36 | |
| 11/2/09 | SO-16 | 140.82 | 186.82 | 140.82 | 4.9 | 46.00 | Full | 4904.80 | 30,729 | 10,243 | 40,972 | 45.35 | |
| " | SO-19 | 138.67 | 185.59 | 138.67 | 4.9 | 46.92 | Full | 5710.07 | 35,774 | 11,925 | 47,699 | 56.13 | |
| " | SO-24 | 145.52 | 185.45 | 145.52 | 4.9 | 39.93 | Full | 4392.36 | 27,518 | 9,173 | 36,691 | 46.78 | |
| 11/3/09 | SO-27 | 147.67 | 185.36 | 147.67 | 4.9 | 37.69 | Full | 3806.71 | 23,849 | 7,950 | 31,799 | 39.85 | |
| " | SO-31 | 157.19 | 185.62 | 156.49 | 4.9 | 29.13 | Full | 2635.42 | 16,511 | 5,504 | 22,015 | 35.70 | |
| " | SI-13 | 138.33 | | | - | - | - | - | - | - | - | - | Tremie grouted |
| " | Int-21 | 139.88 | 187.31 | 139.88 | 4.9 | 47.43 | Full | 5051.21 | 31,646 | 10,549 | 42,195 | 45.29 | |
| 11/4/09 | SI-14 | 135.37 | 147.17 | 135.37 | 4.9 | 11.80 | Full | 1683.74 | 10,549 | 3,516 | 14,065 | 60.69 | |
| " | SI-15 | 134.77 | 186.47 | 135.15 | 4.9 | 51.32 | Full | 5563.66 | 34,857 | 11,619 | 46,476 | 50.00 | |
| 11/5/09 | SI-16 | 134.70 | 186.72 | 134.70 | 4.9 | 52.02 | Full | 6002.89 | 37,608 | 12,536 | 50,145 | 58.18 | Began grouting on 11/4. Batch plant malfunction. Completed grouting on 11/5 |
| " | Int-159 | 137.10 | 162.03 | 137.10 | 4.9 | 24.93 | Full | 3367.48 | 21,097 | 7,032 | 28,130 | 53.30 | |
| " | Int-157 | 137.96 | 162.29 | 137.96 | 4.9 | 24.33 | Full | 3147.86 | 19,722 | 6,574 | 26,295 | 65.23 | |
| " | Int-156 | 141.09 | 151.59 | 141.09 | 4.9 | 10.50 | Full | 1464.12 | 9,173 | 3,058 | 12,230 | 59.30 | |
| " | Int-160 | 138.76 | 186.72 | 138.76 | 4.9 | 47.96 | Full | 5197.63 | 32,563 | 10,854 | 43,418 | 46.09 | |
| 11/6/09 | Int-158 | 138.59 | 151.90 | 138.59 | 4.9 | 13.31 | Full | 2122.97 | 13,301 | 4,434 | 17,734 | 80.42 | |
| 11/7/09 | Int-25 | 133.90 | 186.68 | 133.90 | 4.9 | 52.78 | Full | 7979.45 | 49,992 | 16,664 | 66,656 | 64.30 | |
| " | Int-26 | 134.12 | 187.85 | 134.12 | 4.9 | 53.73 | Full | 5929.69 | 37,150 | 12,383 | 49,533 | 55.64 | |
| 11/9/09 | SI-13A | 135.61 | 148.01 | 135.61 | 4.9 | 12.40 | Full | 1683.74 | 10,549 | 3,516 | 14,065 | 68.46 | |
| " | Int-148 | 134.83 | 153.04 | 134.83 | 4.9 | 18.21 | Full | 2635.42 | 16,511 | 5,504 | 22,015 | 61.55 | |
| " | Int-24 | 133.55 | 186.66 | 133.55 | 4.9 | 53.11 | Full | 6368.92 | 39,902 | 13,301 | 53,202 | 60.46 | |
| " | Int-23 | 134.54 | 187.68 | 134.54 | 4.9 | 53.14 | Full | 5636.86 | 35,315 | 11,772 | 47,087 | 53.48 | |
| 11/10/09 | SI-17 | 138.59 | 152.96 | 138.59 | 4.9 | 14.37 | Full | 2049.77 | 12,842 | 4,281 | 17,123 | 65.79 | |
| " | SO-21 | 141.96 | 185.82 | 141.96 | 4.9 | 43.86 | Full | 4611.98 | 28,894 | 9,631 | 38,526 | 44.72 | |
| " | SO-26 | 146.47 | 185.58 | 146.47 | 4.9 | 39.11 | Full | 4538.77 | 28,436 | 9,479 | 37,914 | 49.36 | |
| " | SO-29 | 153.55 | 185.40 | 153.55 | 4.9 | 31.85 | Full | 3221.06 | 20,180 | 6,727 | 26,907 | 43.01 | |
| 11/11/09 | SI-18 | 137.83 | 164.98 | 137.83 | 4.9 | 27.15 | Full | 3660.30 | 22,932 | 7,644 | 30,576 | 62.18 | |
| " | SI-19 | 138.74 | 150.77 | 138.74 | 4.9 | 12.03 | Full | 2049.77 | 12,842 | 4,281 | 17,123 | 78.59 | |
| " | SI-20 | 138.63 | 186.68 | 138.63 | 4.9 | 48.05 | Full | 5197.63 | 32,563 | 10,854 | 43,418 | 49.89 | |
| " | SI-21 | 139.91 | 155.35 | 139.91 | 4.9 | 15.44 | Full | 2122.97 | 13,301 | 4,434 | 17,734 | 63.42 | |
| " | SI-22 | 138.56 | 187.01 | 138.56 | 4.9 | 48.45 | Full | 5270.83 | 33,022 | 11,007 | 44,029 | 50.18 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added (GAL) | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 11/12/09 | Int-129 | 138.74 | 185.81 | 138.74 | 4.9 | 47.07 | Full | 4758.39 | 29,812 | 9,937 | 39,749 | 46.63 | |
| " | Int-130 | 139.64 | 152.03 | 139.64 | 4.9 | 12.39 | Full | 1317.71 | 8,256 | 2,752 | 11,007 | 45.23 | |
| " | Int-118 | 141.37 | 186.70 | 140.04 | 4.9 | 46.66 | Full | 4978.01 | 31,188 | 10,396 | 41,583 | 45.37 | |
| 11/13/09 | SI-23 | 143.64 | 157.72 | 143.64 | 4.9 | 14.08 | Full | 2196.18 | 13,759 | 4,586 | 18,346 | 78.64 | |
| " | SI-24 | 145.57 | 186.60 | 145.57 | 4.9 | 41.03 | Full | 4465.57 | 27,977 | 9,326 | 37,303 | 50.20 | |
| " | SI-25 | 149.01 | 186.50 | 147.76 | 4.9 | 38.74 | Full | 3953.12 | 24,767 | 8,256 | 33,022 | 47.07 | |
| " | SI-26 | 147.34 | 186.49 | 147.34 | 4.9 | 39.15 | Full | 4172.74 | 26,142 | 8,714 | 34,857 | 49.16 | |
| 11/1409 | SI-27 | 154.37 | 186.78 | 154.37 | 4.9 | 32.41 | Full | 3074.65 | 19,263 | 6,421 | 25,684 | 40.35 | |
| " | SI-28 | 156.51 | 186.89 | 156.51 | 4.9 | 30.38 | Full | 2855.03 | 17,887 | 5,962 | 23,849 | 39.97 | |
| 11/16/09 | Int-131 | 138.71 | 152.12 | 138.71 | 4.9 | 13.41 | Full | 2049.77 | 12,842 | 4,281 | 17,123 | 65.01 | |
| " | Int-119 | 140.87 | 151.23 | 140.87 | 4.9 | 10.36 | Full | 1610.53 | 10,090 | 3,363 | 13,453 | 61.34 | |
| " | Int-109 | 141.39 | 151.56 | 141.39 | 4.9 | 10.17 | Full | 1610.53 | 10,090 | 3,363 | 13,453 | 62.48 | |
| " | Int-105 | 142.49 | 185.88 | 142.49 | 4.9 | 43.39 | Full | 4538.77 | 28,436 | 9,479 | 37,914 | 41.27 | |
| " | Int-132 | 140.28 | 166.65 | 140.28 | 4.9 | 26.37 | Full | 3587.09 | 22,473 | 7,491 | 29,964 | 68.58 | |
| " | Int-133 | 139.90 | 186.75 | 139.90 | 4.9 | 46.85 | Full | 6368.92 | 39,902 | 13,301 | 53,202 | 62.70 | |
| " | Int-120 | 140.56 | 151.74 | 140.56 | 4.9 | 11.18 | Full | 1683.74 | 10,549 | 3,516 | 14,065 | 69.46 | |
| 11/17/09 | Int-110 | 141.31 | 151.21 | 141.31 | 5.9 | 9.90 | Full | 1464.12 | 9,173 | 3,058 | 12,230 | 74.56 | |
| " | Int-134 | 138.20 | 153.94 | 138.20 | 6.9 | 15.74 | Full | 2342.59 | 14,676 | 4,892 | 19,569 | 68.65 | |
| " | Int-121 | 140.28 | 152.05 | 140.28 | 7.9 | 11.77 | Full | 1830.15 | 11,466 | 3,822 | 15,288 | 71.72 | |
| " | Int-111 | 140.98 | 152.59 | 140.98 | 8.9 | 11.61 | Full | 1683.74 | 10,549 | 3,516 | 14,065 | 66.89 | |
| " | Int-106 | 140.41 | 186.07 | 140.41 | 9.9 | 45.66 | Full | 5124.42 | 32,105 | 10,702 | 42,806 | 44.28 | |
| " | Int-112 | 141.22 | 161.03 | 141.22 | 10.9 | 19.81 | Full | 2708.62 | 16,970 | 5,657 | 22,626 | #N/A | |
| " | Int-122 | 138.46 | 186.14 | 138.46 | 11.9 | 47.68 | Full | 5051.21 | 31,646 | 10,549 | 42,195 | 48.86 | |
| 11/18/09 | Int-135 | 137.57 | 186.51 | 137.57 | 12.9 | 48.94 | Full | 5417.24 | 33,939 | 11,313 | 45,252 | 51.05 | |
| " | Int-123 | 140.09 | 159.40 | 140.09 | 13.9 | 19.31 | Full | 2635.42 | 16,511 | 5,504 | 22,015 | 62.95 | |
| " | Int-113 | 140.50 | 159.46 | 140.50 | 14.9 | 18.96 | Full | 2635.42 | 16,511 | 5,504 | 22,015 | 64.11 | |
| " | Int-103 | 144.80 | 155.42 | 144.80 | 15.9 | 10.62 | Full | 1610.53 | 10,090 | 3,363 | 13,453 | 59.83 | |
| " | Int-107 | 142.48 | 186.18 | 142.48 | 16.9 | 43.70 | Full | 4538.77 | 28,436 | 9,479 | 37,914 | 47.90 | |
| " | Int-104 | 144.99 | 185.86 | 144.99 | 17.9 | 40.87 | Full | 4465.57 | 27,977 | 9,326 | 37,303 | 50.40 | |
| 11/19/09 | Int-124 | 140.18 | 186.43 | 140.18 | 4.9 | 46.25 | Full | 5051.21 | 31,646 | 10,549 | 42,195 | 43.09 | |
| " | Int-114 | 141.45 | 157.52 | 141.45 | 4.9 | 16.07 | Full | 2122.97 | 13,301 | 4,434 | 17,734 | 60.93 | |
| " | Int-108 | 142.31 | 185.93 | 142.31 | 4.9 | 43.62 | Full | 4611.98 | 28,894 | 9,631 | 38,526 | 53.31 | |
| " | Int-349 | 141.50 | 183.11 | 140.79 | 4.9 | 42.32 | Full | 5051.21 | 31,646 | 10,549 | 42,195 | 55.05 | |
| " | Int-115 | 142.70 | 158.34 | 142.70 | 4.9 | 15.64 | Full | 2196.18 | 13,759 | 4,586 | 18,346 | 59.72 | |
| " | Int-125 | 145.61 | 159.55 | 145.61 | 4.9 | 13.94 | Full | 2196.18 | 13,759 | 4,586 | 18,346 | 72.66 | |
| " | Int-136 | 147.36 | 162.87 | 147.36 | 4.9 | 15.51 | Full | 2196.18 | 13,759 | 4,586 | 18,346 | 65.31 | |
| " | Int-137 | 147.71 | 149.27 | 145.79 | 4.9 | 3.48 | Full | 585.65 | 3,669 | 1,223 | 4,892 | 77.62 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added (GAL) | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 11/20/09 | Int-116 | 145.65 | 185.70 | 145.65 | 4.9 | 40.05 | Full | 4465.57 | 27,977 | 9,326 | 37,303 | 43.99 | |
| " | Int-126 | 146.12 | 182.78 | 146.12 | 4.9 | 36.66 | Full | 3953.12 | 24,767 | 8,256 | 33,022 | 45.86 | |
| " | Int-117 | 147.72 | 185.97 | 147.72 | 4.9 | 38.25 | Full | 4831.60 | 30,270 | 10,090 | 40,360 | 49.84 | |
| 11/23/09 | Int-127 | 139.78 | 162.01 | 139.78 | 4.9 | 22.23 | Full | 2269.39 | 14,218 | 4,739 | 18,957 | 47.09 | |
| " | Int-128 | 141.24 | 164.46 | 141.24 | 4.9 | 23.22 | Full | 3513.89 | 22,015 | 7,338 | 29,353 | 64.36 | |
| " | Int-139 | 145.77 | 159.88 | 145.77 | 4.9 | 14.11 | Full | 1830.15 | 11,466 | 3,822 | 15,288 | 55.16 | |
| " | Int-138 | 148.16 | 186.57 | 148.16 | 4.9 | 38.41 | Full | 3953.12 | 24,767 | 8,256 | 33,022 | 51.89 | |
| " | Int-140 | 149.43 | 164.35 | 149.43 | 4.9 | 14.92 | Full | 1976.56 | 12,383 | 4,128 | 16,511 | 61.10 | |
| " | Int-141 | 149.60 | 186.66 | 149.60 | 4.9 | 37.06 | Full | 3879.92 | 24,308 | 8,103 | 32,411 | 44.53 | |
| " | Int-338 | 153.57 | 186.77 | 153.53 | 4.9 | 33.24 | Full | 2415.80 | 15,135 | 5,045 | 20,180 | 40.37 | |
| 11/24/09 | Int-339 | 153.87 | 185.95 | 153.87 | 4.9 | 32.08 | Full | 2562.21 | 16,052 | 5,351 | 21,403 | 44.37 | |
| " | Int-335 | 153.84 | 186.02 | 153.84 | 4.9 | 32.18 | Full | 3074.65 | 19,263 | 6,421 | 25,684 | 44.07 | |
| " | Int-336 | 155.89 | 186.24 | 155.89 | 4.9 | 30.35 | Full | 2855.03 | 17,887 | 5,962 | 23,849 | 43.39 | |
| " | Int-337 | 156.78 | 186.27 | 156.78 | 4.9 | 29.49 | Full | 2708.62 | 16,970 | 5,657 | 22,626 | 39.06 | |
| " | SI-29 | 155.87 | 186.48 | 155.87 | 4.9 | 30.61 | Full | 3001.45 | 18,804 | 6,268 | 25,072 | 49.44 | |
| " | SI-30 | 155.66 | 186.24 | 155.60 | 4.9 | 30.64 | Full | 2855.03 | 17,887 | 5,962 | 23,849 | 39.63 | |
| " | SO-32 | 155.72 | 186.53 | 155.72 | 4.9 | 30.81 | Full | 2708.62 | 16,970 | 5,657 | 22,626 | 37.39 | |
| " | SI-31 | 156.27 | 186.00 | 156.27 | 4.9 | 29.73 | Full | 2855.03 | 17,887 | 5,962 | 23,849 | 40.84 | |
| 11/30/09 | Int-328 | 156.88 | 187.19 | 156.88 | 4.9 | 30.31 | Full | 2855.03 | 17,887 | 5,962 | 23,849 | 34.62 | |
| " | Int-331 | 156.89 | 187.01 | 156.89 | 4.9 | 30.12 | Full | 3001.45 | 18,804 | 6,268 | 25,072 | 39.32 | |
| " | Int-333 | 156.92 | 166.14 | 156.92 | 4.9 | 9.22 | Full | 1244.50 | 7,797 | 2,599 | 10,396 | 53.26 | |
| " | Int-332 | 160.11 | 186.06 | 160.11 | 4.9 | 25.95 | Full | 2269.39 | 14,218 | 4,739 | 18,957 | 37.19 | |
| " | Int-334 | 160.19 | 186.38 | 160.19 | 4.9 | 26.19 | Full | 2269.39 | 14,218 | 4,739 | 18,957 | 39.97 | |
| " | Int-330 | 160.08 | 186.49 | 160.08 | 4.9 | 26.41 | Full | 2342.59 | 14,676 | 4,892 | 19,569 | 37.72 | |
| " | Int-329 | 156.82 | 186.21 | 156.82 | 4.9 | 29.39 | Full | 3001.45 | 18,804 | 6,268 | 25,072 | 40.29 | |
| " | Int-325 | 153.92 | 186.37 | 153.92 | 4.9 | 32.45 | Full | 3294.27 | 20,639 | 6,880 | 27,518 | 37.31 | |
| " | Int-326 | 153.89 | 186.53 | 153.98 | 4.9 | 32.55 | Full | 3440.68 | 21,556 | 7,185 | 28,741 | 41.71 | |
| 12/1/09 | Int-83 | 144.35 | 166.45 | 144.35 | 4.9 | 22.10 | Full | 2562.21 | 16,052 | 5,351 | 21,403 | 42.61 | |
| " | Int-73 | 149.55 | 169.29 | 149.55 | 4.9 | 19.74 | Full | 2269.39 | 14,218 | 4,739 | 18,957 | 42.26 | |
| " | Int-74 | 151.01 | 160.19 | 151.01 | 4.9 | 9.18 | Full | 1171.30 | 7,338 | 2,446 | 9,784 | 50.34 | |
| " | Int-70 | 152.19 | 161.27 | 152.19 | 4.9 | 9.08 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 47.72 | |
| " | Int-71 | 148.43 | 160.92 | 148.43 | 4.9 | 12.49 | Full | 1610.53 | 10,090 | 3,363 | 13,453 | 54.84 | |
| " | Int-72 | 147.97 | 160.20 | 147.97 | 4.9 | 12.23 | Full | 1610.53 | 10,090 | 3,363 | 13,453 | 60.74 | |
| " | Int-13 | 146.57 | 186.85 | 146.57 | 4.9 | 40.28 | Full | 4172.74 | 26,142 | 8,714 | 34,857 | 40.87 | |
| " | Int-82 | 144.85 | 165.58 | 144.85 | 4.9 | 20.73 | Full | 2635.42 | 16,511 | 5,504 | 22,015 | 54.07 | |
| " | Int-75 | 146.83 | 167.16 | 146.83 | 4.9 | 20.33 | Full | 3001.45 | 18,804 | 6,268 | 25,072 | 62.79 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added (GAL) | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 12/2/09 | Int-76 | 144.95 | 164.26 | 144.95 | 4.9 | 19.31 | Full | 2562.21 | 16,052 | 5,351 | 21,403 | 52.35 | |
| " | Int-84 | 143.57 | 163.97 | 143.57 | 4.9 | 20.40 | Full | 2708.62 | 16,970 | 5,657 | 22,626 | 61.24 | |
| " | SI-32 | 156.70 | 186.28 | 156.70 | 4.9 | 29.58 | Full | 2855.03 | 17,887 | 5,962 | 23,849 | 41.05 | |
| " | SO-33 | 157.10 | 186.29 | 157.09 | 4.9 | 29.20 | Full | 2635.42 | 16,511 | 5,504 | 22,015 | 38.38 | |
| " | SO-34 | 154.88 | 186.49 | 154.88 | 4.9 | 31.61 | Full | 3221.06 | 20,180 | 6,727 | 26,907 | 40.20 | |
| " | SO-35 | 156.65 | 186.20 | 156.66 | 4.9 | 29.54 | Full | 2781.83 | 17,428 | 5,809 | 23,238 | 37.16 | |
| " | SO-36 | 156.40 | 186.41 | 156.40 | 4.9 | 30.01 | Full | 2928.24 | 18,346 | 6,115 | 24,461 | 41.50 | |
| 12/4/09 | SI-33 | 156.79 | 184.86 | 156.79 | 4.9 | 28.07 | Full | 2708.62 | 16,970 | 5,657 | 22,626 | 41.04 | |
| " | Int-308 | 160.54 | 186.19 | 160.54 | 4.9 | 25.65 | Full | 2415.80 | 15,135 | 5,045 | 20,180 | 34.62 | |
| " | SI-34 | 157.20 | 186.31 | 156.20 | 4.9 | 30.11 | Full | 3367.48 | 21,097 | 7,032 | 28,130 | 51.58 | Partially grouted on 12/2. |
| 12/7/09 | Int-310 | 158.12 | 186.22 | 158.12 | 4.9 | 28.10 | Full | 2635.42 | 16,511 | 5,504 | 22,015 | 34.47 | |
| " | Int-312 | 158.42 | 174.52 | 158.42 | 4.9 | 16.10 | Full | 1756.94 | 11,007 | 3,669 | 14,676 | 46.41 | |
| " | Int-311 | 159.23 | 186.24 | 159.23 | 4.9 | 27.01 | Full | 2708.62 | 16,970 | 5,657 | 22,626 | 46.25 | |
| " | Int-309 | 159.21 | 186.13 | 159.21 | 4.9 | 26.92 | Full | 2415.80 | 15,135 | 5,045 | 20,180 | 38.17 | |
| " | SO-32A | 153.59 | 186.46 | 153.59 | 4.9 | 32.87 | Full | 3294.27 | 20,639 | 6,880 | 27,518 | 46.23 | |
| " | SO-31A | 154.38 | 186.20 | 154.38 | 4.9 | 31.82 | Full | 3074.65 | 19,263 | 6,421 | 25,684 | 44.57 | |
| " | Int-77 | 144.69 | 164.00 | 144.69 | 4.9 | 19.31 | Full | 2708.62 | 16,970 | 5,657 | 22,626 | 55.34 | |
| " | SO-30A | - | - | - | - | - | - | - | - | - | - | - | Obstruction encountered at ~1' bgs |
| 12/8/09 | Int-346 | 147.26 | 159.29 | 147.26 | 4.9 | 12.03 | Full | 1683.74 | 10,549 | 3,516 | 14,065 | 51.45 | |
| " | Int-78 | 146.25 | 165.32 | 146.25 | 4.9 | 19.07 | Full | 2342.59 | 14,676 | 4,892 | 19,569 | 52.24 | |
| " | Int-347 | 146.53 | 184.78 | 146.53 | 4.9 | 38.25 | Full | 4611.98 | 28,894 | 9,631 | 38,526 | 47.57 | |
| " | Int-79 | 146.63 | 165.29 | 146.63 | 4.9 | 18.66 | Full | 2269.39 | 14,218 | 4,739 | 18,957 | 56.09 | |
| " | Int-85 | 145.66 | 163.98 | 145.66 | 4.9 | 18.32 | Full | 2562.21 | 16,052 | 5,351 | 21,403 | 64.51 | |
| " | Int-86 | 145.89 | 165.24 | 145.89 | 4.9 | 19.35 | Full | 2562.21 | 16,052 | 5,351 | 21,403 | 61.07 | |
| " | Int-87 | 148.51 | 165.26 | 148.51 | 4.9 | 16.75 | Full | 2196.18 | 13,759 | 4,586 | 18,346 | 60.47 | |
| " | Int-80 | 148.68 | 160.35 | 148.68 | 4.9 | 11.67 | Full | 1610.53 | 10,090 | 3,363 | 13,453 | 63.65 | |
| 12/9/09 | Int-81 | 150.62 | 185.06 | 149.49 | 4.9 | 35.57 | Full | 3587.09 | 22,473 | 7,491 | 29,964 | 42.89 | |
| " | Int-88 | 146.20 | 160.57 | 146.20 | 4.9 | 14.37 | Full | 1976.56 | 12,383 | 4,128 | 16,511 | 58.50 | |
| " | Int-89 | 147.13 | 165.64 | 147.13 | 4.9 | 18.51 | Full | 2635.42 | 16,511 | 5,504 | 22,015 | 65.67 | |
| " | Int-348 | 148.70 | 185.67 | 148.70 | 4.9 | 36.97 | Full | 4026.33 | 25,225 | 8,408 | 33,634 | 46.32 | |
| 12/10/09 | Int-90 | 146.18 | 157.26 | 146.18 | 4.9 | 11.08 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 54.74 | |
| " | Int-92 | 142.13 | 155.71 | 142.13 | 4.9 | 13.58 | Full | 1903.36 | 11,925 | 3,975 | 15,900 | 55.30 | |
| " | Int-91 | 144.69 | 159.81 | 144.67 | 4.9 | 15.14 | Full | 2049.77 | 12,842 | 4,281 | 17,123 | 68.26 | |
| " | Int-93 | 144.78 | 159.95 | 144.78 | 4.9 | 15.17 | Full | 1976.56 | 12,383 | 4,128 | 16,511 | 55.41 | |
| " | Int-97 | 144.53 | 160.78 | 144.53 | 4.9 | 16.25 | Full | 2122.97 | 13,301 | 4,434 | 17,734 | 48.02 | |
| " | Int-94 | 144.98 | 158.75 | 144.98 | 4.9 | 13.77 | Full | 1830.15 | 11,466 | 3,822 | 15,288 | 56.53 | |
| " | Int-98 | 146.70 | 158.73 | 146.70 | 4.9 | 12.03 | Full | 1683.74 | 10,549 | 3,516 | 14,065 | 59.52 | |
| " | Int-95 | 146.18 | 157.43 | 146.18 | 4.9 | 11.25 | Full | 1903.36 | 11,925 | 3,975 | 15,900 | 78.03 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added (GAL) | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 12/11/09 | Int-99 | 148.10 | 158.91 | 146.41 | 4.9 | 12.50 | Full | 1683.74 | 10,549 | 3,516 | 14,065 | 62.13 | |
| " | Int-96 | 146.24 | 156.89 | 146.24 | 4.9 | 10.65 | Full | 1464.12 | 9,173 | 3,058 | 12,230 | 58.47 | |
| " | Int-100 | 147.82 | 158.21 | 146.50 | 4.9 | 11.71 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 55.83 | |
| " | Int-101 | 148.18 | 158.14 | 148.18 | 4.9 | 9.96 | Full | 1390.91 | 8,714 | 2,905 | 11,619 | 59.39 | |
| " | Int-102 | 146.56 | 165.44 | 146.56 | 4.9 | 18.88 | Full | 2489.00 | 15,594 | 5,198 | 20,792 | 66.47 | |
| " | Int-322 | " | 185.86 | 156.57 | 4.9 | 29.29 | Full | 2489.00 | 15,594 | 5,198 | 20,792 | 31.23 | |
| " | Int-323 | " | 175.81 | 156.45 | 4.9 | 19.36 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 22.38 | |
| 12/14/09 | Int-323 | " | 186.53 | 175.34 | 4.9 | 11.19 | Full | 1024.88 | 6,421 | 2,140 | 8,561 | 38.95 | Grouting began on 12/11. Grouting completed on 12/14 |
| " | Int-324 | " | 186.03 | 156.50 | 4.9 | 29.53 | Full | 2781.83 | 17,428 | 5,809 | 23,238 | 37.17 | |
| " | WO-8A | 139.43 | 155.35 | 139.43 | 4.9 | 15.92 | Full | 2489.00 | 15,594 | 5,198 | 20,792 | 72.11 | |
| 12/15/09 | WO-7 | 139.43 | 184.27 | 139.43 | 4.9 | 44.84 | Full | 5124.42 | 32,105 | 10,702 | 42,806 | 45.09 | |
| " | WO-6 | 149.98 | 184.60 | 138.50 | 4.9 | 46.10 | Full | 5417.24 | 33,939 | 11,313 | 45,252 | 46.36 | Grout surfaced approx. 25 feet north around manhole into sidewalk and into catch basin. |
| " | WO-5 | 139.27 | 184.67 | 139.27 | 4.9 | 45.40 | Full | 4978.01 | 31,188 | 10,396 | 41,583 | 43.26 | |
| " | WO-4 | 139.62 | 185.03 | 139.62 | 4.9 | 45.41 | Full | 4904.80 | 30,729 | 10,243 | 40,972 | 42.62 | |
| 12/16/09 | WO-3 | 140.96 | 184.78 | 140.96 | 4.9 | 43.82 | Full | 5344.04 | 33,481 | 11,160 | 44,641 | 48.12 | |
| " | WO-2 | 141.92 | 185.07 | 141.91 | 4.9 | 43.16 | Full | 4611.98 | 28,894 | 9,631 | 38,526 | 42.16 | |
| " | WO-1 | 141.10 | 185.35 | 141.09 | 4.9 | 44.26 | Full | 4685.18 | 29,353 | 9,784 | 39,137 | 41.77 | |
| " | WI-7 | 141.37 | 184.16 | 141.37 | 4.9 | 42.79 | Full | 4831.60 | 30,270 | 10,090 | 40,360 | 52.08 | |
| " | WI-6 | 141.45 | 163.67 | 141.45 | 4.9 | 22.22 | Full | 3147.86 | 19,722 | 6,574 | 26,295 | 65.34 | |
| 12/17/09 | WI-5 | 136.38 | 162.86 | 136.38 | 4.9 | 26.48 | Full | 3660.30 | 22,932 | 7,644 | 30,576 | 63.76 | |
| " | WI-4 | 141.94 | 170.35 | 141.94 | 4.9 | 28.41 | Full | 3367.48 | 21,097 | 7,032 | 28,130 | 59.76 | |
| " | WI-3 | 139.37 | 185.08 | 139.49 | 4.9 | 45.59 | Full | 4831.60 | 30,270 | 10,090 | 40,360 | 53.43 | |
| " | WI-2 | 140.14 | 185.04 | 140.14 | 4.9 | 44.90 | Full | 4685.18 | 29,353 | 9,784 | 39,137 | 48.13 | |
| " | Int-54 | NA | 184.43 | 158.38 | 4.9 | 26.05 | Full | 2269.39 | 14,218 | 4,739 | 18,957 | 32.02 | |
| " | Int-57 | NA | 184.71 | 154.30 | 4.9 | 30.41 | Full | 4465.57 | 27,977 | 9,326 | 37,303 | 53.98 | |
| 12/18/09 | Int-52 | 146.67 | 155.58 | 146.67 | 4.9 | 8.91 | Full | 1610.53 | 10,090 | 3,363 | 13,453 | 76.87 | |
| " | Int-53 | 145.95 | 156.27 | 145.95 | 4.9 | 10.32 | Full | 1390.91 | 8,714 | 2,905 | 11,619 | 53.18 | |
| " | Int-51 | 143.96 | 154.42 | 143.96 | 4.9 | 10.46 | Full | 1390.91 | 8,714 | 2,905 | 11,619 | 67.04 | |
| " | Int-58 | NA | 185.35 | 150.57 | 4.9 | 34.78 | Full | 3221.06 | 20,180 | 6,727 | 26,907 | 36.54 | |
| " | Int-61 | NA | 185.57 | 150.70 | 4.9 | 34.87 | Full | 3513.89 | 22,015 | 7,338 | 29,353 | 39.76 | |
| " | Int-55 | NA | 185.46 | 152.32 | 4.9 | 33.14 | Full | 3147.86 | 19,722 | 6,574 | 26,295 | 34.91 | |
| " | Int-56 | NA | 185.30 | 152.27 | 4.9 | 33.03 | Full | 3074.65 | 19,263 | 6,421 | 25,684 | 36.73 | |
| 12/21/09 | WI-1 | 139.60 | 154.28 | 139.60 | 4.9 | 14.68 | Full | 2049.77 | 12,842 | 4,281 | 17,123 | 64.40 | Grout surfaced near north perimeter fence and flowed onto the sidewalk. |
| " | Int-320 | NA | 185.71 | 155.96 | 4.9 | 29.75 | Full | 2855.03 | 17,887 | 5,962 | 23,849 | 35.27 | |
| " | Int-319 | NA | 186.00 | 156.80 | 4.9 | 29.20 | Full | 2781.83 | 17,428 | 5,809 | 23,238 | 35.02 | |
| " | Int-321 | NA | 185.90 | 156.01 | 4.9 | 29.89 | Full | 2708.62 | 16,970 | 5,657 | 22,626 | 33.31 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | (GAL) | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 12/22/09 | Int-305 | 161.49 | 175.03 | 161.49 | 4.9 | 13.54 | Full | 1903.36 | 11,925 | 3,975 | 15,900 | 51.67 | |
| " | Int-304 | 161.36 | 174.05 | 161.36 | 4.9 | 12.69 | Full | 1390.91 | 8,714 | 2,905 | 11,619 | 43.25 | |
| " | Int-306 | 163.11 | 173.53 | 163.11 | 4.9 | 10.42 | Full | 878.47 | 5,504 | 1,835 | 7,338 | 35.85 | |
| " | Int-307 | 163.17 | 186.12 | 163.17 | 4.9 | 22.95 | Full | 1976.56 | 12,383 | 4,128 | 16,511 | 33.98 | |
| " | Int-69 | NA | 186.00 | 157.10 | 4.9 | 28.90 | Full | 2562.21 | 16,052 | 5,351 | 21,403 | 32.59 | |
| " | Int-222 | 158.61 | 186.30 | 158.61 | 4.9 | 27.69 | Full | 2781.83 | 17,428 | 5,809 | 23,238 | 39.64 | |
| " | Int-223 | 155.35 | 165.77 | 155.35 | 4.9 | 10.42 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 58.21 | |
| 1/4/10 | Int-301 | 158.29 | 185.27 | 158.29 | 4.9 | 26.98 | Full | 2562.21 | 16,052 | 5,351 | 21,403 | 37.47 | |
| " | Int-302 | 158.92 | 169.96 | 158.92 | 4.9 | 11.04 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 64.23 | |
| " | Int-303 | 161.21 | 185.46 | 161.21 | 4.9 | 24.25 | Full | 2562.21 | 16,052 | 5,351 | 21,403 | 44.94 | |
| " | Int-300 | 163.74 | 185.64 | 163.53 | 4.9 | 22.11 | Full | 2196.18 | 13,759 | 4,586 | 18,346 | 42.24 | |
| 1/5/10 | Int-296 | 161.52 | 185.60 | 161.52 | 4.9 | 24.08 | Full | 2415.80 | 15,135 | 5,045 | 20,180 | 36.88 | |
| " | Int-297 | 162.40 | 171.69 | 162.38 | 4.9 | 9.31 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 59.47 | |
| " | Int-298 | 167.90 | 180.53 | 167.90 | 4.9 | 12.63 | Full | 1171.30 | 7,338 | 2,446 | 9,784 | 39.44 | |
| " | Int-299 | 168.50 | 183.71 | 168.50 | 4.9 | 15.21 | Full | 2269.39 | 14,218 | 4,739 | 18,957 | 63.46 | |
| " | Int-290 | 157.34 | 186.01 | 157.34 | 4.9 | 28.67 | Full | 2781.83 | 17,428 | 5,809 | 23,238 | 35.66 | |
| " | Int-291 | 160.10 | 169.12 | 160.10 | 4.9 | 9.02 | Full | 1024.88 | 6,421 | 2,140 | 8,561 | 48.32 | |
| " | Int-292 | 163.05 | 170.06 | 163.05 | 4.9 | 7.01 | Full | 1024.88 | 6,421 | 2,140 | 8,561 | 73.71 | |
| " | Int-293 | 168.25 | 185.65 | 168.25 | 4.9 | 17.40 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 37.58 | |
| " | Int-294 | 169.93 | 185.93 | 169.93 | 4.9 | 16.00 | Full | 1464.12 | 9,173 | 3,058 | 12,230 | 42.21 | |
| 1/6/10 | Int-285 | 153.57 | 164.62 | 153.57 | 4.9 | 11.05 | Full | 1610.53 | 10,090 | 3,363 | 13,453 | 57.51 | |
| " | Int-286 | 157.30 | 170.25 | 157.30 | 4.9 | 12.95 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 54.75 | |
| " | Int-287 | 165.84 | 186.29 | 165.84 | 4.9 | 20.45 | Full | 2122.97 | 13,301 | 4,434 | 17,734 | 52.34 | |
| " | Int-288 | 168.32 | 186.59 | 168.32 | 4.9 | 18.27 | Full | 1756.94 | 11,007 | 3,669 | 14,676 | 44.35 | |
| " | Int-289 | 169.48 | 186.49 | 170.32 | 4.9 | 16.17 | Full | 1317.71 | 8,256 | 2,752 | 11,007 | 34.66 | |
| " | Int-284 | 169.26 | 186.02 | 169.26 | 4.9 | 16.76 | Full | 1317.71 | 8,256 | 2,752 | 11,007 | 31.02 | |
| 1/7/09 | Int-224 | 157.35 | 164.90 | 157.43 | 4.9 | 7.47 | Full | 1171.30 | 7,338 | 2,446 | 9,784 | 61.87 | |
| " | Int-225 | 157.61 | 166.72 | 157.61 | 4.9 | 9.11 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 47.56 | |
| " | Int-226 | 158.37 | 166.61 | 158.37 | 4.9 | 8.24 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 52.58 | |
| " | Int-227 | 161.03 | 166.92 | 161.03 | 4.9 | 5.89 | Full | 878.47 | 5,504 | 1,835 | 7,338 | 58.85 | |
| " | Int-228 | 160.12 | 184.09 | 160.12 | 4.9 | 23.97 | Full | 2049.77 | 12,842 | 4,281 | 17,123 | 33.74 | |
| " | Int-229 | 161.87 | 186.32 | 161.87 | 4.9 | 24.45 | Full | 1976.56 | 12,383 | 4,128 | 16,511 | 31.90 | |
| " | Int-230 | 162.59 | 185.94 | 162.59 | 4.9 | 23.35 | Full | 1976.56 | 12,383 | 4,128 | 16,511 | 33.40 | |
| " | Int-231 | 163.63 | 186.62 | 163.63 | 4.9 | 22.99 | Full | 1903.36 | 11,925 | 3,975 | 15,900 | 32.67 | |
| " | Int-232 | 157.14 | 165.20 | 157.14 | 4.9 | 8.06 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 57.94 | |
| " | Int-233 | 156.69 | 166.23 | 156.69 | 4.9 | 9.54 | Full | 1317.71 | 8,256 | 2,752 | 11,007 | 63.71 | |
| " | Int-234 | 160.55 | 166.97 | 160.55 | 4.9 | 6.42 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 57.85 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added (GAL) | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 1/8/10 | Int-235 | 161.56 | 169.33 | 161.56 | 4.9 | 7.77 | Full | 878.47 | 5,504 | 1,835 | 7,338 | 52.15 | |
| " | Int-236 | 161.86 | 186.34 | 161.86 | 4.9 | 24.48 | Full | 2196.18 | 13,759 | 4,586 | 18,346 | 41.38 | |
| " | Int-237 | 164.10 | 170.72 | 164.10 | 4.9 | 6.62 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 56.10 | |
| " | Int-243 | 160.77 | 168.44 | 160.77 | 4.9 | 7.67 | Full | 1610.53 | 10,090 | 3,363 | 13,453 | 89.30 | |
| " | Int-238 | 165.12 | 186.24 | 165.12 | 4.9 | 21.12 | Full | 1683.74 | 10,549 | 3,516 | 14,065 | 36.77 | |
| " | Int-239 | 166.57 | 186.30 | 166.57 | 4.9 | 19.73 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 35.94 | |
| " | Int-317 | | 186.44 | 157.21 | 4.9 | 29.23 | Full | 2635.42 | 16,511 | 5,504 | 22,015 | 33.14 | |
| " | Int-240 | 158.62 | 186.11 | 158.62 | 4.9 | 27.49 | Full | 2415.80 | 15,135 | 5,045 | 20,180 | 37.37 | |
| " | Int-241 | 157.90 | 164.19 | 157.90 | 4.9 | 6.29 | Full | 951.68 | 5,962 | 1,987 | 7,950 | 69.78 | |
| " | Int-242 | 159.36 | 165.68 | 159.36 | 4.9 | 6.32 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 64.24 | |
| 1/11/10 | Int-244 | 161.59 | 185.49 | 161.59 | 4.9 | 23.90 | Full | 3367.48 | 21,097 | 7,032 | 28,130 | 64.99 | |
| " | Int-245 | 162.43 | 172.32 | 162.43 | 4.9 | 9.89 | Full | 1830.15 | 11,466 | 3,822 | 15,288 | 93.30 | |
| " | Int-246 | 164.14 | 167.97 | 164.14 | 4.9 | 3.83 | Full | 658.85 | 4,128 | 1,376 | 5,504 | 73.16 | |
| " | Int-247 | 163.35 | 186.01 | 163.35 | 4.9 | 22.66 | Full | 2122.97 | 13,301 | 4,434 | 17,734 | 39.85 | |
| " | Int-248 | 165.11 | 185.96 | 165.11 | 4.9 | 20.85 | Full | 1903.36 | 11,925 | 3,975 | 15,900 | 42.10 | |
| " | Int-249 | 159.12 | 186.67 | 159.12 | 4.9 | 27.55 | Full | 2415.80 | 15,135 | 5,045 | 20,180 | 40.44 | |
| " | Int-250 | 157.09 | 186.50 | 157.09 | 4.9 | 29.41 | Full | 2708.62 | 16,970 | 5,657 | 22,626 | 39.17 | |
| " | Int-251 | 166.09 | 186.25 | 157.09 | 4.9 | 29.16 | Full | 2708.62 | 16,970 | 5,657 | 22,626 | 39.50 | |
| 1/12/10 | Int-252 | 159.43 | 168.22 | 159.43 | 4.9 | 8.79 | Full | 1317.71 | 8,256 | 2,752 | 11,007 | 75.58 | |
| " | Int-253 | 159.72 | 168.28 | 159.72 | 4.9 | 8.56 | Full | 1024.88 | 6,421 | 2,140 | 8,561 | 55.22 | |
| " | Int-254 | 163.50 | 186.30 | 163.50 | 4.9 | 22.80 | Full | 1903.36 | 11,925 | 3,975 | 15,900 | 35.50 | |
| " | Int-255 | 163.90 | 186.63 | 163.90 | 4.9 | 22.73 | Full | 2196.18 | 13,759 | 4,586 | 18,346 | 44.56 | |
| " | Int-318 | NA | 186.89 | 156.32 | 4.9 | 30.57 | Full | 2708.62 | 16,970 | 5,657 | 22,626 | 40.87 | |
| " | Int-256 | 157.20 | 186.81 | 157.20 | 4.9 | 29.61 | Full | 2781.83 | 17,428 | 5,809 | 23,238 | 43.33 | |
| " | Int-257 | 160.61 | 170.64 | 160.61 | 4.9 | 10.03 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 50.50 | |
| " | Int-258 | 160.11 | 168.96 | 160.11 | 4.9 | 8.85 | Full | 951.68 | 5,962 | 1,987 | 7,950 | 49.60 | |
| " | Int-259 | 160.56 | 168.79 | 160.56 | 4.9 | 8.23 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 45.13 | |
| " | Int-260 | 162.60 | 187.06 | 162.68 | 4.9 | 24.38 | Full | 2122.97 | 13,301 | 4,434 | 17,734 | 40.16 | |
| " | Int-261 | 162.99 | 186.80 | 162.99 | 4.9 | 23.81 | Full | 1976.56 | 12,383 | 4,128 | 16,511 | 35.31 | |
| 1/13/10 | Int-262 | 159.32 | 167.48 | 159.32 | 4.9 | 8.16 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 57.23 | |
| " | Int-263 | 160.54 | 169.03 | 160.54 | 4.9 | 8.49 | Full | 951.68 | 5,962 | 1,987 | 7,950 | 47.67 | |
| " | Int-264 | 161.26 | 169.31 | 161.26 | 4.9 | 8.05 | Full | 878.47 | 5,504 | 1,835 | 7,338 | 46.41 | |
| " | Int-265 | 164.41 | 186.49 | 164.41 | 4.9 | 22.08 | Full | 1903.36 | 11,925 | 3,975 | 15,900 | 43.46 | |
| " | Int-266 | 165.21 | 186.19 | 165.21 | 4.9 | 20.98 | Full | 1610.53 | 10,090 | 3,363 | 13,453 | 32.65 | |
| " | Int-267 | 158.30 | 169.06 | 158.30 | 4.9 | 10.76 | Full | 1976.56 | 12,383 | 4,128 | 16,511 | 78.12 | |
| " | Int-268 | 153.22 | 164.76 | 153.22 | 4.9 | 11.54 | Full | 1610.53 | 10,090 | 3,363 | 13,453 | 59.35 | |
| " | Int-350 | 156.41 | 186.68 | 156.41 | 4.9 | 30.27 | Full | 2855.03 | 17,887 | 5,962 | 23,849 | 47.55 | |
| " | Int-269 | 158.33 | 167.24 | 158.33 | 4.9 | 8.91 | Full | 1024.88 | 6,421 | 2,140 | 8,561 | 48.92 | |
| " | Int-270 | 159.72 | 169.29 | 159.72 | 4.9 | 9.57 | Full | 951.68 | 5,962 | 1,987 | 7,950 | 45.87 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added (GAL) | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 1/14/10 | Int-272 | 163.85 | 186.67 | 163.85 | 4.9 | 22.82 | Full | 1830.15 | 11,466 | 3,822 | 15,288 | 36.99 | |
| " | Int-271 | 164.91 | 186.79 | 163.41 | 4.9 | 23.38 | Full | 1756.94 | 11,007 | 3,669 | 14,676 | 34.66 | |
| " | Int-273 | 153.04 | 165.49 | 153.04 | 4.9 | 12.45 | Full | 1756.94 | 11,007 | 3,669 | 14,676 | 60.02 | |
| " | Int-274 | 155.31 | 186.70 | 155.31 | 4.9 | 31.39 | Full | 3001.45 | 18,804 | 6,268 | 25,072 | 40.67 | |
| " | Int--275 | 156.82 | 168.72 | 156.82 | 4.9 | 11.90 | Full | 1390.91 | 8,714 | 2,905 | 11,619 | 58.93 | |
| " | Int-276 | 161.66 | 166.77 | 161.66 | 4.9 | 5.11 | Full | 439.24 | 2,752 | 917 | 3,669 | 39.65 | |
| " | Int-277 | 165.08 | 186.83 | 165.08 | 4.9 | 21.75 | Full | 1756.94 | 11,007 | 3,669 | 14,676 | 34.35 | |
| " | Int-351 | 164.89 | 186.80 | 164.89 | 4.9 | 21.91 | Full | 1683.74 | 10,549 | 3,516 | 14,065 | 35.44 | |
| " | Int-352 | 164.33 | 186.84 | 164.33 | 4.9 | 22.51 | Full | 1830.15 | 11,466 | 3,822 | 15,288 | 37.50 | |
| 1/15/10 | Int-279 | 153.98 | 164.89 | 153.98 | 4.9 | 10.91 | Full | 1683.74 | 10,549 | 3,516 | 14,065 | 71.18 | |
| " | Int-280 | 156.47 | 165.74 | 156.47 | 4.9 | 9.27 | Full | 1171.30 | 7,338 | 2,446 | 9,784 | 70.19 | |
| " | Int-281 | 161.63 | 186.68 | 161.63 | 4.9 | 25.05 | Full | 2049.77 | 12,842 | 4,281 | 17,123 | 45.45 | |
| " | Int-282 | 166.15 | 186.70 | 166.15 | 4.9 | 20.55 | Full | 1976.56 | 12,383 | 4,128 | 16,511 | 53.43 | |
| " | Int-283 | 167.71 | 186.60 | 167.71 | 4.9 | 18.89 | Full | 1464.12 | 9,173 | 3,058 | 12,230 | 43.05 | |
| " | Int-278 | 167.75 | 186.67 | 167.75 | 4.9 | 18.92 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 40.97 | |
| " | Int-295 | 169.03 | 186.34 | 169.03 | 4.9 | 17.31 | Full | 1464.12 | 9,173 | 3,058 | 12,230 | 39.01 | |
| 1/18/10 | JGW-1-S | 138.42 | 178.83 | 139.92 | 4 | 38.91 | Panel | 2342.59 | 14,676 | 4,892 | 19,569 | NA | JGW-1 has only one segment |
| " | JGW-3-W | 139.50 | 184.70 | 141.00 | 4 | 43.70 | Panel | 2489.00 | 15,594 | 5,198 | 20,792 | NA | |
| " | JGW-3-E | 139.50 | 184.73 | 141.00 | 4 | 43.73 | Panel | 3733.51 | 23,391 | 7,797 | 31,188 | NA | |
| 1/19/10 | JGW-5-W | 140.58 | 185.58 | 142.08 | 4 | 43.50 | Panel | 2415.80 | 15,135 | 5,045 | 20,180 | NA | |
| " | JGW-5-E | 140.58 | 185.65 | 142.08 | 4 | 43.57 | Panel | 2635.42 | 16,511 | 5,504 | 22,015 | NA | |
| " | JGW-7-W | 147.75 | 185.67 | 149.25 | 4 | 36.42 | Panel | 1830.15 | 11,466 | 3,822 | 15,288 | NA | |
| " | JGW-7-E | 147.75 | 185.64 | 149.25 | 4 | 36.39 | Panel | 1830.15 | 11,466 | 3,822 | 15,288 | NA | |
| " | JGW-9-W | 147.48 | 185.80 | 148.98 | 4 | 36.82 | Panel | 1903.36 | 11,925 | 3,975 | 15,900 | NA | |
| " | JGW-9-E | 147.48 | 185.73 | 148.98 | 4 | 36.75 | Panel | 1903.36 | 11,925 | 3,975 | 15,900 | NA | |
| " | JGW-11-W | 150.87 | 186.23 | 150.87 | 4 | 35.36 | Panel | 1903.36 | 11,925 | 3,975 | 15,900 | NA | |
| " | JGW-11-E | 150.87 | 186.36 | 152.37 | 4 | 33.99 | Panel | 1756.94 | 11,007 | 3,669 | 14,676 | NA | |
| " | JGW-13-W | 155.99 | 185.15 | 157.49 | 4 | 27.66 | Panel | 1244.50 | 7,797 | 2,599 | 10,396 | NA | |
| " | JGW-13-E | 155.99 | 185.18 | 157.49 | 4 | 27.69 | Panel | 1317.71 | 8,256 | 2,752 | 11,007 | NA | |
| " | JGW-15-W | 159.96 | 185.51 | 161.46 | 4 | 24.05 | Panel | 1024.88 | 6,421 | 2,140 | 8,561 | NA | |
| " | JGW-15-E | 159.96 | 185.02 | 161.46 | 4 | 23.56 | Panel | 1024.88 | 6,421 | 2,140 | 8,561 | NA | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added (GAL) | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 1/20/10 | JGW-2-S | 138.13 | 179.59 | 139.63 | 4 | 39.96 | Panel | 2562.21 | 16,052 | 5,351 | 21,403 | NA | |
| " | JGW-2-E | 138.13 | 179.59 | 139.63 | 4 | 39.96 | Panel | 2269.39 | 14,218 | 4,739 | 18,957 | NA | |
| " | JGW-4-W | 141.84 | 185.53 | 143.34 | 4 | 42.19 | Panel | 2855.03 | 17,887 | 5,962 | 23,849 | NA | |
| " | JGW-4-E | 141.84 | 185.53 | 143.34 | 4 | 42.19 | Panel | 2196.18 | 13,759 | 4,586 | 18,346 | NA | |
| " | JGW-6-W | 146.14 | 185.84 | 147.64 | 4 | 38.20 | Panel | 1976.56 | 12,383 | 4,128 | 16,511 | NA | |
| " | JGW-6-E | 146.14 | 185.80 | 147.64 | 4 | 38.16 | Panel | 1903.36 | 11,925 | 3,975 | 15,900 | NA | |
| " | JGW-8-W | 149.46 | 184.56 | 150.96 | 4 | 33.60 | Panel | 1756.94 | 11,007 | 3,669 | 14,676 | NA | |
| " | JGW-8-E | 149.46 | 184.56 | 150.96 | 4 | 33.60 | Panel | 1683.74 | 10,549 | 3,516 | 14,065 | NA | |
| " | JGW-10-W | 150.74 | 184.49 | 152.24 | 4 | 32.25 | Panel | 1537.33 | 9,631 | 3,210 | 12,842 | NA | |
| " | JGW-10-E | 150.74 | 184.55 | 152.24 | 4 | 32.31 | Panel | 1537.33 | 9,631 | 3,210 | 12,842 | NA | |
| " | JGW-12-W | 152.42 | 184.69 | 153.92 | 4 | 30.77 | Panel | 1537.33 | 9,631 | 3,210 | 12,842 | NA | |
| " | JGW-12-E | 152.42 | 184.69 | 153.92 | 4 | 30.77 | Panel | 1610.53 | 10,090 | 3,363 | 13,453 | NA | |
| 1/21/10 | JGW-14-W | 157.49 | 184.75 | 158.99 | 4 | 25.76 | Panel | 1171.30 | 7,338 | 2,446 | 9,784 | NA | |
| " | JGW-14-E | 157.49 | 184.91 | 158.99 | 4 | 25.92 | Panel | 1171.30 | 7,338 | 2,446 | 9,784 | NA | |
| " | JGW-17-W | 163.84 | 184.86 | 163.34 | 4 | 21.52 | Panel | 805.27 | 5,045 | 1,682 | 6,727 | NA | |
| " | JGW-17-E | 163.84 | 185.06 | 163.34 | 4 | 21.72 | Panel | 878.47 | 5,504 | 1,835 | 7,338 | NA | |
| " | JGW-19-W | 168.31 | 185.44 | 167.79 | 4 | 17.65 | Panel | 732.06 | 4,586 | 1,529 | 6,115 | NA | |
| " | JGW-19-E | 168.31 | 185.44 | 167.79 | 4 | 17.65 | Panel | 658.85 | 4,128 | 1,376 | 5,504 | NA | |
| " | Int-214 | 157.36 | 185.07 | 157.36 | 4.9 | 27.71 | Full | 2635.42 | 16,511 | 5,504 | 22,015 | 37.52 | |
| " | Int-215 | 157.52 | 163.55 | 157.52 | 4.9 | 6.03 | Full | 732.06 | 4,586 | 1,529 | 6,115 | 55.99 | |
| " | Int-216 | 157.70 | 163.59 | 157.70 | 4.9 | 5.89 | Full | 732.06 | 4,586 | 1,529 | 6,115 | 57.33 | |
| " | Int-217 | 158.31 | 163.68 | 158.31 | 4.9 | 5.37 | Full | 658.85 | 4,128 | 1,376 | 5,504 | 56.59 | |
| " | Int-218 | 159.16 | 165.78 | 159.16 | 4.9 | 6.62 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 56.10 | |
| " | Int-219 | 159.58 | 167.99 | 159.58 | 4.9 | 8.41 | Full | 878.47 | 5,504 | 1,835 | 7,338 | 48.18 | |
| 1/22/10 | Int-220 | 163.04 | 185.80 | 163.04 | 4.9 | 22.76 | Full | 2122.97 | 13,301 | 4,434 | 17,734 | 47.03 | |
| " | Int-221 | 161.90 | 185.74 | 161.90 | 4.9 | 23.84 | Full | 1976.56 | 12,383 | 4,128 | 16,511 | 38.24 | |
| " | Int-211 | 162.49 | 186.36 | 162.49 | 4.9 | 23.87 | Full | 1903.36 | 11,925 | 3,975 | 15,900 | 31.46 | |
| " | Int-212 | 160.99 | 186.00 | 160.99 | 4.9 | 25.01 | Full | 2122.97 | 13,301 | 4,434 | 17,734 | 36.10 | |
| " | Int-213 | 163.87 | 176.16 | 163.87 | 4.9 | 12.29 | Full | 1756.94 | 11,007 | 3,669 | 14,676 | 65.94 | |
| " | JGW-16-W | 160.38 | 183.83 | 161.88 | 4.9 | 21.95 | Panel | 951.68 | 5,962 | 1,987 | 7,950 | NA | |
| " | JGW-16-E | 160.38 | 183.76 | 161.88 | 4.9 | 21.88 | Panel | 1024.88 | 6,421 | 2,140 | 8,561 | NA | |
| " | JGW-18-W | 166.00 | 184.07 | 167.50 | 4.9 | 16.57 | Panel | 658.85 | 4,128 | 1,376 | 5,504 | NA | |
| " | JGW-18-E | 166.00 | 183.94 | 167.50 | 4.9 | 16.44 | Panel | 658.85 | 4,128 | 1,376 | 5,504 | NA | |
| " | JGW-20-W | 167.99 | 184.42 | 169.49 | 4.9 | 14.93 | Panel | 732.06 | 4,586 | 1,529 | 6,115 | NA | |
| " | JGW-20-E | 167.99 | 184.48 | 169.49 | 4.9 | 14.99 | Panel | 585.65 | 3,669 | 1,223 | 4,892 | NA | |
| 1/25/10 | Int-187 | 154.97 | 185.62 | 154.97 | 4.9 | 30.65 | Full | 2855.03 | 17,887 | 5,962 | 23,849 | 34.24 | |
| " | Int-188 | 154.63 | 185.53 | 154.63 | 4.9 | 30.90 | Full | 2708.62 | 16,970 | 5,657 | 22,626 | 34.59 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added (GAL) | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 1/26/10 | Int-189 | 156.48 | 185.53 | 156.48 | 4.9 | 29.05 | Full | 2562.21 | 16,052 | 5,351 | 21,403 | 44.47 | |
| " | Int-190 | 156.16 | 166.09 | 156.16 | 4.9 | 9.93 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 51.00 | |
| " | Int-191 | 156.07 | 166.75 | 156.07 | 4.9 | 10.68 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 47.42 | |
| " | Int-192 | 156.45 | 166.24 | 156.45 | 4.9 | 9.79 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 51.73 | |
| " | Int-193 | 157.86 | 168.15 | 157.86 | 4.9 | 10.29 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 49.22 | |
| " | Int-194 | 159.63 | 173.33 | 159.63 | 4.9 | 13.70 | Full | 1244.50 | 7,797 | 2,599 | 10,396 | 41.90 | |
| " | Int-195 | 163.04 | 174.09 | 163.04 | 4.9 | 11.05 | Full | 878.47 | 5,504 | 1,835 | 7,338 | 36.67 | |
| " | Int-196 | 163.74 | 185.49 | 163.74 | 4.9 | 21.75 | Full | 1683.74 | 10,549 | 3,516 | 14,065 | 35.71 | |
| " | Int-197 | 164.26 | 173.34 | 164.26 | 4.9 | 9.08 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 55.78 | |
| " | Int-198 | 156.83 | 185.64 | 156.83 | 4.9 | 28.81 | Full | 2562.21 | 16,052 | 5,351 | 21,403 | 41.02 | |
| " | Int-199 | 157.24 | 164.58 | 157.24 | 4.9 | 7.34 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 50.60 | |
| " | Int-200 | 157.42 | 165.74 | 157.42 | 4.9 | 8.32 | Full | 1244.50 | 7,797 | 2,599 | 10,396 | 68.99 | |
| 1/27/10 | Int-201 | 156.68 | 167.08 | 156.68 | 4.9 | 10.40 | Full | 1171.30 | 7,338 | 2,446 | 9,784 | 51.95 | |
| " | Int-202 | 158.52 | 168.57 | 158.52 | 4.9 | 10.05 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 50.40 | |
| " | Int-203 | 160.06 | 168.78 | 160.06 | 4.9 | 8.72 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 42.59 | |
| " | Int-204 | 162.35 | 173.04 | 162.35 | 4.9 | 10.69 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 34.74 | |
| " | Int-205 | 162.65 | 172.87 | 162.65 | 4.9 | 10.22 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 36.34 | |
| " | Int-206 | 162.94 | 186.02 | 162.94 | 4.9 | 23.08 | Full | 1830.15 | 11,466 | 3,822 | 15,288 | 36.57 | |
| " | Int-207 | 162.42 | 186.47 | 162.42 | 4.9 | 24.05 | Full | 2049.77 | 12,842 | 4,281 | 17,123 | 42.97 | |
| " | Int-208 | 157.79 | 164.69 | 157.79 | 4.9 | 6.90 | Full | 951.68 | 5,962 | 1,987 | 7,950 | 69.54 | |
| " | Int-209 | 158.40 | 164.76 | 158.40 | 4.9 | 6.36 | Full | 878.47 | 5,504 | 1,835 | 7,338 | 76.72 | |
| " | Int-210 | 158.05 | 164.70 | 158.05 | 4.9 | 6.65 | Full | 878.47 | 5,504 | 1,835 | 7,338 | 73.38 | |
| " | Int-68 | 157.23 | 185.83 | 157.23 | 4.9 | 28.60 | Full | 2415.80 | 15,135 | 5,045 | 20,180 | 31.05 | |
| 1/28/10 | Int-67 | 155.66 | 185.84 | 157.16 | 4.9 | 28.68 | Full | 2562.21 | 16,052 | 5,351 | 21,403 | 32.84 | |
| " | XO-3 | 141.66 | 185.48 | 141.66 | 4.9 | 43.82 | Full | 4392.36 | 27,518 | 9,173 | 36,691 | 36.84 | Grout spill onto sidewalk |
| " | XO-1 | 141.09 | 185.43 | 141.09 | 4.9 | 44.34 | Full | 4392.36 | 27,518 | 9,173 | 36,691 | 39.08 | Grout spill onto sidewalk |
| 1/29/10 | XO-5 | 142.99 | 186.85 | 142.99 | 4.9 | 43.86 | Full | 4538.77 | 28,436 | 9,479 | 37,914 | 40.83 | Grout spill onto sidewalk |
| " | XO-7 | 146.29 | 186.31 | 146.29 | 4.9 | 40.02 | Full | 4026.33 | 25,225 | 8,408 | 33,634 | 39.70 | Grout spill onto sidewalk |
| 2/1/10 | XO-9 | 149.63 | 183.94 | 149.63 | 4.9 | 34.31 | Full | 3367.48 | 21,097 | 7,032 | 28,130 | 36.08 | |
| " | XO-11 | 153.62 | 183.93 | 153.62 | 4.9 | 30.31 | Full | 3001.45 | 18,804 | 6,268 | 25,072 | 36.40 | |
| " | XO-13 | 158.65 | 184.20 | 158.65 | 4.9 | 25.55 | Full | 3221.06 | 20,180 | 6,727 | 26,907 | 46.34 | |
| " | XO-15 | 164.20 | 184.36 | 164.20 | 4.9 | 20.16 | Full | 1756.94 | 11,007 | 3,669 | 14,676 | 32.03 | |
| " | XO-17 | 167.67 | 184.55 | 167.67 | 4.9 | 16.88 | Full | 1244.50 | 7,797 | 2,599 | 10,396 | 27.10 | |
| 2/2/10 | XO-2 | 142.00 | 185.13 | 142.00 | 4.9 | 43.13 | Full | 4392.36 | 27,518 | 9,173 | 36,691 | 37.43 | Grout spill onto sidewalk |
| " | XO-4 | 142.77 | 184.36 | 142.77 | 4.9 | 41.59 | Full | 4245.95 | 26,601 | 8,867 | 35,468 | 43.42 | |
| " | XO-16 | 164.64 | 183.82 | 164.64 | 4.9 | 19.18 | Full | 1976.56 | 12,383 | 4,128 | 16,511 | 43.83 | |
| " | XO-14 | 160.08 | 183.82 | 160.08 | 4.9 | 23.74 | Full | 2122.97 | 13,301 | 4,434 | 17,734 | 38.03 | |
| " | XO-12 | 156.46 | 184.04 | 156.46 | 4.9 | 27.58 | Full | 2489.00 | 15,594 | 5,198 | 20,792 | 38.38 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added (GAL) | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 2/3/10 | Int-186 | 162.72 | 185.43 | 162.72 | 4.9 | 22.71 | Full | 1756.94 | 11,007 | 3,669 | 14,676 | 30.52 | |
| " | Int-185 | 165.00 | 185.11 | 165.00 | 4.9 | 20.11 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 35.26 | |
| " | Int-179 | 166.94 | 185.45 | 166.94 | 4.9 | 18.51 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 30.53 | |
| " | Int-180 | 166.90 | 186.40 | 166.90 | 4.9 | 19.50 | Full | 1683.74 | 10,549 | 3,516 | 14,065 | 36.72 | |
| " | Int-184 | 167.28 | 185.59 | 167.28 | 4.9 | 18.31 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 38.73 | |
| " | Int-178 | 165.65 | 171.61 | 165.65 | 4.9 | 5.96 | Full | 658.85 | 4,128 | 1,376 | 5,504 | 47.01 | |
| " | Int-183 | 167.01 | 172.48 | 167.01 | 4.9 | 5.47 | Full | 585.65 | 3,669 | 1,223 | 4,892 | 53.98 | |
| " | Int-177 | 165.46 | 172.53 | 165.46 | 4.9 | 7.07 | Full | 878.47 | 5,504 | 1,835 | 7,338 | 52.84 | |
| 2/4/10 | Int-181 | 160.80 | 184.61 | 160.80 | 4.9 | 23.81 | Full | 1830.15 | 11,466 | 3,822 | 15,288 | 30.33 | |
| " | Int-182 | 165.87 | 184.78 | 165.87 | 4.9 | 18.91 | Full | 1464.12 | 9,173 | 3,058 | 12,230 | 43.01 | |
| " | Int-176 | 161.16 | 184.91 | 161.16 | 4.9 | 23.75 | Full | 1756.94 | 11,007 | 3,669 | 14,676 | 34.12 | |
| " | Int-175 | 160.64 | 184.79 | 160.64 | 4.9 | 24.15 | Full | 1976.56 | 12,383 | 4,128 | 16,511 | 34.81 | |
| " | XO-10 | 151.97 | 182.63 | 151.97 | 4.9 | 30.66 | Full | 2781.83 | 17,428 | 5,809 | 23,238 | 38.59 | |
| " | XO-8 | 149.22 | 182.15 | 149.22 | 4.9 | 32.93 | Full | 2928.24 | 18,346 | 6,115 | 24,461 | 37.82 | Grout spill onto sidewalk |
| " | XO-6 | 147.07 | 183.10 | 147.07 | 4.9 | 36.03 | Full | 3879.92 | 24,308 | 8,103 | 32,411 | 45.80 | Grout spill onto sidewalk |
| 2/5/10 | XI-2 | 140.25 | 184.25 | 140.25 | 4.9 | 44.00 | Full | 4831.60 | 30,270 | 10,090 | 40,360 | 46.70 | |
| " | XI-3 | 143.99 | 152.65 | 143.99 | 4.9 | 8.66 | Full | 1464.12 | 9,173 | 3,058 | 12,230 | 77.98 | |
| " | XI-4 | 143.56 | 182.06 | 143.56 | 4.9 | 38.50 | Full | 4245.95 | 26,601 | 8,867 | 35,468 | 50.87 | |
| " | XI-5 | 145.14 | 184.41 | 144.50 | 4.9 | 39.91 | Full | 4245.95 | 26,601 | 8,867 | 35,468 | 49.07 | |
| 2/11/10 | JGW-21-W | 167.35 | 185.05 | 167.35 | 4.9 | 17.70 | Panel | NA | NA | NA | NA | NA | |
| " | JGW-21-E | 167.35 | 185.27 | 167.35 | 4.9 | 17.92 | Panel | NA | NA | NA | NA | NA | |
| " | XI-6 | 146.78 | 184.91 | 146.78 | 4.9 | 38.13 | Full | 4172.74 | 26,142 | 8,714 | 34,857 | 46.54 | |
| 2/12/10 | XI-1 | 141.28 | 149.68 | 141.28 | 4.9 | 8.40 | Full | 1610.53 | 10,090 | 3,363 | 13,453 | 106.50 | |
| " | JGW-22 | 170.33 | 184.46 | 170.33 | 4.9 | 14.13 | Panel | 732.06 | 4,586 | 1,529 | 6,115 | NA | Grout spill onto sidewalk |
| " | XI-7 | 147.74 | 156.03 | 147.74 | 4.9 | 8.29 | Full | 1317.71 | 8,256 | 2,752 | 11,007 | 73.31 | |
| " | XI-8 | 149.31 | 156.61 | 149.31 | 4.9 | 7.30 | Full | 1171.30 | 7,338 | 2,446 | 9,784 | 80.89 | |
| " | XI-9 | 150.12 | 157.30 | 150.12 | 4.9 | 7.18 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 77.11 | |
| 2/15/10 | XI-10 | 153.44 | 157.69 | 153.44 | 4.9 | 4.25 | Full | 878.47 | 5,504 | 1,835 | 7,338 | 104.21 | |
| " | XI-11 | 155.89 | 161.78 | 155.89 | 4.9 | 5.89 | Full | 878.47 | 5,504 | 1,835 | 7,338 | 75.19 | |
| " | XI-12 | 157.98 | 161.71 | 157.98 | 4.9 | 3.73 | Full | 658.85 | 4,128 | 1,376 | 5,504 | 89.05 | |
| " | XI-13 | 159.90 | 165.01 | 159.90 | 4.9 | 5.11 | Full | 732.06 | 4,586 | 1,529 | 6,115 | 66.08 | |
| " | XI-14 | 162.86 | 165.67 | 162.86 | 4.9 | 2.81 | Full | 439.24 | 2,752 | 917 | 3,669 | 78.81 | |
| " | XI-15 | 164.08 | 168.40 | 164.08 | 4.9 | 4.32 | Full | 732.06 | 4,586 | 1,529 | 6,115 | 85.44 | |
| " | XI-16 | 167.28 | 170.36 | 167.28 | 4.9 | 3.08 | Full | 439.24 | 2,752 | 917 | 3,669 | 79.22 | |
| " | XO-18 | 170.02 | 184.87 | 169.43 | 4.9 | 15.44 | Full | 2342.59 | 14,676 | 4,892 | 19,569 | 64.53 | Grout spill onto sidewalk |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | (GAL) | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 2/16/10 | XO-19 | 170.60 | 184.88 | 168.48 | | 16.40 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 43.24 | |
| " | INT-62 | NA | 185.63 | 150.49 | 4.9 | 35.14 | Full | 3587.09 | 22,473 | 7,491 | 29,964 | 56.70 | |
| | INT-63 | NA | 188.45 | 150.43 | | 38.02 | Full | 3733.51 | 23,391 | 7,797 | 31,188 | 41.76 | |
| " | INT-59 | NA | 185.44 | 154.07 | 4.9 | 31.37 | Full | 3221.06 | 20,180 | 6,727 | 26,907 | 47.36 | |
| 2/17/10 | INT-60 | 149.28 | 185.63 | 149.28 | 4.9 | 36.35 | Full | 4099.54 | 25,684 | 8,561 | 34,245 | 41.45 | |
| " | INT-64 | " | 184.96 | 153.20 | 4.9 | 31.76 | Full | 3074.65 | 19,263 | 6,421 | 25,684 | 41.17 | |
| " | INT-353 | 154.16 | 185.16 | 154.16 | 4.9 | 31.00 | Full | 2928.24 | 18,346 | 6,115 | 24,461 | 40.17 | |
| " | XI-17 | 168.38 | 178.38 | 168.38 | 4.9 | 10.00 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 61.00 | |
| " | XI-18 | 169.46 | 171.98 | 169.46 | 4.9 | 2.52 | Full | 439.24 | 2,752 | 917 | 3,669 | 96.82 | |
| " | XI-19 | 169.15 | 184.86 | 169.15 | 4.9 | 15.71 | Full | 2122.97 | 13,301 | 4,434 | 17,734 | 68.13 | |
| 2/18/10 | INT-65 | NA | 185.07 | 156.64 | 4.9 | 28.43 | Full | 2708.62 | 16,970 | 5,657 | 22,626 | 35.02 | |
| " | INT-354 | NA | 184.74 | 159.66 | 4.9 | 25.08 | Full | 2122.97 | 13,301 | 4,434 | 17,734 | 36.00 | |
| " | INT-174 | 160.86 | 166.78 | 160.74 | 4.9 | 6.04 | Full | 658.85 | 4,128 | 1,376 | 5,504 | 46.39 | |
| " | INT-66 | NA | 184.58 | 157.08 | 4.9 | 27.50 | Full | 2635.42 | 16,511 | 5,504 | 22,015 | 37.81 | |
| 2/19/10 | XO-20 | NA | 184.54 | 170.36 | 4.9 | 14.18 | Full | 1244.50 | 7,797 | 2,599 | 10,396 | 37.33 | |
| " | XI-20 | 170.32 | 184.42 | 170.32 | 4.9 | 14.10 | Full | 1171.30 | 7,338 | 2,446 | 9,784 | 35.33 | |
| 2/22/10 | NO-25 | 167.04 | 175.58 | 167.04 | 4.9 | 8.54 | Half | 1024.88 | 6,421 | 2,140 | 8,561 | 94.70 | |
| " | NO-26 | 168.05 | 176.12 | 168.05 | 4.9 | 8.07 | Half | 658.85 | 4,128 | 1,376 | 5,504 | 69.44 | |
| " | NO-27 | 169.29 | 176.39 | 169.29 | 4.9 | 7.10 | Half | 658.85 | 4,128 | 1,376 | 5,504 | 78.93 | |
| " | XO-22 | 170.85 | 184.16 | 170.85 | 4.9 | 13.31 | Half | 1098.09 | 6,880 | 2,293 | 9,173 | 60.65 | |
| " | XO-23 | 170.94 | 183.66 | 170.94 | 4.9 | 12.72 | Half | 1098.09 | 6,880 | 2,293 | 9,173 | 68.12 | |
| " | XO-24 | 170.78 | 184.03 | 170.78 | 4.9 | 13.25 | Half | 1683.74 | 10,549 | 3,516 | 14,065 | 100.28 | |
| 2/23/10 | XO-25 | 170.09 | 184.14 | 170.09 | 4.9 | 14.05 | Half | 1464.12 | 9,173 | 3,058 | 12,230 | 82.23 | |
| " | NO-23 | 169.63 | 176.69 | 169.63 | 4.9 | 7.06 | Half | 585.65 | 3,669 | 1,223 | 4,892 | 65.46 | |
| " | NO-24 | 168.85 | 175.17 | 168.85 | 4.9 | 6.32 | Half | 439.24 | 2,752 | 917 | 3,669 | 59.12 | |
| " | NO-28 | 169.41 | 176.21 | 169.41 | 4.9 | 6.80 | Half | 585.65 | 3,669 | 1,223 | 4,892 | | |
| " | NO-29A | - | - | - | - | - | - | - | - | - | - | - | |
| " | NO-29B | 171.16 | 183.88 | 171.16 | 4.9 | 12.72 | Half | 1098.09 | 6,880 | 2,293 | 9,173 | 63.46 | |
| " | NO-30 | 171.83 | 176.80 | 171.83 | 4.9 | 4.97 | Half | 585.65 | 3,669 | 1,223 | 4,892 | 92.99 | |
| " | NO-31 | 170.85 | 177.11 | 170.85 | 4.9 | 6.26 | Half | 585.65 | 3,669 | 1,223 | 4,892 | 73.82 | |
| " | NO-32 | 169.77 | 177.27 | 169.77 | 4.9 | 7.50 | Half | 951.68 | 5,962 | 1,987 | 7,950 | 100.13 | |
| " | NO-33 | 169.14 | 179.76 | 169.14 | 4.9 | 10.62 | Half | 1024.88 | 6,421 | 2,140 | 8,561 | 76.15 | |
| " | NO-34 | 169.38 | 180.54 | 169.38 | 4.9 | 11.16 | Half | 951.68 | 5,962 | 1,987 | 7,950 | 67.29 | |
| 2/24/2010 | NO-35 | 169.91 | 181.50 | 169.91 | 4.9 | 11.59 | Half | 878.47 | 5,504 | 1,835 | 7,338 | 59.81 | |
| " | NO-36 | 169.99 | 181.63 | 169.99 | 4.9 | 11.64 | Half | 878.47 | 5,504 | 1,835 | 7,338 | 59.55 | |
| " | NO-37 | 169.96 | 181.49 | 169.96 | 4.9 | 11.53 | Half | 951.68 | 5,962 | 1,987 | 7,950 | 65.13 | |
| " | EO-17 | 171.16 | 181.36 | 171.16 | 4.9 | 10.20 | Half | 805.27 | 5,045 | 1,682 | 6,727 | 58.04 | |
| " | EO-16 | 168.54 | 184.04 | 168.54 | 4.9 | 15.50 | Half | 1244.50 | 7,797 | 2,599 | 10,396 | 63.36 | |
| " | EO-15 | 170.13 | 183.52 | 170.13 | 4.9 | 13.39 | Half | 1244.50 | 7,797 | 2,599 | 10,396 | 73.34 | |
| " | EO-14 | 168.80 | 183.70 | 168.80 | 4.9 | 14.90 | Half | 1390.91 | 8,714 | 2,905 | 11,619 | 73.66 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added (GAL) | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 3/1/2010 | EO-12 | 168.19 | 184.11 | 168.19 | 4.9 | 15.92 | Half | 1976.56 | 12,383 | 4,128 | 16,511 | 91.27 | |
| " | EO-11 | 168.61 | 183.71 | 168.61 | 4.9 | 15.10 | Half | 1464.12 | 9,173 | 3,058 | 12,230 | 76.51 | |
| " | EO-11A | 171.63 | 181.53 | 171.63 | 4.9 | 9.90 | Half | 805.27 | 5,045 | 1,682 | 6,727 | 64.19 | |
| " | EO-13 | 169.65 | 185.42 | 169.65 | 4.9 | 15.77 | Half | 1317.71 | 8,256 | 2,752 | 11,007 | 71.07 | |
| " | EO-11B | 167.36 | 182.64 | 167.36 | 4.9 | 15.28 | Half | 1171.30 | 7,338 | 2,446 | 9,784 | 60.49 | |
| " | EO-18 | 176.88 | 183.27 | 176.88 | 4.9 | 6.39 | Half | 512.44 | 3,210 | 1,070 | 4,281 | 63.28 | |
| " | EO-19 | 176.87 | 183.64 | 176.87 | 4.9 | 6.77 | Half | 585.65 | 3,669 | 1,223 | 4,892 | 68.26 | |
| " | EO-20 | 178.19 | 184.19 | 178.19 | 4.9 | 6.00 | Half | 512.44 | 3,210 | 1,070 | 4,281 | 67.40 | |
| " | EO-21 | 177.98 | 184.04 | 177.98 | 4.9 | 6.06 | Half | 585.65 | 3,669 | 1,223 | 4,892 | 76.26 | |
| 3/2/2010 | NO-32R | - | 181.40 | 175.26 | 4.9 | 6.14 | Half | 878.47 | 5,504 | 1,835 | 7,338 | 144.27 | |
| " | NO-31R | - | 181.44 | 175.07 | 4.9 | 6.37 | Half | 732.06 | 4,586 | 1,529 | 6,115 | 115.88 | |
| " | NO-29AR | 172.15 | 183.88 | 172.15 | 4.9 | 11.73 | Half | 951.68 | 5,962 | 1,987 | 7,950 | 74.84 | |
| " | NI-23 | 170.19 | 176.61 | 170.19 | 4.9 | 6.42 | Full | 585.65 | 3,669 | 1,223 | 4,892 | 45.99 | |
| " | NI-22 | 169.96 | 177.14 | 169.96 | 4.9 | 7.18 | Full | 512.44 | 3,210 | 1,070 | 4,281 | 35.98 | |
| " | NI-21 | 168.42 | 181.16 | 168.42 | 4.9 | 12.74 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 36.66 | |
| " | NI-20 | 171.30 | 176.16 | 171.30 | 4.9 | 4.86 | Full | 585.65 | 3,669 | 1,223 | 4,892 | 55.58 | |
| " | NI-19A | 171.05 | 177.99 | 171.05 | 4.9 | 6.94 | Full | 512.44 | 3,210 | 1,070 | 4,281 | 31.40 | |
| " | XI-25 | 170.87 | 179.01 | 170.87 | 4.9 | 8.14 | Full | 732.06 | 4,586 | 1,529 | 6,115 | 41.48 | |
| " | XI-24 | 169.91 | 178.73 | 169.91 | 4.9 | 8.82 | Full | 732.06 | 4,586 | 1,529 | 6,115 | 41.85 | |
| " | NI-33 | 172.95 | 182.32 | 172.95 | 4.9 | 9.37 | Full | 951.68 | 5,962 | 1,987 | 7,950 | 56.42 | |
| " | NI-32 | 172.25 | 182.34 | 172.25 | 4.9 | 10.09 | Full | 878.47 | 5,504 | 1,835 | 7,338 | 43.89 | |
| 3/3/2010 | NI-31 | 171.38 | 182.16 | 171.38 | 4.9 | 10.78 | Full | 951.68 | 5,962 | 1,987 | 7,950 | 37.55 | |
| " | NI-30 | 169.74 | 186.18 | 169.01 | 4.9 | 17.17 | Full | 1317.71 | 8,256 | 2,752 | 11,007 | 35.40 | |
| " | NI-29 | 170.57 | 182.11 | 170.57 | 4.9 | 11.54 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 43.89 | |
| " | NI-28 | 172.09 | 183.00 | 172.09 | 4.9 | 10.91 | Full | 2489.00 | 15,594 | 5,198 | 20,792 | 105.22 | |
| " | NI-27 | 171.66 | 181.40 | 171.66 | 4.9 | 9.74 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 72.80 | |
| 3/4/2010 | NI-34 | 172.92 | 182.44 | 172.92 | 4.9 | 9.52 | Full | 2781.83 | 17,428 | 5,809 | 23,238 | 124.27 | |
| " | EI-16 | 173.84 | 181.49 | 173.84 | 4.9 | 7.65 | Full | 658.85 | 4,128 | 1,376 | 5,504 | 39.72 | |
| " | EI-15 | 170.39 | 180.58 | 170.39 | 4.9 | 10.19 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 36.45 | |
| " | EI-14 | 170.81 | 174.86 | 170.81 | 4.9 | 4.05 | Full | 439.24 | 2,752 | 917 | 3,669 | 50.02 | |
| 3/5/2010 | NI-24 | 172.50 | 180.80 | 172.50 | 4.9 | 8.30 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 38.28 | |
| " | NI-25 | 171.25 | 181.56 | 171.25 | 4.9 | 10.31 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 33.22 | |
| " | NI-26 | 171.55 | 182.50 | 171.55 | 4.9 | 10.95 | Full | 3953.12 | 24,767 | 8,256 | 33,022 | 182.01 | |
| " | XO-21 | 169.34 | 177.93 | 169.34 | 4.9 | 8.59 | Half | 1464.12 | 9,173 | 3,058 | 12,230 | 134.50 | |
| " | XO-22A | 170.98 | 179.02 | 170.98 | 4.9 | 8.04 | Half | 658.85 | 4,128 | 1,376 | 5,504 | 69.70 | |
| " | XO-21A | 170.90 | 179.33 | 170.90 | 4.9 | 8.43 | Half | 805.27 | 5,045 | 1,682 | 6,727 | 75.38 | |
| " | SO-37 | 156.16 | 185.84 | 156.16 | 4.9 | 29.68 | Half | 2928.24 | 18,346 | 6,115 | 24,461 | 83.92 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | (GAL) | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 3/8/2010 | SO-38 | 159.72 | 185.83 | 159.72 | 4.9 | 26.11 | Half | 2415.80 | 15,135 | 5,045 | 20,180 | 73.01 | |
| " | SO-39 | 161.59 | 185.85 | 161.59 | 4.9 | 24.26 | Half | 2269.39 | 14,218 | 4,739 | 18,957 | 73.82 | |
| " | SO-40 | 162.93 | 186.01 | 162.93 | 4.9 | 23.08 | Half | 1830.15 | 11,466 | 3,822 | 15,288 | 62.57 | |
| " | SO-41 | 162.84 | 185.85 | 162.84 | 4.9 | 23.01 | Half | 1976.56 | 12,383 | 4,128 | 16,511 | 67.78 | |
| " | SO-42 | 161.49 | 183.28 | 161.49 | 4.9 | 21.79 | Half | 1830.15 | 11,466 | 3,822 | 15,288 | 66.28 | |
| 3/9/2010 | SO-43 | 163.40 | 185.61 | 163.40 | 4.9 | 22.21 | Half | 1756.94 | 11,007 | 3,669 | 14,676 | 62.42 | |
| " | SO-44 | 163.39 | 180.62 | 163.39 | 4.9 | 17.23 | Half | 1390.91 | 8,714 | 2,905 | 11,619 | 63.70 | |
| " | SO-45 | 161.25 | 179.66 | 161.25 | 4.9 | 18.41 | Half | 1537.33 | 9,631 | 3,210 | 12,842 | 65.89 | |
| " | SO-46 | 162.95 | 180.10 | 162.95 | 4.9 | 17.15 | Half | 1317.71 | 8,256 | 2,752 | 11,007 | 60.63 | |
| " | SO-47 | 161.13 | 185.51 | 161.13 | 4.9 | 24.38 | Half | 2049.77 | 12,842 | 4,281 | 17,123 | 66.34 | |
| " | SO-48 | 161.82 | 182.26 | 161.82 | 4.9 | 20.44 | Half | 1903.36 | 11,925 | 3,975 | 15,900 | 73.48 | |
| 3/10/2010 | SO-49 | 162.01 | 177.52 | 162.01 | 4.9 | 15.51 | Half | 1317.71 | 8,256 | 2,752 | 11,007 | 67.04 | |
| " | SO-50 | 160.99 | 177.91 | 160.99 | 4.9 | 16.92 | Half | 4172.74 | 26,142 | 8,714 | 34,857 | 194.61 | |
| " | SO-51 | 160.83 | 174.94 | 160.83 | 4.9 | 14.11 | Half | 1464.12 | 9,173 | 3,058 | 12,230 | 81.88 | |
| " | SO-52 | 161.19 | 175.13 | 161.19 | 4.9 | 13.94 | Half | 1464.12 | 9,173 | 3,058 | 12,230 | 82.88 | |
| " | SO-53 | 159.96 | 177.76 | 159.96 | 4.9 | 17.80 | Half | 1976.56 | 12,383 | 4,128 | 16,511 | 87.62 | |
| 3/15/2010 | INT-313 | 159.67 | 185.48 | 159.63 | 4.9 | 25.85 | Full | 2562.21 | 16,052 | 5,351 | 21,403 | 42.15 | |
| " | SI-35 | 159.25 | 185.06 | 159.18 | 4.9 | 25.88 | Full | 2269.39 | 14,218 | 4,739 | 18,957 | 44.21 | |
| " | INT-314 | 161.66 | 185.17 | 161.62 | 4.9 | 23.55 | Full | 2708.62 | 16,970 | 5,657 | 22,626 | 48.92 | |
| " | SI-36 | 163.12 | 185.46 | 163.12 | 4.9 | 22.34 | Full | 1756.94 | 11,007 | 3,669 | 14,676 | 39.65 | |
| " | INT-315 | 163.38 | 185.69 | 163.38 | 4.9 | 22.31 | Full | 2049.77 | 12,842 | 4,281 | 17,123 | 39.07 | |
| " | SI-37 | 164.67 | 182.19 | 163.95 | 4.9 | 18.24 | Full | 1390.91 | 8,714 | 2,905 | 11,619 | 38.45 | |
| 3/16/2010 | INT-316 | 165.53 | 185.64 | 165.50 | 4.9 | 20.14 | Full | 1683.74 | 10,549 | 3,516 | 14,065 | 35.56 | |
| " | SI-38 | 164.54 | 181.79 | 163.87 | 4.9 | 17.92 | Full | 1464.12 | 9,173 | 3,058 | 12,230 | 37.68 | |
| " | SI-39 | 163.76 | 181.34 | 163.72 | 4.9 | 17.62 | Full | 1464.12 | 9,173 | 3,058 | 12,230 | 38.33 | |
| " | SI-40 | 163.47 | 182.14 | 163.47 | 4.9 | 18.67 | Full | 1464.12 | 9,173 | 3,058 | 12,230 | 36.17 | |
| " | SI-41 | 162.02 | 176.14 | 162.00 | 4.9 | 14.14 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 35.82 | |
| " | SI-42 | 161.96 | 174.48 | 161.95 | 4.9 | 12.53 | Full | 951.68 | 5,962 | 1,987 | 7,950 | 35.03 | |
| " | SI-43 | 162.10 | 180.59 | 162.10 | 4.9 | 18.49 | Full | 1464.12 | 9,173 | 3,058 | 12,230 | 36.52 | |
| 3/17/2010 | SI-44 | 162.60 | 176.25 | 162.56 | 4.9 | 13.69 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 37.00 | |
| " | SI-45 | 162.94 | 176.67 | 162.89 | 4.9 | 13.78 | Full | 1171.30 | 7,338 | 2,446 | 9,784 | 39.20 | |
| " | SI-46 | 164.00 | 172.45 | 163.69 | 4.9 | 8.76 | Full | 658.85 | 4,128 | 1,376 | 5,504 | 34.69 | |
| " | SI-47 | 161.61 | 168.13 | 161.60 | 4.9 | 6.53 | Full | 732.06 | 4,586 | 1,529 | 6,115 | 51.71 | |
| " | SI-48 | 162.06 | 180.16 | 162.01 | 4.9 | 18.15 | Full | 1610.53 | 10,090 | 3,363 | 13,453 | 40.93 | |
| " | SI-49 | 162.37 | 174.33 | 162.15 | 4.9 | 12.18 | Full | 1830.15 | 11,466 | 3,822 | 15,288 | 69.30 | |
| 3/18/2010 | XI-21 | 169.12 | 175.49 | 169.10 | 4.9 | 6.39 | Full | 4172.74 | 26,142 | 8,714 | 34,857 | 301.19 | |
| " | XI-22 | 170.75 | 182.85 | 175.75 | 4.9 | 7.10 | Full | 439.24 | 2,752 | 917 | 3,669 | 28.53 | |
| " | XI-23 | 171.42 | 177.28 | 171.41 | 4.9 | 5.87 | Full | 512.44 | 3,210 | 1,070 | 4,281 | 40.26 | |
| " | WI-4R | - | 174.07 | 164.99 | 4.9 | 9.08 | Full | 878.47 | 5,504 | 1,835 | 7,338 | 48.78 | |
| " | INT-400 | - | 174.21 | 165.69 | 4.9 | 8.52 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 47.65 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added (GAL) | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 3/19/2010 | XI-1R | - | 186.28 | 169.18 | 4.9 | 17.10 | Full | 1390.91 | 8,714 | 2,905 | 11,619 | 41.01 | |
| " | WI-1R | - | 181.93 | 153.32 | 4.9 | 28.61 | Full | 2781.83 | 17,428 | 5,809 | 23,238 | 49.02 | |
| " | INT-401 | - | 186.19 | 169.14 | 4.9 | 17.05 | Full | 1756.94 | 11,007 | 3,669 | 14,676 | 47.53 | |
| " | XI-3R | - | 185.61 | 170.47 | 4.9 | 15.14 | Full | 1171.30 | 7,338 | 2,446 | 9,784 | 35.68 | |
| " | INT-402 | - | 185.61 | 169.67 | 4.9 | 15.94 | Full | 1317.71 | 8,256 | 2,752 | 11,007 | 35.16 | |
| " | XI-7R | - | 185.09 | 156.12 | 4.9 | 28.97 | Full | 2781.83 | 17,428 | 5,809 | 23,238 | 48.41 | |
| 3/22/10 | INT-403 | - | 186.12 | 173.56 | 4.9 | 12.56 | Full | 1024.88 | 6,421 | 2,140 | 8,561 | 41.14 | |
| " | INT-404 | - | 186.1 | 174.38 | 4.9 | 11.72 | Full | 951.68 | 5,962 | 1,987 | 7,950 | 40.94 | |
| " | XI-9R | - | 186.28 | 176.96 | 4.9 | 9.32 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 43.56 | |
| " | INT-405 | - | 186.3 | 179.21 | 4.9 | 7.09 | Full | 585.65 | 3,669 | 1,223 | 4,892 | 38.10 | |
| | INT-406 | - | 186.55 | 177.04 | 4.9 | 9.51 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 39.06 | |
| " | XI-12R | - | 186.36 | 177.92 | 4.9 | 8.44 | Full | 732.06 | 4,586 | 1,529 | 6,115 | 48.18 | |
| " | INT-407 | - | 185.06 | 169.08 | 4.9 | 15.98 | Full | 1390.91 | 8,714 | 2,905 | 11,619 | 43.88 | |
| " | XI-14R | - | 184.21 | 171.12 | 4.9 | 13.09 | Full | 1317.71 | 8,256 | 2,752 | 11,007 | 62.20 | |
| 3/23/10 | XI-15R | - | 178.46 | 166.39 | 4.9 | 12.07 | Full | 1390.91 | 8,714 | 2,905 | 11,619 | 64.01 | |
| " | INT-174R | - | 184.88 | 170.71 | 4.9 | 14.17 | Full | 2415.80 | 15,135 | 5,045 | 20,180 | 105.34 | |
| " | XI-13R2 | - | 186.4 | 177.50 | 4.9 | 8.90 | Full | 658.85 | 4,128 | 1,376 | 5,504 | 45.74 | |
| " | XI-17R | - | 185.4 | 170.77 | 4.9 | 14.63 | Full | 1317.71 | 8,256 | 2,752 | 11,007 | 50.03 | |
| " | EI-13 | - | 176.59 | 170.79 | 4.9 | 5.80 | Full | 512.44 | 3,210 | 1,070 | 4,281 | 40.75 | |
| 3/24/10 | EI-12 | 169.63 | 175.56 | 169.62 | 4.9 | 5.94 | Full | 658.85 | 4,128 | 1,376 | 5,504 | 47.17 | |
| " | EI-11 | 166.98 | 175.65 | 166.92 | 4.9 | 8.73 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 42.54 | |
| " | EI-10 | 168.22 | 183.68 | 168.22 | 2 | 15.46 | Full | 1244.50 | 7,797 | 2,599 | 10,396 | 34.24 | |
| " | EI-10A | 170.66 | 183.81 | 170.66 | 4.9 | 13.15 | Full | 1024.88 | 6,421 | 2,140 | 8,561 | 33.15 | |
| " | EI-10C | 171.49 | 180.71 | 171.49 | 4.9 | 9.22 | Full | 732.06 | 4,586 | 1,529 | 6,115 | 36.62 | |
| 3/25/10 | EO-2 | 165.3 | 186.62 | 165.30 | 4.9 | 21.32 | Half | 1756.94 | 11,007 | 3,669 | 14,676 | 65.03 | |
| " | EO-3 | 164.75 | 186.97 | 164.73 | 4.9 | 22.24 | Half | 1756.94 | 11,007 | 3,669 | 14,676 | 62.34 | |
| " | EO-4 | 164.2 | 187.26 | 164.19 | 4.9 | 23.07 | Half | 1830.15 | 11,466 | 3,822 | 15,288 | 62.60 | |
| " | EO-5 | 164.2 | 187.32 | 164.19 | 4.9 | 23.13 | Half | 2708.62 | 16,970 | 5,657 | 22,626 | 92.41 | |
| 3/26/10 | EO-6 | 164.71 | 186.83 | 164.69 | 4.9 | 22.14 | Half | 2122.97 | 13,301 | 4,434 | 17,734 | 75.67 | |
| " | EO-7 | 166.98 | 186.8 | 166.98 | 4.9 | 19.82 | Half | 1830.15 | 11,466 | 3,822 | 15,288 | 72.86 | |
| " | AEO-19 | 173.13 | 184.36 | 172.97 | 4.9 | 11.39 | Half | 1024.88 | 6,421 | 2,140 | 8,561 | 71.00 | |
| " | AEO-18 | 173.33 | - | - | - | - | - | - | - | - | - | - | Tremie Grouted |
| 3/29/10 | AEO-17 | 172.49 | - | - | - | - | - | - | - | - | - | - | Tremie Grouted |
| " | AEO-16 | 177.98 | 182.38 | 177.96 | 4.9 | 4.42 | Half | 585.65 | 3,669 | 1,223 | 4,892 | 104.56 | |
| " | AEO-15 | 172.98 | - | - | - | - | - | - | - | - | - | - | Tremie Grouted |
| " | AEO-14 | 172.49 | - | - | - | - | - | - | - | - | - | - | Tremie Grouted |
| " | AEO-13 | - | - | - | - | - | - | - | - | - | - | - | Tremie Grouted |
| " | AEO-11 | 168.35 | 181.19 | 168.33 | 4.9 | 12.86 | Half | 1024.88 | 6,421 | 2,140 | 8,561 | 62.89 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added (GAL) | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 3/30/10 | AEO-10 | 169.26 | 180.42 | 169.26 | 4.9 | 11.16 | Half | 1024.88 | 6,421 | 2,140 | 8,561 | 72.47 | |
| " | AEO-9 | 168.99 | 178.47 | 168.99 | 4.9 | 9.48 | Half | 732.06 | 4,586 | 1,529 | 6,115 | 60.94 | |
| " | AEO-12 | 171.13 | 185.11 | 171.13 | 4.9 | 13.98 | Half | 1098.09 | 6,880 | 2,293 | 9,173 | 66.81 | |
| 3/31/10 | ASO-54 | 160.04 | 176.18 | 160.04 | 4.9 | 16.14 | Half | 1610.53 | 10,090 | 3,363 | 13,453 | 78.74 | |
| " | ASO-55 | 161 | 177.87 | 161.00 | 4.9 | 16.87 | Half | 1537.33 | 9,631 | 3,210 | 12,842 | 71.91 | |
| " | ASO-56 | 162.37 | 180.85 | 162.37 | 4.9 | 18.48 | Half | 1244.50 | 7,797 | 2,599 | 10,396 | 53.14 | |
| " | ASO-57 | 162.13 | 180.15 | 162.13 | 4.9 | 18.02 | Half | 1464.12 | 9,173 | 3,058 | 12,230 | 64.11 | |
| 4/1/10 | ASO-58 | 163.96 | 181.81 | 163.96 | 4.9 | 17.85 | Half | 1464.12 | 9,173 | 3,058 | 12,230 | 69.77 | |
| " | EO-8 | 169.33 | - | - | - | - | - | - | - | - | - | - | Tremie Grouted |
| " | AEI-7 | 168.66 | 181.69 | 168.66 | 4.9 | 13.03 | Full | 1390.91 | 8,714 | 2,905 | 11,619 | 45.40 | |
| " | EI-6 | 172.85 | 180.71 | 172.77 | 4.9 | 7.94 | Full | 585.65 | 3,669 | 1,223 | 4,892 | 31.37 | |
| 4/2/10 | EI-5 | 166.64 | 183.74 | 166.64 | 4.9 | 17.10 | Full | 1390.91 | 8,714 | 2,905 | 11,619 | 37.52 | |
| " | EI-4 | 163.78 | 178.93 | 163.78 | 4.9 | 15.15 | Full | 1171.30 | 7,338 | 2,446 | 9,784 | 35.66 | |
| " | EO-9 | 169.46 | 184.75 | 169.46 | 4.9 | 15.29 | Half | 1244.50 | 7,797 | 2,599 | 10,396 | 64.23 | |
| " | EO-10 | 170.03 | 182.7 | 170.03 | 4.9 | 12.67 | Half | 1024.88 | 6,421 | 2,140 | 8,561 | 63.83 | |
| " | EO-24 | 171.57 | 181.32 | 171.57 | 4.9 | 9.75 | Half | 732.06 | 4,586 | 1,529 | 6,115 | 59.25 | |
| " | EO-23 | 173.99 | 183.73 | 173.99 | 4.9 | 9.74 | Half | 805.27 | 5,045 | 1,682 | 6,727 | 65.24 | |
| " | EO-22 | 174.76 | 184.74 | 174.76 | 4.9 | 9.98 | Half | 951.68 | 5,962 | 1,987 | 7,950 | 81.11 | |
| 4/5/10 | EI-17 | - | - | - | - | - | - | - | - | - | - | - | |
| " | EI-18 | 171.1 | 181.06 | 171.06 | 4.9 | 10.00 | Full | 878.47 | 5,504 | 1,835 | 7,338 | 37.36 | |
| " | EI-19 | 173.62 | 178.73 | 173.58 | 4.9 | 5.15 | Full | 439.24 | 2,752 | 917 | 3,669 | 39.34 | |
| " | EI-20 | 173.13 | 179.68 | 173.09 | 4.9 | 6.59 | Full | 512.44 | 3,210 | 1,070 | 4,281 | 35.87 | |
| " | EI-21 | 172.86 | 180.6 | 172.86 | 4.9 | 7.74 | Full | 585.65 | 3,669 | 1,223 | 4,892 | 34.90 | |
| " | EI-22 | 172.81 | 183.7 | 172.80 | 4.9 | 10.90 | Full | 878.47 | 5,504 | 1,835 | 7,338 | 37.17 | |
| " | EI-23 | 171.81 | 182.48 | 171.78 | 4.9 | 10.70 | Full | 878.47 | 5,504 | 1,835 | 7,338 | 37.87 | |
| " | EI-9 | 170.4 | 185.47 | 169.69 | 4.9 | 15.78 | Full | 1244.50 | 7,797 | 2,599 | 10,396 | 36.38 | |
| " | EI-8 | 170.86 | 180.64 | 169.02 | 4.9 | 11.62 | Full | 1171.30 | 7,338 | 2,446 | 9,784 | 46.49 | |
| " | EI-3 | 164.83 | 178.95 | 164.81 | 4.9 | 14.14 | Full | 1098.09 | 6,880 | 2,293 | 9,173 | 35.82 | |
| " | EI-2 | 164.8 | 181.71 | 164.79 | 4.9 | 16.92 | Full | 1244.50 | 7,797 | 2,599 | 10,396 | 33.92 | |
| 4/6/10 | SO-54 | 164.08 | 175.74 | 164.06 | 4.9 | 11.68 | Half | 1390.91 | 8,714 | 2,905 | 11,619 | 93.97 | |
| " | SO-55 | 161.5 | 177.6 | 161.45 | 4.9 | 16.15 | Half | 1317.71 | 8,256 | 2,752 | 11,007 | 64.38 | |
| " | SO-56 | 161.48 | 179.24 | 161.33 | 4.9 | 17.91 | Half | 1464.12 | 9,173 | 3,058 | 12,230 | 64.51 | |
| " | SO-57 | 162.24 | 180.94 | 162.24 | 4.9 | 18.70 | Half | 1537.33 | 9,631 | 3,210 | 12,842 | 64.87 | |
| " | SO-58 | 161.18 | 185.96 | 161.12 | 4.9 | 24.84 | Half | 2562.21 | 16,052 | 5,351 | 21,403 | 81.40 | |
| " | EO-1 | 162.52 | 186.67 | 162.52 | 4.9 | 24.15 | Half | 2415.80 | 15,135 | 5,045 | 20,180 | 85.09 | |

**Table 4.5**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grout Tracking Log**

| Date | Column ID | Reported Bedrock Elevation | Column Top Elevation | Column Bottom Elevation | Column Dimensions | | | Water Added (GAL) | Reagents Added | | | | Notes |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | Diameter (FT) | Length (FT) | Type | | Slag (LBS) | Portland (LBS) | Total (LBS) | Estimated Total % Added | |
| 4/7/10 | ASI-55 | 163.51 | 179.14 | 162.38 | 4.9 | 16.76 | Full | 1537.33 | 9,631 | 3,210 | 12,842 | 39.01 | |
| " | ASI-54 | 162.24 | 178.18 | 162.24 | 4.9 | 15.94 | Full | 1756.94 | 11,007 | 3,669 | 14,676 | 46.88 | |
| " | ASI-53 | 163.29 | 178.72 | 163.29 | 4.9 | 15.43 | Full | 1244.50 | 7,797 | 2,599 | 10,396 | 37.20 | |
| " | ASI-52 | 166.04 | 176.32 | 169.04 | 4.9 | 7.28 | Full | 658.85 | 4,128 | 1,376 | 5,504 | 38.49 | |
| " | ASI-51 | 163.99 | 175.52 | 164.89 | 4.9 | 10.63 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 32.22 | |
| " | ASI-50 | 162.61 | 172.82 | 162.31 | 4.9 | 10.51 | Full | 805.27 | 5,045 | 1,682 | 6,727 | 35.34 | |
| 4/8/10 | WI-19R | NA | - | - | - | - | Full | - | - | - | - | - | |
| " | WI-17R | NA | - | - | - | - | Full | - | - | - | - | - | |
| " | WI-12R | NA | - | - | - | - | Full | - | - | - | - | - | |

**Table 4.6**
**Cons Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Excavator-ISS Testing Results**

| | Sample Date | Sample ID | Unconfined Compressive Strength (UCS) (psi) | | | | | Hydraulic Conductivity (HC) * (cm/sec) | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | 3 Days | 7 Days | 14 Days | 28 Days | 56 Days | 3 Days | 7 Days | 14 Days | 28 Days | 28+ Days |
| TEST CELLS | ~~1/22/09~~ | ~~TP103-1~~ | ~~1.4~~ | ~~2.0~~ | ~~3.3~~ | ~~2.9~~ | | ~~2.0E-06~~ | ~~8.4E-06~~ | ~~2.4E-06~~ | ~~1.2E-06~~ | |
| | | ~~TP103-2~~ | ~~1.7~~ | ~~3.7~~ | ^ | ^ | | ^ | ^ | ^ | ^ | |
| | **Remixed** | ~~TP106-1~~ | ~~1.8~~ | ~~2.6~~ | ~~3.2~~ | ^ | | ~~3.1E-06~~ | ~~3.2E-06~~ | ~~2.9E-06~~ | ~~1.2E-06~~ | |
| | **2/20/09** | ~~TP106-2~~ | ~~1.6~~ | ~~2.1~~ | ^ | ^ | | ^ | ^ | ^ | ^ | |
| | | ~~TP114-1~~ | ~~1.4~~ | ~~1.7~~ | ~~2.6~~ | ~~3.7~~ | | ~~2.6E-06~~ | ~~1.8E-06~~ | ~~2.1E-06~~ | ~~3.0E-06~~ | |
| | | ~~TP114-2~~ | ~~1.7~~ | ~~2.6~~ | ^ | ^ | | ^ | ^ | ^ | " | |
| | ~~1/26/09~~ | ~~TP103A-1~~ | ~~6.0~~ | ~~28.0~~ | ~~87.1~~ | ~~162.6~~ | | ~~2.4E-06~~ | ~~1.2E-06~~ | ~~1.7E-06~~ | ~~2.9E-06~~ | |
| | | ~~TP103A-2~~ | ~~6.5~~ | ~~30.6~~ | ^ | ^ | | ^ | ^ | ^ | ^ | |
| | **Remixed** | ~~TP107A-1~~ | ~~8.3~~ | ~~30.4~~ | ~~100.7~~ | ~~168.7~~ | | ~~1.4E-06~~ | ~~3.7E-06~~ | ~~2.1E-06~~ | ~~2.3E-06~~ | |
| | **2/20/09** | ~~TP107A-2~~ | ~~7.2~~ | ~~31.0~~ | ^ | ^ | | ^ | ^ | ^ | ^ | |
| | | ~~TP114A-1~~ | ~~5.3~~ | ~~20.8~~ | ~~36.1~~ | ~~107.5~~ | | ~~2.2E-06~~ | ~~1.7E-06~~ | ~~1.6E-06~~ | ~~3.0E-06~~ | |
| | | ~~TP114A-2~~ | ~~7.7~~ | ~~22.2~~ | ^ | ^ | | ^ | ^ | ^ | ^ | |
| | ~~1/27/09~~ | ~~TP202-1~~ | ~~57.0~~ | ~~182.9~~ | ~~298.6~~ | ~~327.6~~ | | ~~2.7E-07~~ | ~~1.2E-06~~ | ~~1.8E-06~~ | ~~1.7E-06~~ | |
| | | ~~TP202-2~~ | ~~54.2~~ | ~~101.6~~ | ^ | ^ | | ^ | ^ | ^ | ^ | |
| | **Remixed** | ~~TP206-1~~ | ~~44.2~~ | ~~130.6~~ | ~~314.2~~ | ~~345.9~~ | | ~~2.3E-06~~ | ~~4.6E-06~~ | ~~1.7E-06~~ | ~~1.6E-06~~ | |
| | **2/19/09** | ~~TP206-2~~ | ~~52.8~~ | ~~186.9~~ | ^ | ^ | | | | ^ | ^ | |
| | | ~~TP212-1~~ | ~~54.0~~ | ~~159.1~~ | ~~265.6~~ | ~~343.2~~ | | ~~1.4E-06~~ | ~~4.1E-07~~ | ~~1.6E-06~~ | ~~1.6E-06~~ | |
| | | ~~TP212-2~~ | ~~60.3~~ | ~~185.4~~ | ^ | ^ | | ^ | ^ | ^ | ^ | |
| | 1/28/09 | TP302-1 | 59.0 | 128.3 | 264.3 | 343.7 | | 1.9E-06 | 1.9E-06 | 1.7E-06 | 1.6E-06 | 9.7E-07 |
| | | TP302-2 | 56.7 | 118.6 | ^ | ^ | | ^ | ^ | ^ | ^ | 37 days |
| | | TP306-1 | 40.9 | 104.5 | 231.7 | 340.9 | | 1.6E-06 | 1.6E-06 | 1.7E-06 | 1.9E-06 | 1.0E-06 |
| | | TP306-2 | 40.7 | 92.2 | ^ | ^ | | ^ | ^ | ^ | ^ | 37 days |
| | | TP312-1 | 29.1 | 80.5 | 126.3 | 149.8 | | 1.5E-06 | 2.9E-06 | 1.8E-06 | 2.0E-06 | 9.7E-07 |
| | | TP312-2 | 27.8 | 69.3 | ^ | ^ | | ^ | ^ | ^ | ^ | 37 days |
| | 1/29/09 | TP404-1 | 178.7 | 80.5 | 344.2 | 700.8 | | 1.1E-06 | 3.2E-06 | 1.7E-06 | 1.5E-06 | 9.8E-07 |
| | | TP404-2 | 182.7 | 338.4 | ^ | ^ | | ^ | ^ | ^ | ^ | 37 days |
| | | TP409-1 | 221.2 | 341.4 | 769.1 | 580.5 | | 7.2E-07 | 3.6E-07 | 1.9E-06 | 1.8E-06 | 9.8E-07 |
| | | TP409-2 | 229.3 | 341.5 | ^ | ^ | | ^ | ^ | ^ | ^ | 37 days |
| | | TP416-1 | 201.1 | 340.4 | 775.6 | 839.4 | | 7.3 E-07 | 2.1E-06 | 1.8E-06 | 1.1E-06 | 9.8E-07 |
| | | TP416-2 | 212.6 | 341.6 | ^ | ^ | | ^ | ^ | ^ | ^ | 37 days |
| PRODUCTION CELLS | 1/30/09 | TP516-1 | 93.4 | 176.5 | ^ | 795.9 | | ^ | ^ | 2.6E-06 | 9.3E-07 | |
| | | TP516-2 | 95.3 | 194.2 | ^ | 728.7 | | ^ | ^ | ^ | ^ | |
| | 2/2/09 | P7 | **NO SAMPLES TAKEN** | | | | | **NO SAMPLES TAKEN** | | | | |
| | | P810-1 | 51.4 | 177.0 | | 811.7 | | | | | 1.10E-06 | 7.0E-07 |
| | | P810-2 | 54.3 | 144.2 | | 776.3 | | | | | ^ | 36 days |
| | | P9 | **NO SAMPLES TAKEN** | | | | | **NO SAMPLES TAKEN** | | | | |
| | 2/3/09 | P1004-1 | 33.5 | 112.6 | | 353.5 | | | | | 1.6E-06 | 8.4E-07 |
| | | P1004-2 | 36.6 | 120.3 | | 706.9 | | | | | ^ | 35 days |
| | ~~2/4/09~~ | ~~P1108-1~~ | ~~74.1~~ | ~~96~~ | | ^ | | | | ~~2.3E-06~~ | ^ | |
| | | ~~P1108-2~~ | ~~68.0~~ | ~~116.3~~ | | ^ | | | | ^ | | |
| | **Remixed 2/26/09** | | | | | | | | | | | |
| | 2/6/09 | P1212-1 | 75.4 | 150.1 | | 647.7 | | | | 1.2E-06 | 3.5E-07 | |
| | | P1212-2 | 77.1 | 179.4 | | 689.9 | | | | ^ | ^ | |
| | | P6 | **NO SAMPLES TAKEN** | | | | | **NO SAMPLES TAKEN** | | | | |
| | 2/7/09 | P1304-1 | 24.2 | 92.4 | | 681.2 | | | | 1.3E-06 | 9.7E-07 | |
| | | P1304-2 | 30.6 | 77.7 | | 638.2 | | | | ^ | ^ | |
| | 2/9/09 | P14 | **NO SAMPLES TAKEN** | | | | | **NO SAMPLES TAKEN** | | | | |
| | | P1510-1 | 102.4 | 167.0 | | 705.2 | | | | 1.8E-06 | 6.3E-07 | |
| | | P1510-1 | 89.5 | 181.5 | | 721.8 | | | | ^ | ^ | |
| | 2/10/09 | EM115-1 | 69.8 | 206.4 | | 750.8 | | | | 1.2E-06 | 7.4E-07 | |
| | | EM115-2 | 66.1 | 144.8 | | 666.4 | | | | ^ | ^ | |
| | | EM2 | **NO SAMPLES TAKEN** | | | | | **NO SAMPLES TAKEN** | | | | |
| | | EM3 | **NO SAMPLES TAKEN** | | | | | **NO SAMPLES TAKEN** | | | | |
| | 2/11/09 | P506-1 | 214.7 | 231.0 | | 802.9 | | | | 1.7E-06 | 9.7E-07 | |
| | | P506-2 | 158.3 | 217.1 | | 812.8 | | | | ^ | ^ | |
| | | EM4 | **NO SAMPLES TAKEN** | | | | | **NO SAMPLES TAKEN** | | | | |
| | 2/13/09 | P406-1 | 69.8 | 210.1 | | 762.3 | | | | 1.20E-06 | 5.7E-07 | |
| | | P406-2 | 71.8 | 189.7 | | 757.6 | | | | ^ | ^ | |
| | 2/16/09 | P313-1 | 106.1 | 249.8 | | 625.9 | | | | 1.1E-06 | 6.9E-07 | |
| | | P313-2 | 139.4 | 188.8 | | 593.2 | | | | ^ | ^ | |
| | | P16 | **NO SAMPLES TAKEN** | | | | | **NO SAMPLES TAKEN** | | | | |

**Cons Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Excavator-ISS Testing Results**

**PRODUCTION CELLS**

| Sample Date | Sample ID | Unconfined Compressive Strength (UCS) (psi) | | | | | Hydraulic Conductivity (HC) * (cm/sec) | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | | 3 Days | 7 Days | 14 Days | 28 Days | 56 Days | 3 Days | 7 Days | 14 Days | 28 Days | 28+ Days |
| 2/17/09 | EM505-1 | 126.0 | 298.9 | | 745.5 | | | | 9.3E-07 | 4.5E-07 | |
| | EM505-2 | 126.4 | 319.1 | | 750.8 | | | | ^ | ^ | |
| | EM6 | NO SAMPLES TAKEN | | | | | NO SAMPLES TAKEN | | | | |
| 2/18/09 | EM704-1 | 344.9 | 341.6 | | 709.0 | | | | 2.3E-07 | 5.3E-07 | |
| | EM704-2 | 248.0 | 309.8 | | 713.3 | | | | ^ | ^ | |
| | P17 | NO SAMPLES TAKEN | | | | | NO SAMPLES TAKEN | | | | |
| 2/19/09 | TP-2 (Remix) | 344.1 | 784.9 | | 714.2 | | | | | 9.1E-07 | |
| | TP-2 (Remix) | 328.6 | 672.9 | | 651.8 | | | | | ^ | |
| 2/20/09 | TP-1 (Remix) | 237.8 | 348.5 | | 752.1 | | | | | 5.7E-07 | |
| | TP-1 (Remix) | 213.1 | 345.2 | | 756.5 | | | | | ^ | |
| 2/21/09 | P206-1 | 36.2 | 96.4 | | 701.2 | | | | | 5.4E-07 | |
| | P206-2 | 47.0 | 109.5 | | 691.4 | | | | | ^ | |
| 2/23/09 | P111-1 | 72.6 | 219.4 | | 739.8 | | | | | 6.1E-07 | |
| | P111-2 | 76.9 | 238.2 | | 722.3 | | | | | ^ | |
| | EM-8 | NO SAMPLES TAKEN | | | | | NO SAMPLES TAKEN | | | | |
| 2/24/09 | EM910-1 | 81.9 | 203.7 | | 720.0 | | | | | 7.2E-07 | |
| | EM910-2 | 47.1 | 179.7 | | 712.3 | | | | | ^ | |
| 2/25/09 | EM1007-1 | 197.1 | 253.8 | | 702.2 | | | | | 7.0E-07 | |
| | EM1007-2 | 285.2 | 321.4 | | 719.0 | | | | | ^ | |
| 2/26/09 | P1108-1(Remix) | 850.8 | 349.9 | | 762.2 | | | | | 9.3E-07 | |
| | P1108-2(Remix) | 338.7 | 350.7 | | 707.1 | | | | | ^ | |
| | EM11 | NO SAMPLES TAKEN | | | | | NO SAMPLES TAKEN | | | | |
| 2/27/09 | EM1210-1 | 514.6 | 726.4 | | 739.9 | | | | | 6.1E-07 | |
| | EM1210-2 | 692.5 | 728.0 | | 703.0 | | | | | ^ | |
| | EM13 | NO SAMPLES TAKEN | | | | | NO SAMPLE TAKEN | | | | |

**Requirements: UCS $\geq$ 50 psi @ 28 days**
**HC $\leq$ 1x10$^{-6}$ cm/sec**

**SAMPLES TAKEN ONCE PER DAY OR EVERY 500 CYs WHICHEVER PRODUCED THE GREATEST NUMBER OF SAMPLES**

Denotes that sample did not achieve the required result.

^ Denotes sample not tested.

* Hydraulic conductivity testing initially performed with a hydraulic gradient of 20. The hydraulic gradient was reduced to 15 on 2/19/09 for TP-2 Remix and the 37-day test for TP3 & TP4. This modification was within ASTM D 5084 Method A standards which require a maximum hydraulic gradient of 20 for hydraulic conductivities within a range of 10-6 to 10-7 cm/sec.

**Table 4.7**
**Cons Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Auger-ISS Testing Results**

| | Sample Date | Sample ID | Unconfined Compressive Strength (UCS) (psi) | | | | | Hydraulic Conductivity (HC) * (cm/sec) | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | | | 3 Days | 7 Days | 14 Days | 28 Days | 56 Days | 14 Days | 28 Days | 28+ Days |
| TEST COLUMNS | 3/30/09 | M10-10 | 57.5 | 204.3 | 709.4 | 714.0 | ^ | 9.6E-07 | ^ | ^ |
| | | " | 62.2 | 159.4 | ^ | ^ | ^ | ^ | ^ | ^ |
| | | M10-15 | 68.5 | 172.3 | 659.8 | 727.0 | ^ | 9.9E-07 | ^ | ^ |
| | | " | 45.0 | 253.1 | ^ | ^ | ^ | ^ | ^ | ^ |
| | | M10-20 | 73.6 | 206.2 | 715.4 | 751.5 | ^ | 9.8E-07 | ^ | ^ |
| | | " | 90.9 | 186.8 | ^ | ^ | ^ | ^ | ^ | ^ |
| | 3/31/09 | N14-08 | 87.4 | 186.4 | 342.8 | 776.0 | ^ | 9.9E-07 | ^ | ^ |
| | | " | 82.5 | 156.2 | ^ | ^ | ^ | ^ | ^ | ^ |
| | | N14-16 | 72.7 | 163.9 | 252.3 | 772.2 | ^ | 9.8E-07 | ^ | ^ |
| | | " | 86.5 | 191.7 | ^ | ^ | ^ | ^ | ^ | ^ |
| | | N14-24 | 40.6 | 157.1 | 334.5 | 752.4 | ^ | 9.6E-07 | ^ | ^ |
| | | " | 75.9 | 139.8 | ^ | ^ | ^ | ^ | ^ | ^ |
| | | N15-05 | 32.3 | 127.6 | 256.1 | 717.7 | ^ | 9.7E-07 | ^ | ^ |
| | | " | 35.1 | 97.5 | ^ | ^ | ^ | ^ | ^ | ^ |
| | | N15-15 | 101.1 | 203.2 | 336.2 | 867.7 | ^ | 9.8E-07 | ^ | ^ |
| | | " | 105.6 | 206.7 | ^ | ^ | ^ | ^ | ^ | ^ |
| | | N15-20 | 101.2 | 194.3 | 333.4 | 767.4 | ^ | 9.8E-07 | ^ | ^ |
| | | " | 95.1 | 167.9 | ^ | ^ | ^ | ^ | ^ | ^ |
| PRODUCTION COLUMNS | 4/2/09 | N5-20 | 110.0 | 239.9 | ^ | 710.8 | 705.1 | 1.7E-06 | 1.0E-06 | ^ |
| | | " | 89.7 | 192.5 | ^ | 702.8 | 699.7 | ^ | ^ | ^ |
| | 4/3/09 | N7-17 | 32.4 | 31.5 | ^ | 600.2 | 657.4 | 1.5E-06 | 9.4E-07 | ^ |
| | | " | 22.3 | 37.8 | ^ | 614.6 | 669.8 | ^ | ^ | ^ |
| | 4/7/09 | M3-17 | 81.9 | 120.2 | ^ | 498.0 | 718.7 | 1.1E-06 | 1.2E-06 | 8.3E-07 |
| | | " | 54.3 | 112.6 | ^ | ^ | ^ | ^ | ^ | ^ |
| | 4/8/09 | N3-34 | 98.0 | 214.9 | ^ | 836.3 | 750.2 | 1.4E-06 | 9.4E-07 | ^ |
| | | " | 97.1 | 196.9 | ^ | 860.8 | 690.6 | ^ | ^ | ^ |
| | 4/9/09 | J3-25 | 247.9 | 335.8 | ^ | 745.1 | 686.8 | 1.0E-06 | ^ | ^ |
| | | " | 204.0 | 299.4 | ^ | 742.1 | 669.2 | ^ | ^ | ^ |
| | 4/10/09 | N2-15 | 61.0 | 97.8 | ^ | 687.5 | 674.3 | 9.4E-07 | ^ | ^ |
| | | " | 47.3 | 129.9 | ^ | 688.0 | 660.5 | ^ | ^ | ^ |
| | 4/16/09 | 7n1-15 | 22.0 | 42.7 | ^ | 587.3 | 532.3 | 1.6E-06 | 1.2E-06 | 8.3E-07 |
| | | " | 21.3 | 19.4 | ^ | 589.4 | 470.9 | ^ | ^ | ^ |
| | 4/17/09 | M1-36 | 199.3 | 529.8 | ^ | 729.7 | 727.7 | 1.4E-06 | 9.0E-07 | |
| | | " | 182.5 | 515.3 | ^ | 715.0 | 691.4 | ^ | ^ | |
| | 4/22/09 | 7008-20 | 19.0 | 204.2 | ^ | 659.2 | 718.2 | 1.1E-06 | 1.1E-06 | 8.0E-07 |
| | | " | 16.2 | 193.8 | ^ | 665.4 | 721.3 | ^ | ^ | |
| | 4/23/09 | 7m10-15 | 56.4 | 99.1 | ^ | 672.4 | 658.3 | 1.1E-06 | 4.8E-07 | ^ |
| | | " | 49.0 | 130.8 | ^ | 556.3 | 661.2 | ^ | ^ | ^ |
| | 4/24/09 | 7k8-20 | 95.1 | 631.9 | ^ | 551.4 | 677.6 | 1.1E-06 | 1.6E-07 | ^ |
| | | " | 86.1 | 630.5 | ^ | 685.6 | 713.3 | ^ | ^ | ^ |
| | 4/27/09 | 7o9-15(remix) | 167.3 | 344.8 | ^ | 728.6 | 576.9 | 1.1E-06 | 8.3E-07 | ^ |
| | | " | 156.7 | 598.6 | ^ | 704.2 | 698.7 | ^ | ^ | ^ |
| | 4/28/09 | 7p8-18 | 67.4 | 158.8 | ^ | 712.4 | 687.9 | 1.4E-06 | 8.1E-07 | ^ |
| | | " | 75.9 | 133.3 | ^ | 710.6 | 679.9 | ^ | ^ | ^ |
| | 4/29/09 | 7m8-15 | 41.1 | 273.9 | ^ | 720.1 | 672.6 | 1.2E-06 | 1.6E-07 | ^ |
| | | " | 36.3 | 398.5 | ^ | 730.2 | 671.0 | ^ | ^ | ^ |
| | 4/30/09 | 7L7-20 | 176.6 | 324.3 | ^ | 769.1 | 673.4 | 1.2E-06 | 1.2E-07 | ^ |
| | | " | 145.3 | 277.3 | ^ | 690.4 | 646.4 | ^ | ^ | ^ |
| | 5/12/09 | 6T13-20 | 166.1 | 349.4 | ^ | 723.6 | ^ | 7.5E-07 | 8.5E-07 | ^ |
| | | " | 196.8 | 346.9 | ^ | 689.7 | ^ | ^ | ^ | ^ |
| | 5/29/09 | 4o2-25 | 157.8 | 269.6 | ^ | 676.0 | ^ | 1.5E-06 | 1.3E-06 | 9.5E-07 |
| | | " | 175.5 | 347.1 | ^ | 652.8 | ^ | ^ | ^ | ^ |
| | 5/30/09 | 4b11-18 | 12.1 | 33.2 | ^ | 629.6 | ^ | 2.4E-06 | 9.0E-07 | ^ |
| | | " | 12.1 | 30.0 | ^ | 600.9 | ^ | ^ | ^ | ^ |
| | 6/1/09 | 8test3-18 | 61.9 | 183.4 | ^ | 636.1 | ^ | 2.0E-06 | 9.3E-07 | ^ |
| | | " | 74.1 | 203.6 | ^ | 648.3 | ^ | ^ | ^ | ^ |
| | 6/2/09 | 8e1-23 | 13.7 | 57.1 | ^ | 666.0 | ^ | 2.4E-06 | 1.0E-06 | ^ |
| | | " | 16.6 | 49.0 | ^ | 668.9 | ^ | ^ | ^ | ^ |
| | 6/3/09 | 8d1-18 | 16.0 | 119.6 | ^ | 653.8 | ^ | 2.1E-06 | 9.30E-07 | ^ |
| | | " | 15.8 | 84.7 | ^ | 574.5 | ^ | ^ | ^ | ^ |
| | 6/15/09 | 8a5-5 | 12.6 | 38.5 | ^ | 630.3 | ^ | 1.1E-06 | 8.70E-07 | ^ |
| | | " | 9.2 | 33.5 | ^ | 660.0 | ^ | ^ | ^ | ^ |

**Table 4.7**
**Cons Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Auger-ISS Testing Results**

| Sample Date | Sample ID | Unconfined Compressive Strength (UCS) (psi) | | | | | Hydraulic Conductivity (HC) * (cm/sec) | | |
|---|---|---|---|---|---|---|---|---|---|
| | | 3 Days | 7 Days | 14 Days | 28 Days | 56 Days | 14 Days | 28 Days | 28+ Days |
| 6/19/09 | 8c3-20 | 47.4 | 91.4 | ^ | 630.1 | ^ | 1.90E-06 | 9.70E-07 | ^ |
| | " | 54.1 | 109.4 | ^ | 644.7 | ^ | ^ | ^ | ^ |
| 7/6/09 | 8d5-20 | 140.0 | 350.1 | ^ | 712.7 | ^ | 1.30E-06 | 8.7E-07 | ^ |
| | " | 108.6 | 667.6 | ^ | 767.8 | ^ | " | ^ | ^ |
| 7/7/09 | 8e7-20 | 54.9 | 193.3 | ^ | 722.8 | ^ | 2.20E-06 | 9.4E-0.7 | ^ |
| | " | 40.5 | 125.2 | ^ | 657.5 | ^ | ^ | ^ | ^ |
| 7/8/09 | 8g2-25 | 160.5 | 234.4 | ^ | 870.0 | ^ | 1.90E-06 | 8.8E-07 | ^ |
| | " | 200.9 | 314.7 | ^ | 834.7 | ^ | ^ | ^ | ^ |
| 7/9/09 | 8h3-25 | 161.5 | 284.6 | ^ | 897.1 | ^ | 1.50E-06 | 9.3E-07 | ^ |
| | " | 123.3 | 308.4 | ^ | 711.1 | ^ | ^ | ^ | ^ |
| 7/10/09 | 8i8-22 | 103.1 | 205.2 | ^ | 550.2 | ^ | 1.10E-06 | 9.7E-07 | ^ |
| | " | 90.2 | 182.0 | ^ | 604.0 | ^ | ^ | ^ | ^ |
| 7/11/09 | 8b9-15 | 58.6 | 135.8 | ^ | 748.6 | ^ | 1.30E-06 | 9.4E-07 | ^ |
| | " | 58.3 | 160.4 | ^ | 504.0 | ^ | ^ | ^ | ^ |
| 7/13/09 | 8d10-15 | 59.5 | 185.9 | ^ | 694.6 | ^ | 1.50E-06 | 9.6E-07 | ^ |
| | " | 58.5 | 206.7 | ^ | 739.7 | ^ | ^ | ^ | ^ |
| 7/14/09 | 8f10-17 | 171.8 | 176.7 | ^ | 644.1 | ^ | 1.40E-06 | 9.5E-07 | ^ |
| | " | 130.1 | 185.9 | ^ | 722.3 | ^ | ^ | ^ | ^ |
| 7/16/09 | 8p4-35 | 225.1 | 348.7 | ^ | 919.5 | ^ | 1.60E-06 | 9.4E-07 | ^ |
| | " | 340.6 | 339.6 | ^ | 795.4 | ^ | ^ | ^ | ^ |
| 7/17/09 | 8q7-30 | 201.1 | 346.8 | ^ | 930.6 | ^ | 1.20E-06 | 9.5E-07 | ^ |
| | " | 259.0 | 345.5 | ^ | 937.6 | ^ | ^ | ^ | ^ |
| 7/18/09 | 8p8-25 | 81.3 | 217.4 | ^ | 601.6 | ^ | 1.6E-06 | 9.4E-07 | ^ |
| | " | 96.6 | 295.0 | ^ | 649.2 | ^ | ^ | ^ | ^ |
| 7/21/09 | 8o6-30 | 56.8 | 345.6 | ^ | 690.1 | ^ | 1.3E-06 | 9.4E-07 | ^ |
| | " | 74.9 | 347.2 | ^ | 723.9 | ^ | ^ | ^ | ^ |
| 7/22/09 | 8n3-28 | 238.2 | 348.4 | ^ | 759.6 | ^ | 2.3E-06 | 9.5E-07 | ^ |
| | " | 196.0 | 345.8 | ^ | 716.1 | ^ | ^ | ^ | ^ |
| 7/23/09 | 8m2-15 | 185.8 | 231.9 | ^ | 821.5 | ^ | 1.5E-06 | 9.5E-07 | ^ |
| | " | 199.8 | 188.6 | ^ | 771.2 | ^ | ^ | ^ | ^ |
| 7/24/09 | 8L2-20 | 154.0 | 235.2 | ^ | 671.3 | ^ | 1.5E-06 | 9.3E-07 | ^ |
| | " | 120.6 | 254.4 | ^ | 725.2 | ^ | ^ | ^ | ^ |
| 7/25/09 | 8k2-22 | 66.3 | 283.3 | ^ | 777.5 | ^ | 1.6E-06 | 9.5E-07 | ^ |
| | " | 65.1 | 191.6 | ^ | 678.5 | ^ | ^ | ^ | ^ |
| 7/27/09 | 8j3-22 | 101.9 | 346.9 | ^ | 678.8 | ^ | 2.3E-06 | 9.4E.07 | ^ |
| | " | 126.2 | 346.5 | ^ | 720.3 | ^ | ^ | ^ | ^ |
| 7/28/09 | 8x5-12 | 27.1 | 121.8 | ^ | 750.7 | ^ | 2.3E-06 | 9.5E-07 | ^ |
| | " | 29.3 | 102.2 | ^ | 689.0 | ^ | ^ | ^ | ^ |
| 7/30/09 | 4xx4-18-1 | 151.8 | 235.9 | ^ | 689.2 | ^ | 1.3E-06 | 9.3E-07 | ^ |
| | " | 127.1 | 191.5 | ^ | 686.7 | ^ | ^ | ^ | ^ |
| 7/30/09 | 4xx4-18-2 | 74.7 | 306.5 | ^ | 674.2 | ^ | 1.5E-06 | 9.5E-07 | ^ |
| | " | 158.0 | 152.9 | ^ | 683.4 | ^ | ^ | ^ | ^ |
| 7/31/09 | 4xz2-20 | 96.8 | 352.4 | ^ | 690.4 | ^ | 1.6E-06 | 9.4E-07 | ^ |
| | " | 142.2 | 250.6 | ^ | 668.5 | ^ | ^ | ^ | ^ |
| 8/3/09 | 4xy15-22 | 188.0 | 348.6 | ^ | 669.2 | ^ | 2.0E-06 | 9.4E-07 | ^ |
| | " | 230.5 | 341.5 | ^ | 657.8 | ^ | ^ | ^ | ^ |

PRODUCTION COLUMNS

**Requirements: UCS ≥ 50 psi @ 28 days**
**HC ≤ 1x10$^{-6}$ cm/sec**

**SAMPLES TAKEN ONCE PER DAY OR EVERY 500 CYs WHICHEVER PRODUCES THE GREATEST NUMBER OF SAMPLES**

Denotes that sample did not achieve the required result.

^ Denotes sample not tested.

* Hydraulic conductivity testing initially performed with a hydraulic gradient of 15. The hydraulic gradient was reduced to 10 on 5/12/09 for 6T13-20. This modification was within ASTM D 5084 Method A standards which require a maximum hydraulic gradient of 20 for hydraulic conductivities within a range of 10-6 to 10-7 cm/sec.

Sample ID: Sample number is characters before dash/sample depth is numbers after dash

**Table 4.8**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grouting Testing Results**

| | Sample Date | Sample ID | Unconfined Compressive Strength (UCS) (psi) | | | | | Hydraulic Conductivity (HC) * (cm/sec) | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | | | 3 Days | 7 Days | 14 Days | 28 Days | 56 Days | 14 Days | 28 Days | 28+ Days |
| TEST COLUMNS | 6/26/09 | JG-Test1-27 | 739.3 | 553.8 | 785.4 | 2121.8 | ^ | 1.9E-06 | 1.2E-07 | ^ |
| | | " | 763.8 | 858.3 | ^ | ^ | ^ | ^ | ^ | ^ |
| | 6/27/09 | JG-Test2-10 | 264.9 | 1149.0 | 754.5 | 2100.5 | ^ | 1.6E-06 | 9.6E-07 | ^ |
| | | " | 359.8 | 49.0 | ^ | ^ | ^ | ^ | ^ | ^ |
| | 6/27/09 | JG-Test2-16 | 301.0 | 662.6 | 754.3 | 2091.9 | ^ | 1.7E-06 | 9.5E-07 | ^ |
| | | " | 354.6 | 602.1 | ^ | ^ | ^ | ^ | ^ | ^ |
| | | JG-Test2-31 | 227.5 | 761.3 | 788.8 | 2060.7 | ^ | 1.7E-06 | 4.0E-07 | ^ |
| | | " | 431.3 | 530.8 | ^ | ^ | ^ | ^ | ^ | ^ |
| | 6/29/09 | JG-Test3-10 | 565.7 | 369.6 | 755.7 | 645.1 | ^ | 1.3E-06 | 9.7E-07 | ^ |
| | | " | 514.3 | 479.3 | ^ | ^ | ^ | ^ | ^ | ^ |
| | | JG-Test3-15 | 629.6 | 682.5 | 758.8 | 2094.7 | ^ | 1.4E-06 | 9.6E-07 | ^ |
| | | " | 680.6 | 591.8 | ^ | ^ | ^ | ^ | ^ | ^ |
| | | JG-Test3-30 | 494.3 | 372.3 | 749.4 | 2099.0 | ^ | 1.3E-06 | 9.6E-07 | ^ |
| | | " | 357.2 | 370.4 | ^ | ^ | ^ | ^ | ^ | ^ |
| | 6/30/09 | JG-Test4-52 | 494.7 | 640.4 | 798.3 | 2130.8 | ^ | 2.6E-06 | 9.6E-07 | ^ |
| | | " | 1279.6 | 644.2 | ^ | ^ | ^ | ^ | ^ | ^ |
| | 7/1/09 | JG-Test5-15 | 661.6 | 759.1 | 763.8 | 774.9 | ^ | 1.4E-06 | 9.8E-07 | ^ |
| | | " | 557.0 | 755.2 | ^ | ^ | ^ | ^ | ^ | ^ |
| | | JG-Test5-25 | 770.0 | 730.0 | 772.9 | 770.8 | ^ | 1.3E-06 | 9.6E-07 | ^ |
| | | " | 771.2 | 748.6 | ^ | ^ | ^ | ^ | ^ | ^ |
| | | JG-Test5-50 | 773.8 | 753.4 | 768.4 | 788.5 | ^ | 1.6E-06 | 9.4E-07 | ^ |
| | | " | 776.5 | 764.2 | ^ | ^ | ^ | ^ | ^ | ^ |
| | | JG-Test6-15 | 449.0 | 588.0 | 731.3 | 770.3 | ^ | 1.3E-06 | 9.7E-07 | ^ |
| | | " | 676.1 | 764.4 | ^ | | ^ | ^ | ^ | ^ |
| | | JG-Test6-25 | 652.5 | 732.1 | 740.4 | 766.7 | ^ | 1.3E-06 | 9.7E-07 | ^ |
| | | " | 665.9 | 754.1 | ^ | ^ | ^ | ^ | ^ | ^ |
| | | JG-Test6-50 | 612.2 | 749.1 | 747.4 | 763.4 | ^ | 1.1E-06 | 9.7E-07 | ^ |
| | | " | 708.2 | 593.1 | ^ | ^ | ^ | ^ | ^ | ^ |
| PRODUCTION COLUMNS | 8/24/09 | WO13-40 | 188.9 | 738.4 | ^ | 772.3 | ^ | 1.4E-06 | 9.2E-07 | ^ |
| | | | 180.5 | 761.5 | ^ | 776.3 | ^ | | | ^ |
| | 8/25/09 | WO14-20 | 79.9 | 86.5 | ^ | 743.6 | ^ | 1.4E-06 | 9.5E-07 | ^ |
| | | | 73.0 | 138.0 | ^ | 757.7 | ^ | ^ | ^ | ^ |
| | 8/26/09 | WO17-48 | 537.9 | 791.4 | ^ | 778.9 | ^ | 1.4E-06 | 8.6E-07 | ^ |
| | | | 533.8 | 694.8 | ^ | 782.0 | ^ | ^ | ^ | ^ |
| | 8/27/09 | WO19-35 | 195.8 | 418.1 | ^ | 776.9 | ^ | 1.4E-06 | 9.4E-07 | ^ |
| | | | 166.2 | 503.0 | ^ | 778.8 | ^ | ^ | ^ | ^ |
| | 9/1/09 | WI10-30 | 192.3 | 519.4 | ^ | 761.9 | ^ | 1.3E-06 | 9.3E-07 | ^ |
| | | | 174.0 | 473.2 | ^ | 770.8 | ^ | ^ | ^ | ^ |
| | 9/2/09 | WI14-25 | 153.5 | 751.8 | ^ | 763.3 | ^ | 1.3E-06 | 9.5E-07 | ^ |
| | | | 183.0 | 739.7 | ^ | 788.2 | ^ | ^ | ^ | ^ |
| | 9/3/09 | WI17-35 | 472.5 | 452.5 | ^ | 770.1 | ^ | 1.2E-06 | 9.4E-07 | ^ |
| | | | 449.7 | 482.9 | ^ | 758.3 | ^ | ^ | ^ | ^ |
| | 9/4/09 | WO10-35 | 472.0 | 759.8 | ^ | 758.1 | ^ | 1.5E-06 | 9.5E-07 | ^ |
| | | | 382.9 | 703.6 | ^ | 761.2 | ^ | ^ | ^ | ^ |
| | 9/5/09 | WI19-30 | 227.8 | 487.2 | ^ | 757.5 | ^ | 1.1E-06 | 9.3E-07 | ^ |
| | | | 281.7 | 433.4 | ^ | 766.4 | ^ | ^ | ^ | ^ |
| | 9/8/09 | INT03-40 | 411.7 | 379.7 | ^ | 790.3 | ^ | 1.4E-06 | 9.3E-07 | ^ |
| | | | 338.6 | 368.0 | ^ | 768.8 | ^ | ^ | ^ | ^ |
| | 9/9/09 | INT05-30 | 108.9 | 609.0 | ^ | 770.5 | ^ | 2.1E-06 | 9.5E-07 | ^ |
| | | | 118.9 | 540.1 | ^ | 765.0 | ^ | ^ | ^ | ^ |
| | 9/10/09 | INT39-35 | 423.4 | 594.2 | ^ | 757.5 | ^ | 1.1E-06 | 9.4E-07 | ^ |
| | | | 393.2 | 691.7 | ^ | 766.1 | ^ | ^ | ^ | ^ |
| | 9/11/09 | WO19A-40 | 340.3 | 657.1 | ^ | 764.7 | ^ | 1.2E-06 | 9.3E-07 | ^ |
| | | | 304.2 | 588.2 | ^ | 726.6 | ^ | ^ | ^ | ^ |
| | 9/12/09 | WO24-35 | 103.3 | 329.4 | ^ | 750.6 | ^ | 1.3E-06 | 9.4E-07 | ^ |
| | | | 109.2 | 356.2 | ^ | 747.9 | ^ | ^ | ^ | ^ |
| | 9/14/09 | WO22-40 | 229.1 | 678.7 | ^ | 760.3 | ^ | 1.2E-06 | 9.3E-07 | ^ |
| | | | 248.0 | 485.4 | ^ | 758.3 | ^ | ^ | ^ | ^ |
| | 9/15/09 | WI20-40 | 189.6 | 479.8 | ^ | 772.3 | ^ | 1.3E-06 | 9.4E-07 | ^ |
| | | | 207.1 | 486.9 | ^ | 746.5 | ^ | ^ | ^ | ^ |
| | 9/16/09 | WI28-35 | 76.3 | 406.9 | ^ | 781.3 | ^ | 1.3E-06 | 9.3E-07 | ^ |
| | | | 81.0 | 467.8 | ^ | 768.4 | ^ | ^ | ^ | ^ |
| | 9/17/09 | WI29-40 | 379.8 | 643.0 | ^ | 772.1 | ^ | 1.2E-06 | 9.3E-07 | ^ |
| | | | 366.9 | 592.1 | ^ | 763.5 | ^ | ^ | ^ | ^ |
| | 9/18/09 | WI24-40 | 231.7 | 521.8 | ^ | 769.7 | ^ | 1.2E-06 | 9.3E-07 | ^ |
| | | | 198.5 | 455.1 | ^ | 773.1 | ^ | ^ | ^ | ^ |

**Table 4.8**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grouting Testing Results**

| Sample Date | Sample ID | Unconfined Compressive Strength (UCS) (psi) | | | | | Hydraulic Conductivity (HC) * (cm/sec) | | |
|---|---|---|---|---|---|---|---|---|---|
| | | 3 Days | 7 Days | 14 Days | 28 Days | 56 Days | 14 Days | 28 Days | 28+ Days |
| 9/19/09 | WI27-35 | 108.9 | 341.3 | ^ | 760.9 | ^ | 1.3E-06 | 5.1E-07 | ^ |
| | | 139.2 | 332.1 | ^ | 759.5 | ^ | ^ | ^ | ^ |
| 9/21/09 | WO27-40 | 168.1 | 286.3 | ^ | 759.7 | ^ | 1.4E-06 | 9.1E-07 | ^ |
| | | 156.7 | 260.8 | ^ | 765.6 | ^ | ^ | ^ | ^ |
| 9/22/09 | WI25-36 | 165.2 | 580.2 | ^ | 762.9 | ^ | 1.2E-06 | 9.5E-07 | ^ |
| | | 179.7 | 553.7 | ^ | 764.5 | ^ | ^ | ^ | ^ |
| 9/23/09 | WI21-50 | 269.4 | 431.9 | ^ | 770.0 | ^ | 1.2E-06 | 9.5E-07 | ^ |
| | | 276.8 | 450.3 | ^ | 774.1 | ^ | ^ | ^ | ^ |
| 9/24/09 | INT15-36 | 161.6 | 311.5 | ^ | 750.8 | ^ | 1.2E-06 | 7.4E-07 | ^ |
| | | 158.3 | 269.5 | ^ | 763.4 | ^ | ^ | ^ | ^ |
| 9/25/09 | INT16-36 | 229.6 | 395.5 | ^ | 763.6 | ^ | 1.3E-06 | 2.6E-07 | ^ |
| | | 240.0 | 340.9 | ^ | 774.3 | ^ | ^ | ^ | ^ |
| 9/26/09 | INT14-36 | 34.5 | 130.1 | ^ | 466.6 | ^ | 1.3E-06 | 9.3E-07 | ^ |
| | | 46.6 | 130.3 | ^ | 552.3 | ^ | ^ | ^ | ^ |
| 9/28/09 | INT163-36 | 178.4 | 419.3 | ^ | 768.2 | ^ | ^ | 7.3E-07 | ^ |
| | | 157.1 | 510.5 | ^ | 752.8 | ^ | ^ | ^ | ^ |
| 9/29/09 | INT143-36 | 148.9 | 394.0 | ^ | 756.2 | ^ | ^ | 2.4E-07 | ^ |
| | | 149.4 | 379.0 | ^ | 744.1 | ^ | ^ | ^ | ^ |
| 9/30/09 | INT152-36 | 68.9 | 134.3 | ^ | 537.2 | ^ | ^ | 9.2E-07 | ^ |
| | | 69.7 | 136.9 | ^ | 493.0 | ^ | ^ | ^ | ^ |
| 10/1/09 | INT147-36 | 149.3 | 306.8 | ^ | 726.7 | ^ | ^ | 9.3E-07 | ^ |
| | | 154.4 | 288.4 | ^ | 761.5 | ^ | ^ | ^ | ^ |
| 10/2/09 | INT155-40 | 204.6 | 327.2 | ^ | 764.6 | ^ | ^ | 9.3E-07 | ^ |
| | | 209.1 | 335.7 | ^ | 769.4 | ^ | ^ | ^ | ^ |
| 10/5/09 | WO32-46 | 166.5 | ^ | ^ | 768.1 | ^ | ^ | 9.2E-07 | ^ |
| | | 176.2 | ^ | ^ | 759.2 | ^ | ^ | ^ | ^ |
| 10/6/09 | WO33-50 | 392.7 | ^ | ^ | 766.4 | ^ | ^ | 9.4E-07 | ^ |
| | | 372.5 | ^ | ^ | 769.5 | ^ | ^ | ^ | ^ |
| 10/7/09 | SO2-50 | 340.8 | ^ | ^ | 770.2 | ^ | ^ | 9.3E-07 | ^ |
| | | 350.4 | ^ | ^ | 787.3 | ^ | ^ | ^ | ^ |
| 10/8/09 | SO4-55 | 163.1 | ^ | ^ | 739.7 | ^ | ^ | 9.4E-07 | ^ |
| | | 158.6 | ^ | ^ | 762.5 | ^ | ^ | ^ | ^ |
| 10/9/09 | SO10-20 | 214.8 | ^ | ^ | 752.1 | ^ | ^ | 8.7E-07 | ^ |
| | | 232.8 | ^ | ^ | 764.2 | ^ | ^ | ^ | ^ |
| 10/10/09 | WI31-20 | 149.2 | ^ | ^ | 765.5 | ^ | ^ | 9.3E-07 | ^ |
| | | 158.1 | ^ | ^ | 766.7 | ^ | ^ | ^ | ^ |
| 10/12/09 | INT153-20 | 389.1 | ^ | ^ | 749.3 | ^ | ^ | 2.2E-06 | 9.6E-07 |
| | | 318.3 | ^ | ^ | 749.7 | ^ | ^ | ^ | ^ |
| 10/13/09 | SI1-20 | 427.7 | ^ | ^ | 767.9 | ^ | ^ | 9.0E-07 | ^ |
| | | 374.5 | ^ | ^ | 762.9 | ^ | ^ | ^ | ^ |
| 10/14/09 | INT34-20 | 129.3 | ^ | ^ | 532.9 | ^ | ^ | 9.4E-07 | ^ |
| | | 124.3 | ^ | ^ | 556.4 | ^ | ^ | ^ | ^ |
| 10/15/09 | INT38-30 | 93.1 | ^ | ^ | 684.7 | ^ | ^ | 9.3E-07 | ^ |
| | | 90.8 | ^ | ^ | 472.1 | ^ | ^ | ^ | ^ |
| 10/19/09 | INT36-35 | 89.9 | ^ | ^ | 746.0 | ^ | ^ | 9.7E-07 | ^ |
| | | 94.8 | ^ | ^ | 718.8 | ^ | ^ | ^ | ^ |
| 10/20/09 | SI6-40 | 268.5 | ^ | ^ | 770.9 | ^ | ^ | 2.7E-07 | ^ |
| | | 254.5 | ^ | ^ | 743.5 | ^ | ^ | ^ | ^ |
| 10/21/09 | SI7-20 | 280.0 | ^ | ^ | 756.5 | ^ | ^ | 2.8E-07 | ^ |
| | | 277.0 | ^ | ^ | 757.5 | ^ | ^ | ^ | ^ |
| 10/22/09 | SI8-20 | 144.5 | ^ | ^ | 736.6 | ^ | ^ | 8.5E-07 | ^ |
| | | 208.5 | ^ | ^ | 749.0 | ^ | ^ | ^ | ^ |
| 10/23/09 | INT341-20 | 198.9 | ^ | ^ | 765.6 | ^ | ^ | 3.3E-07 | ^ |
| | | 221.7 | ^ | ^ | 752.5 | ^ | ^ | ^ | ^ |
| 10/24/09 | INT29-35 | 218.0 | ^ | ^ | 767.0 | ^ | ^ | 3.3E-07 | ^ |
| | | 229.7 | ^ | ^ | 769.2 | ^ | ^ | ^ | ^ |
| 10/26/09 | SO18-40 | 152.8 | ^ | ^ | 733.6 | ^ | ^ | 4.2E-07 | ^ |
| | | 112.8 | ^ | ^ | 757.3 | ^ | ^ | ^ | ^ |
| 10/27/09 | INT151-40 | 238.5 | ^ | ^ | 740.8 | ^ | ^ | 9.4E-07 | ^ |
| | | 185.8 | ^ | ^ | 737.2 | ^ | ^ | ^ | ^ |
| 10/28/09 | SO15-20 | 319.3 | ^ | ^ | 764.3 | ^ | ^ | 6.2E-07 | ^ |
| | | 286.5 | ^ | ^ | 770.8 | ^ | ^ | ^ | ^ |
| 10/29/09 | S020-30 | 228.8 | ^ | ^ | 779.2 | ^ | ^ | 8.2E-07 | ^ |
| | | 185.0 | ^ | ^ | 554.8 | ^ | ^ | ^ | ^ |
| 10/30/09 | SO17-30 | 121.4 | ^ | ^ | 685.9 | ^ | ^ | 8.3E-07 | ^ |
| | | 133.1 | ^ | ^ | 762.5 | ^ | ^ | ^ | ^ |

PRODUCTION COLUMNS

**Table 4.8**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grouting Testing Results**

| Sample Date | Sample ID | Unconfined Compressive Strength (UCS) (psi) | | | | | Hydraulic Conductivity (HC) * (cm/sec) | | |
|---|---|---|---|---|---|---|---|---|---|
| | | 3 Days | 7 Days | 14 Days | 28 Days | 56 Days | 14 Days | 28 Days | 28+ Days |
| 11/2/09 | SO16-20 | 267.8 | ^ | ^ | 759.0 | ^ | ^ | 6.5E-07 | ^ |
| | | 303.4 | ^ | ^ | 763.9 | ^ | ^ | ^ | ^ |
| 11/3/09 | SO27-30 | 217.5 | ^ | ^ | 770.7 | ^ | ^ | 6.4E-07 | ^ |
| | | 189.7 | ^ | ^ | 755.6 | ^ | ^ | ^ | ^ |
| 11/4/09 | SI15-40 | 270.9 | ^ | ^ | 728.1 | ^ | ^ | 5.4E-07 | ^ |
| | | 240.3 | ^ | ^ | 616.1 | ^ | ^ | ^ | ^ |
| 11/5/09 | SI16-20 | 232.6 | ^ | ^ | 762.4 | ^ | ^ | 2.9E-07 | ^ |
| | | 237.9 | ^ | ^ | 758.6 | ^ | ^ | ^ | ^ |
| 11/6/09 | INT158-40 | 279.9 | ^ | ^ | 736.4 | ^ | ^ | 9.4E-07 | ^ |
| | | 270.0 | ^ | ^ | 767.1 | ^ | ^ | ^ | ^ |
| 11/7/09 | INT25-45 | 244.2 | ^ | ^ | 772.5 | ^ | ^ | 9.4E-07 | ^ |
| | (100% Portland) | 301.6 | ^ | ^ | 798.7 | ^ | ^ | ^ | ^ |
| 11/9/09 | INT24-50 | 346.1 | ^ | ^ | 839.6 | ^ | ^ | 9.3E-07 | ^ |
| | (100% Portland) | 363.5 | ^ | ^ | 773.7 | ^ | ^ | ^ | ^ |
| 11/10/09 | SO21-20 | 301.4 | ^ | ^ | 762.6 | ^ | ^ | 3.1E-07 | ^ |
| | | 315.9 | ^ | ^ | 774.5 | ^ | ^ | ^ | ^ |
| 11/11/09 | SI18-30 | 402.9 | ^ | ^ | 773.5 | ^ | ^ | 3.5E-07 | ^ |
| | | 381.0 | ^ | ^ | 771.1 | ^ | ^ | ^ | ^ |
| 11/12/09 | INT129-45 | 487.9 | ^ | ^ | 773.5 | ^ | ^ | 3.2E-07 | ^ |
| | | 463.4 | ^ | ^ | 784.2 | ^ | ^ | ^ | ^ |
| 11/13/09 | SI23-35 | 294.6 | ^ | ^ | 786.6 | ^ | ^ | 3.9E-07 | ^ |
| | | 270.8 | ^ | ^ | 783.8 | ^ | ^ | ^ | ^ |
| 11/14/09 | SI27-25 | 88.2 | ^ | ^ | 521.6 | ^ | ^ | 9.4E-07 | ^ |
| | | 83.4 | ^ | ^ | 474.0 | ^ | ^ | ^ | ^ |
| 11/16/09 | INT131-40 | 298.4 | ^ | ^ | 792.5 | ^ | ^ | 2.2E-07 | ^ |
| | | 290.5 | ^ | ^ | 632.9 | ^ | ^ | ^ | ^ |
| 11/17/09 | INT134-45 | 431.0 | ^ | ^ | 765.4 | ^ | ^ | 2.2E-07 | ^ |
| | | 426.9 | ^ | ^ | 774.4 | ^ | ^ | ^ | ^ |
| 11/18/09 | INT135-21 | 93.8 | ^ | ^ | 511.9 | ^ | ^ | 4.3E-07 | ^ |
| | | 88.1 | ^ | ^ | 562.1 | ^ | ^ | ^ | ^ |
| 11/19/09 | INT124-35 | 276.9 | ^ | ^ | 849.8 | ^ | ^ | 7.3E-07 | ^ |
| | | 287.0 | ^ | ^ | 756.6 | ^ | ^ | ^ | ^ |
| 11/20/09 | INT116-25 | 165.8 | ^ | ^ | 756.4 | ^ | ^ | 2.0E-07 | ^ |
| | | 167.8 | ^ | ^ | 761.4 | ^ | ^ | ^ | ^ |
| 11/23/09 | INT127-32 | 331.7 | ^ | ^ | 742.3 | ^ | ^ | 9.3E-07 | ^ |
| | | 262.5 | ^ | ^ | 753.1 | ^ | ^ | ^ | ^ |
| 11/24/09 | INT335-25 | 382.6 | ^ | ^ | 749.8 | ^ | ^ | 9.3E-07 | ^ |
| | | 318.3 | ^ | ^ | 772.4 | ^ | ^ | ^ | ^ |
| 11/30/09 | INT328-25 | 67.9 | ^ | ^ | 608.4 | ^ | ^ | 8.4E-07 | ^ |
| | | 60.0 | ^ | ^ | 622.6 | ^ | ^ | ^ | ^ |
| 12/1/09 | INT73-30 | 255.5 | ^ | ^ | 640.9 | ^ | ^ | 2.2E-07 | ^ |
| | | 255.1 | ^ | ^ | 637.9 | ^ | ^ | ^ | ^ |
| 12/2/09 | SO33-25 | 117.0 | ^ | ^ | 433.7 | ^ | ^ | 9.6E-07 | ^ |
| | | 122.3 | ^ | ^ | 466.3 | ^ | ^ | ^ | ^ |
| 12/4/09 | SI33-17 | 203.4 | ^ | ^ | 545.9 | ^ | ^ | 3.4E-07 | ^ |
| | | 199.5 | ^ | ^ | 653.1 | ^ | ^ | ^ | ^ |
| 12/7/09 | INT311-20 | 124.6 | ^ | ^ | 695.0 | ^ | ^ | 3.7E-07 | ^ |
| | | 107.1 | ^ | ^ | 743.5 | ^ | ^ | ^ | ^ |
| 12/8/09 | INT347-30 | 139.5 | ^ | ^ | 561.0 | ^ | ^ | 7.0E-07 | ^ |
| | | 149.6 | ^ | ^ | 533.7 | ^ | ^ | ^ | ^ |
| 12/9/09 | INT81-25 | 167.5 | ^ | ^ | 689.9 | ^ | ^ | 9.7E-07 | ^ |
| | | 174.4 | ^ | ^ | 730.3 | ^ | ^ | ^ | ^ |
| 12/10/09 | INT92-25 | 224.3 | ^ | ^ | 707.9 | ^ | ^ | 9.5E-07 | ^ |
| | | 206.2 | ^ | ^ | 763.3 | ^ | ^ | ^ | ^ |
| 12/11/09 | INT102-25 | 67.7 | ^ | ^ | 486.8 | ^ | ^ | 9.4E-07 | ^ |
| | | 58.5 | ^ | ^ | 495.7 | ^ | ^ | ^ | ^ |
| 12/14/09 | INT324-25 | 186.3 | ^ | ^ | 785.8 | ^ | ^ | 6.5E-07 | ^ |
| | | 190.5 | ^ | ^ | 840.2 | ^ | ^ | ^ | ^ |
| 12/15/09 | WO7-35 | 101.0 | ^ | ^ | 641.8 | ^ | ^ | 9.2E-07 | ^ |
| | | 122.1 | ^ | ^ | 678.8 | ^ | ^ | ^ | ^ |
| 12/16/09 | WO3-30 | 159.5 | ^ | ^ | 742.1 | ^ | ^ | 9.3E-07 | ^ |
| | | 188.3 | ^ | ^ | 704.3 | ^ | ^ | ^ | ^ |
| 12/17/09 | WI5-30 | 165.5 | ^ | ^ | 643.1 | ^ | ^ | 9.4E-07 | ^ |
| | | 166.8 | ^ | ^ | 649.4 | ^ | ^ | ^ | ^ |
| 12/18/09 | INT51-25 | 167.8 | ^ | ^ | 784.6 | ^ | ^ | 7.8E-07 | ^ |
| | | 166.6 | ^ | ^ | 640.6 | ^ | ^ | ^ | ^ |

PRODUCTION COLUMNS

**Table 4.8**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grouting Testing Results**

| Sample Date | Sample ID | Unconfined Compressive Strength (UCS) (psi) | | | | | Hydraulic Conductivity (HC) * (cm/sec) | | |
|---|---|---|---|---|---|---|---|---|---|
| | | 3 Days | 7 Days | 14 Days | 28 Days | 56 Days | 14 Days | 28 Days | 28+ Days |
| 12/21/09 | INT319-25 | 55.2 | ^ | ^ | 568.3 | ^ | ^ | 9.4E-07 | ^ |
| | | 63.3 | ^ | ^ | 740.1 | ^ | ^ | ^ | ^ |
| 12/22/09 | INT305-23 | 20.7 | 156.9 | ^ | 396.6 | ^ | ^ | 9.2E-07 | ^ |
| | | 22.1 | 148.4 | ^ | 411.6 | ^ | ^ | ^ | ^ |
| 1/4/10 | INT-301-20 | 95.8 | ^ | ^ | 619.1 | ^ | ^ | 7.2E-07 | ^ |
| | | 78.8 | ^ | ^ | 593.0 | ^ | ^ | ^ | ^ |
| 1/5/10 | INT-296-20 | 69.0 | ^ | ^ | 669.8 | ^ | ^ | 3.0E-07 | ^ |
| | | 71.2 | ^ | ^ | 680.1 | ^ | ^ | ^ | ^ |
| 1/5/10 | INT-297-SPOILS | 106.8 | ^ | ^ | 753.8 | ^ | ^ | 3.5E-07 | ^ |
| | | 88.3 | ^ | ^ | 786.7 | ^ | ^ | ^ | ^ |
| 1/6/10 | INT-285-30 | 25.5 | 369.1 | ^ | 585.5 | ^ | ^ | 9.7E-07 | ^ |
| | | 26.1 | 370.5 | ^ | 573.0 | ^ | ^ | ^ | ^ |
| 1/7/10 | INT-226-26 | 294.7 | ^ | ^ | 765.8 | ^ | ^ | 3.4E-07 | ^ |
| | | 269.3 | ^ | ^ | 762.1 | ^ | ^ | ^ | ^ |
| 1/8/10 | INT-239-18 | 239.6 | ^ | ^ | 760.5 | ^ | ^ | 3.3E-07 | ^ |
| | | 244.1 | ^ | ^ | 766.5 | ^ | ^ | ^ | ^ |
| 1/11/10 | INT-244-18 | 93.1 | ^ | ^ | 748.1 | ^ | ^ | 4.2E-07 | ^ |
| | | 91.4 | ^ | ^ | 772.2 | ^ | ^ | ^ | ^ |
| 1/12/10 | INT-252-25 | 147.3 | ^ | ^ | 635.4 | ^ | ^ | 2.3E-07 | ^ |
| | | 106.9 | ^ | ^ | 637.9 | ^ | ^ | ^ | ^ |
| 1/13/10 | INT-265-20 | 150.4 | ^ | ^ | 760.4 | ^ | ^ | 2.6E-07 | ^ |
| | | 157.8 | ^ | ^ | 774.7 | ^ | ^ | ^ | ^ |
| 1/14/10 | INT-272-18 | 155.3 | ^ | ^ | 767.9 | ^ | ^ | 2.3E-07 | ^ |
| | | 135.2 | ^ | ^ | 763.6 | ^ | ^ | ^ | ^ |
| 1/15/10 | INT-282-18 | 96.8 | ^ | ^ | 767.9 | ^ | ^ | 2.2E-07 | ^ |
| | | 121.0 | ^ | ^ | 768.9 | ^ | ^ | ^ | ^ |
| 1/18/10 | JGW-3-20 | 105.1 (5 day) | 283.7 | ^ | 777.2 | ^ | ^ | Not tested | ^ |
| | | 113.6 (5 day) | 247.2 | ^ | 768.5 | ^ | ^ | ^ | ^ |
| 1/19/10 | JGW-5-19 | 117.6 (4 day) | 210.6 | Insufficient sample volume to make 28-day molds | | | ^ | Not tested | ^ |
| | | ^ | ^ | | | | ^ | ^ | ^ |
| 1/20/10 | JGW-2-30 | 90.6 | 318.6 | ^ | 766.6 | ^ | ^ | Not tested | ^ |
| | | 83.6 | 355.6 | ^ | 772.8 | ^ | ^ | ^ | ^ |
| 1/21/10 | JGW-14-25 | 30.7 | 372.5 | ^ | 774.4 | ^ | ^ | Not tested | ^ |
| | | 28.2 | 300.1 | ^ | 772.1 | ^ | ^ | ^ | ^ |
| 1/22/10 | JGW-18-20 | 58.0 | 182.8 | ^ | 626.5 | ^ | ^ | Not tested | ^ |
| | | 55.1 | 170.9 | ^ | 760.4 | ^ | ^ | ^ | ^ |
| 1/25/10 | INT-187-23 | 71.5 | ^ | ^ | 646.3 | ^ | ^ | 7.4E-07 | ^ |
| | | 61.6 | ^ | ^ | 767.2 | ^ | ^ | ^ | ^ |
| 1/26/10 | INT-189-20 | 105.7 | ^ | ^ | 776.3 | ^ | ^ | 3.9E-07 | ^ |
| | | 97.6 | ^ | ^ | 773.6 | ^ | ^ | ^ | ^ |
| 1/27/10 | INT-207-19 | 146.5 | ^ | ^ | 768.2 | ^ | ^ | 5.0E-07 | ^ |
| | | 144.5 | ^ | ^ | 766.4 | ^ | ^ | ^ | ^ |
| 1/28/10 | XO-3-20 | 162.2 | ^ | ^ | 780.4 | ^ | ^ | 5.2E-07 | ^ |
| | | 199.2 | ^ | ^ | 776.1 | ^ | ^ | ^ | ^ |
| 2/1/10 | XO-9-24 | 75.8 | ^ | ^ | 764.1 | ^ | ^ | 4.9E-07 | ^ |
| | | 78.0 | ^ | ^ | 602.9 | ^ | ^ | ^ | ^ |
| 2/2/10 | XO-2-30 | 148.1 | ^ | ^ | 562.8 | ^ | ^ | 3.4E-07 | ^ |
| | | 152.1 | ^ | ^ | 641.9 | ^ | ^ | ^ | ^ |
| 2/3/10 | INT-186-17 | 129.7 | ^ | ^ | 756.0 | ^ | ^ | 6.9E-07 | ^ |
| | | 118.8 | ^ | ^ | 766.2 | ^ | ^ | ^ | ^ |
| 2/4/10 | XO-10-18 | 212.4 | ^ | ^ | 781.8 | ^ | ^ | 7.2E-07 | ^ |
| | | 262.2 | ^ | ^ | 779.8 | ^ | ^ | ^ | ^ |
| 2/5/10 | XI-4 | 229.8 | ^ | ^ | 777.8 | ^ | ^ | 6.3E-07 | ^ |
| | | 256.1 | ^ | ^ | 780.8 | ^ | ^ | ^ | ^ |
| 2/11/10 | JGW-21-14 | 48.3 | 94.5 | ^ | 562.4 | ^ | ^ | Not tested | ^ |
| | | 43.2 | 117.2 | ^ | 681.7 | ^ | ^ | ^ | ^ |
| 2/12/10 | JGW-22-12 | 60.1 | ^ | ^ | 656.4 | ^ | ^ | Not tested | ^ |
| | | 65.0 | ^ | ^ | 615.9 | ^ | ^ | ^ | ^ |
| 2/15/10 | XI-11-25 | 47.2 | 7-day test not run (3-day Avg >50 psi) | | 666.8 | ^ | ^ | 2.0E-07 | ^ |
| | | 57.3 | | | 707.5 | ^ | ^ | ^ | ^ |
| 2/16/10 | XO-19-15 | 33.5 | 306.0 | ^ | 780.4 | ^ | ^ | 1.8E-07 | ^ |
| | | 29.0 | 326.6 | ^ | 759.8 | ^ | ^ | ^ | ^ |
| 2/17/10 | INT-60-18 | 123.9 | ^ | ^ | 743.5 | ^ | ^ | 2.6E-07 | ^ |
| | | 137.0 | ^ | ^ | 622.7 | ^ | ^ | ^ | ^ |
| 2/18/10 | INT-65-10 | 153.2 | ^ | ^ | 765.7 | ^ | ^ | 4.5E-07 | ^ |
| | | 180.1 | ^ | ^ | 773.3 | ^ | ^ | ^ | ^ |

**PRODUCTION COLUMNS**

**Table 4.8**
**Con Edison White Plains Former MGP Site**
**Operable Unit 2 (OU-2)**
**Final Engineering Report**
**Jet Grouting Testing Results**

| Sample Date | Sample ID | Unconfined Compressive Strength (UCS) (psi) | | | | | Hydraulic Conductivity (HC) * (cm/sec) | | |
|---|---|---|---|---|---|---|---|---|---|
| | | 3 Days | 7 Days | 14 Days | 28 Days | 56 Days | 14 Days | 28 Days | 28+ Days |
| 2/19/10 | XO-20-10 | 119.7 | ^ | ^ | 772.5 | ^ | ^ | 5.8E-07 | ^ |
| | | 106.8 | ^ | ^ | 779.2 | ^ | ^ | ^ | ^ |
| 2/22/10 | NO-26-14 | 68.0 | ^ | ^ | 723.3 | ^ | ^ | 5.6E-07 | ^ |
| | | 57.7 | ^ | ^ | 587.6 | ^ | ^ | ^ | ^ |
| 2/23/10 | NO-23-12 | 193.8 | ^ | ^ | 767.9 | ^ | ^ | 5.2E-07 | ^ |
| | | 196.1 | ^ | ^ | 756.6 | ^ | ^ | ^ | ^ |
| 2/24/10 | EO-17-17 | 213.8 | ^ | ^ | 751.1 | ^ | ^ | 2.8E-07 | ^ |
| | | 199.7 | ^ | ^ | 768.0 | ^ | ^ | ^ | ^ |
| 3/1/10 | EO-12-15 | 64.7 | ^ | ^ | 764.4 | ^ | ^ | 3.4E-07 | ^ |
| | | 63.5 | ^ | ^ | 770.7 | ^ | ^ | ^ | ^ |
| 3/2/10 | NI-22-14 | 370.0 | ^ | ^ | 782.2 | ^ | ^ | 3.1E-07 | ^ |
| | | 310.8 | ^ | ^ | 788.8 | ^ | ^ | ^ | ^ |
| 3/3/10 | NI-29-10 | 130.0 | ^ | ^ | 771.6 | ^ | ^ | 3.0E-07 | ^ |
| | | 137.6 | ^ | ^ | 770.9 | ^ | ^ | ^ | ^ |
| 3/4/10 | EI-15-12 | 120.1 | ^ | ^ | 773.1 | ^ | ^ | 3.3E-07 | ^ |
| | | 80.7 | ^ | ^ | 776.6 | ^ | ^ | ^ | ^ |
| 3/5/10 | XO-22A-12 | 139.0 | ^ | ^ | 774.3 | ^ | ^ | 2.3E-07 | ^ |
| | | 154.3 | ^ | ^ | 759.9 | ^ | ^ | ^ | ^ |
| 3/8/10 | SO-39-20 | 120.8 | ^ | ^ | 768.4 | ^ | ^ | 2.9E-07 | ^ |
| | | 112.1 | ^ | ^ | 774.8 | ^ | ^ | ^ | ^ |
| 3/9/10 | SO-46-15 | 92.2 | ^ | ^ | 775.3 | ^ | ^ | 2.9E-07 | ^ |
| | | 97.7 | ^ | ^ | 778.0 | ^ | ^ | ^ | ^ |
| 3/10/10 | SO-51-24 | 96.8 | ^ | ^ | 628.6 | ^ | ^ | 7.2E-07 | ^ |
| | | 128.4 | ^ | ^ | 772.9 | ^ | ^ | ^ | ^ |
| 3/15/10 | INT-314-15.5 | 55.3 | ^ | ^ | 678.6 | ^ | ^ | 7.4E-07 | ^ |
| | | 56.3 | ^ | ^ | 663.5 | ^ | ^ | ^ | ^ |
| 3/16/10 | SI-39-18 | 100.7 | ^ | ^ | 749.0 | ^ | ^ | 4.0E-07 | ^ |
| | | 84.6 | ^ | ^ | 745.3 | ^ | ^ | ^ | ^ |
| 3/17/10 | SI-45-14 | 188.9 | ^ | ^ | 773.9 | ^ | ^ | 9.3E-07 | ^ |
| | | 236.0 | ^ | ^ | 778.9 | ^ | ^ | ^ | ^ |
| 3/18/10 | INT-400-18 | 227.4 | ^ | ^ | 759.0 | ^ | ^ | 8.7E-07 | ^ |
| | | 239.2 | ^ | ^ | 757.9 | ^ | ^ | ^ | ^ |
| 3/19/10 | XI-1R-15 | 131.1 | ^ | ^ | 769.2 | ^ | ^ | 9.3E-07 | ^ |
| | | 136.7 | ^ | ^ | 770.0 | ^ | ^ | ^ | ^ |
| 3/22/10 | XI-14R-12 | 52.0 | ^ | ^ | 780.2 | ^ | ^ | 9.3E-07 | ^ |
| | | 53.5 | ^ | ^ | 755.1 | ^ | ^ | ^ | ^ |
| 3/23/10 | XI-15R-18 | 95.5 | ^ | ^ | 583.3 | ^ | ^ | 9.3E-07 | ^ |
| | | 83.9 | ^ | ^ | 747.0 | ^ | ^ | ^ | ^ |
| 3/24/10 | EI-10-14 | 126.7 | ^ | ^ | 741.0 | ^ | ^ | 9.6E-07 | ^ |
| | | 140.5 | ^ | ^ | 766.1 | ^ | ^ | ^ | ^ |
| 3/25/10 | EO-2-18 | 133.5 | ^ | ^ | 764.6 | ^ | ^ | 9.5E-07 | ^ |
| | | 117.2 | ^ | ^ | 684.3 | ^ | ^ | ^ | ^ |
| 3/26/10 | EO-6-16 | 90.5 | ^ | ^ | 752.9 | ^ | ^ | 9.4E-07 | ^ |
| | | 83.6 | ^ | ^ | 730.2 | ^ | ^ | ^ | ^ |
| 3/29/10 | AEO-16-8 | 85.0 | ^ | ^ | 749.5 | ^ | ^ | 9.5E-07 | ^ |
| | | 81.7 | ^ | ^ | 756.6 | ^ | ^ | ^ | ^ |
| 3/30/10 | AEO-12-8 | 350.9 | ^ | ^ | 777.7 | ^ | ^ | 6.1E-07 | ^ |
| | | 308.3 | ^ | ^ | 770.2 | ^ | ^ | ^ | ^ |
| 3/31/10 | ASO-55-22 | 263.8 | ^ | ^ | 770.8 | ^ | ^ | 5.2E-07 | ^ |
| | | 284.0 | ^ | ^ | 754.7 | ^ | ^ | ^ | ^ |
| 4/2/10 | EI-5-9 | 134.4 | ^ | ^ | 773.1 | ^ | ^ | 5.0E-07 | ^ |
| | | 142.5 | ^ | ^ | 771.7 | ^ | ^ | ^ | ^ |
| 4/5/10 | EI-22-10 | 187.8 | ^ | ^ | 779.7 | ^ | ^ | 6.1E-07 | ^ |
| | | 228.1 | ^ | ^ | 768.7 | ^ | ^ | ^ | ^ |
| 4/6/10 | SO-55-18 | 89.1 | ^ | ^ | 764.6 | ^ | ^ | 2.8E-07 | ^ |
| | | 94.5 | ^ | ^ | 767.3 | ^ | ^ | ^ | ^ |
| 4/7/10 | ASI-52-17 | 190.6 | ^ | ^ | 782.5 | ^ | ^ | 8.8E-07 | ^ |
| | | 236.0 | ^ | ^ | 768.3 | ^ | ^ | ^ | ^ |

PRODUCTION COLUMNS

**Requirements: UCS $\geq$ 50 psi @ 28 days**
**HC $\leq$ $1x10^{-6}$ cm/sec**

**SAMPLES TAKEN ONCE PER DAY OR EVERY 500 CYs WHICHEVER PRODUCES THE GREATEST NUMBER OF SAMPLES**

Denotes that sample did not achieve the required result.

^ Denotes sample not tested.

* Hydraulic conductivity testing performed with a hydraulic gradient of 10. This hydraulic gradient was within ASTM D 5084 Method A standards which require a maximum hydraulic gradient of 20 for hydraulic conductivities within a range of 10-6 to 10-7 cm/sec.

Notes: UCS testing at 7 days eliminated starting 10/10/09 when 3-day UCS results are greater than 50 psi.
HC testing at 14 days eliminated starting 10/10/09.
Sample ID: Sample number is characters before dash/sample depth is numbers after dash